

# Mars Propellant Liquefaction Modeling in Thermal Desktop

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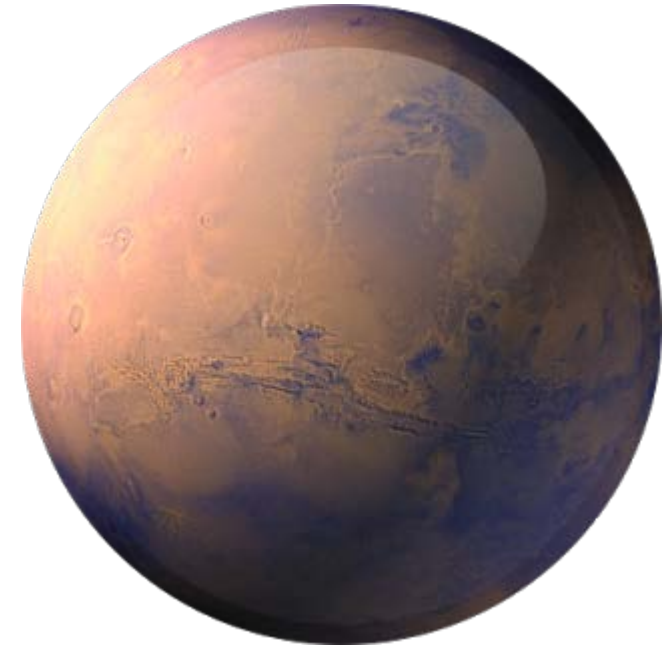
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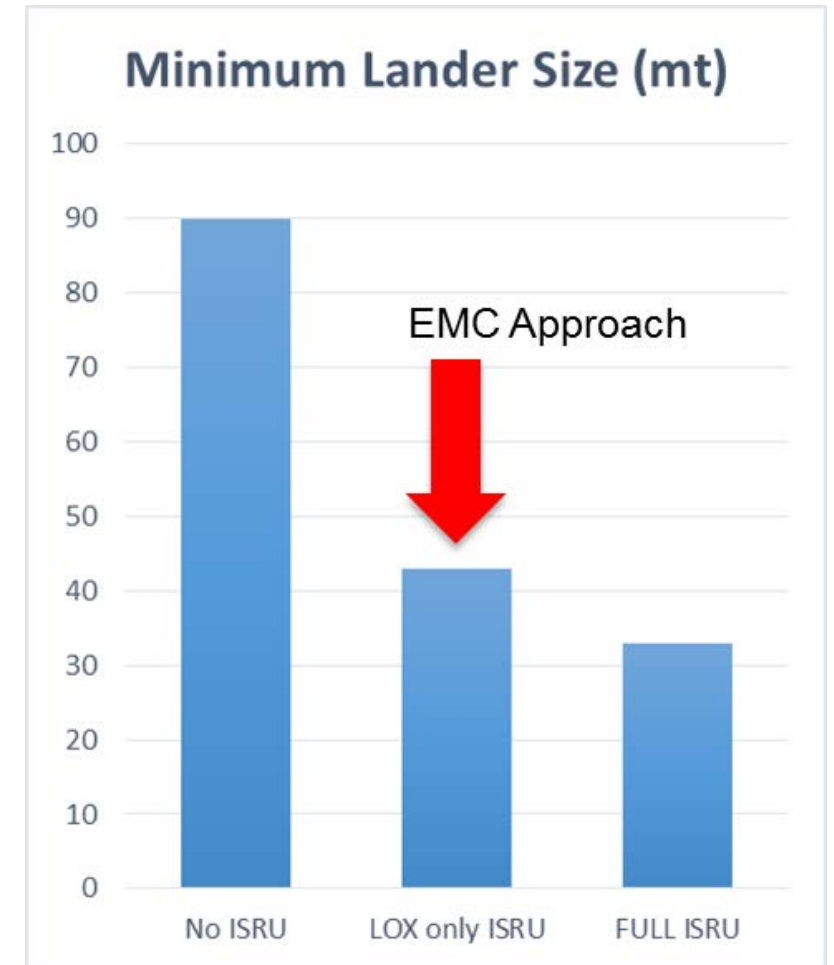
# Agenda

- Background/Purpose for Liquefaction
- Broad Area Cooling (Method of Liquefaction) Overview
- MAV Model Overview and Results
- Overview of Zero Boil-off testing campaign at Glenn Research Center
- ZBO Model Overview (similar to MAV Model)
- ZBO Model Validation with Test Results
- Future Work



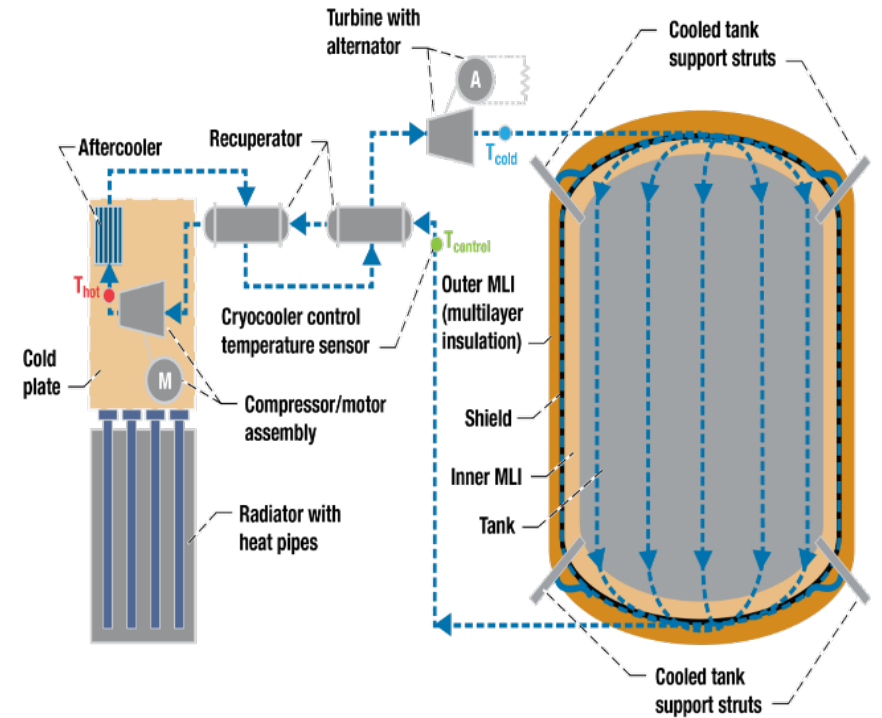
# Background

- Current Mars human architectures point to using In-Situ Resource Utilization
- An ISRU plant could potentially reduce the landed mass required by 30000 kilograms
- Gaseous oxygen and methane that ISRU produces must be liquefied and stored as propellants for the Mars Ascent Vehicle (MAV)
- 23 tons (~21000 kg) of liquid oxygen needed in 500+ days
- An energy efficient liquefaction system required



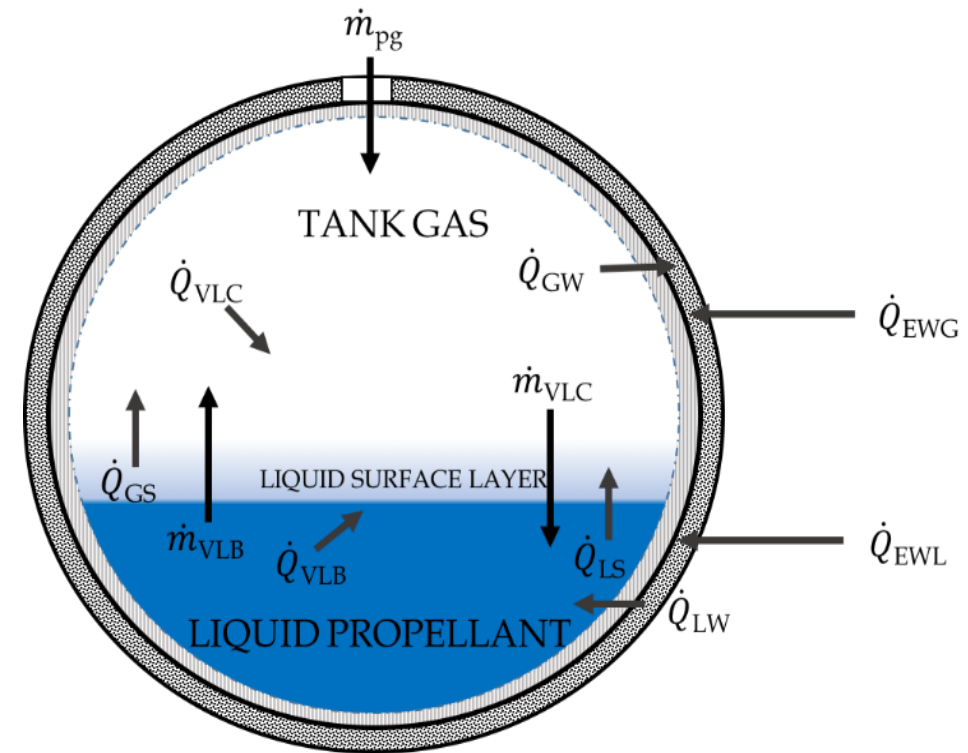
# Broad Area Cooling (BAC)

- Working fluid is circulated by a reverse Turbo-Brayton (RTB) cycle cryocooler through a tubing network welded over the whole surface of a cryogenic tank
- Working fluid intercepts the heat that would otherwise go into the propellant
- Interest in using BAC as cooling system for zero boil-off for storage of cryogenic rocket engine propellants
- Now also being considered as a liquefaction method



# Model Scope

- Integrated model of MAV sized propellant tank with an integrated reverse Turbo-Brayton cycle cryocooler created in Thermal Desktop
- Predicts liquefaction performance and operation
- Includes Martian daily cycle heat loads and radiator temperatures
- First step: Create a MAV sized spherical propellant tank for liquid oxygen

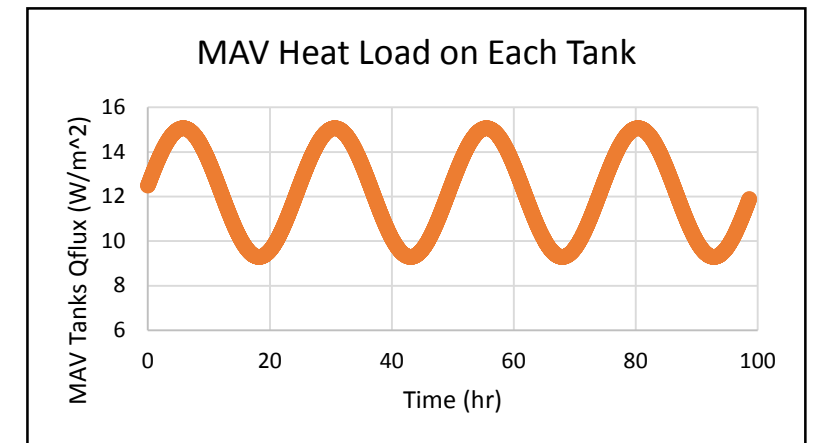
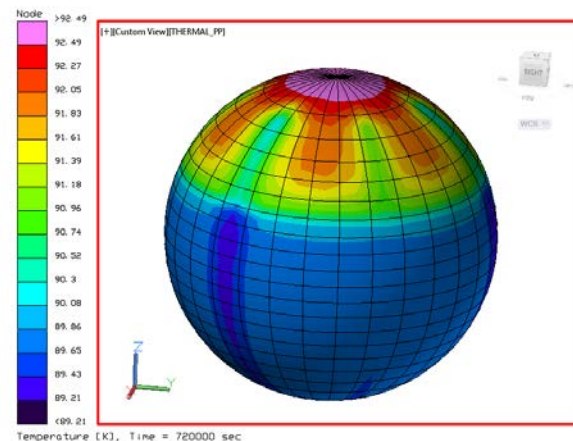
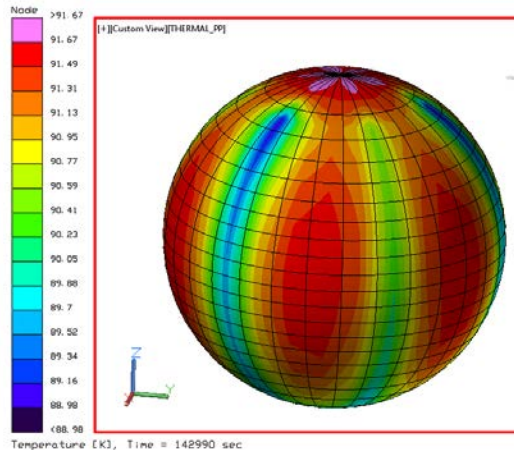
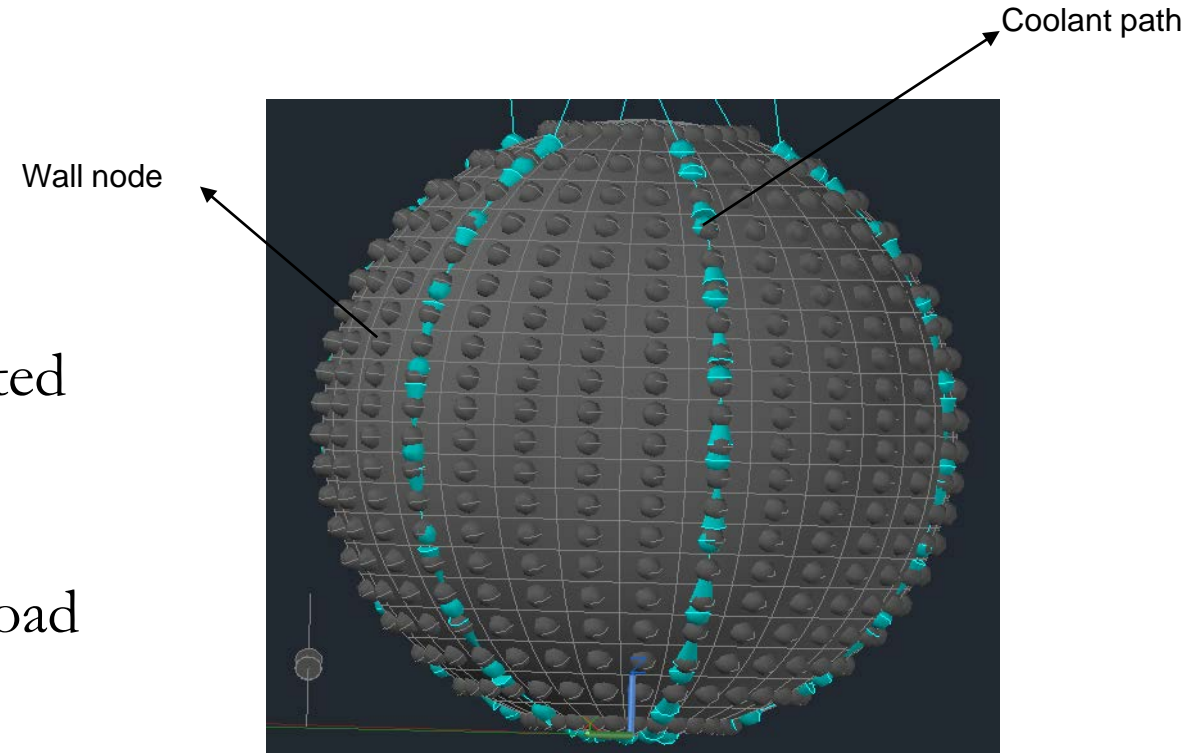


## NOMENCLATURE

- GS: gas surface
- GW: gas wall
- LS: liquid surface
- LW: liquid wall
- VLB: boiling
- VLC: condensed liquid vapor

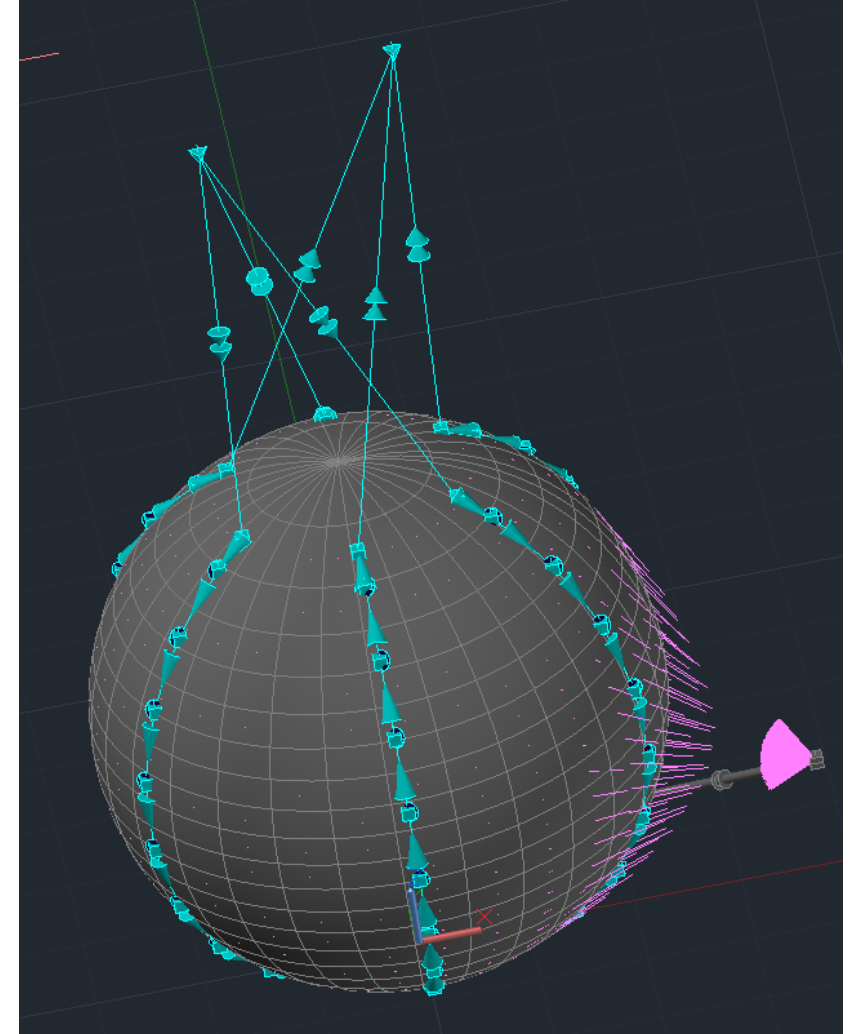
# Thermal Desktop Tank Model Details

- Tank model is a thin walled spherical aluminum tank with a liquid volume and a gas volume (twinned lump), propellant: liquid oxygen
- Heat transfer between wall and fluid is represented by pool boiling ties ( $\dot{Q}_{VLB}$  and  $\dot{Q}_{VLC}$ )
- Heat transfer from environment to tank is represented by a given Martian daily cycle heat load
- No stratification is modeled



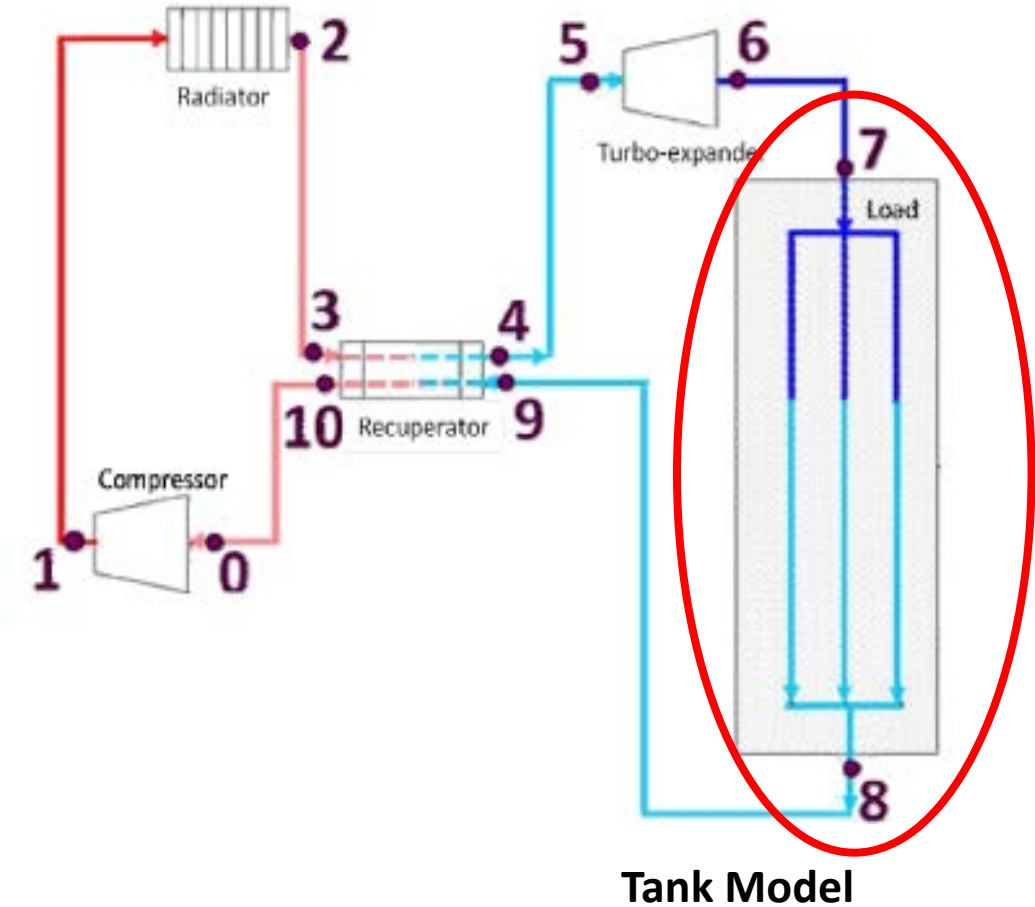
# Thermal Desktop Tank Model Details

Tank Material	Aluminum 6061-T6			
Tank Outer Diameter	2.65 m	104.33 in	based on MAV tank estimates	
Tank Thickness	0.00635 m	0.25 in		
<b>Starting Conditions in Tank</b>				
Liquid oxygen temperature	90 K			
Vapor Temperature	273.15 K			
Pressure	101325 Pa	1 atm		
Void Fraction	0.99			
Initial Tank and Pipe Wall Temperature	90 K			
<b>Flow into Tank</b>				
Mass Flow	2.2 kg/hr		from ISRU estimates	
Temperature	273.15 K			
Pressure	101325 Pa	1 atm		
<b>Heat Load</b>	<b>9 to 15</b> W/m <sup>2</sup>		modeled as a sine curve	
<b>3 pipe loops</b>				
Material	Aluminum 6061-T6			
Outer Diameter	0.009525 m	0.375 in		
Thickness	0.000889 m	0.035 in		
Coolant	Neon			



# Tank Model integration with Creare Cryocooler Model

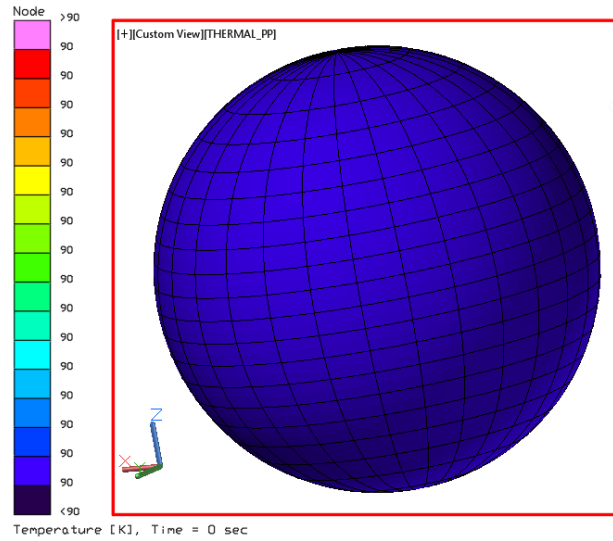
- Between 7-8 is the tank model
- Rest of the system is represented by equations for the Creare 90 K and 500 W cryocooler (given by Creare)
- Integrated system modeled in Thermal Desktop



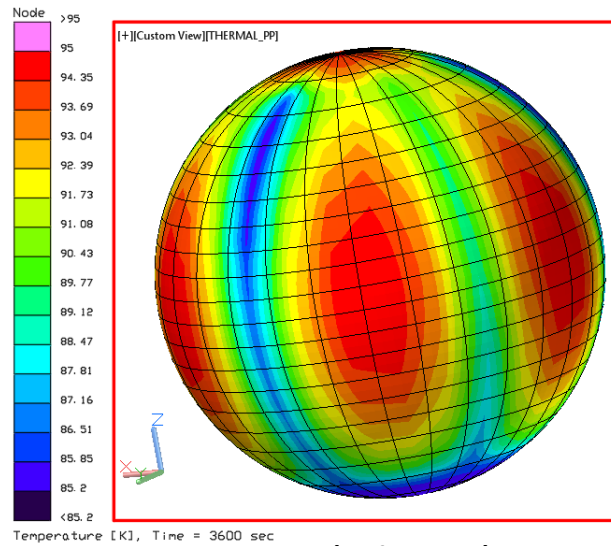
Tank Model	Creare Cryocooler Model
<p><i>Inputs from Cryocooler</i></p> <p>BAC inlet temperature (T7) Coolant Mass flow Rate (mdot)</p>	<p><i>Inputs from TD Model</i></p> <p>BAC outlet temperatre (T8) Pressure drop from 7 to 8</p>
<p><i>Outputs</i></p> <p>Tank Wall Temperatures Coolant Temperatures Coolant Pressures Liquid Temperature Tank Pressure Ullage Volume Fraction Liquid Mass</p>	<p><i>Outputs</i></p> <p>Net refrigeration Coolant Mass Flow</p>



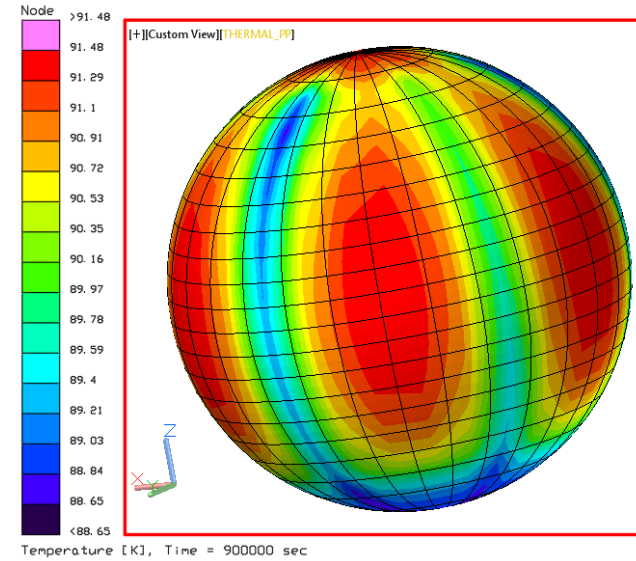
# Results - Tank Wall Temperatures (K)



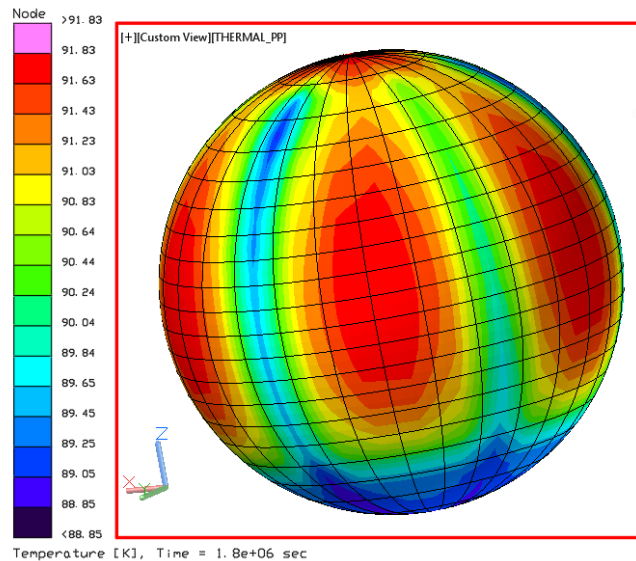
(Initial condition)



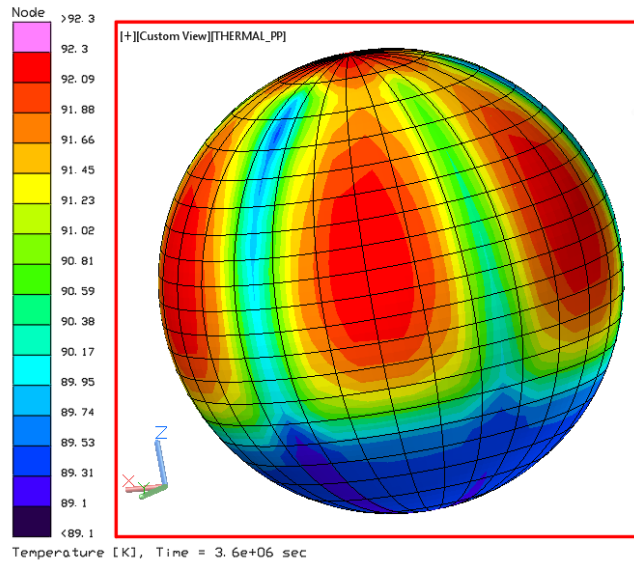
(1 hour )



(250 hours)

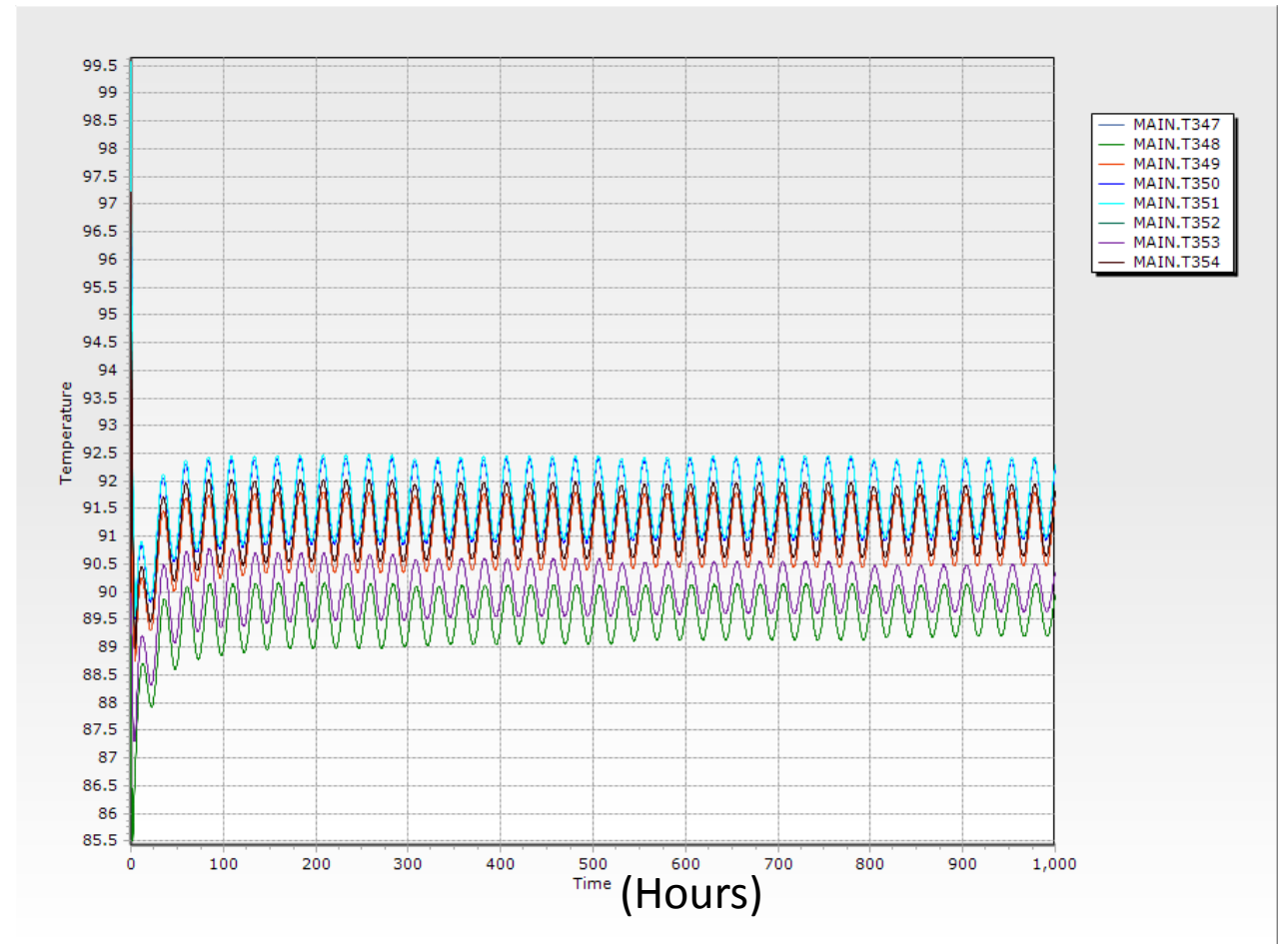
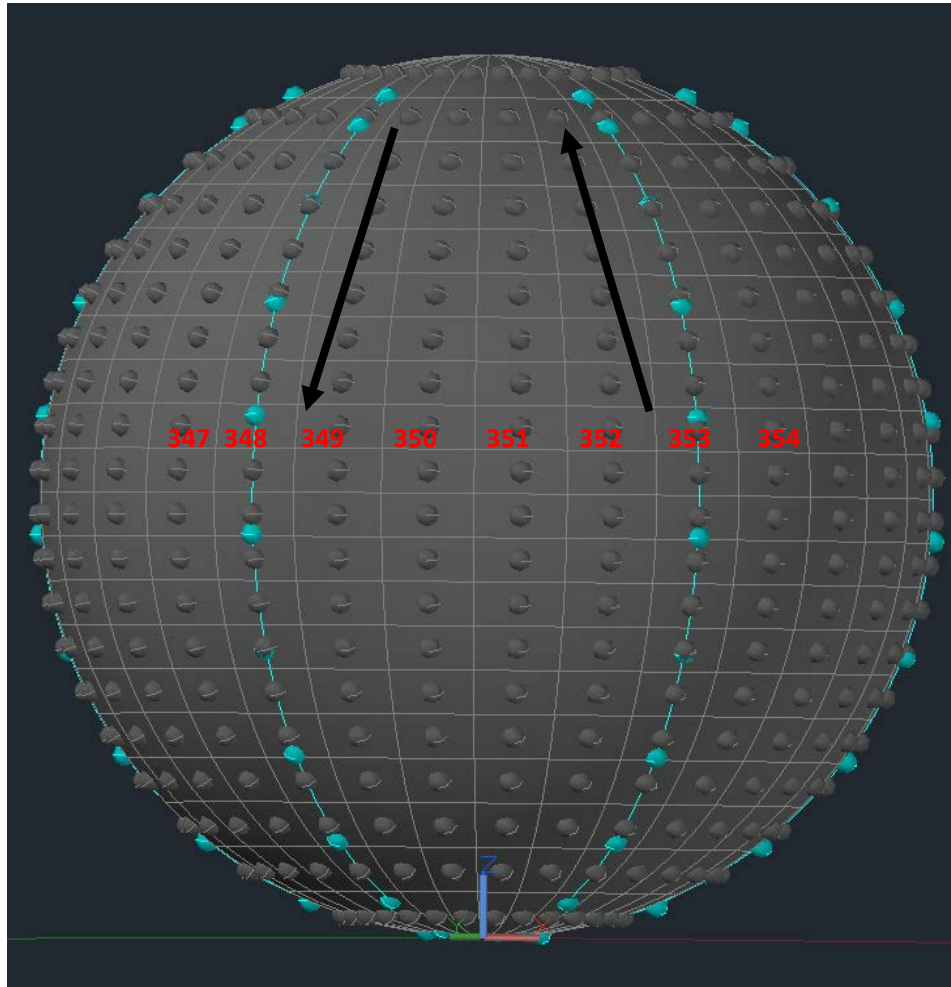


(500 hours)

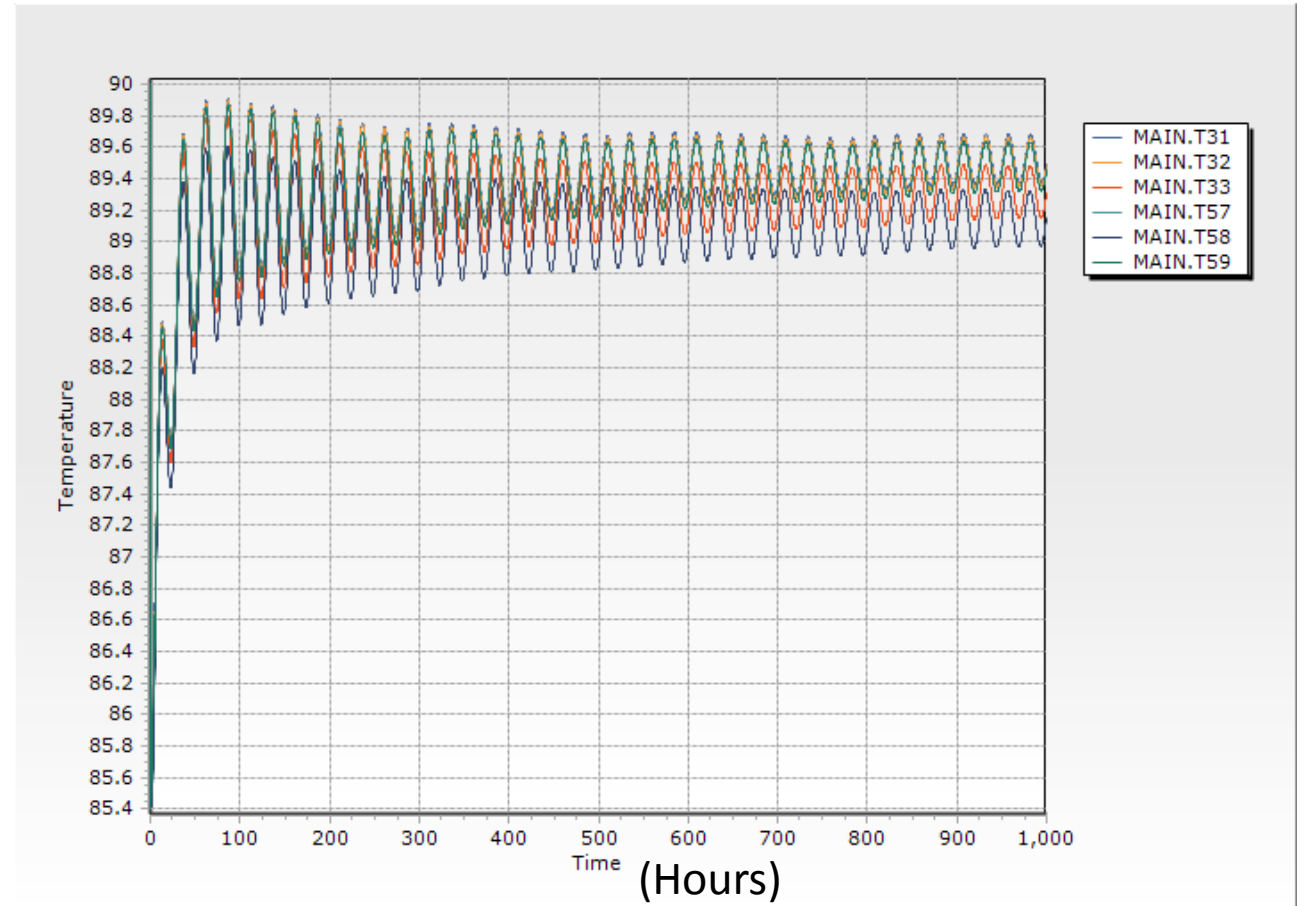
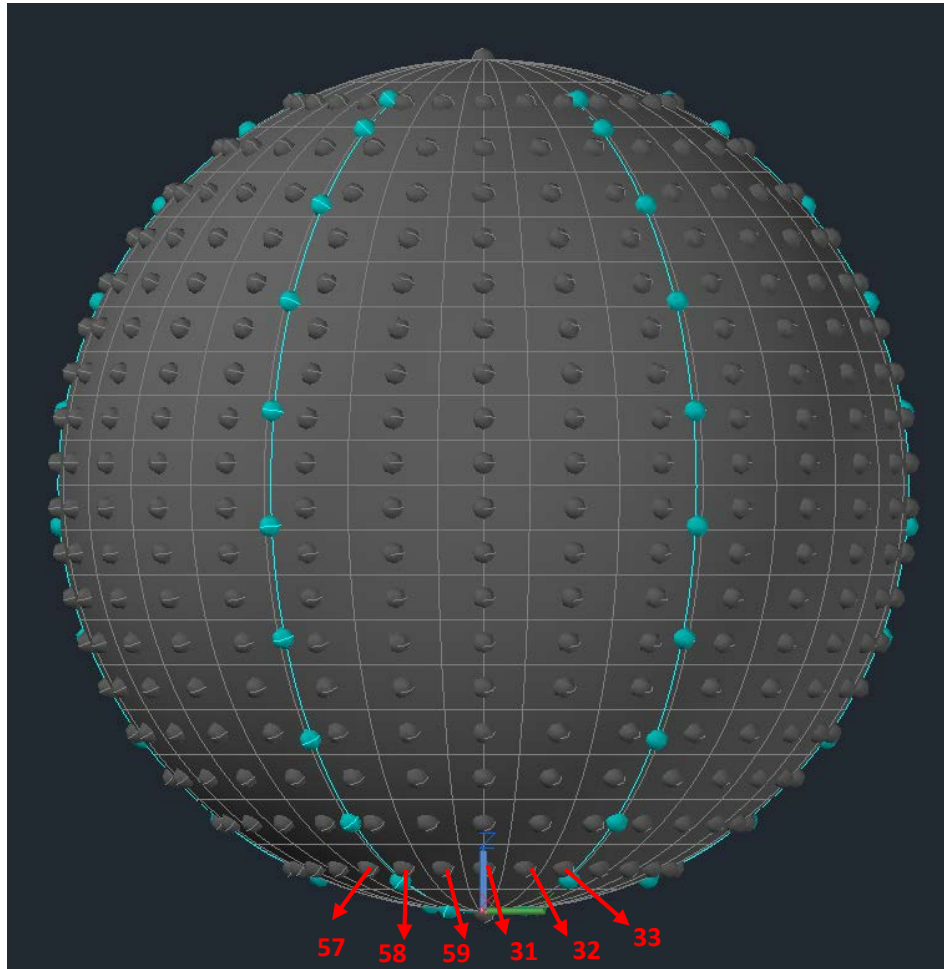


(1000 hours)

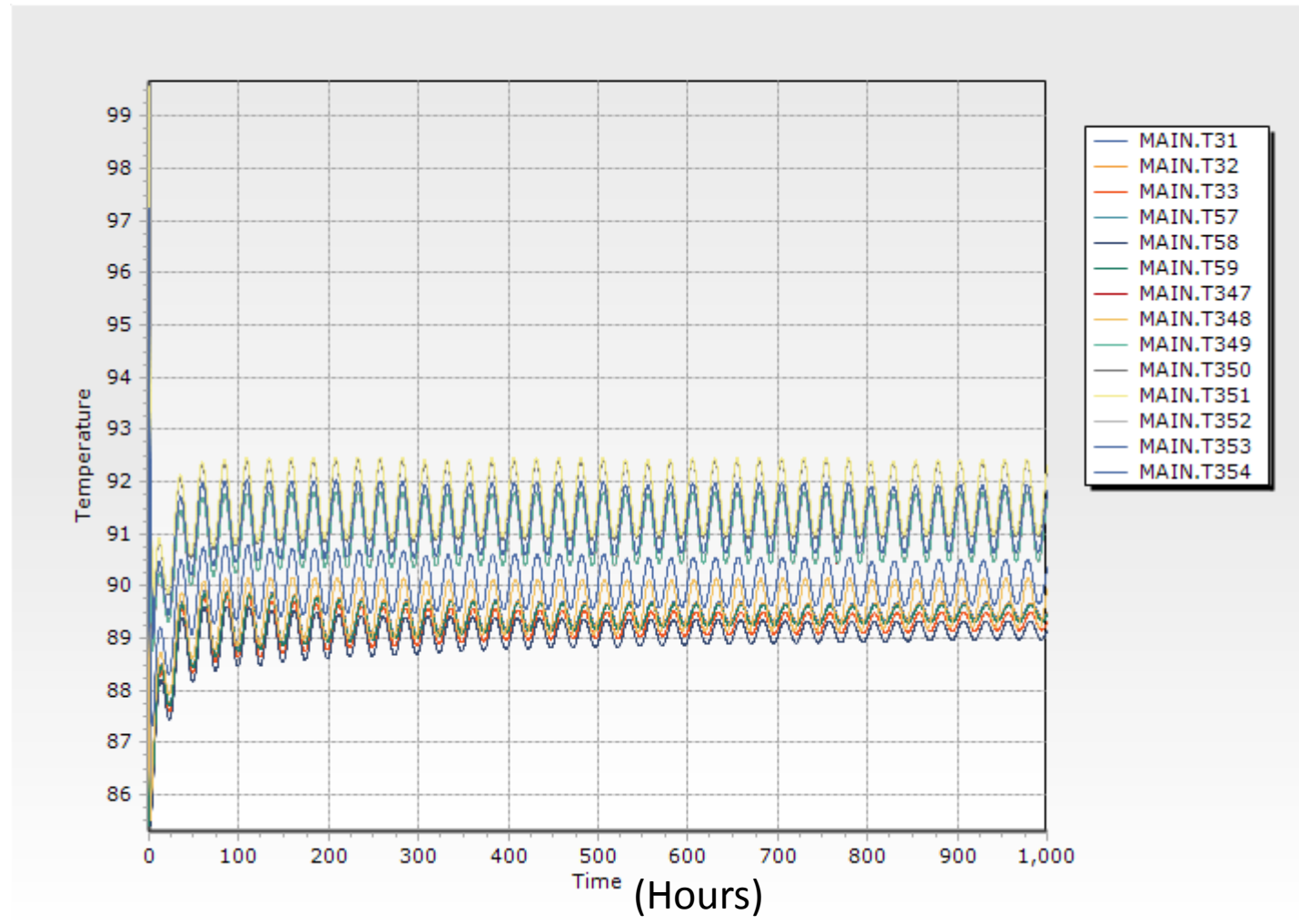
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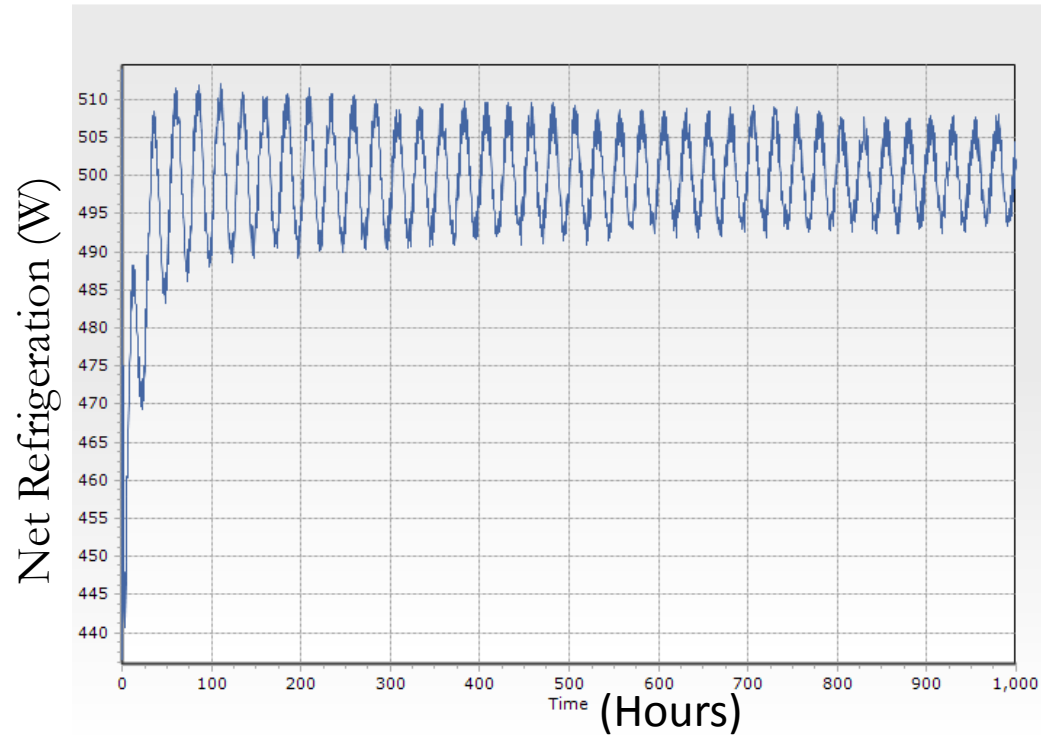


# Results - Tank Wall Temperatures (K)

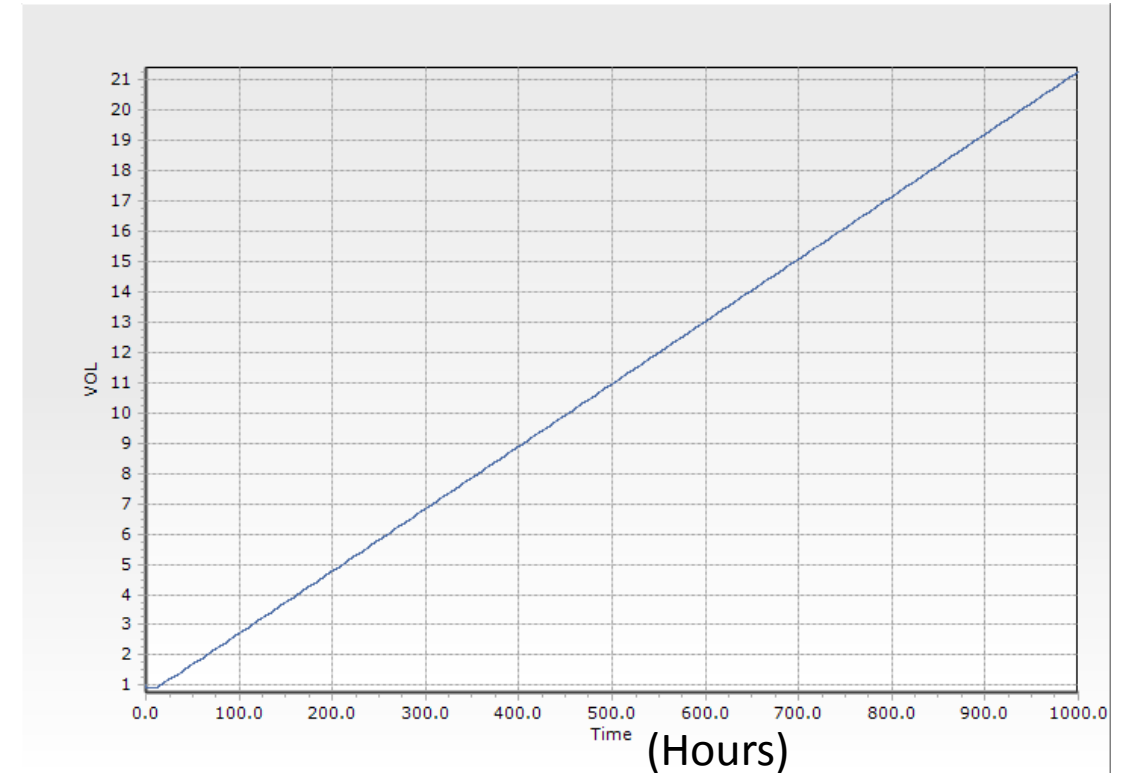


# Results – Net Refrigeration (W) and Liquid Volume Fraction (%)

## Net Refrigeration (W)

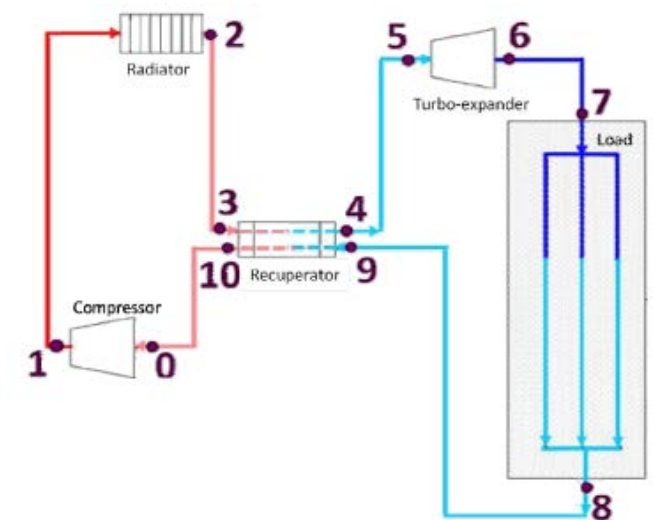
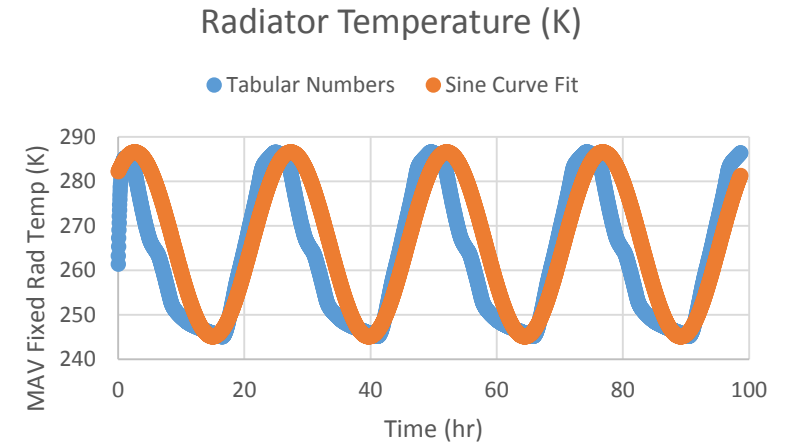


## Liquid Volume Fraction (%)



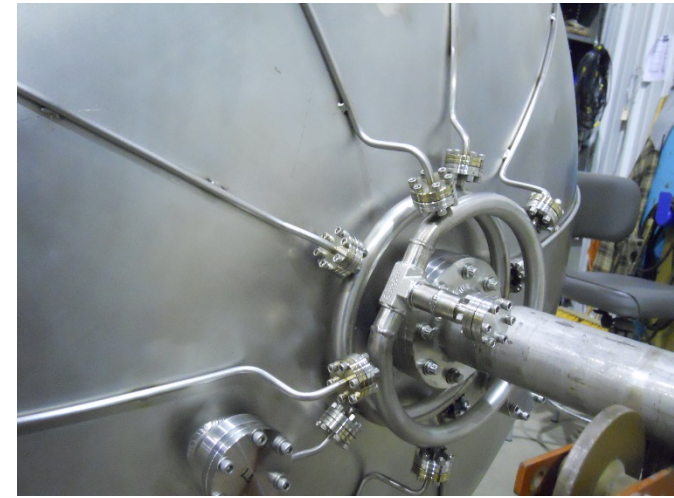
# Model Case Runs

- Radiator temperature is the temperature at point 2 in the diagram (where cryocooler rejects heat)
- Two cases ran: one with a constant radiator temperature of 300 K and one with a sine curve fit from MAV thermal analysis
- Tank starts at an initial ullage volume fraction of 0.99
- Results:
  - Constant Trad – 4750 W
  - Changing Trad – 4000 W
- Mars environmental temperature cycles can potentially reduce cryocooler power and mass by 15-20% with current radiator design

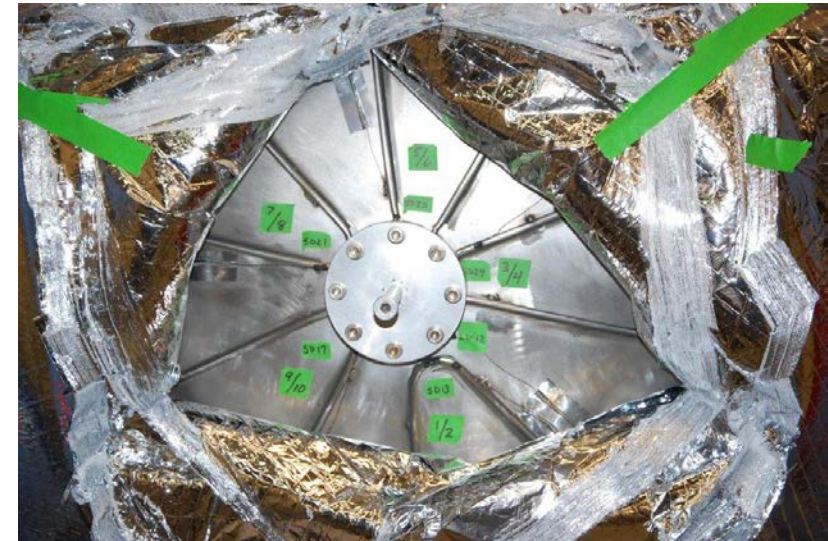


# ZBO Model Overview

- Assembly consists of Zero Boiloff (ZBO) test tank, with the tube-on-tank BAC system, covered with insulation
- Propellant: liquid nitrogen
- Coolant: neon
- 10 tests were performed with the ZBO tank
  - Test 1: Passive Boiloff (15 days)
  - Test 2: Passive Pressurization (1 day)
  - Test 3: Active ZBO (6 days)
  - Test 4: Active high power A (1 day)
  - Test 5: Active low power (1 day)
  - Test 6: Active de-stratification (2 days)
  - Test 7: Active high power B (1 day)
  - Test 8: Active low-fill ZBO (7 days)
  - Test 9: Active low fill and high power (1 day)
  - Test 10: Passive boiloff at 300 K (10 days)



Top of ZBO tank



Bottom of ZBO tank

# ZBO Test Descriptions

- Test 2: Passive Pressurization
  - Tank fill level at 90%, tank pressure at 82 psi
  - Tank's vent valve was closed, tank self-pressurized
  - Tank pressurization rate – 0.33 psi/hr
  - Tank heat leak - 4.64 W
  - No mixing or cooling occurred
- Test 4: Active Zero Boiloff
  - Cryocooler power increased from 145 W (test 3) to 272 W
  - Initial tank pressure at 82 psi
  - Cryocooler mass flow increased to 2.2 g/s
  - Pressure drop was 0.14 psi/hr (over 16 hours)
- Test 6: Active destratification
  - Cryocooler power on, heaters also powered on to match heat loads in Test 2
  - Compare pressure rise to Test 2
- Test 9: Active Low Fill, High Power
  - Cryocooler power increased to 208 W
  - Tank pressure drop was 0.11 psi/hr (over 23 hours)

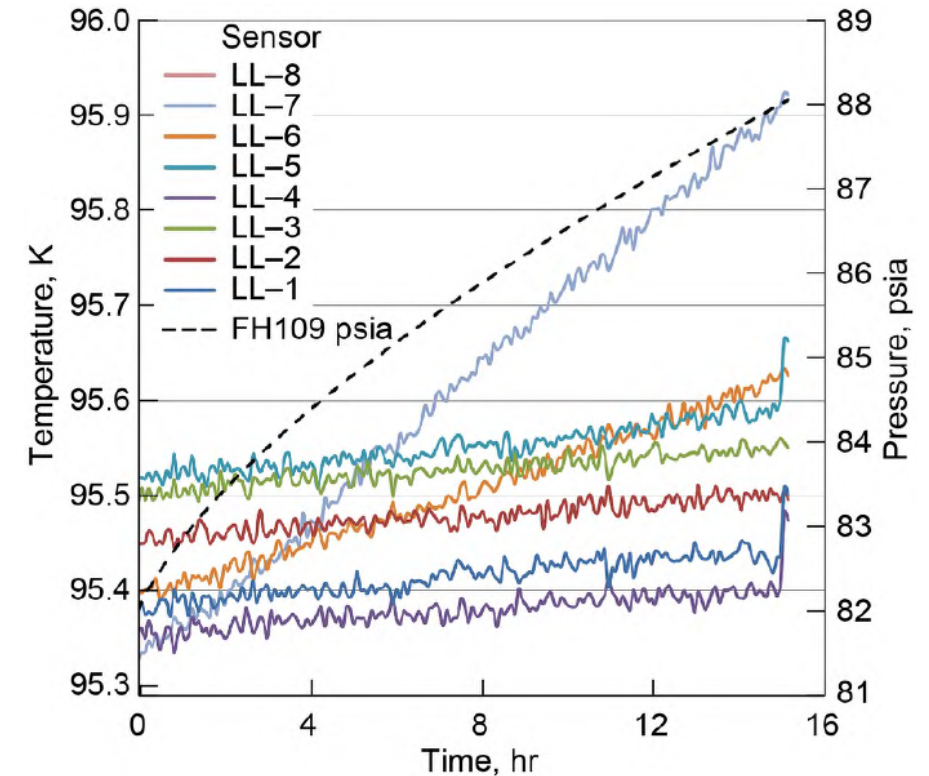
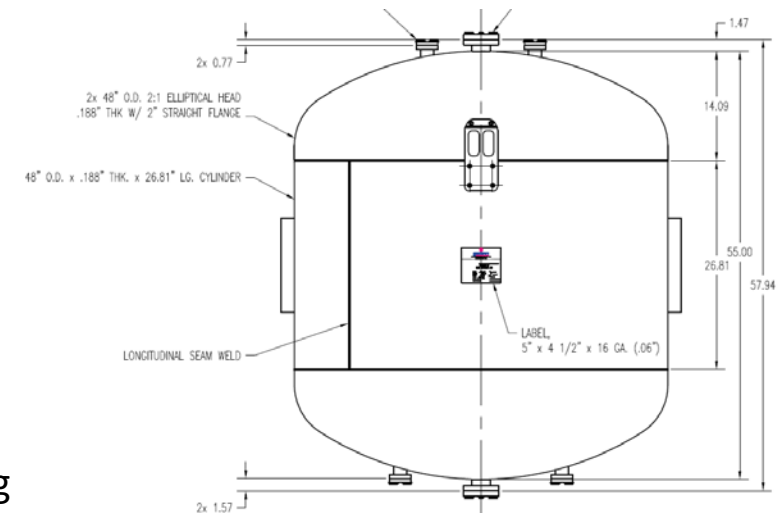
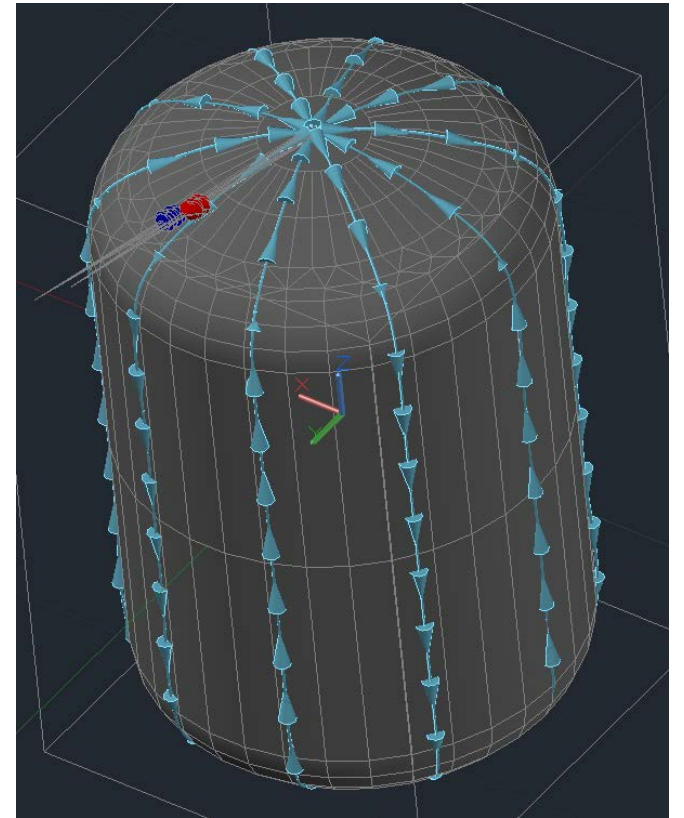


Figure 31.—Test 2 tank pressure and liquid temperatures.



# ZBO Modeling Overview

- **Goal:** Compare ZBO thermal desktop model with available data
- Created a model in Thermal Desktop of the liquid nitrogen test tank and BAC cooling loops
  - Tank and pipe walls are modeled with MLI insulation attached
  - No stratification modeled in tank (liquid lump and vapor lump each at one temperature)
  - Strut heat load included as heat loads on 3 tank wall nodes
    - (0.136 W on each wall node)
  - Vent, fill, nipple, strap, and parasitic heat loads applied on tank wall nodes near top of tank



Tank Drawing

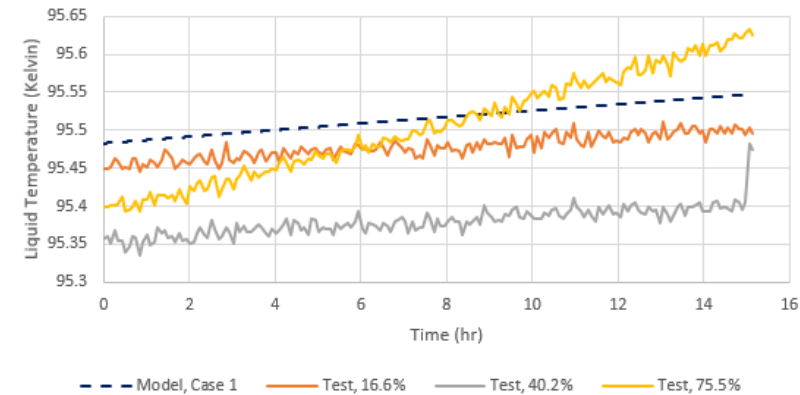
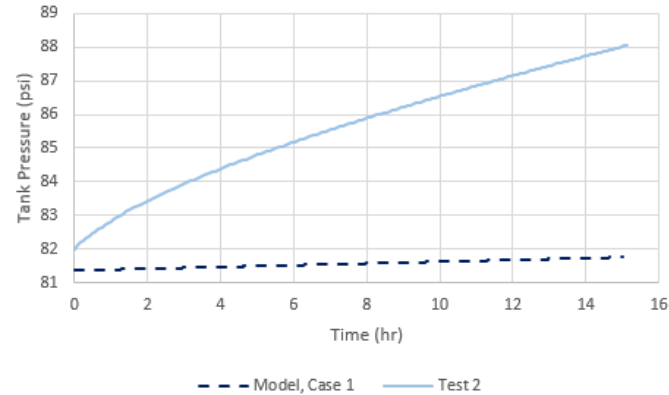
# ZBO Model Cases

Test Number and Type	Test Description	Test Duration	dP/dt (psi/hr)	Qfluid (W)
2 – Passive Pressurization	Tank fill level at 90%, vent valve closed, tank self-pressurized	1 day	0.33	3.80
4 – Active High Power at High Fill	Tank fill level at 90%, cryocooler power on at 272 W	1 day	-0.096	-7.13
6 – Active Destratification	Tank fill level at 90%, cryocooler on to homogenize liquid temperature, heat added to tank to compare with test 2	1 day	0.024	2.75
9 – Active High Power at Low Fill	Tank fill level at 27%, cryocooler power on at 208 W	1 day	-0.11	-2.73

Cases	Test to Compare	Time Duration (hr)	Fill Volume (%)	Initial Tank Vapor Wall Temperature (K)	Initial Tank Liquid Wall Temperature (K)	Initial Tank Liquid Temperature (K)	Initial Tank Vapor Temperature (K)	Initial Tank Pressure (psi)	Coolant Mass Flow (g/s)
1	2	20	95%	105.2	95.3	95.4	98.3	82	0
2	6	20	95%	98.7	95	95.3	96.1	82	0
3	4	20	95%	98.7	95.1	95.4	96.2	82	2.2
4	9	20	27%	98.9	95.3	95.4	96.5	82	1.7

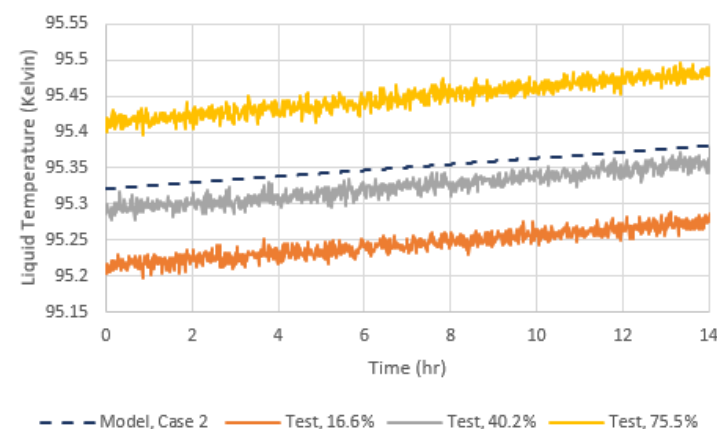
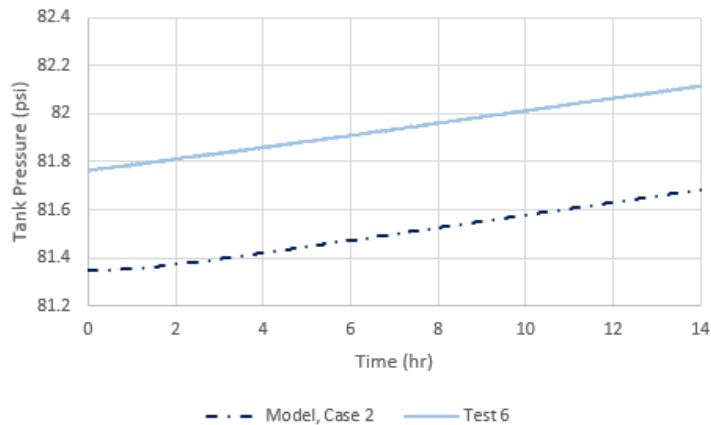
# ZBO Model Results – Net Heat Addition Positive

Test 2:  
Propellant  
Stratified



	Model	Data (Test 2)
Pressure rise (psi/hr)	0.026	0.33
Temperature rise (K/hr)	0.0031	0.0043

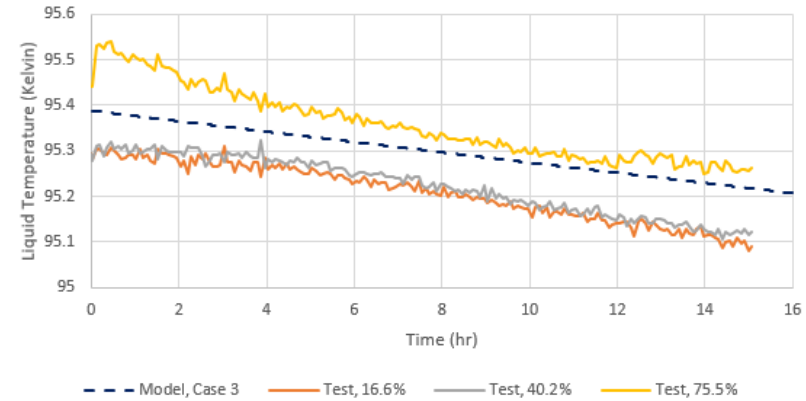
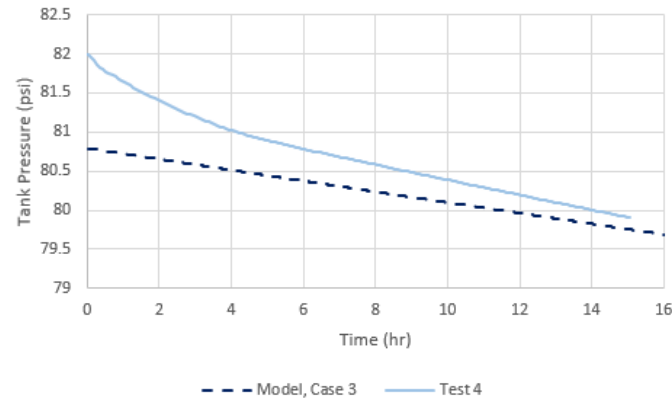
Test 6:  
Propellant  
Behaved  
De-Stratified



	Model	Data (Test 6)
Pressure rise (psi/hr)	0.0259	0.024
Temperature rise (K/hr)	0.0047	0.0043

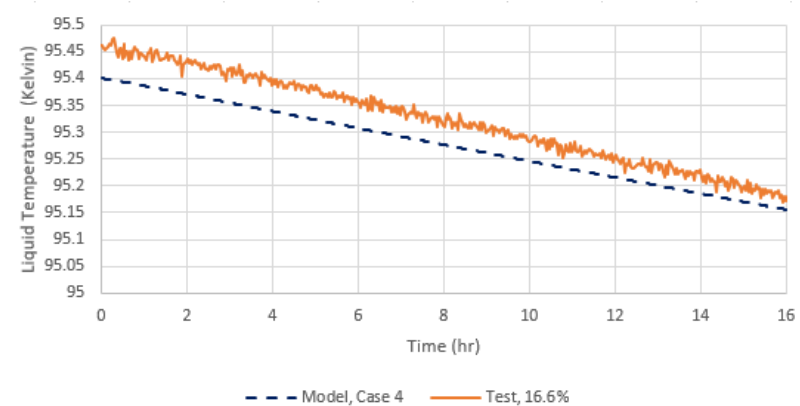
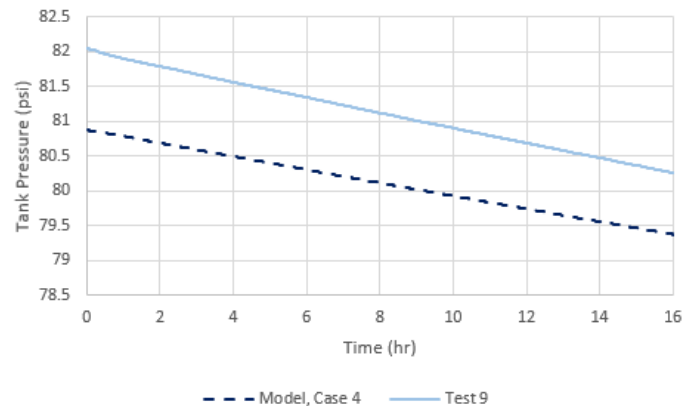
# ZBO Model Results – Cryocooler on, Net Heat Addition Negative

Test 4:  
95% Fill Level



	Model	Data (Test 4)
Pressure rise (psi/hr)	-0.068	-0.096
Temperature rise (K/hr)	-0.014	-0.011

Test 9:  
27% Fill Level



	Model	Data (Test 9)
Pressure rise (psi/hr)	-0.093	-0.011
Temperature rise (K/hr)	-0.018	-0.015

# Future Work

- Further testing on ZBO test tank
- Validate test matrix by running simulations of planned tests with ZBO model
  - Look at constant versus batch liquefaction
- Look at effects of non-condensable gases on liquefaction performance
- MAV model – also look at constant versus batch liquefaction
  - Cryocooler 12 hours on/12 hours off