



Heat Loads Due to Small Penetrations in Multilayer Insulation Blankets

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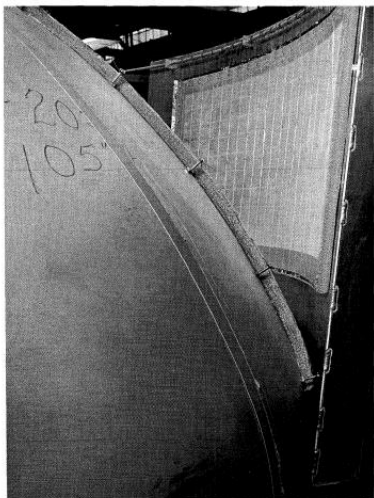
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Cryogenic Engineering Conference





Improved Fundamental Understanding of Super Insulation (IFUSI)



Skirt Integration

Penetration Integration:

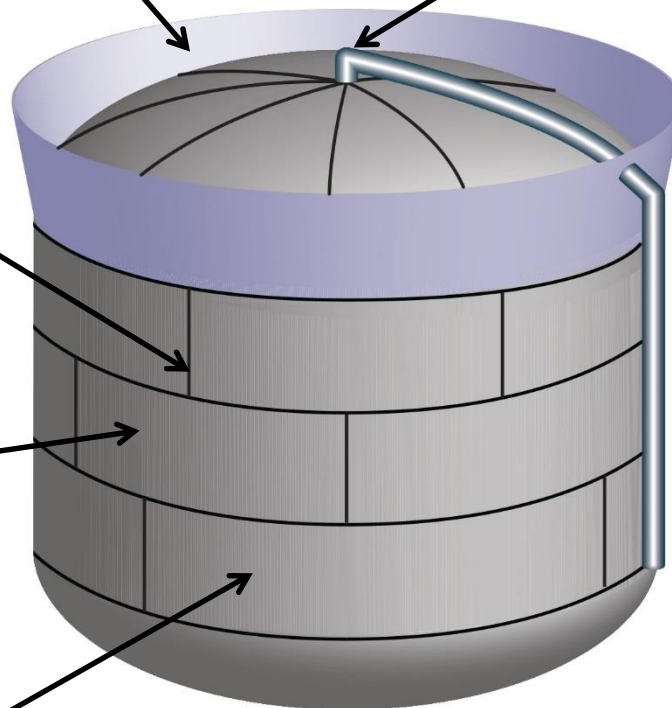
- NASA-TP-2012-216315

Seams

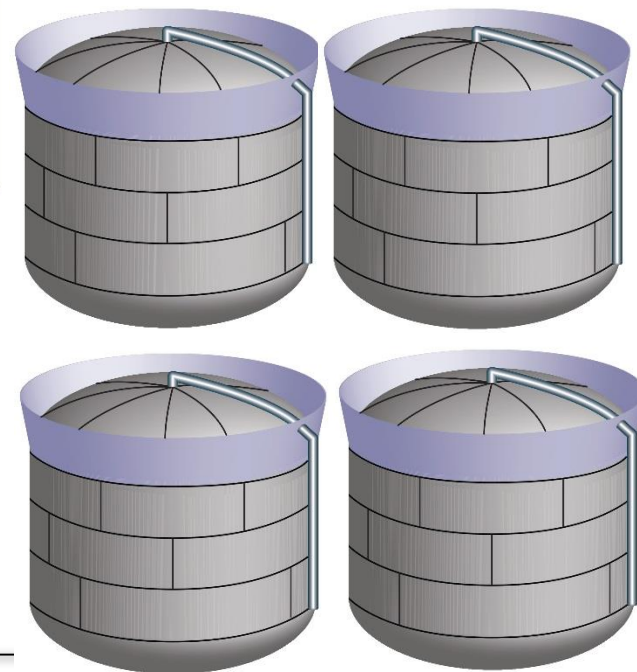
MLI Blankets

- Traditional
- SS-MLI
- Hybrid

Tape, Pins & Attachments



Repeatability



Is this really an issue?

ATV 1 (Joules Verne) incident

- During launch, more power draw required than expected, was traced to blanket disengagement.
- Root causes came down to improper structural attachment
- AIAA-2010-6197



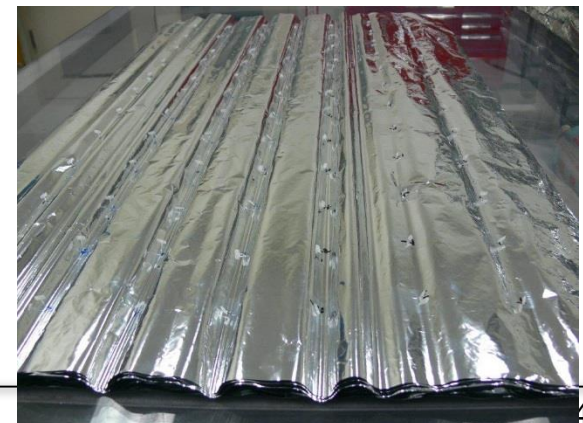
Nylon Tag Testing

- **Nylon tags have long been used to hold MLI together**
- **Installed 56 pins into an existing 10 layer LB-MLI blanket**
 - Individual pins have a really small heat load (~ 0.9 mW each)
 - Needed repeatable MLI coupon to do initial test and pinned test
 - Pin spacing ~ 3 inch
- **Blanket Heat flux (KSC – Cryostat 100):**
 - A164 July 2012¹: 0.92 W/m²
 - A191 March 2015: 1.04 W/m²
 - Was also used in Hybrid MLI testing² (A174, A175, A181, A182)
- **Predicted disturbance:**
 - Variable tag geometry
 - 20 node conduction model (NIST nylon props): 0.5 mW/tag
 - Direct radiation through hole: 8 μ W/tag

Cold side



Hot side



¹Johnson, W.L., Heckle, K.W., and Hurd, J. "Thermal coupon testing of Load-Bearing Multilayer Insulation", *AIP Conference Proceedings* 1573, pg. 725, 2014.

²Johnson, W.L., Fesmire, J.E., and Heckle, K.W., **Demonstration of Hybrid Multilayer Insulation of Fixed Thickness Applications**, *IOP Conf. Ser.: Mater. Sci. Eng.* **101** 012015, 2015.

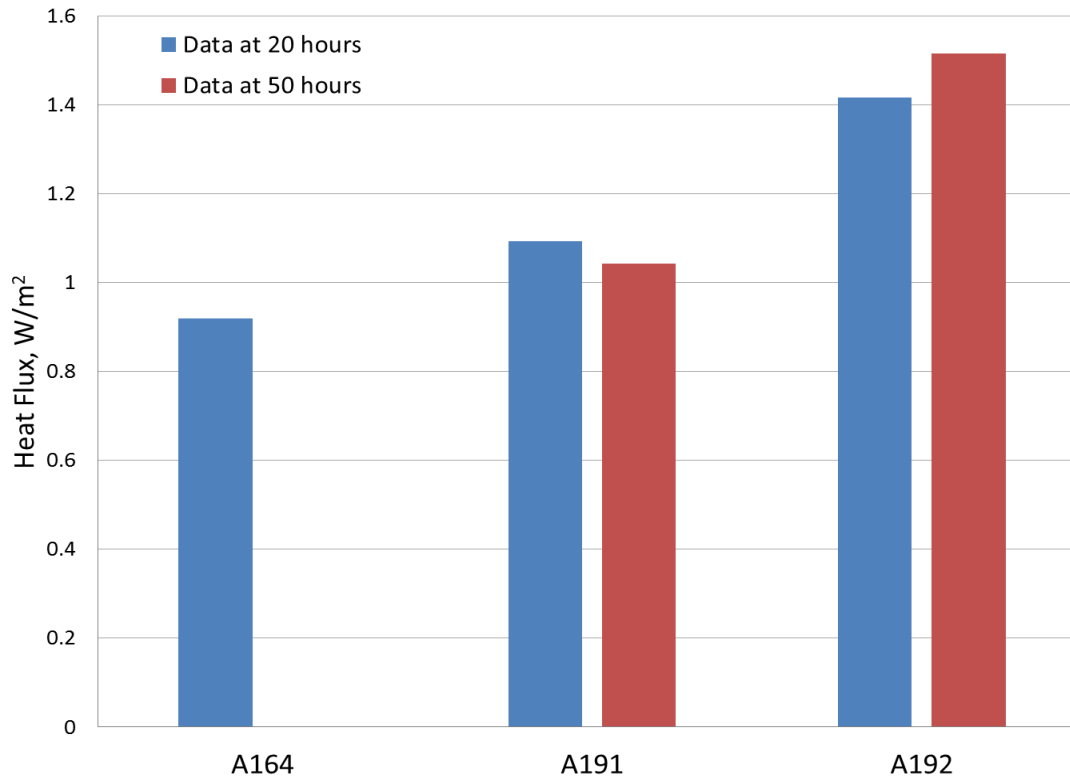
Test matrix

Test Series	# layers [n]	Thickness [x] (mm)	Layer Density [z] (layers/mm)*	Effective Area [A_e] (m^2)	CVP Tested (torr)	Warm Boundary Temperature (K)	# pins
A164	10	16.5	0.54	0.334	$\sim 10^{-6}$	~ 293	0
A191	10	15.2	0.59	0.331	$\sim 10^{-6}$	~ 293	0
A192	10	15.1	0.60	0.331	$\sim 10^{-6}$	~ 293	56





Results



Test Series (Data Time)	CVP (Torr)	WBT (K)	Q (W)	k _e (mW/m/K)	q (W/m ²)
A164	5x10 ⁻⁶	291.7	0.31	0.072	0.92
A191 (20 hrs)	2x10 ⁻⁵	292.4	0.37	0.078	1.11
A191 (50 hrs)	2x10 ⁻⁵	293.0	0.35	0.074	1.04
A192 (20 hrs)	7x10 ⁻⁶	293.3	0.47	0.099	1.41
A192 (50 hrs)	7x10 ⁻⁶	292.4	0.51	0.106	1.51

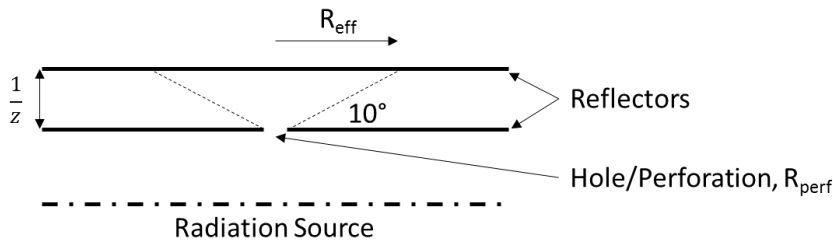


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- ³Black, I.A, Glaser, P.E., Reid, R.C., “Heat Loss Through Evacuated Multilayer Insulation Penetrated By a Low-Conductivity Pin”, Bull. IIR, Annex 1966-2, 233-243 (Meeting Of Commission 2, Trondheim, Norway, Jun 22-24, 1966)

Revised model

- Based on perforations model developed for MHTB large perforations, the radiation through a perforation is not limited to direct radiation⁴
- Instead the effective radiation area is defined by a 10 deg angle
- Using layer density as the spacing for LB-MLI, this can be extrapolated to a tag hole.



$$\theta = 10 \text{ deg} = 0.175 \text{ rad}$$

$$r_{eff} = \frac{1}{z \cos \theta} + r_{perf}$$

$$A_{eff} = \pi r_{eff}^2$$

$$\dot{Q} = A_{eff} \epsilon_{layer} \sigma (T_h^4 - T_c^4) + \int \frac{A}{dx} \int k dT$$

- Revised model estimates 3.6 mW per tag on recent testing (~30% more than actual)
- Revised model estimates 3.6 mW heat load for tag & hole in ADL test

⁴Fox, E.C., Keifel, E.R., and McIntosh, G.L., et.al. "Multipurpose Hydrogen Test Bed System Definition and Insulated Tank Development", Martin Marietta Astronautics, NASA CR-194355, July 1993.



Conclusions

- Completed testing on an MLI blanket with multiple small penetrations.
- Results show that heat load much more than conduction only.
- Analytical approach with combined radiation and conduction shows uncertainty less than 30%.
 - Change in vacuum level may account for difference

Test Series	Hole Radius (mm)	# layers	Layer Density (lay/mm)	Q_{hole} (mW)	Q_{pin} (mW)	Q_{total} (mW)	Q_{meas} (mW)
A192	0.5	10	0.6	3.1	0.52	3.6	2.0-2.8
Black [9]	0.5	10	1.3	3.3	0.3	3.6	~3