

Orion Powered Flight Guidance Burn Options for near term exploration

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Powered Flight Guidance to support MPCV Mandate

“...missions beyond low-Earth orbit ...conduct regular in-space operations...alternative means for delivery of crew and cargo to the ISS...capacity for efficient and timely evolution...”

- NASA Authorization Act of 2010

- Provide Burn Guidance for Range of Missions

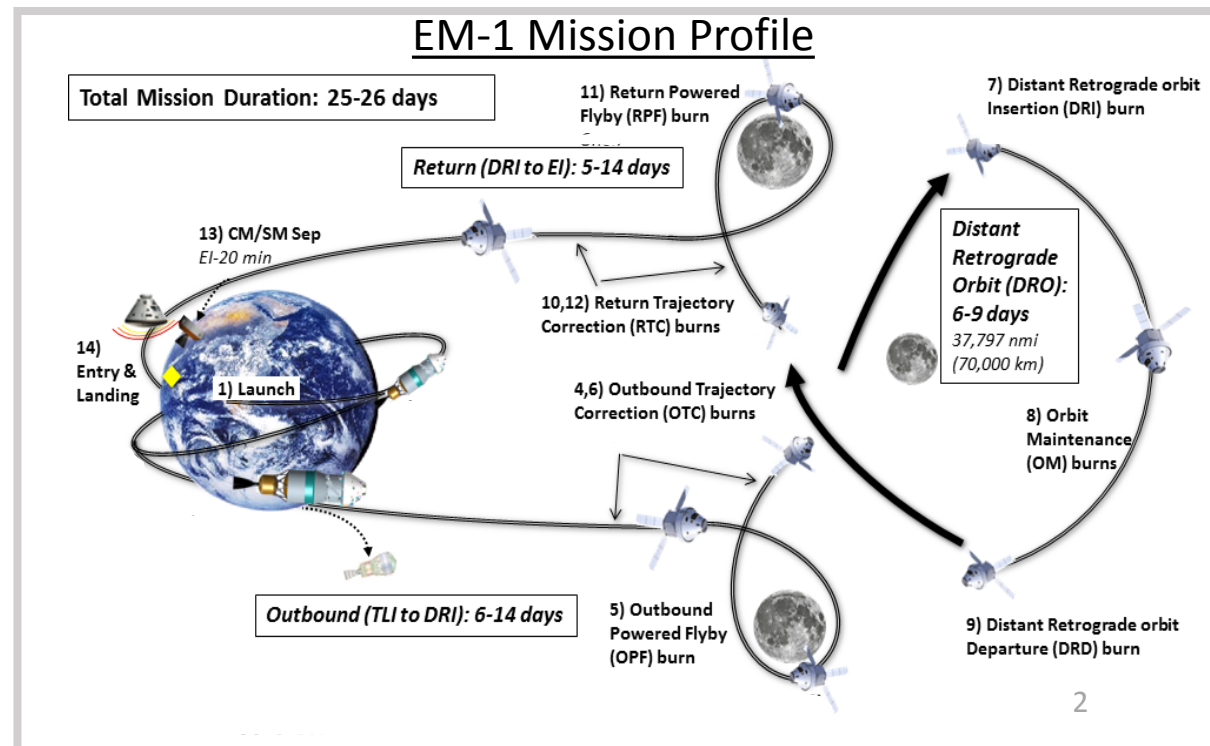
- LEO & Beyond

- Flexibility

- Nominal
- Abort

- Evolutionary

- EM-1 and Beyond





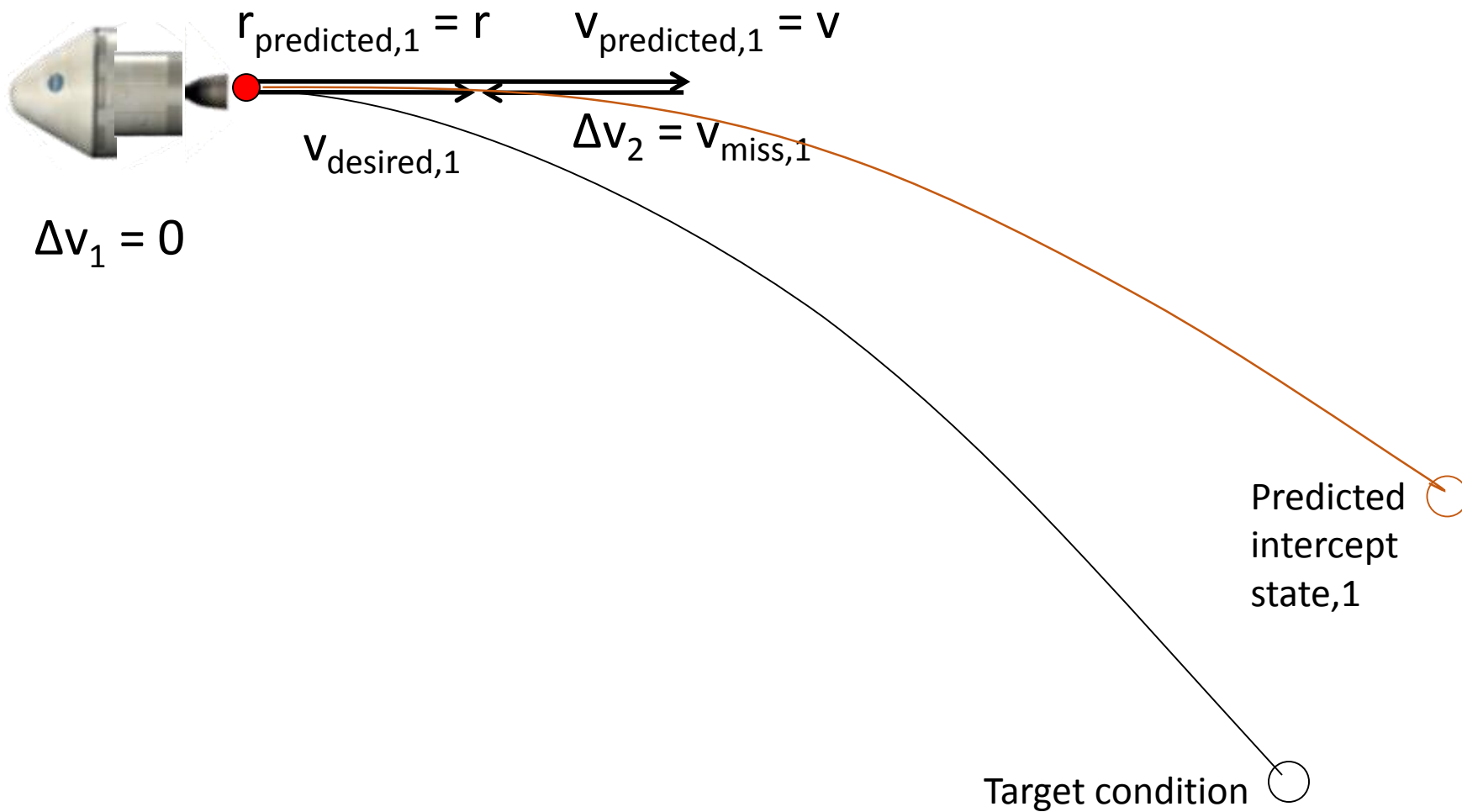
OrbGuid: Executive Summary



- Primary Function: Guide the vehicle through a burn such that, vehicle achieves a desired trajectory at burn cutoff.
- Uses the Powered Explicit Guidance (PEG) algorithm.
 - Shuttle heritage with numerous extensions and added capability.
 - Explicit – no reliance on an a reference trajectory.
- OrbGuid acts as a wrapper executive to call the PEG algorithm.
- Architecture supports a menu of desired (burn cutoff) velocity options.
 - Current suite of five options
 - New desired velocity options can be added as necessitated by the mission.

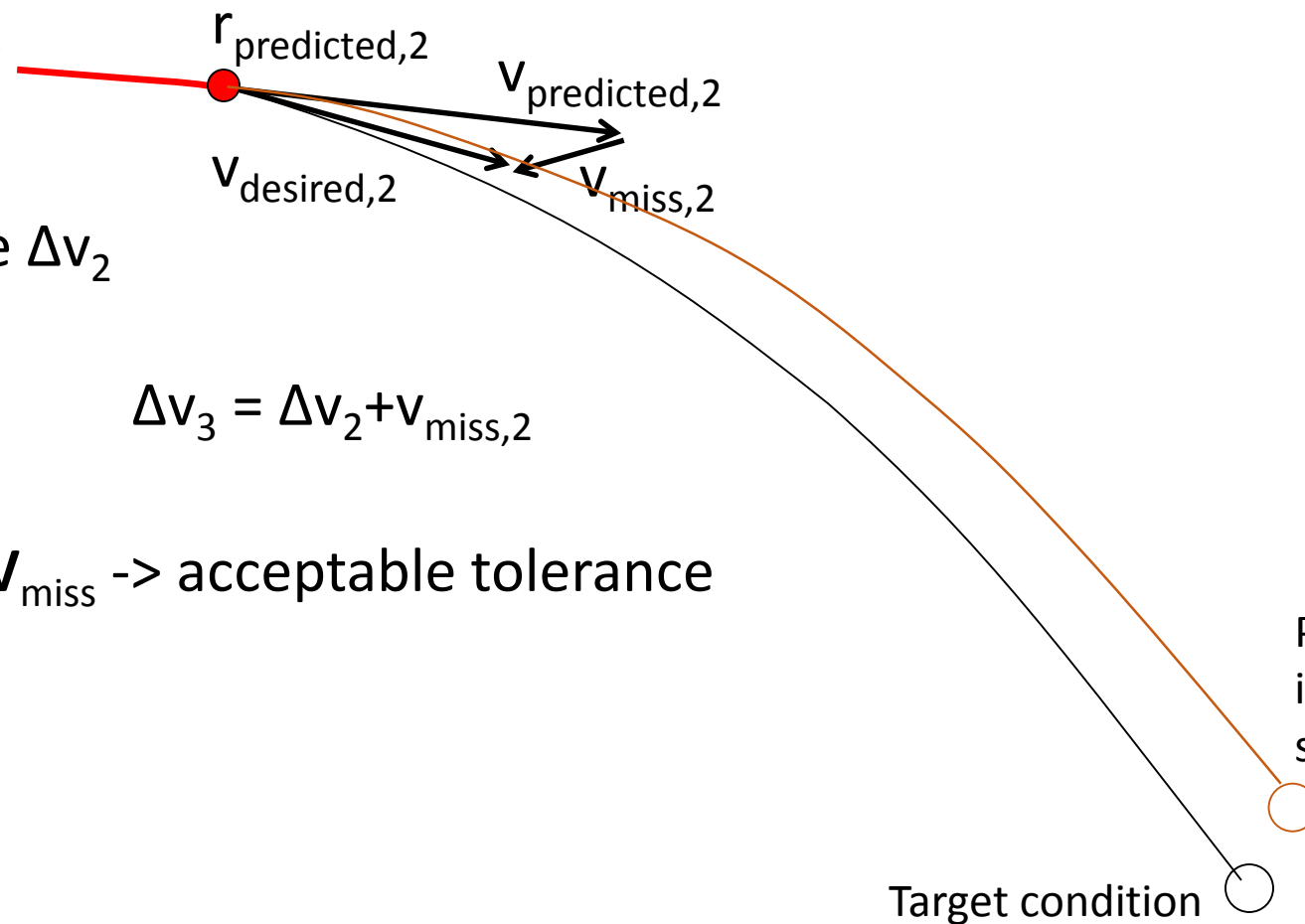


Powered Explicit Guidance





Powered Explicit Guidance



Propagate Δv_2

$$\Delta v_3 = \Delta v_2 + v_{\text{miss},2}$$

Etc. until $\mathbf{V}_{\text{miss}} \rightarrow$ acceptable tolerance

Predicted intercept state,2

Target condition



OrbGuid Executive

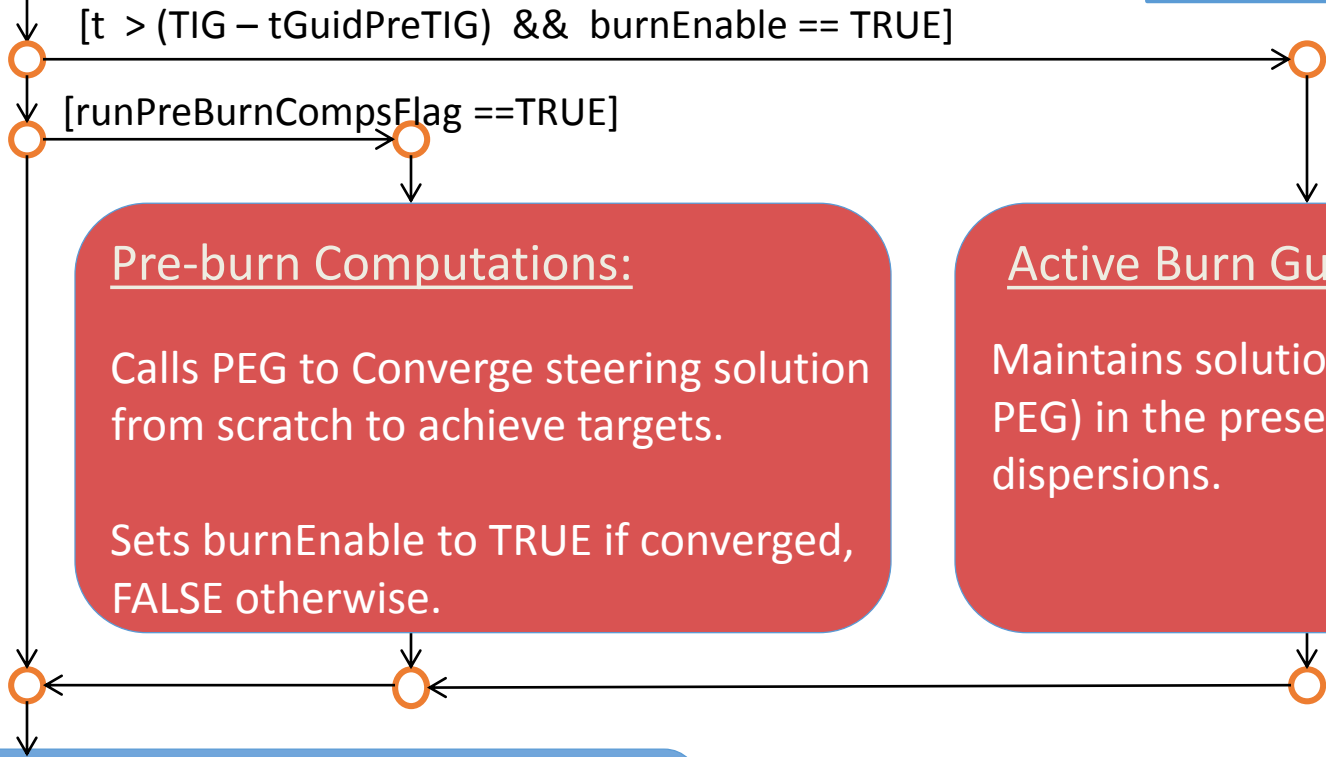


Exec:

Controls execution initializations, resets, transitions

OrbGuid runs in two execution modes, shown in brown boxes:

- Pre-burn computations:
- Active burn guidance:



Pre-burn Computations:

Calls PEG to Converge steering solution from scratch to achieve targets.

Sets burnEnable to TRUE if converged, FALSE otherwise.

Active Burn Guidance:

Maintains solution (via call to PEG) in the presence of dispersions.

Output Processing:

Burn cutoff time, Steering outputs



OrbGuid (PEG)

START

$$\mathbf{v}_{go} = \mathbf{v}_{go} - \Delta \mathbf{v}$$
$$nCycles = 0$$

[nCycles < NMAX && norm(\mathbf{v}_{miss}) < tolerance]

$$nCycles = nCycles + 1$$

Solve for burn time using rocket equation (t_{go})

Solve for elements of steering law

Predictor: predict cutoff state ($t_p, \mathbf{r}_p, \mathbf{v}_p$)

Compute desired state ($t_d, \mathbf{r}_d, \mathbf{v}_d$)

Insert appropriate burn option desired velocity solution algorithm (LTVC, etc.)

$$\mathbf{v}_{miss} = \mathbf{v}_p - \mathbf{v}_d$$

Corrector: update \mathbf{v}_{go} to null \mathbf{v}_{miss}

END

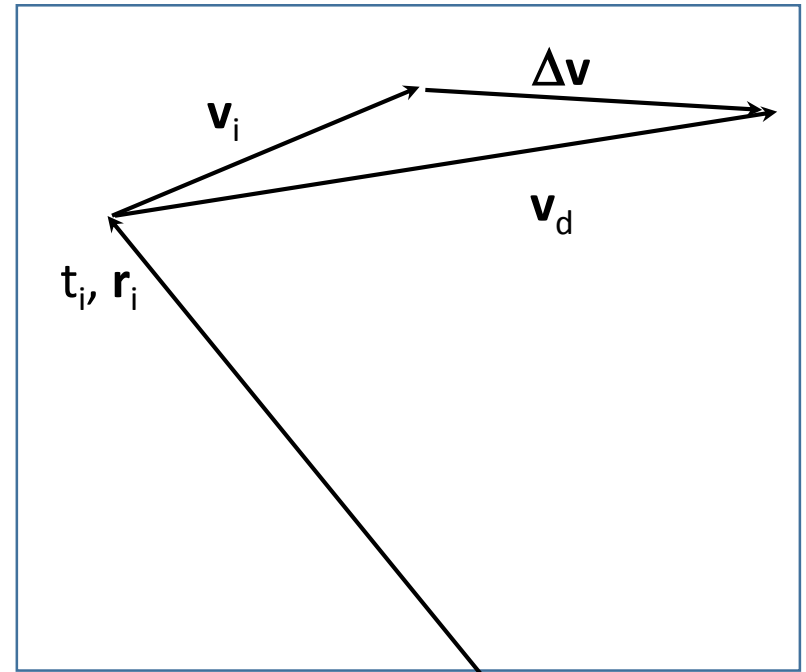
OrbGuid solution algorithm uses a predictor/corrector methodology to converge & maintain a stable guidance solution. Iteration variable is \mathbf{v}_{go} (the velocity to be gained by thrust)



External DV



- Spec: Ext- $\Delta\mathbf{V}$
 - in either TIG LVLH or inertial Frame
- Typical Usage
 - Trajectory Correction Burns
 - Orbit maintenance
- PEG yields $\mathbf{V}_{go} = \text{Ext-}\Delta\mathbf{V}$





Linear Terminal Velocity Constraint (LTVC)

- Space Shuttle heritage transfer problem
 - Result of a search for a generalized targeting algorithm.

- Linear Velocity Constraint imposed at Intercept

$$\vec{v}_r = C_1 + C_2 \vec{v}_h$$

- Spec r_T, C_1, C_2 (& TIG)

- r_T : sometime as a spec altitude a spec transfer angle from TIG

- Used on Shuttle Orbit insertion & Deorbit

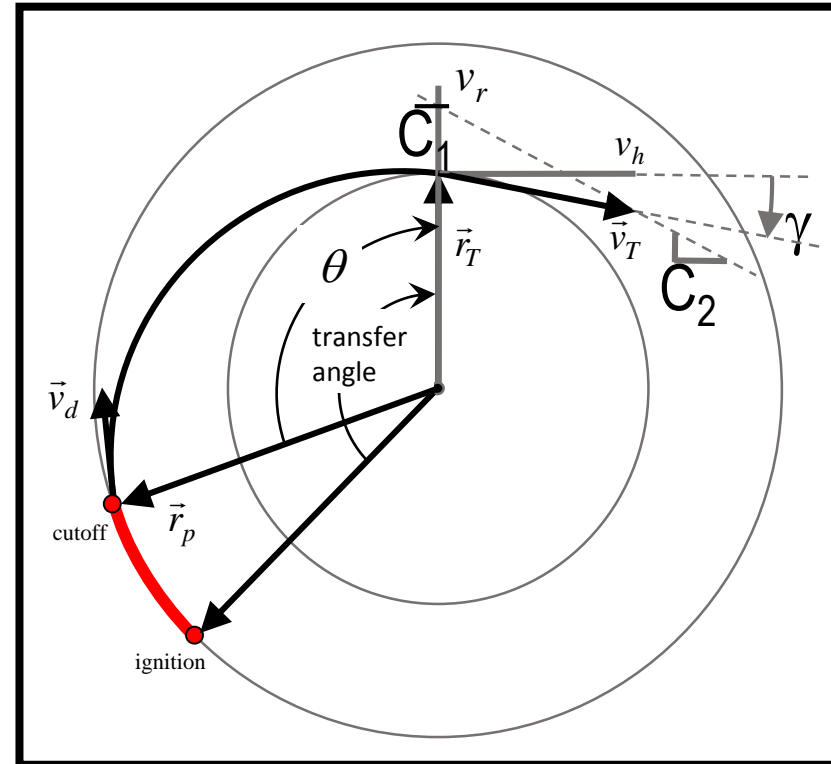
- Common Transfers

- Line-of-Apsides Control / Hohmann-like transfers
 - Target defines desired Apsis altitude and location
 - $C_1 = C_2 = 0$
- Deorbit
 - Target defined Entry Interface
 - $C_1 = 0; C_2 = \tan(\gamma_{EI})$

- Solution is a quadratic in the unknown $v_{T,h}$

$$[k(1+w^2) + 2(1-wC_2)](v_{T,h})^2 - 2wC_1 v_{T,h} - \frac{2\mu}{r_T} = 0$$

- $v_{T,r}$ From constraint; Map \vec{v}_T back to \vec{r}_p to obtain \vec{v}_d



$$k = \frac{r_T - r_d}{r_d}$$

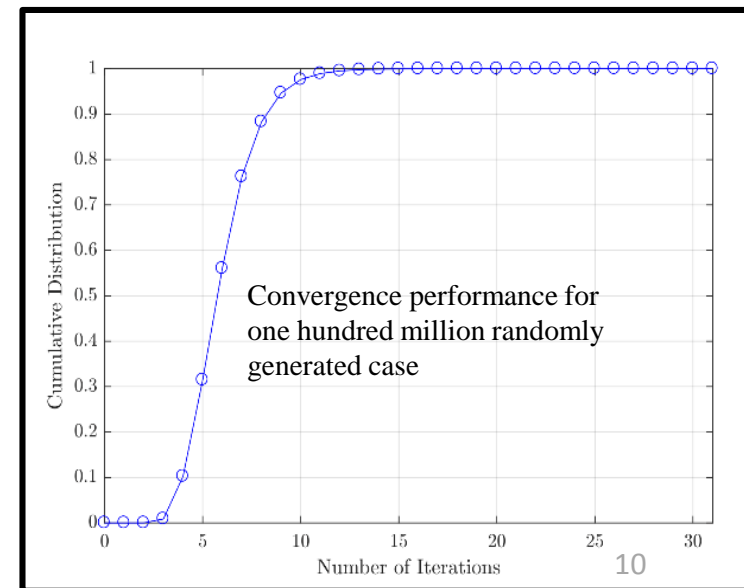
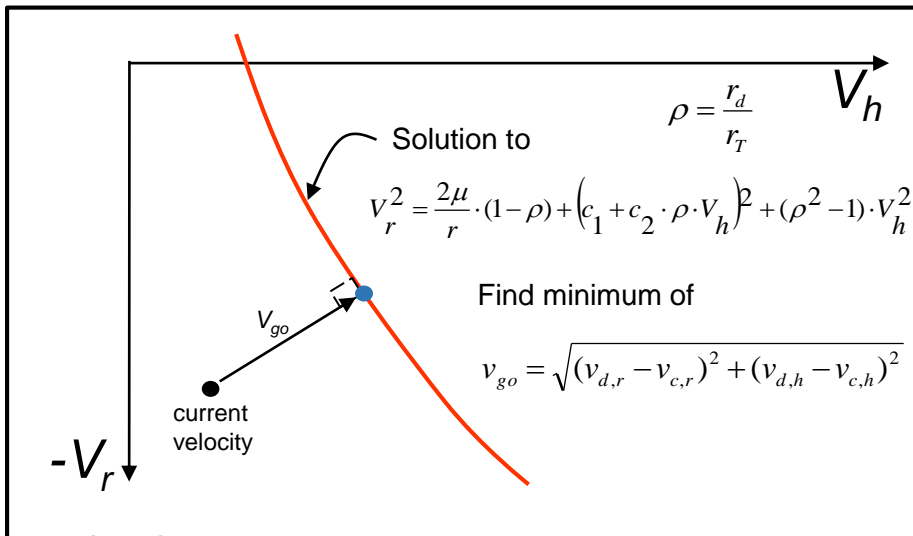
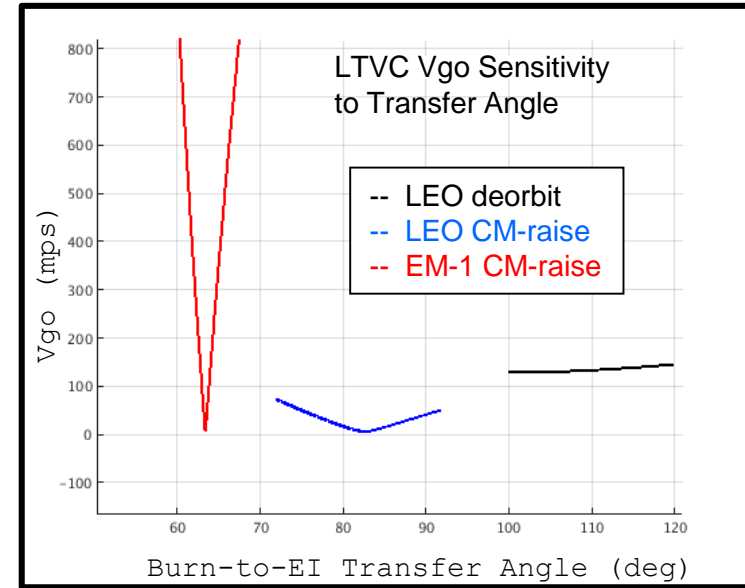
$$w = \cot \frac{\theta}{2} = \frac{\sin \theta}{1 - \cos \theta}$$



Free-Range LTVC (FRLTVC)



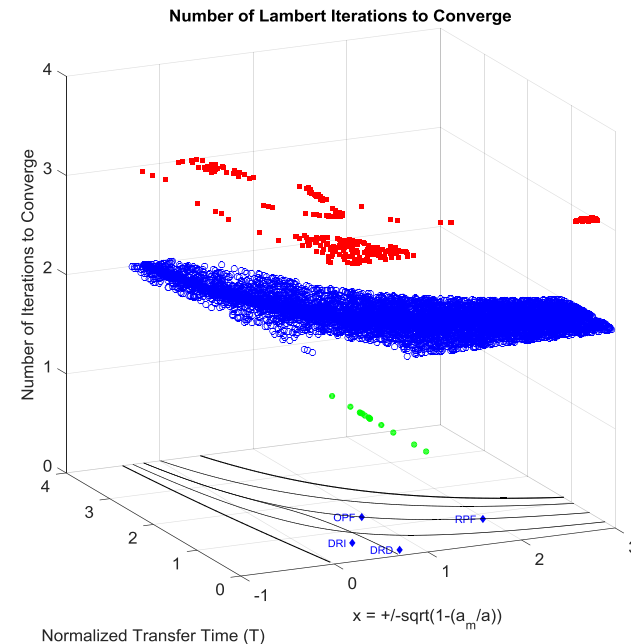
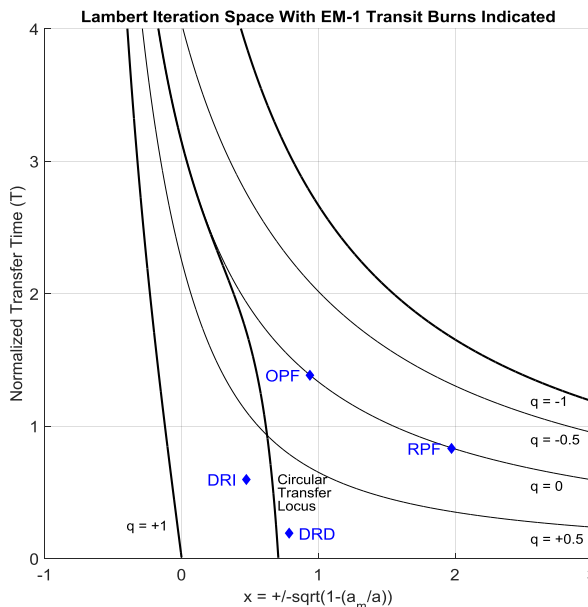
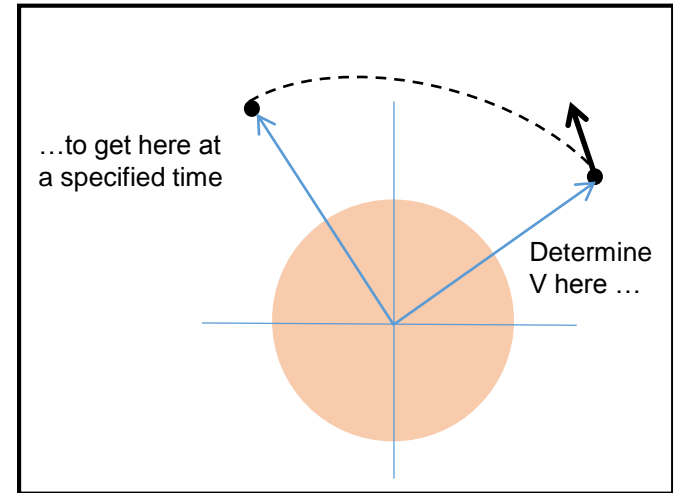
- Orion CM executes short burn to separate from the SM prior to Entry
 - Via Shallower flight-path angle at EI
- FRLTC created to address extreme sensitivity of LTVC ΔV on return-from-moon Trajectory
 - CM-raise is a mini-deorbit adjustment burn
 - But Vehicle is close to EI
 - Eccentricity is near parabolic
- Resolution: relax transfer angle specification
- Spec r_T (magnitude only) , c_1 , c_2 (& TIG)
 - Optionally altitude





Transit / Lambert Desired Velocity

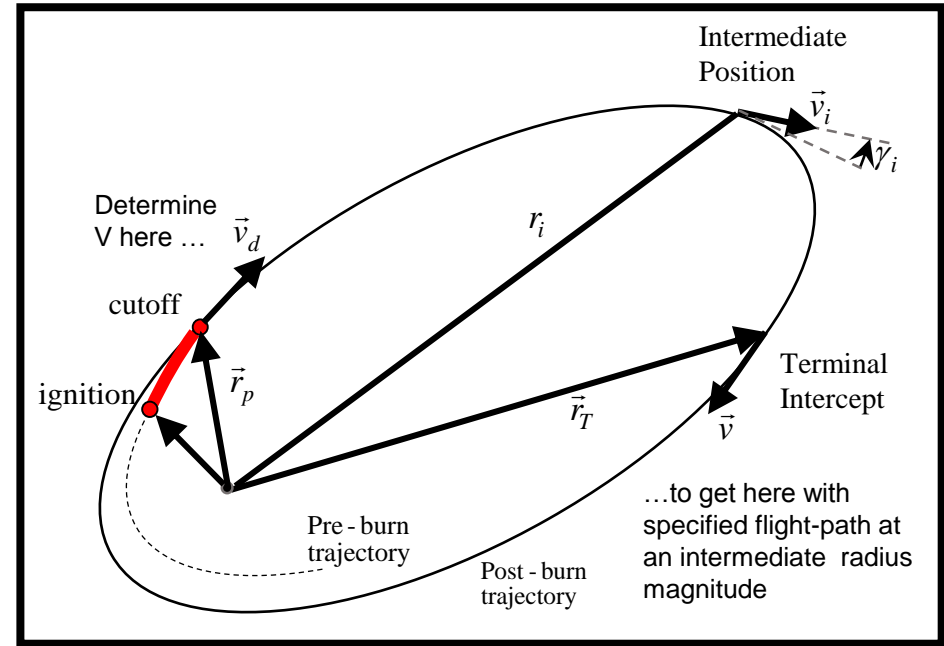
- Lambert guidance solves the two-point boundary value problem constrained by time-of-flight (TOF)
 - Adds a new parameter to define time-of-flight by specifying the time-of-intercept (i.e., transit time from ignition to intercept)
- Spec r_T , Transfer Time (& TIG)
- Algorithm based on work by Lancaster, Blanchard and Devaney (1966), but enhanced by Gooding.
 - Lancaster, Blanchard and Devaney based algorithm used on Shuttle
 - Gooding algorithm using for Constellation and is basis for Orion algorithm.
 - Gooding's new developments achieve a desired level of solution accuracy throughout the iteration space in a fixed number of iterations





Constrained Intermediate Terminal Intercept (CITI)

- Determines velocity required to intercept a specified target position vector (\vec{r}_T) while attaining a specified flight-path angle at an intermediate radius (r_i).
- Flight-path angle at the intercept target is not specified.
- Intermediate radius location is unimportant
- Spec r_T , r_i , γ_i (& TIG)
- An analytic solution exists:
 - Robertson (1972): “Closed Form Solution of a Certain Common Conic De-orbit Problem”.
 - Genesis is Return-to-Earth Targeting during Apollo.



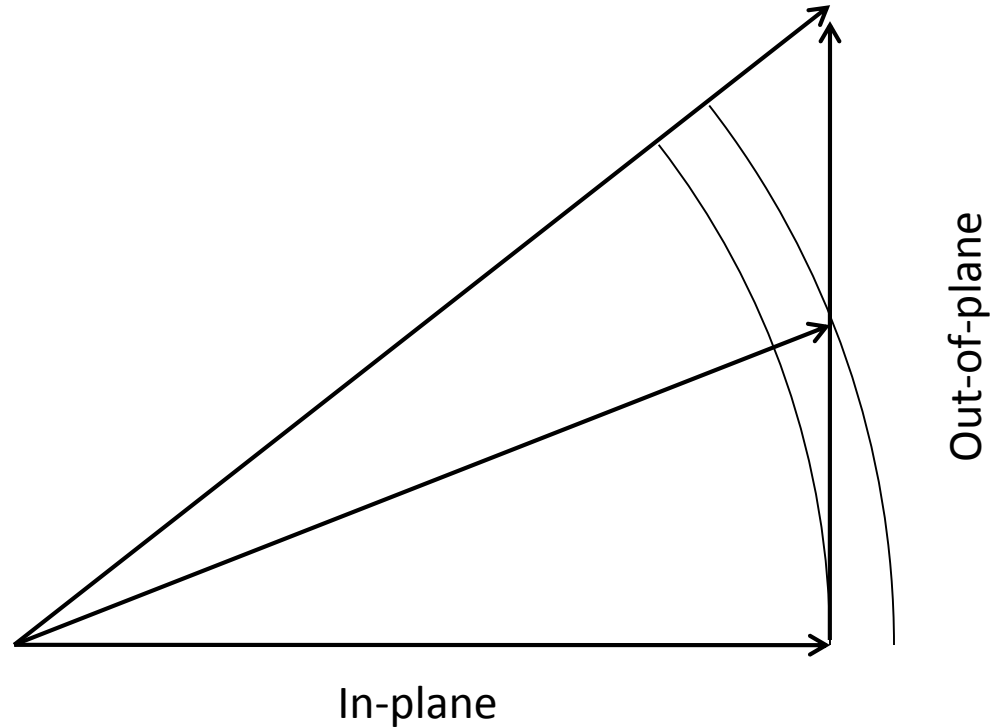
- Solution is a quadratic in the unknown Tangent of Flightpath angle at burn cutoff ($\Gamma_d = \tan(\gamma_d)$)

$$\Gamma_d^2 + 2\left(\frac{r_d}{r_i} - 1\right) \cot\left(\frac{\theta}{2}\right) \Gamma_d + \left[1 - \left(\frac{r_d}{r_i}\right)^2 (1 + \Gamma_i^2) + \frac{2}{1 - \cos\theta} \left(\frac{r_d}{r_i} - 1\right) \left(\frac{r_d}{r_T} - \cos\theta\right) \right] = 0$$

- Roots dependent on relationship between r_d , r_i & r_T (6 regions in all)
- Scenarios of current interest are $r_i > r_d > r_T$ (lunar and Earth orbit maintenance burns), and $r_d > r_i > r_T$ (direct return aborts during the outbound leg to the Moon and deorbit burns from LEO).



Out-of-Plane Constraints



$$\Delta v_{max, mass} = v_{ex} \ln (mass / mass_{min}) \quad (\text{preserve propellant reserves})$$

$$\Delta v_{max, tti} = -v_{ex} \ln(1 - (t_{go} + tti + tti_{min}) / \tau_A) \quad (\text{preserve coast time-to-intercept})$$



Questions?