

June 8, 2017

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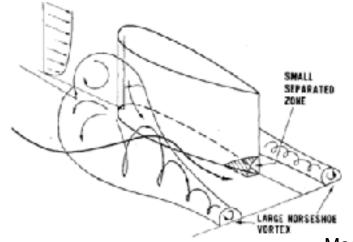
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Mike Kegerise
NASA Langley Research Center

Juncture Flow



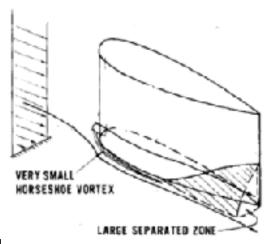
Sponsored by NASA's Transformative Aeronautics Concepts Program's Transformational Tools and Technologies (T³) project

- Substantial effort to investigate the origin of separation bubbles found in wing-body juncture zones
- Primary goal is to gather validation level data, for future CFD code & turbulence model development
- Multi-year effort including several large-scale wind tunnel tests
- Computational Fluid Dynamics (CFD) used in both design and support of risk reduction experiment



(a) thick boundary layer

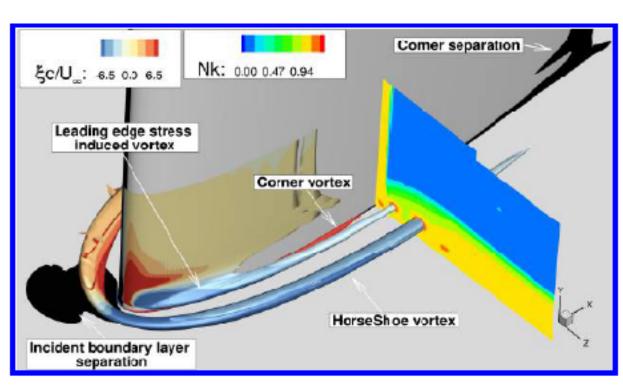
Model proposed by Barber *et al.*



Background



- Flow physics of juncture flows is complex
 - Several vortical structures coexist: e.g., Horseshoe Vortex (HSV), corner vortex, stress-induced vortex
 - Many factors—such as incoming boundary layer momentum thickness, wing bluntness, and wing sweep—also play some role
- Previous juncture flow work:
 - Simpson et al
 - Gand et al
 - other references mentioned therein



From AIAA-2014-2690 (Bordji et al)

Background



- Geometric junctures (corners) are common on aircraft
 - CFD predictive capability is currently uncertain
 - E.g. Drag Prediction Workshops, participants predicted a wide range of wing-body corner separation bubble sizes (none to very large)
- Computed juncture bubble may be influenced by: grid size, grid topology, and numerical treatments
 - Accurate modeling of the Reynolds stresses is needed
 - Non-linear turbulence modeling
- Because of the high degree of uncertainty in the CFD predictions, relevant separated corner flow experiments focused specifically on obtaining high-quality data for CFD validation are needed

Past Experiments

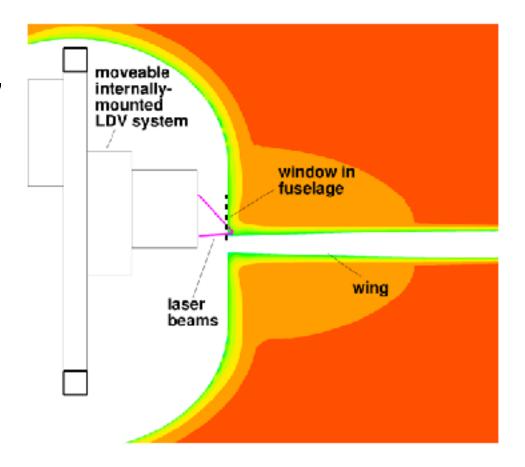


- Simpson et al experiments:
 - Mostly focused on HSV (not so much on corner separation)
- Gand et al experiments:
 - NACA 0012 wing (no sweep) mounted on flat plate did not separate
 - Twisted NACA 0015 wing (no sweep) mounted on flat plate - produced corner separation at alpha=12 deg
- New NASA experiment originally conceived by members of the DPW steering committee
 - Swept wing / fuselage full-span configuration
 - To focus primarily on collecting data for CFD validation
 - A main objective: to obtain flow field details very near the corner

Goals and Purpose



- Decision made early: to use internal Laser Doppler Velocimetry (LDV) system
 - Mounted inside of the fuselage on a movable three-axis traverse system
 - Will measure the flow field very near the wing-body juncture through window(s) in the fuselage



Goals and Purpose



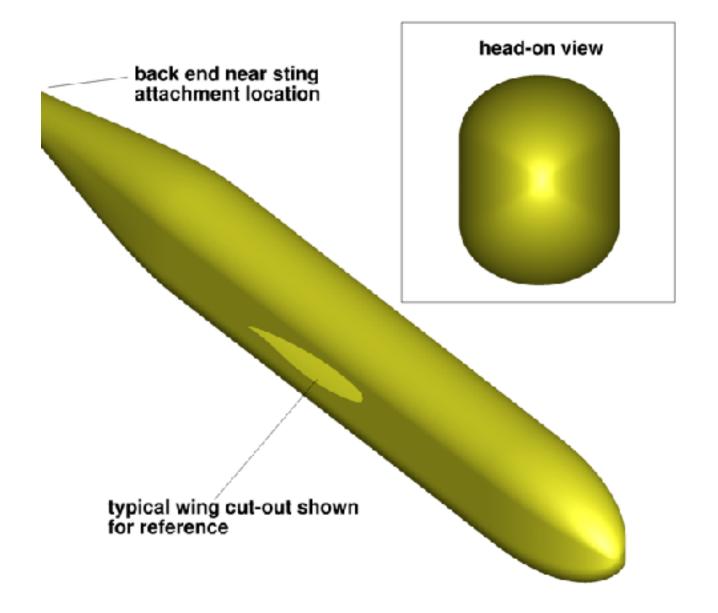
- Decision made to perform a subsonic experiment
 - Subsonic testing venues of sufficient size were readily available
 - M=0.2
 - 8% model based on full scale CRM (~16 ft long, 11 ft wide)
- "CFD Validation-Quality"
 - Boundary conditions, geometry information, experimental uncertainties, etc., necessary for a thorough and unambiguous CFD validation study
 - See, e.g., Aeschliman & Oberkampf (AIAA J 36(5):733-741, 1998)

Main purpose:

- Assess the ability of existing models to predict the onset and extent of the three-dimensionally separated flow near the Wing Juncture Trailing Edge region of a full-span wing-body configuration, in terms of the surface topology of the flowfield structure.
- To provide a range of prediction difficulty, a variation of low fields are required, including the onset and progression of corner separation

Fuselage Configuration

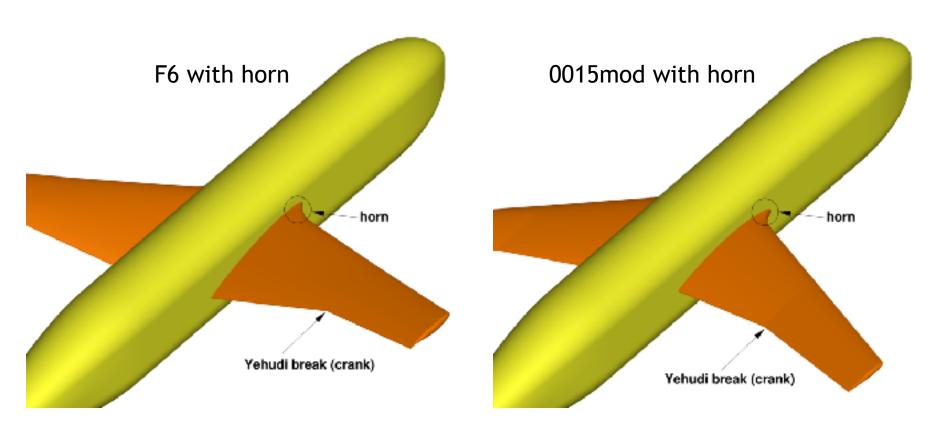




Wing Configuration



 Planforms based on truncated DLR-F6 or truncated CRM



Juncture Flow Model Design



- Preliminary model design done with CFD
 - Overflow 2.2L: SARC-QCR2000
 - Fun3d: SARC-QCR2000
- Evaluated 20+ wing candidates
- Committee down-selected the wing candidates
- Selected 6 wing candidates that combined satisfied the goals
- Risk reduction experiment tests proposed: further evaluate 6 wing candidates

Wing Candidates

- 6 Wing candidates
- DLR-F6 no horn
 - Used in DPW3
 - Showed side of body separation
- DLR-F6: with LE horn
- NACA 0015 with horn: symmetric wing
- NACA 0015mod: slightly steeper pressure recovery
- F6S12: symmetric F6 variant
- COCA
 - Coder-Campbell design
 - CDISC/skin-friction constraints



COCA

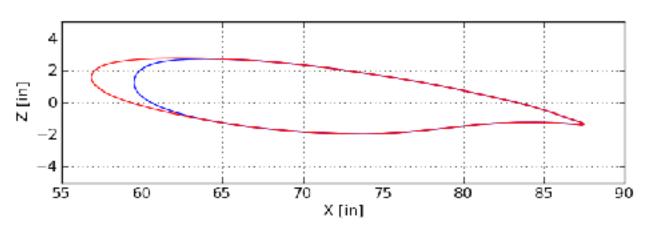
0015

F6-S12

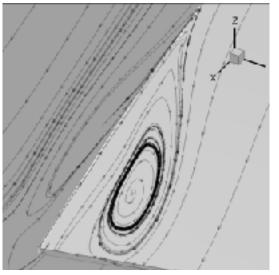
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DLR-F6





Blue: F6 without horn, Red: F6 with horn

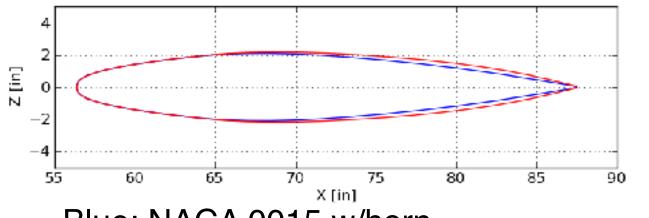


Side of Body Separation

Wing Planform

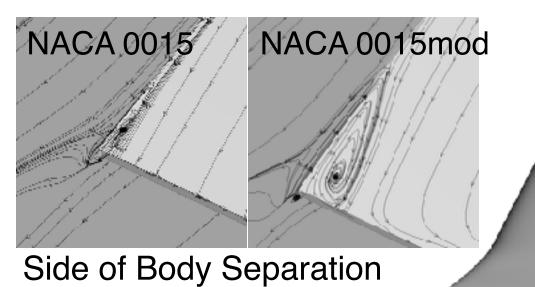
NACA 0015 — NACA 0015mod





Blue: NACA 0015 w/horn,

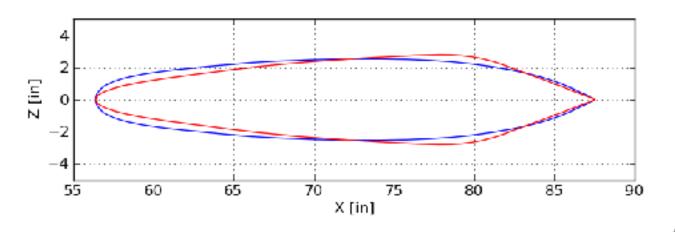
Red: NACA 0015mod with horn



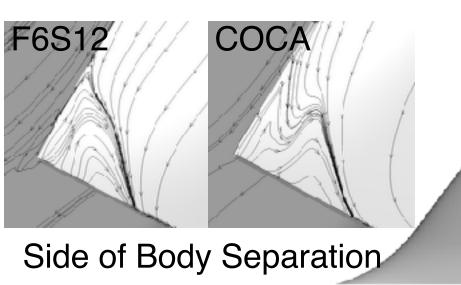
Wing Planform

F6S12 — COCA





Blue: F6S12 w/horn, Red: COCA w/horn

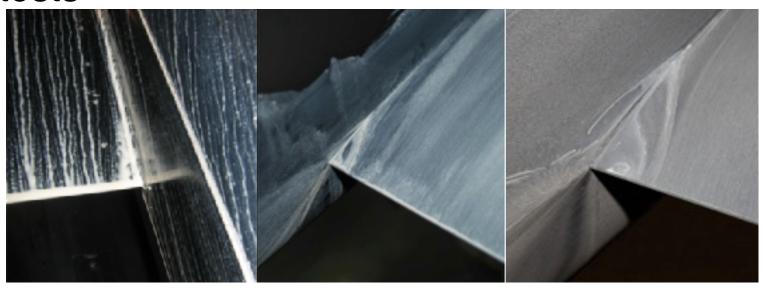


Wing Planform

Risk Reduction Tests



- Series of risk reduction tests
 - Ames TC2 3% wall mounted model, low RE
 - Virginia Tech 2.5% fullspan low RE
 - Langley 14x22 6% fullspan high RE
- CFD solutions were run concurrently with all tests

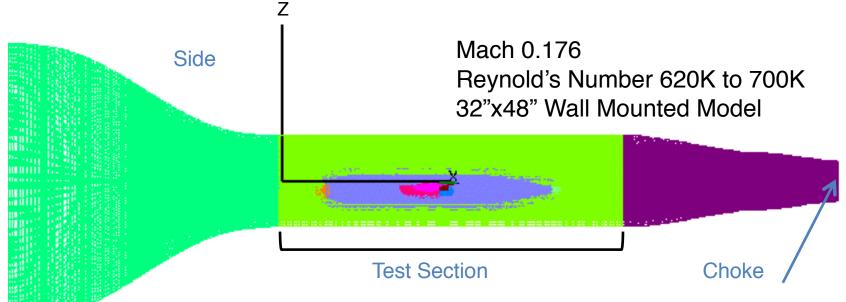


TC2 VA Tech 14x22

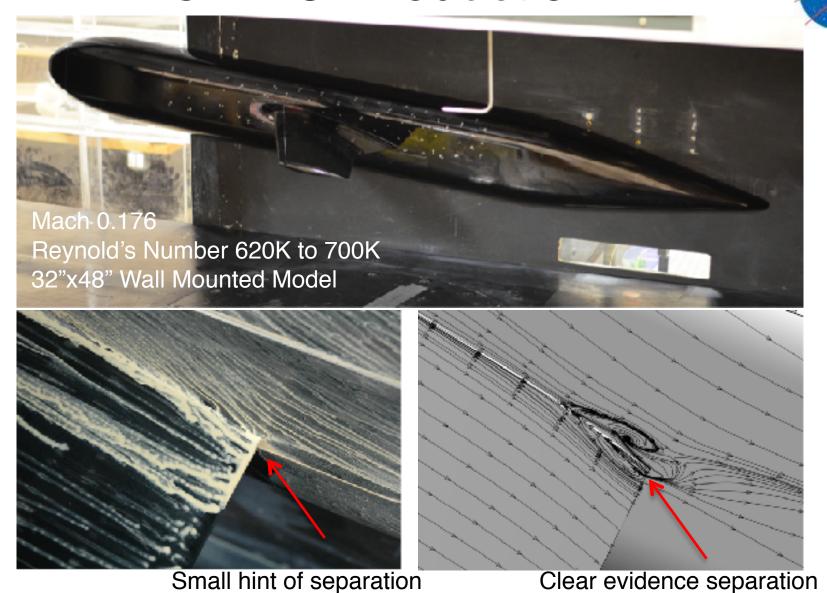
Model in TC2 and CFD Geometry







TC2 Risk Reduction



Determined Wall Mounted model is not ideal for this test

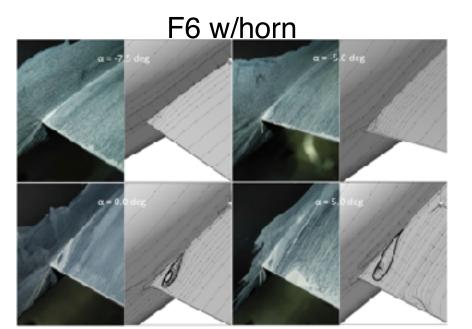
Virginia Tech 2.5% Full Span Test





Mach 0.176, Reynolds Number of 620K, 6' Test Section



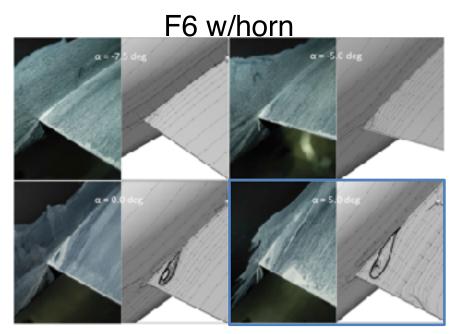


F6S12 w/horn

a = 5.0 deg a = 7.5 deg a = 5.0 deg a = 7.5 deg

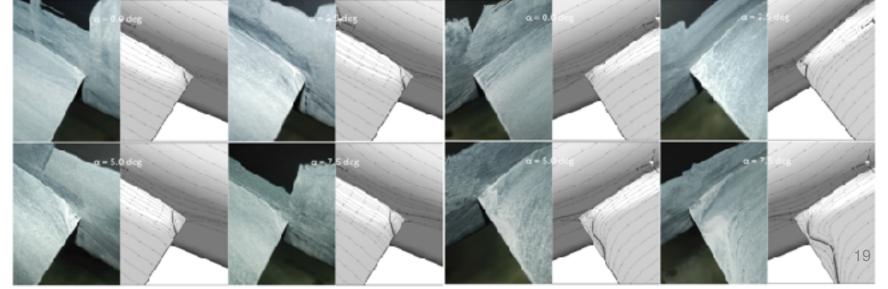
COCA w/horn



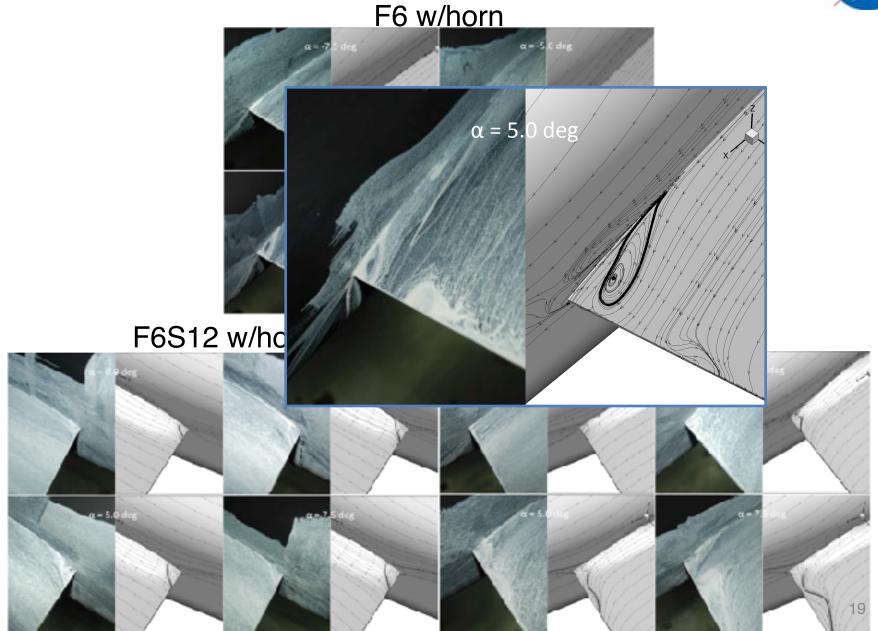


F6S12 w/horn

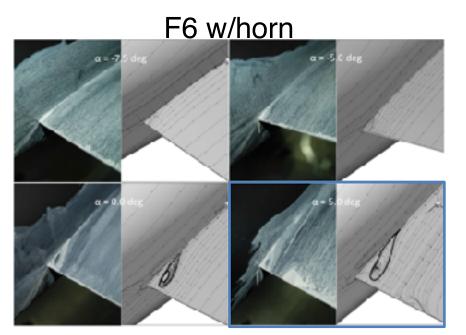
COCA w/horn





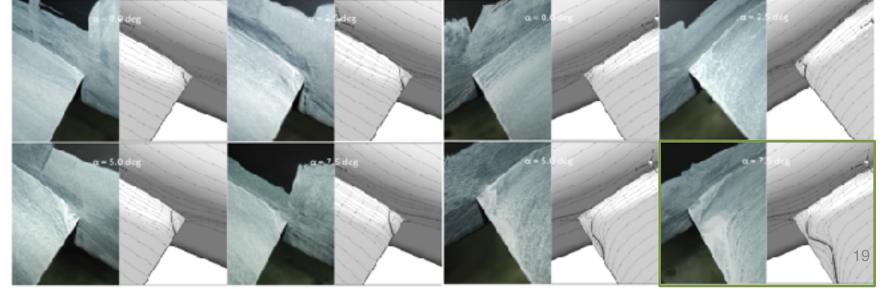




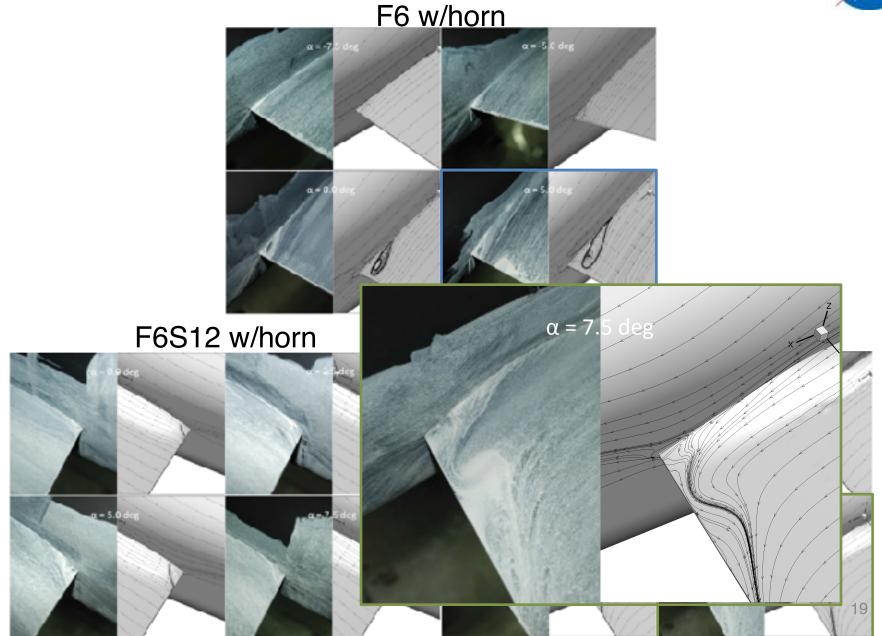


F6S12 w/horn

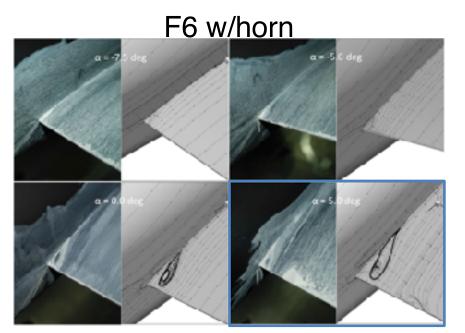
COCA w/horn





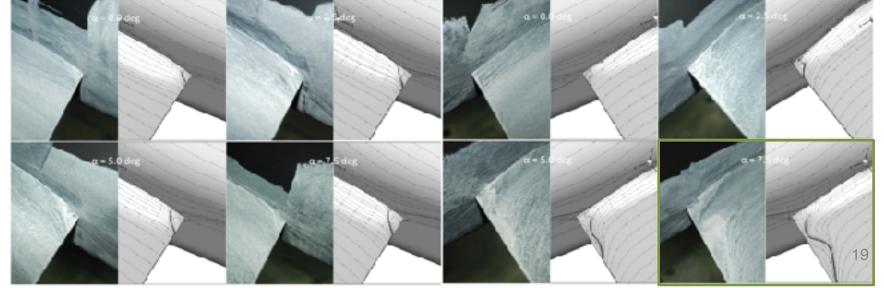






F6S12 w/horn

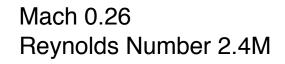
COCA w/horn



14x22 6% Risk Reduction Test







14x22 6% Risk Reduction Setup

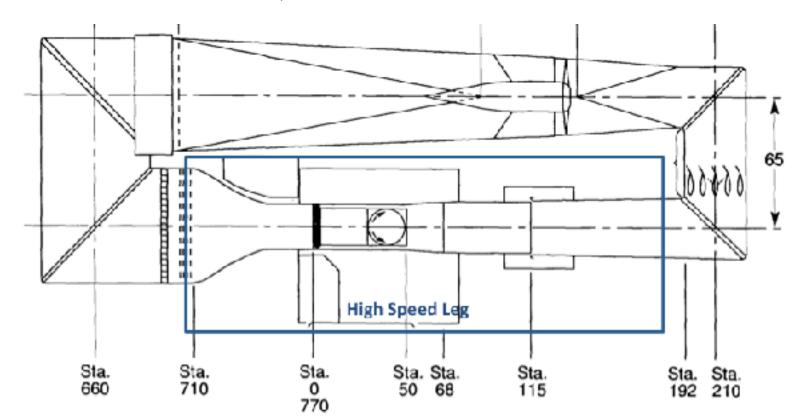


- Three data sources
 - Experiment
 - CFD in Free Air
 - CFD with 14x22 wind tunnel walls
- Comparisons: oil flow vs streamlines
- Additional results for $\alpha = -10.0 10.0$ degrees in paper
- Additional experimental results in NASA TM-219348

NASA Langley 14- by 22-Foot Subsonic Tunnel



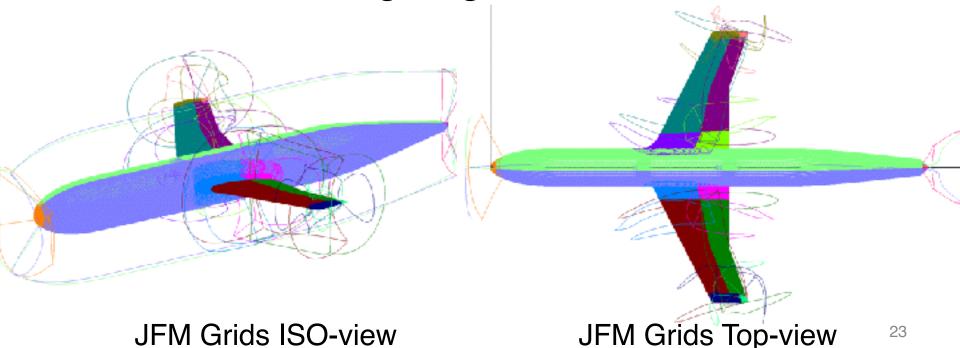
- 14.5 ft high by 21.75 ft wide test section
- Closed-circuit wind tunnel
- Blue box represents high speed leg
- RE = 2.4 million, Mach 0.26



Juncture Flow Model Grids



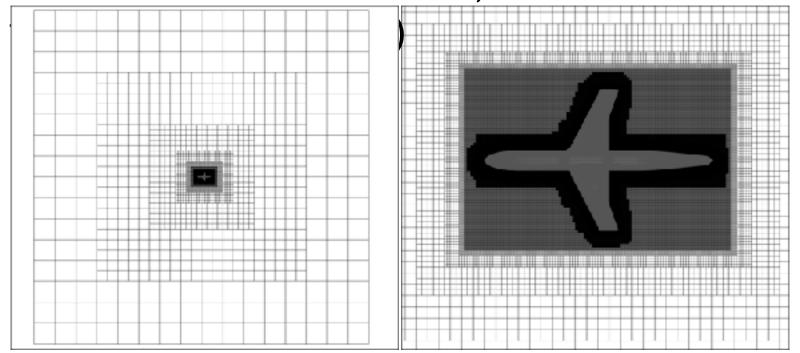
- Grids created based on best practices, as defined by AIAA workshops (DPW, HiLift, etc)
- Grid resolution study was performed early on to establish grid guidelines for all cases



JFM Free Air Cases



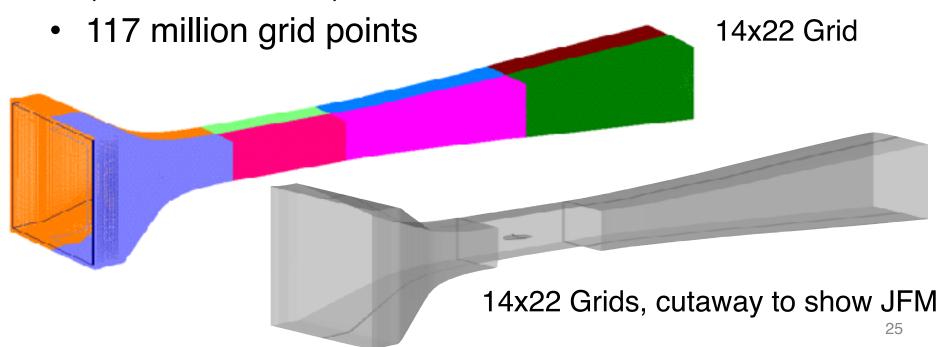
- JFM grids, imbedded in Overflow's off body grids
- Fairfield at 100 chord lengths away
- 108 Million grid points
- 420 Intel Broadwell cores, 12 hours wall



JFM Wind Tunnel Cases



- JFM grids, installed in the 14x22 wind tunnel grids
- Inflow BC: Stagnation pressure/temperature
- Outflow BC: Back pressure iterated to match tunnel speed.
- 1200 Intel Ivy Bridge cores, 60-120 hours wall time (NASA Pleiades)

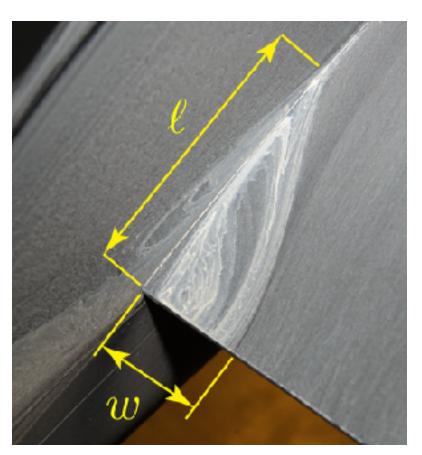


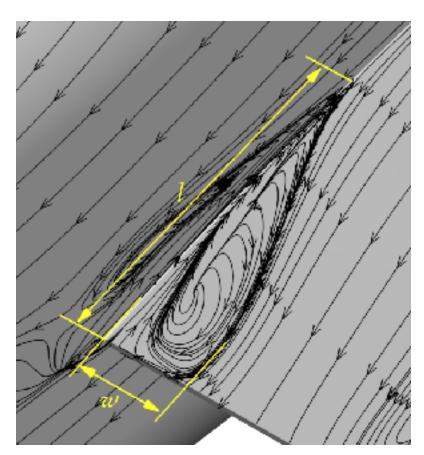
SOB Bubble Size Definitions



Experiment Oil Flow





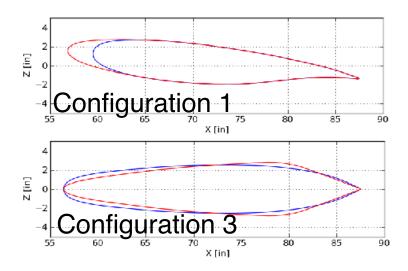


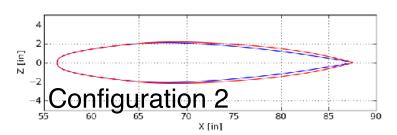
length I and width w bubble size definitions

Wing Configurations



Configuration	Port Wing	Starboard Wing	Data
1	F6 no horn	F6 w/horn	Exp, CFD Free Air, CFD WT
2	NACA 0015 w/horn	NACA 0015mod w/horn	Exp, CFD Free Air, CFD WT
3	F6S12 w/horn	COCA w/horn	Exp, CFD Free Air



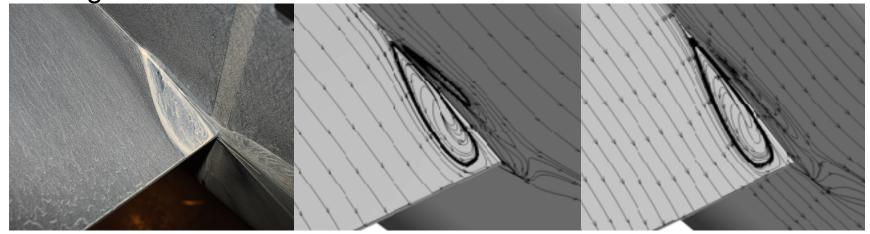


- Port Wing (blue)
- Starboard Wing (red)

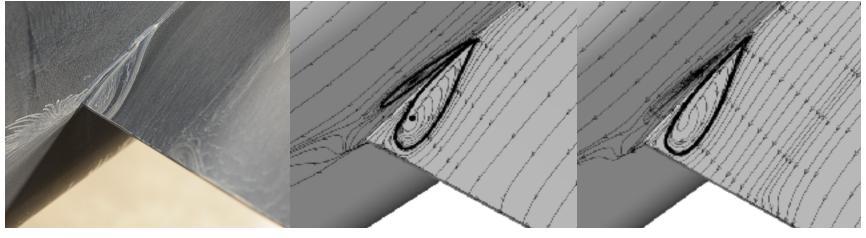
Configuration 1: F6 no horn—F6 w/horn, α =5.0°



Port Wing: F6 no horn



Starboard Wing: F6 w/horn



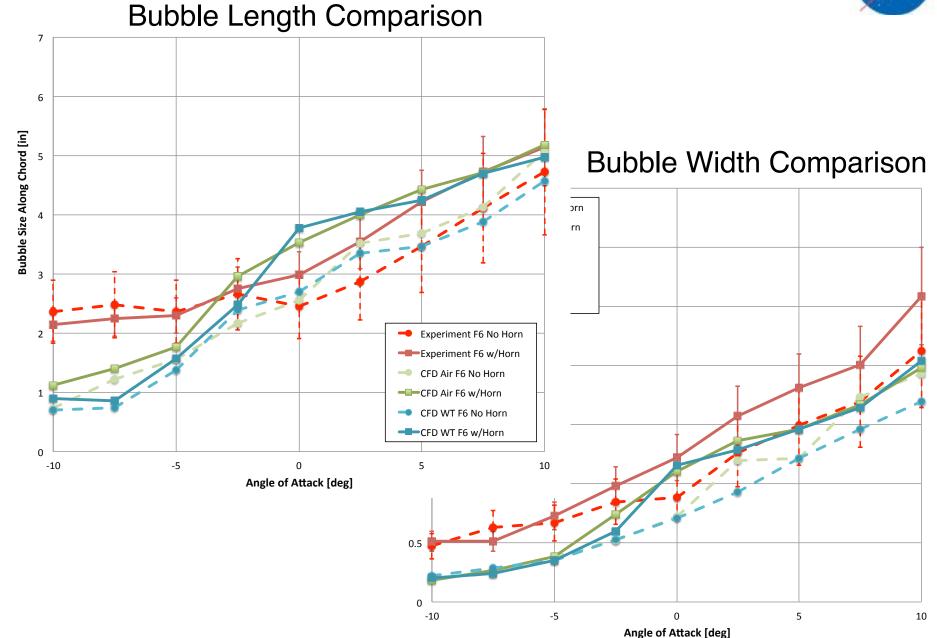
Experiment

CFD Free Air

CFD WT

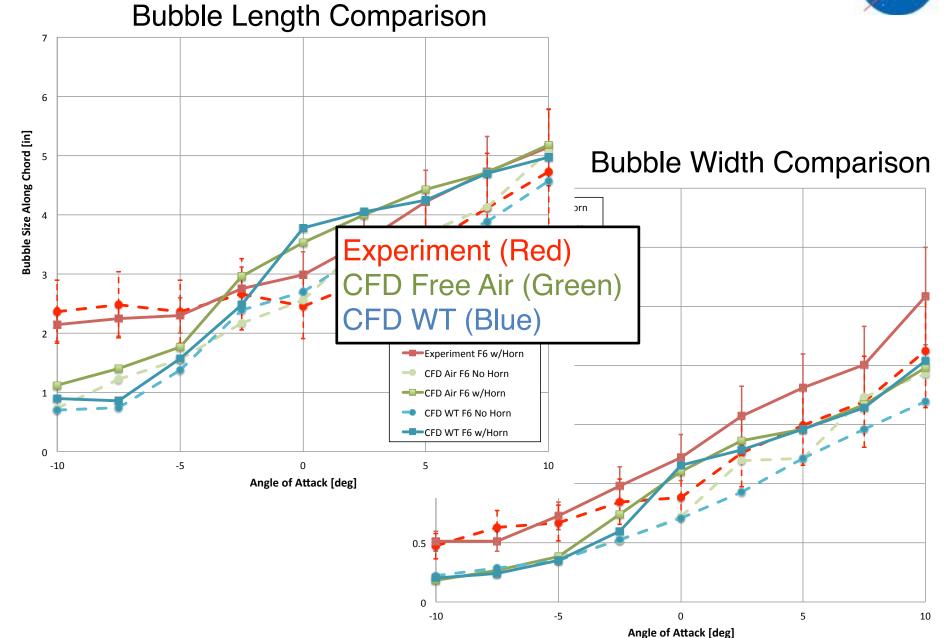
Configuration 1: F6 no horn—F6 w/horn





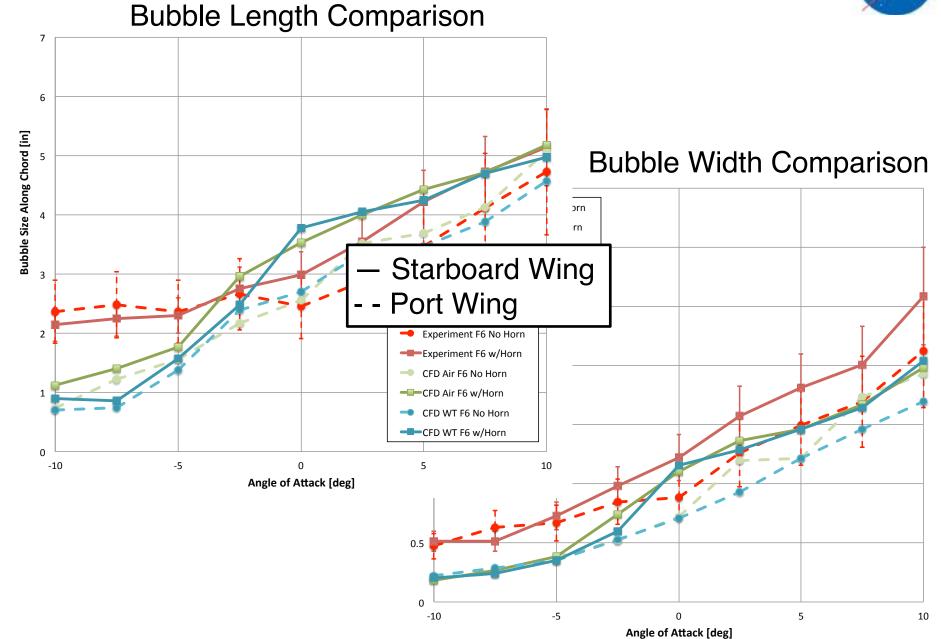
Configuration 1: F6 no horn—F6 w/horn





Configuration 1: F6 no horn—F6 w/horn

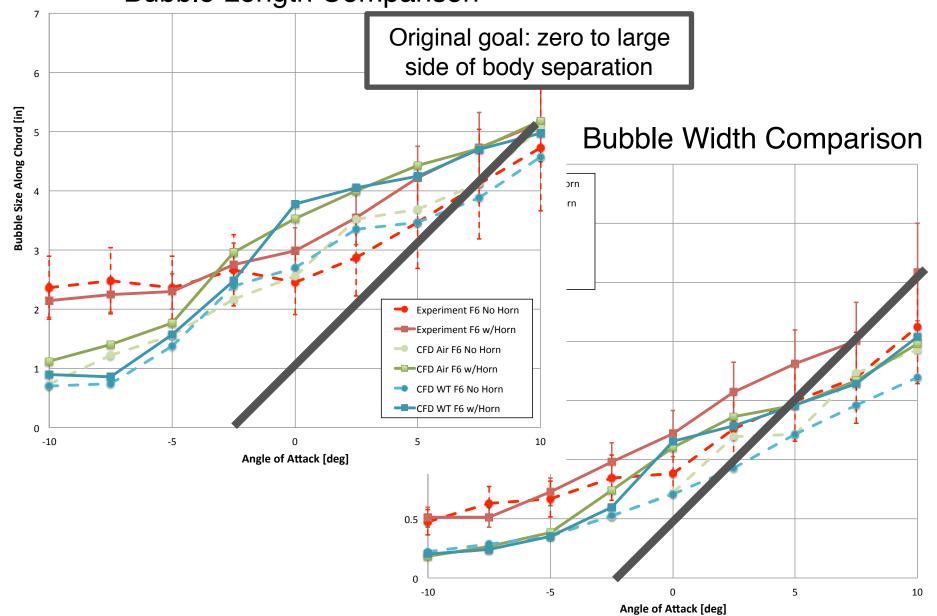




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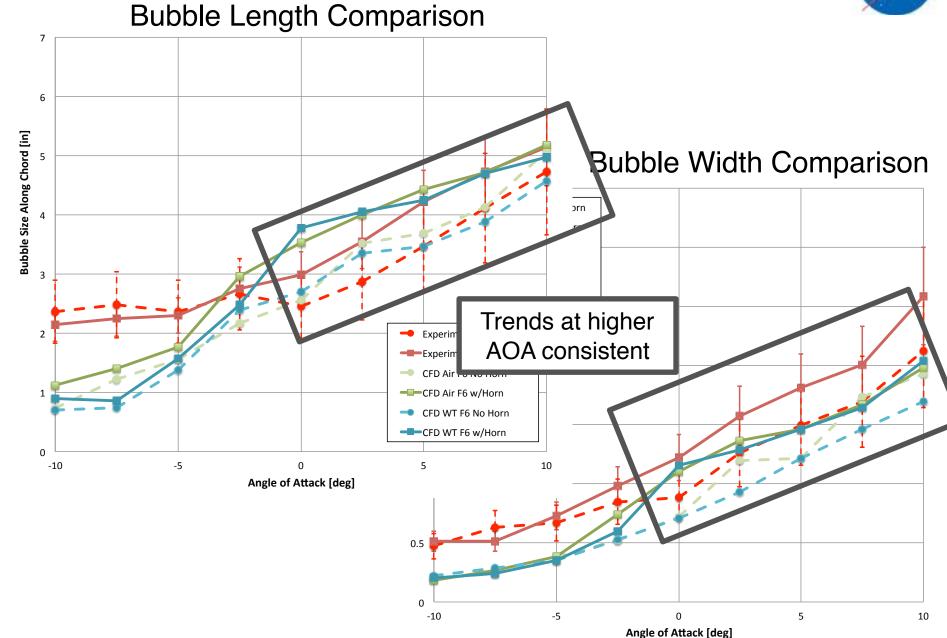


Bubble Length Comparison



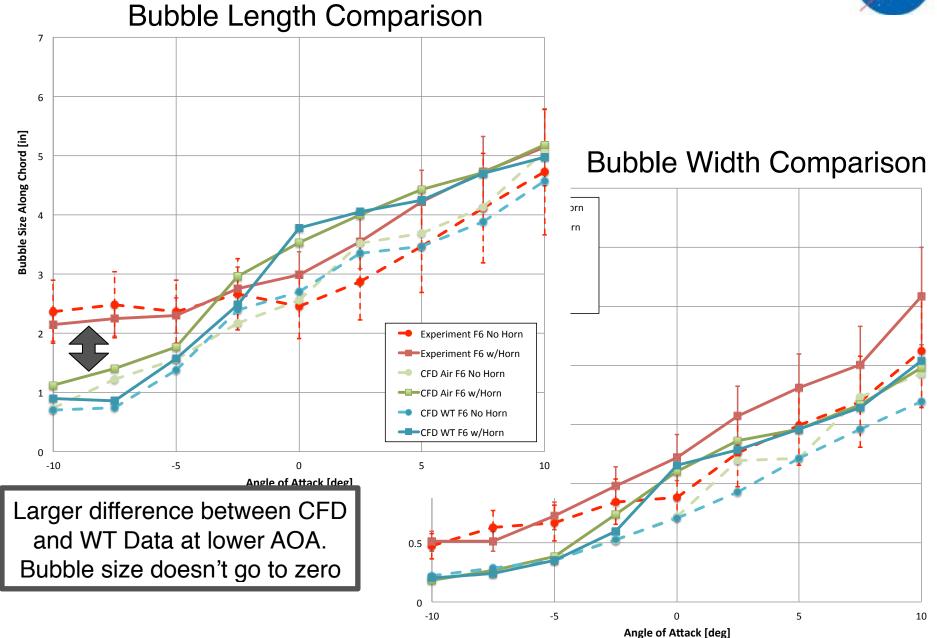
Configuration 1: F6 no horn—F6 w/horn



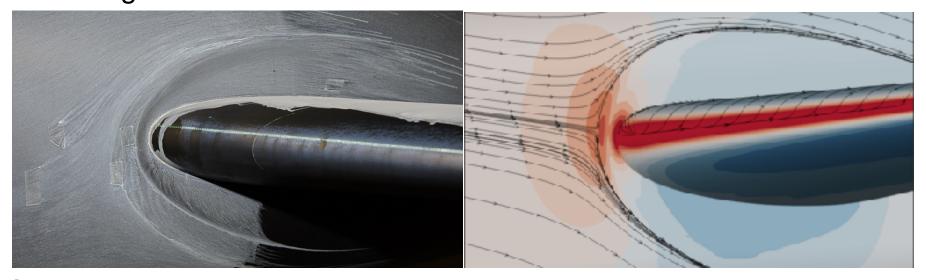


Configuration 1: F6 no horn—F6 w/horn

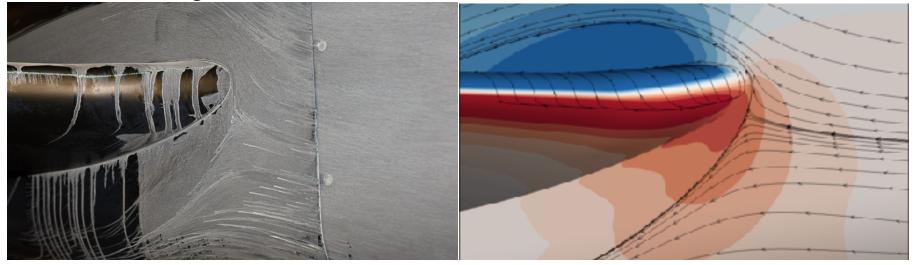




Configuration 1: F6 no horn—F6 w/horn, α =5.0° LE Port Wing: F6 no horn



Starboard Wing: F6 w/horn



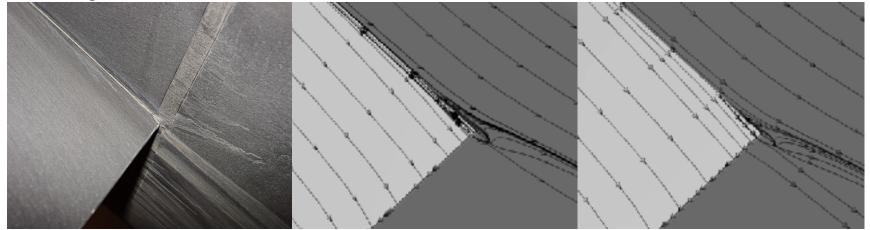
Experiment

CFD WT

Configuration 2: NACA 0015—NACA 0015mod, α =5.0°

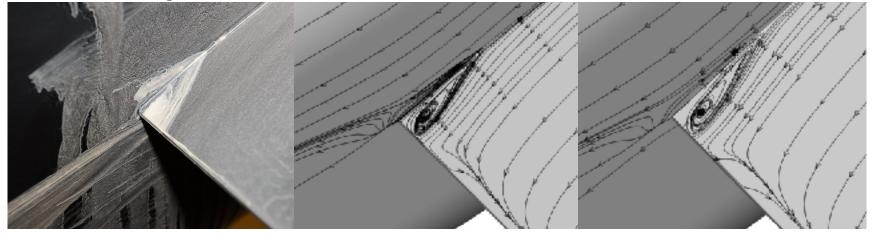


Port Wing: NACA 0015 w/horn



*Was run without horn

Starboard Wing: NACA 0015mod w/horn



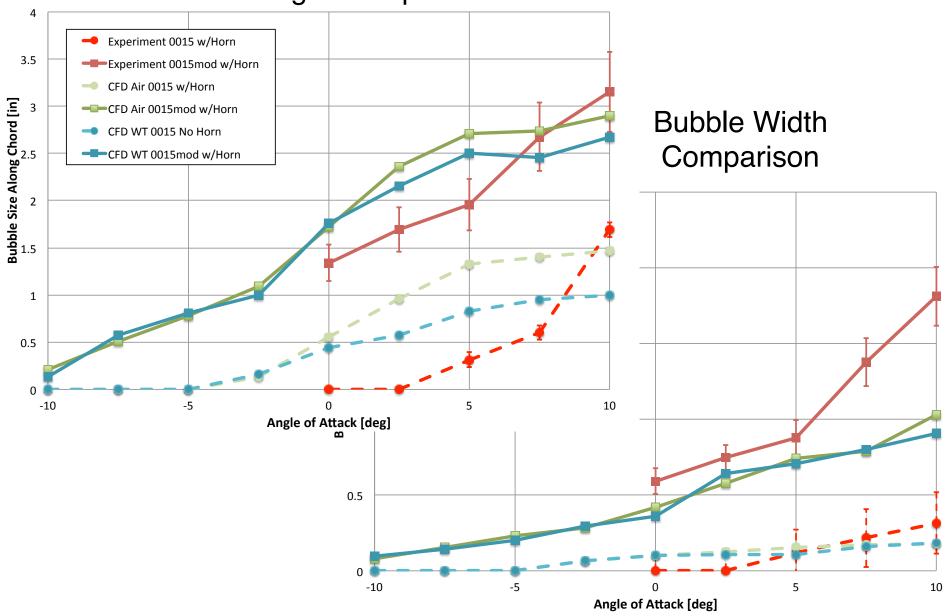
Experiment

CFD Free Air

CFD WT

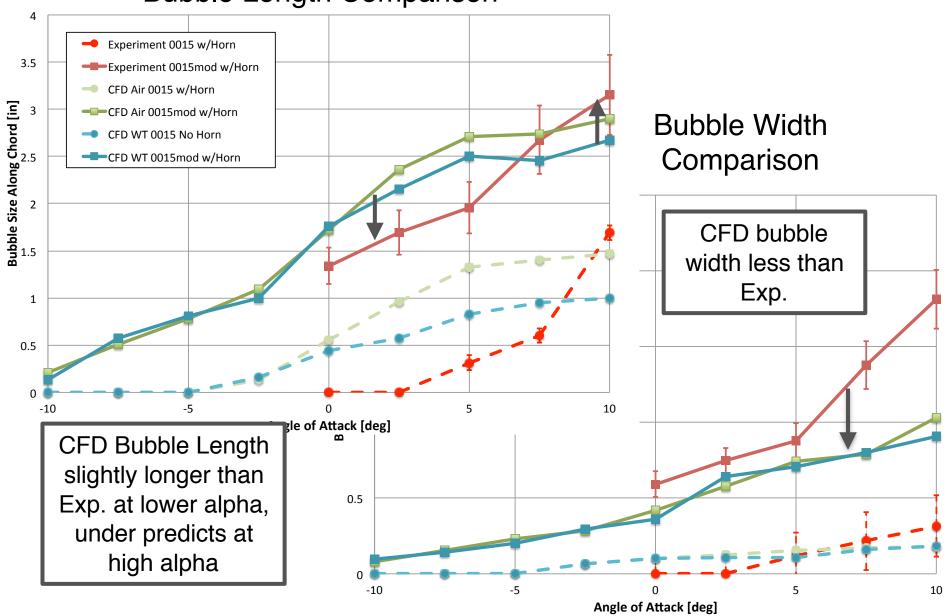






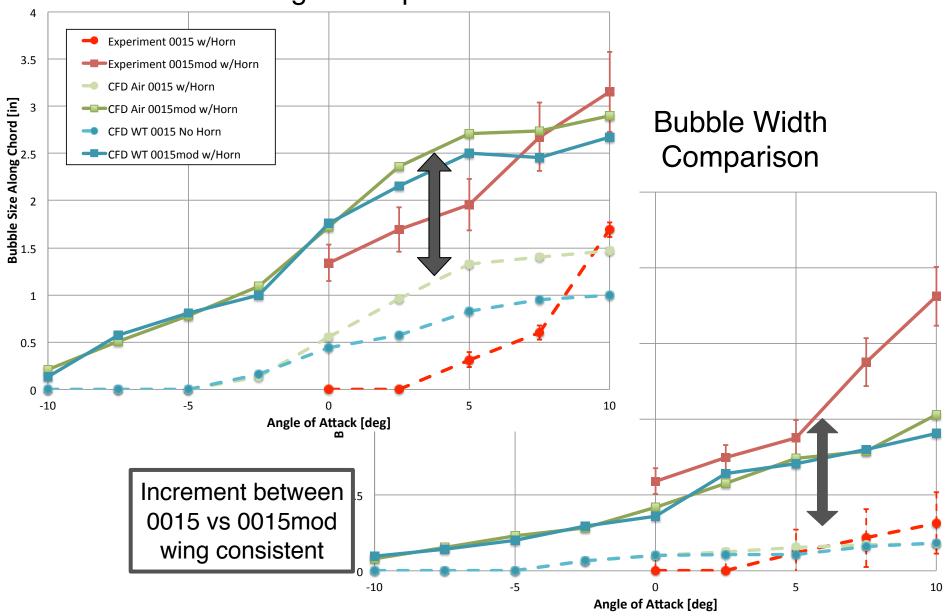






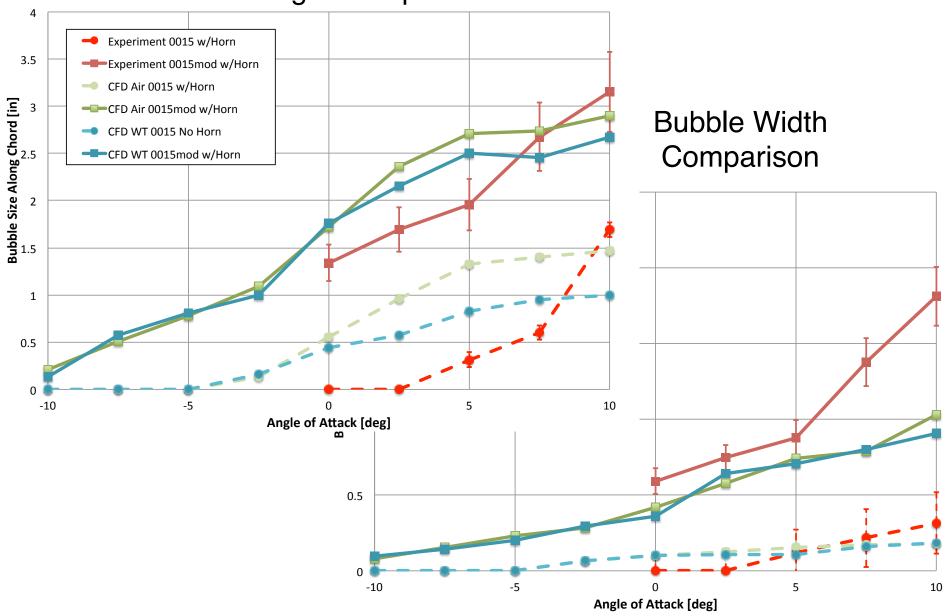






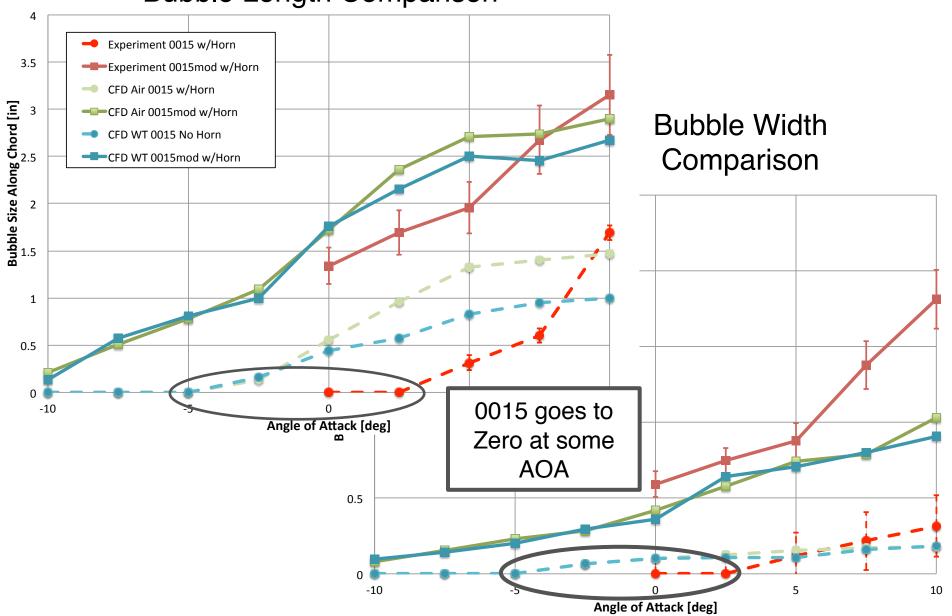












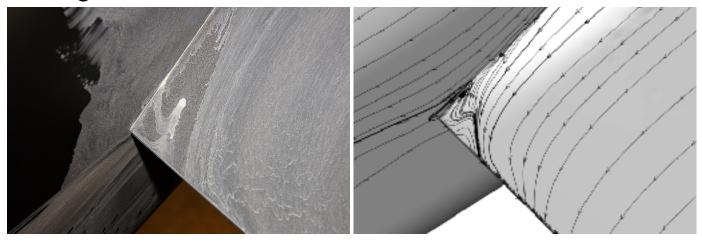
Configuration 3: F6S12—COCA, α =5.0°



Port Wing: F6S12 w/horn



Starboard Wing: COCA w/horn



Experiment

CFD Free Air

Wing Evaluations



- Trends between CFD and Experiment are very good
- F6 showed medium to large side of body separations
- NACA 0015 showed none to small separation
- NACA 0015mod showed small to medium separation
- COCA wing and F6S12 ruled out
- LE-horn indicates smaller LE horseshoe vortex





- Performed wing design evaluations with CFD
- Performed companion CFD risk assessments with the risk reduction experiments
- CFD analysis combined with risk reduction experiments, results in high confidence in selecting the final models



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 Fuselage Model & Wing models delivered May 2017





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 Fuselage Model & Wing models delivered May 2017

Tunnel entry 1: November 2017





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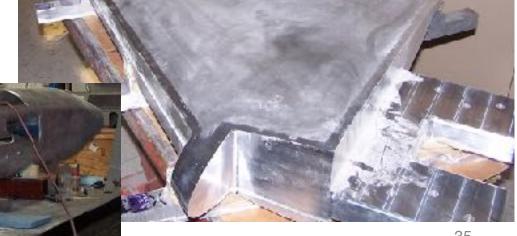
• F6 (primary)

• 0015 (secondary)

 Fuselage Model & Wing models delivered May 2017

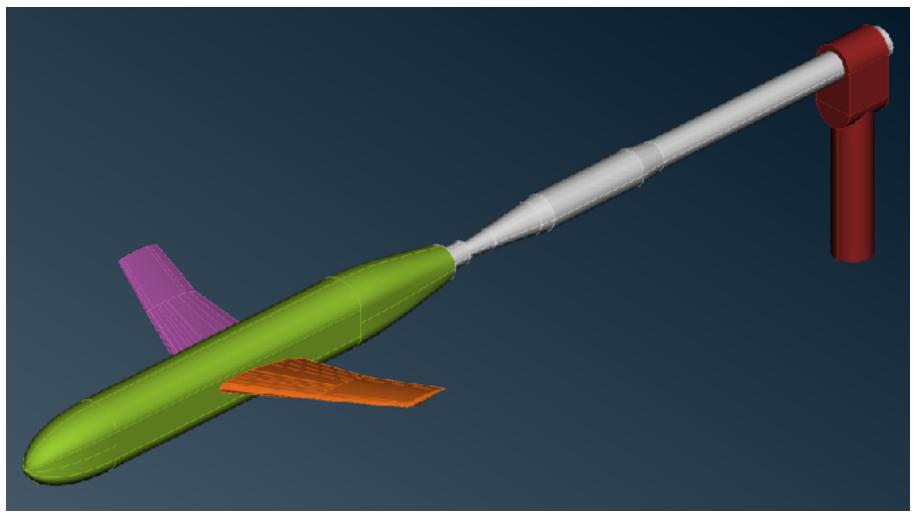
Tunnel entry 1: November 2017

Tunnel entry 2: March 2018



Upcoming CFD



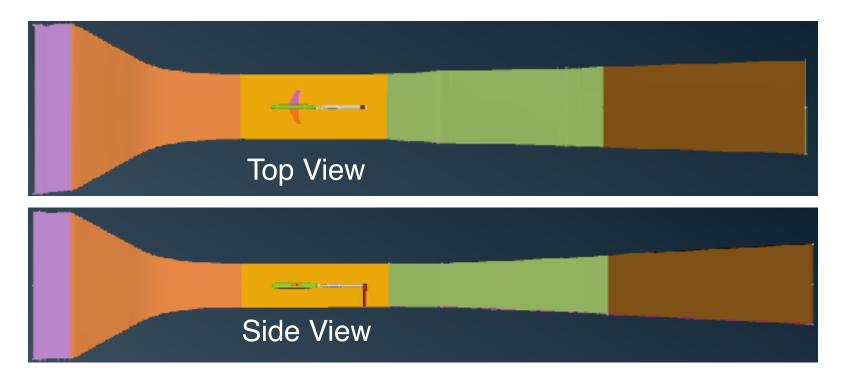


Mock up of the JFM 8% model with roll sting and mast

Upcoming CFD



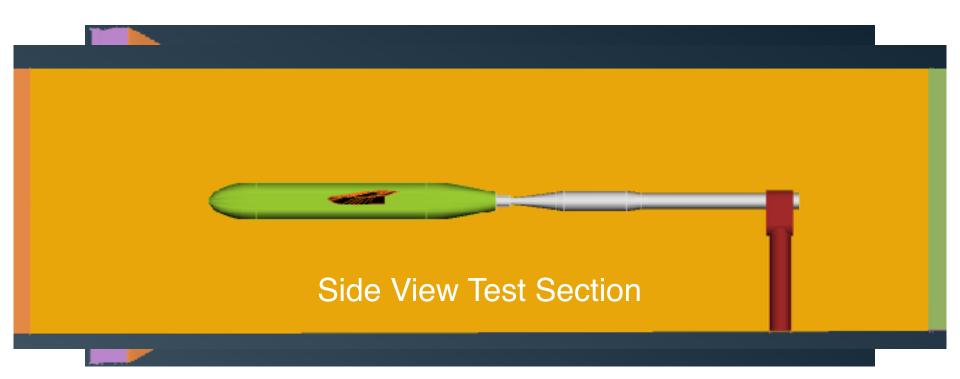
- Run with Overflow & Fun3D
- Incremental buildup
 - Free air: JFM, JFM + Sting, JFM + Sting + Mast
 - 14x22 WT: JFM, JFM + Sting, JFM + Sting + Mast



Upcoming CFD



- Run with Overflow & Fun3D
- Incremental buildup
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 - 14x22 WT: JFM, JFM + Sting, JFM + Sting + Mast



Acknowledgements



NASA's Transformational Tools and Technologies (T3) Project

Chris Rumsey and the Juncture Flow committee:

NASA Langley: P. Balakumar, Mark Cagle, Dick Campbell, Jan-Renee Carlson, Andy Davenport, Kevin Distill, Judy Hannon, Luther Jenkins, Bil Kleb, Mujeeb Malik, Cathy McGinley, Joe Morrison, Frank Quinto, Don Smith, Sandy Webb

NASA Ames: James Bell, Nettie Roozeboom, Laura Simurda, Greg Zilliac

Boeing: Mike Beyer, Neal Harrison, Peter Hartwich, Philippe Spalart, Tony Sclafani, John Vassberg

AUR: Gwibo Byun and Roger Simpson

Virginia Tech: Aurelien Borgoltz and Todd Lowe

University of Kentucky: Jim Coder

Bill Oberkampf