

Signals of Opportunity Airborne Demonstrator (SoOp-AD)

Earth Science Technology Forum

2014 ESTO Instrument Incubator Program (IIP)

June 25th, 2015

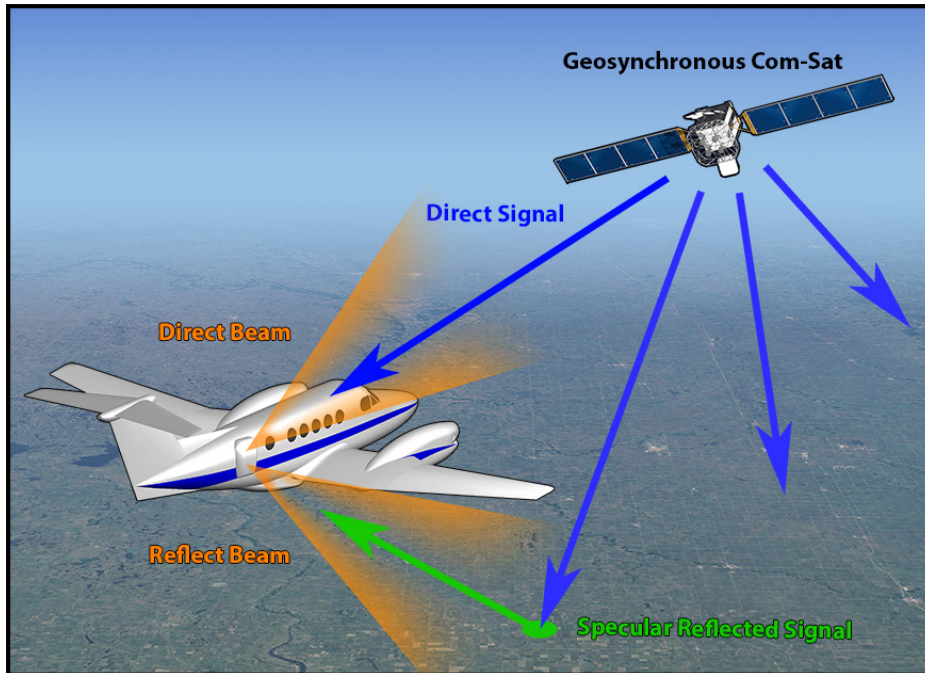


Outline

- Overview
- Project Team
- Science Background and Motivations
- P-Band Signal Details
- Instrument Architecture
- Measurement Simulation
- Next Steps

Measurement Overview

P-Band Reflectometry



We propose to measure Root Zone Soil Moisture (RZSM) through cross-correlation of direct and reflected P-Band geosynchronous communication satellite signals.

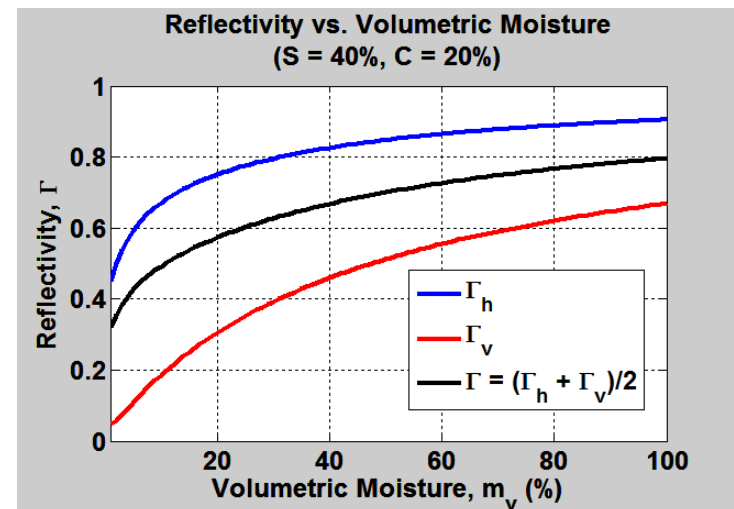
Expected Performance

Parameter	SoOP Airborne	SoOP Spaceborne
Resolution*	100m	870m
Sensing Depth	0-30cm	0-30cm
Sensing Precision**	0.04m ³ /m ³	0.04m ³ /m ³
Biomass Saturation	> 350 t/ha	> 350 t/ha
Antenna Size	75 x 75 cm	75 x 75 cm

*Specular Reflection Assumed

**SMAP Requirement

Basis of Measurement



Project Team

- Purdue University
Simulation, Retrieval Algorithms, Requirements Def.
 - PI: Jim Garrison (Assoc. Prof)
 - Georges Stienne (Post-doc)
 - Yao-Cheng “Zenki” Lin (PhD candidate)
- NASA GSFC
Systems Engineering, RF Design, Aircraft Integration
 - Co-I: Jeff Piepmeier (555)
 - Co-I: Joe Knuble (555)
 - Ken Hersey (AS&D)
 - Cornelus Du Toit (AS&D)
 - Co-I: Alicia Joseph (617)
- Exelis, Inc
Digital Receiver Design
 - George Alikakos
 - Co-I: Steve O’Brien
- Langley Research Center
Aircraft Operations
 - Bruce Fisher
- Dr. Stephen Katzberg – Consultant
Scattering Model, Signal Processing

Scientific Motivation

- Root Zone Soil Moisture (RZSM):
 - Water in top ~meter of soil
 - Critical link between surface hydrology and deeper process
 - Drainage and absorption by plant roots
 - Connection between near-term precipitation and long-term availability of fresh water
- Biomass: a related measurement
 - Carbon storage in vegetation – key part of CO₂ balance
 - Raw material and source of 9-13% of World's energy

Current Sensing Limitations

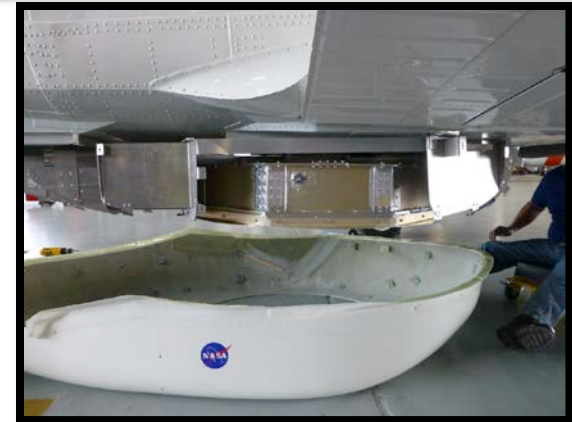
- L-Band
 - L-band (SMAP) penetrates only few cm of soil
 - Saturation at L-band limits the ability to sense soil moisture through vegetation
 - SMAP Level 4 data product to estimate RZSM
- P-band radar
 - Difficult to find allocation in heavily utilized spectrum
 - ESA-BIOMASS cannot operate in North America or Europe due to interference with Space Object Tracking Radar
 - 4G mobile network may also cause problems
 - Expensive from space

SoOp Solution

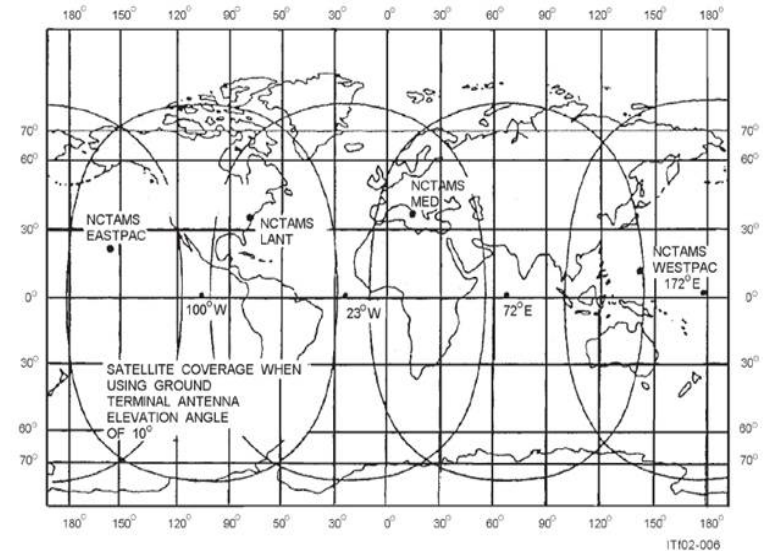
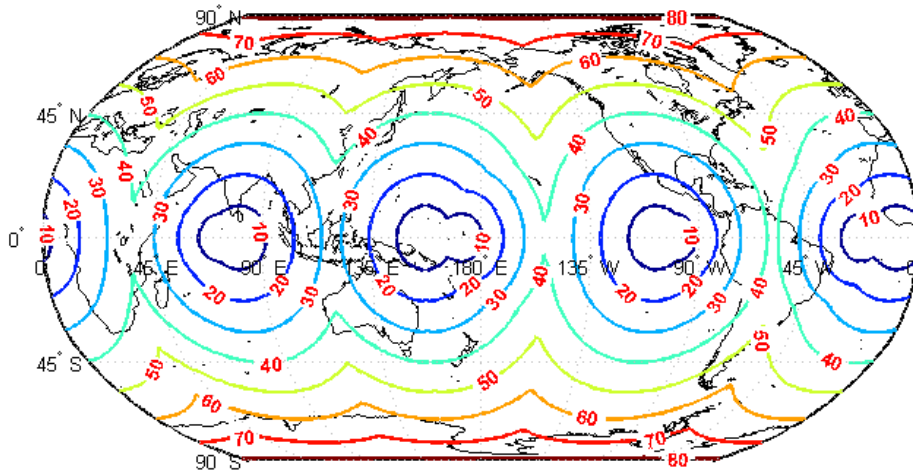
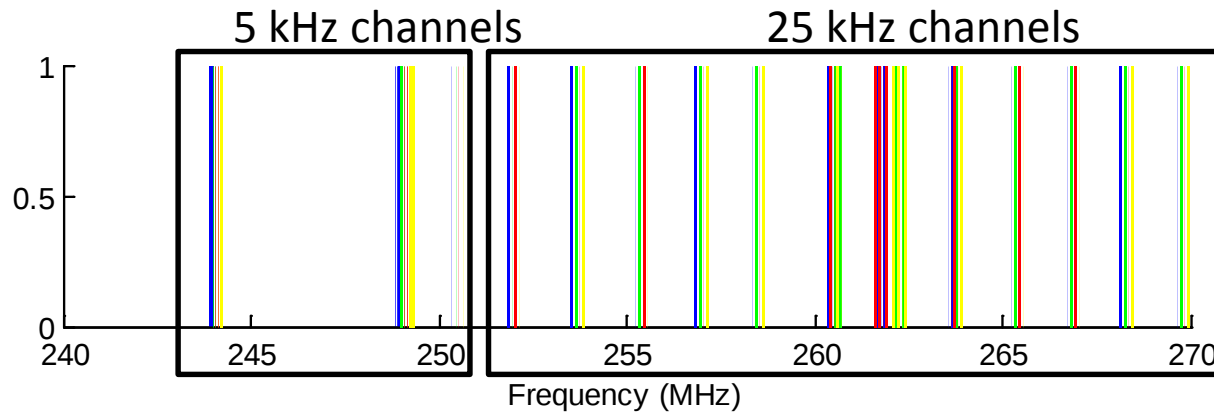
- **We propose to use the principles of reflectometry and reflected SATCOM signals to measure RZSM.**
 - Cross correlation of direct and reflected signals will be used to measure reflection coefficient.
 - SoOP-AD will first measure RZSM from an aircraft.
- SoOP-AD will use the geostationary P-band satcom systems
 - 225-420MHz allocation for government use, SoOP will focus on 240-270MHz band: 18 25KHz channels, 20 5KHz channels.
 - Continuous use by US since 1978
 - SoOP-AD method measures correlation of direct and reflected signals - does not require demod / decode of the transmission.

SoOp-AD Mission Highlights

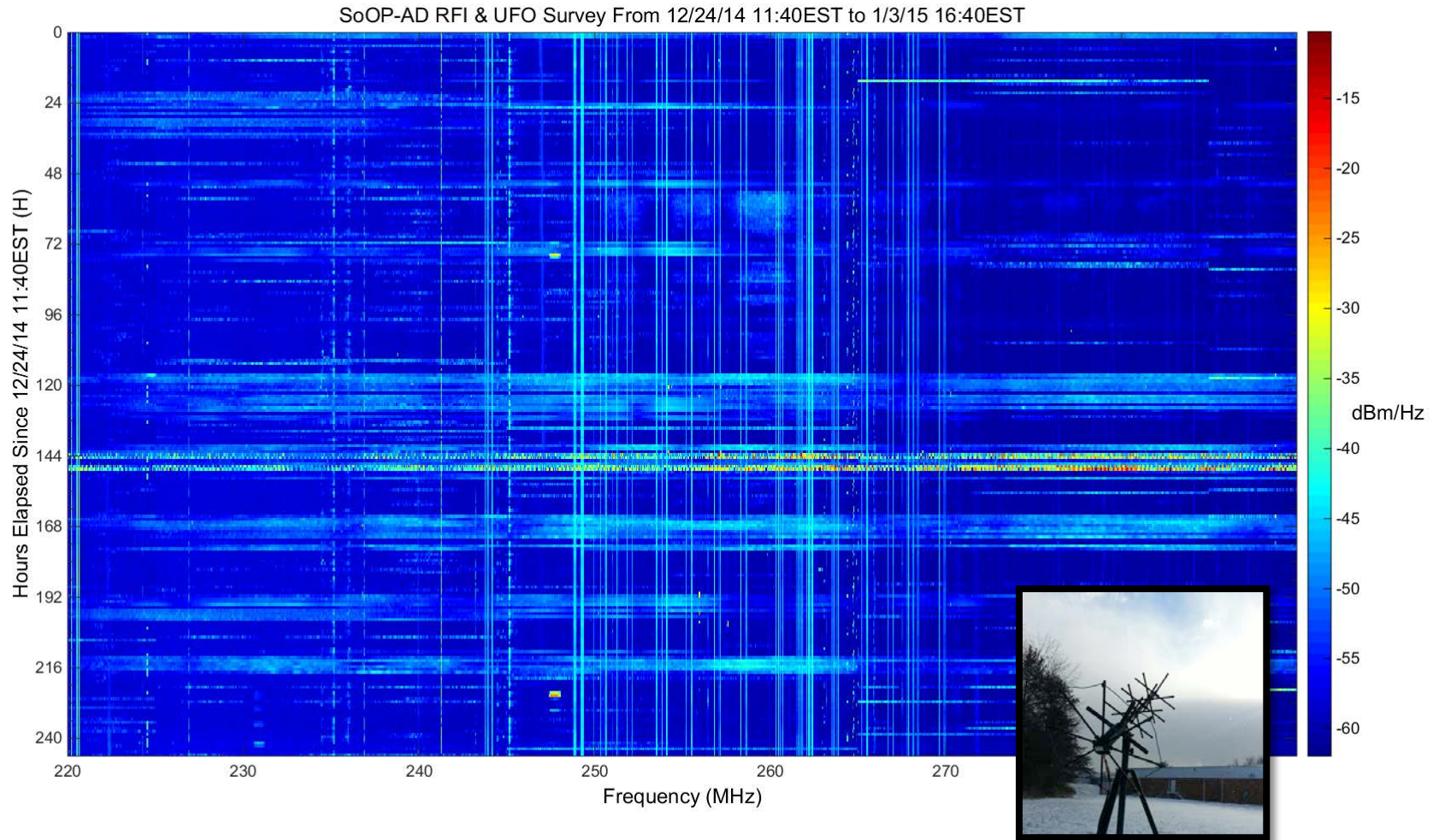
- IIP Timeline
 - Awarded in April '14.
 - Subsystem I&T at GSFC this summer.
 - Science flights in Fall of '16.
- Instrument
 - Antennas: Patch, Dual Linear Pol, Null Steering
 - Receivers: Standard P-Band Receivers w/ internal calibration. S-Band receiver for XM Radio included. Brassboard and compact card.
 - Digital System: FPGA based. 7TB Storage: 1 hour of raw data or many days of processed data.
- Aircraft Campaign
 - Flying on NASA Langley B200.
 - Co-Flying with SLAP instrument (GSFC's Active / Passive L-Band).
 - Science flights over the St. Joseph's Watershed.
 - Two aircraft racks: 12U Total



Signal Bands and Coverage



Measured Signal Details & RFI

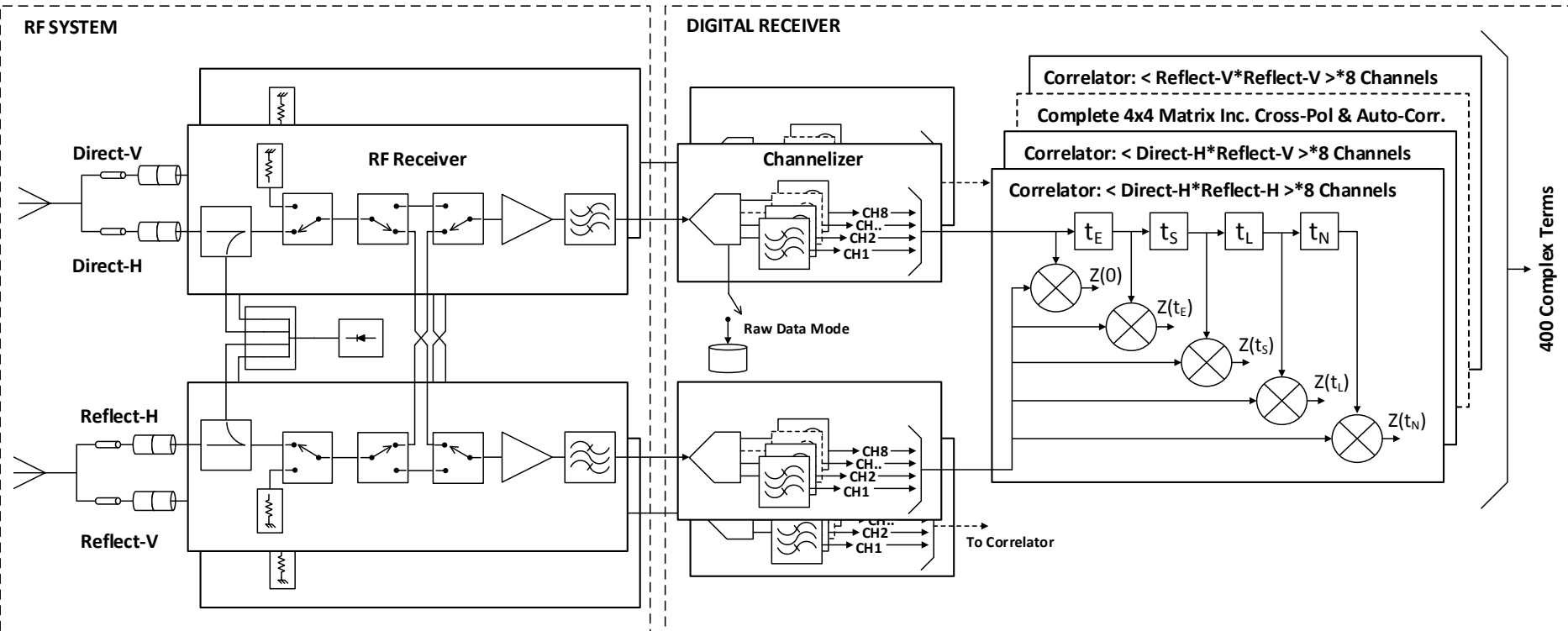


Waterfall spectrum measured at GSFC over 11 days. Note persistence of satcom signals and broad-band RFI.

Direct Signal Link Budgets

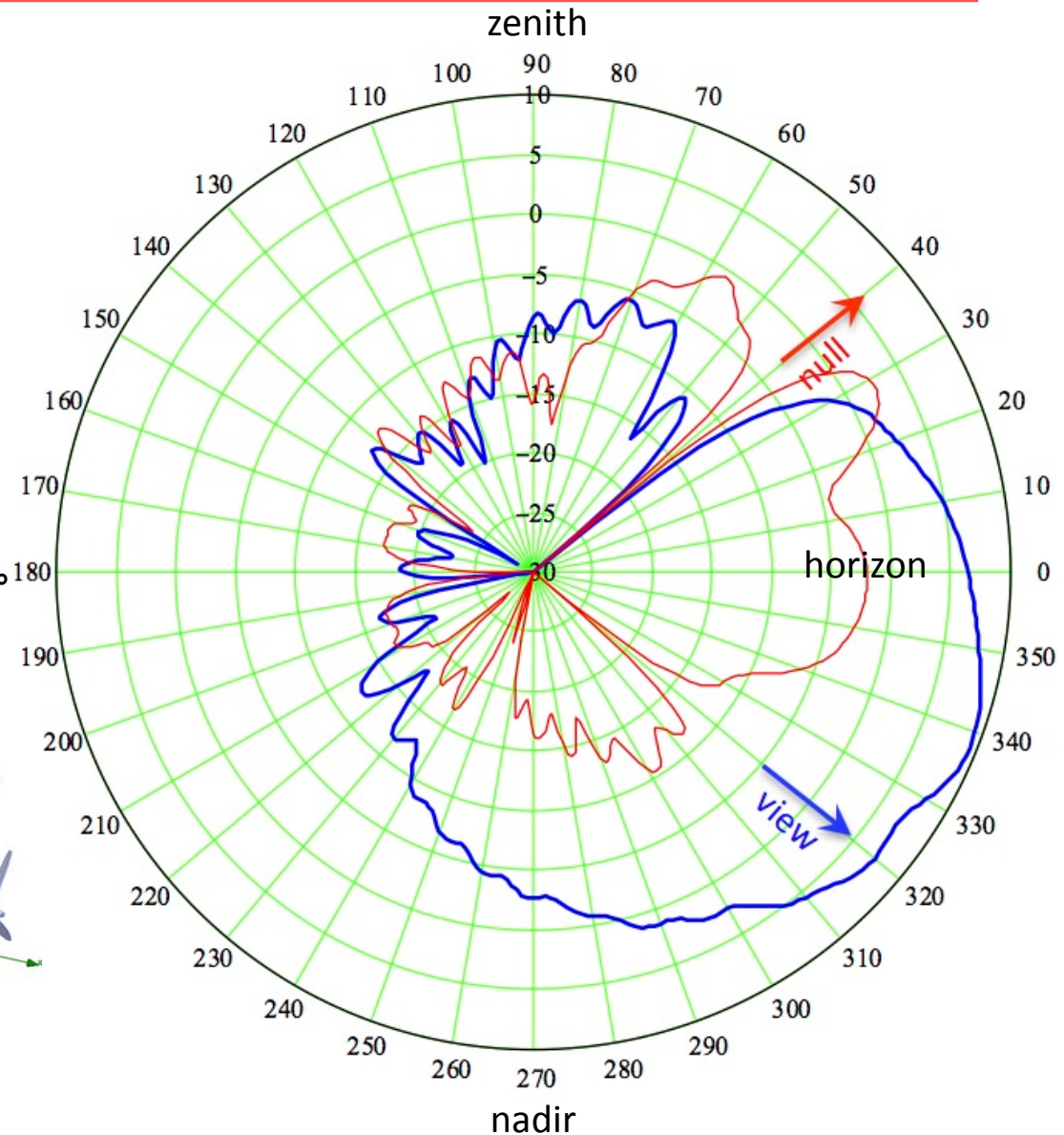
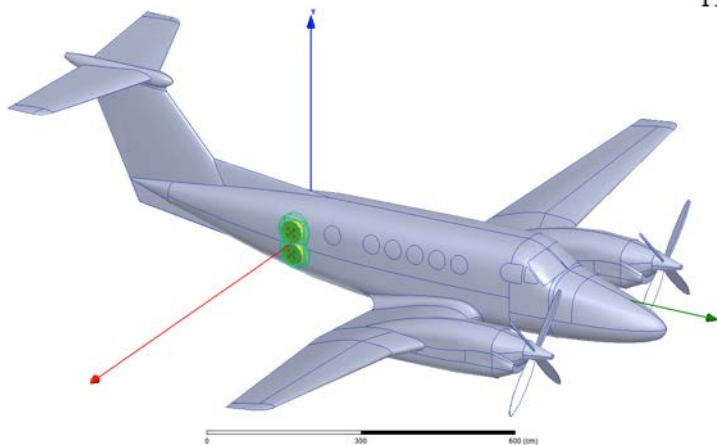
	P-Band		S-Band	
EIRP (dBW)	26		68	
Frequency (MHz)	240-270		2332.5-2045.0	
Bandwidth	25 kHz		1.886 MHz	
Longitude (deg)	-99.2	-105.6	-85	-105
Distance (km)	38128	38512	37447	38474
Path loss (dB)	-172.44	-172.53	-191.31	-191.54
Atmospheric loss (dB)	-1 dB			
Sky-view antenna gain	7 dB			
Sky-view antenna noise	145.0 K			
Pre-switch noise	212.2 K			
Post-switch noise	350.0 K			
Total noise	707.2 K / -156.12 dBW		707.2 K / -137.35 dBW	
SNR (dB)	15.7	15.6	20.1	19.8

SoOp-AD System Architecture



Antenna System Considerations

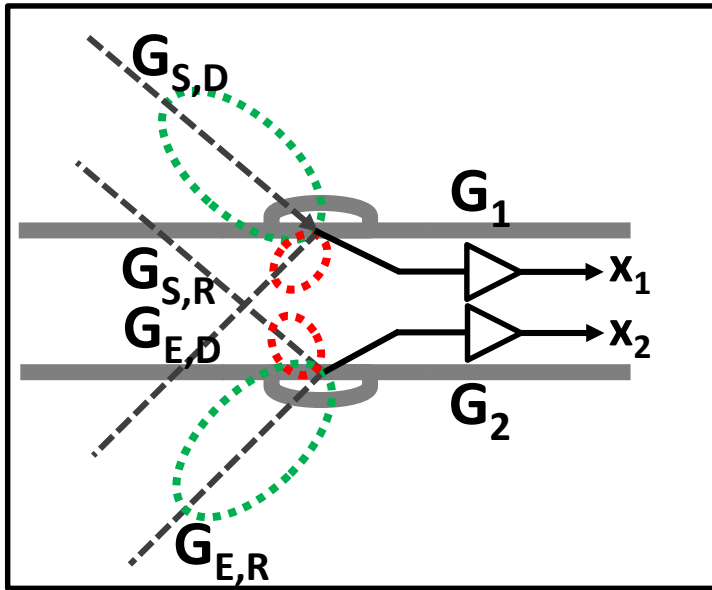
- Direct-to-Reflect Isolation is Driving Requirement
- Using “Smart Antenna” to steer a null as necessary in post-processing.
- Simulation: Earth View Beam
 - Co-pol (blue): LHCP
 - X-pol (red): RHCP
- Results simulate a post-processed pattern with a null steered to $+40^\circ$



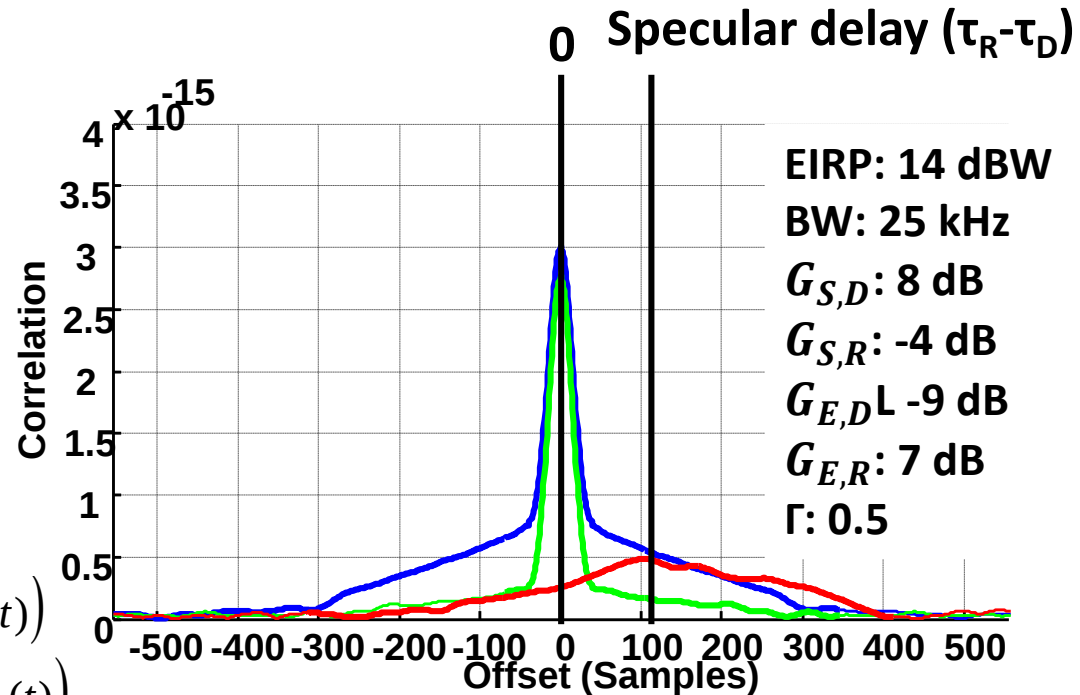
Measurement Simulation

- Purpose:
 - Science requirement flow-down to technology requirements
 - Error budget
 - First generation retrieval algorithms
- Two Methods: Synthetic (IF) Signal Generator (forward) and Extended Kalman Filter (inverse estimator)
- Evaluate Error Sources against $0.04\text{m}^3/\text{m}^3$ Precision Req.
 - SNR
 - Direct signal leakage into reflect antenna (easier in orbit!)
 - Multiple Satellite Interference / Isolation
 - Antenna Pattern Knowledge
 - Aircraft Position & Attitude Knowledge
 - Number of correlation delays
 - Terrain Height Fluctuation
 - RFI

Modelling Details



Measurements are made on samples of Z_{11} (autocorrelation of channel 1), Z_{22} (autocorrelation of channel 2) and Z_{12} (cross-correlation between channel 1 and channel 2)



Space signals models:

$$x_D(t) = \sqrt{C_D} a(t - \tau_D) e^{j\omega_b t} e^{-j\omega_e \tau_D}$$

$$x_R(t) = \sqrt{C_R} a(t - \tau_R) e^{j\omega_b t} e^{-j\omega_e \tau_R}$$

Receiver channels signals models:

$$x_1(t) = f_{RF} \left(\sqrt{G_1 G_{S,D}} x_D(t) + \sqrt{G_1 G_{S,R}} x_R(t) + n_1(t) \right)$$

$$x_2(t) = f_{RF} \left(\sqrt{G_2 G_{E,D}} x_D(t) + \sqrt{G_2 G_{E,R}} x_R(t) + n_2(t) \right)$$

Extended Kalman Filter Method

Measurements: signals auto- and cross- correlations

$$\begin{aligned}
 Z_{1,1}(\tau) &= \langle x_1(t) x_1^*(t - \tau) \rangle \\
 Z_{1,2}(\tau) &= \langle x_1(t) x_2^*(t - \tau) \rangle \\
 Z_{2,2}(\tau) &= \langle x_2(t) x_2^*(t - \tau) \rangle
 \end{aligned}
 = \underbrace{f(g_{1D}, g_{1R}, g_{2D}, g_{2R}, \sigma_1, \sigma_2, \tau_{RD})}_{\substack{\text{Extended Kalman Filter} \\ \text{state vector}}}$$

Chosen delays: $\tau = 0, \tau_{RD} - \Delta\tau, \tau_{RD}, \tau_{RD} + \Delta\tau \Rightarrow$ 12 complex measurements
(22 real + imaginary parts)

$$g_{1D} = G_1 G_{SD}$$

$$g_{1R} = G_1 G_{SR} \sqrt{\Gamma}$$

$$g_{2D} = G_2 G_{ED}$$

$$g_{2R} = G_2 G_{ER} \sqrt{\Gamma}$$

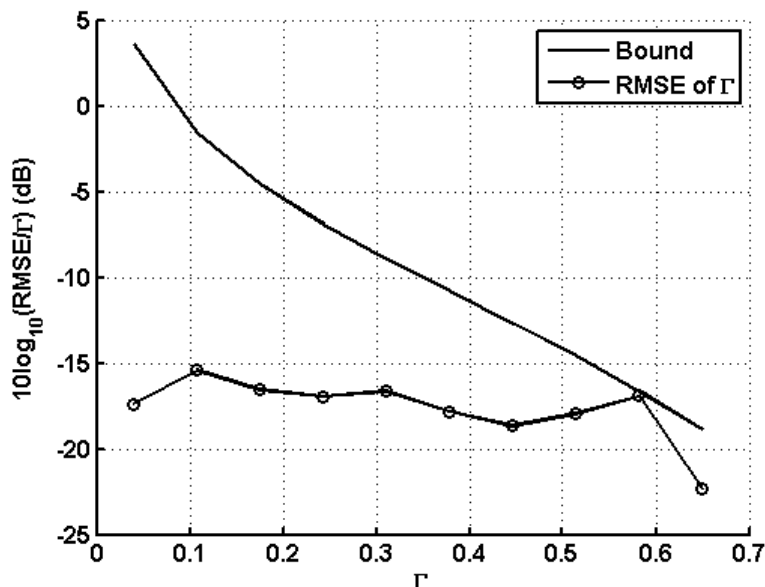
$$\Gamma = \frac{g_{2R}^2}{g_{1D}^2} \times \frac{G_1^2}{G_2^2} \times \frac{G_{SD}^2}{G_{ER}^2}$$

EKF estimates $\nearrow$
 estimated using $\uparrow$
 the transfer switch or noise source $\nwarrow$ antenna patterns (calibrated) + aircraft attitude (IMU)

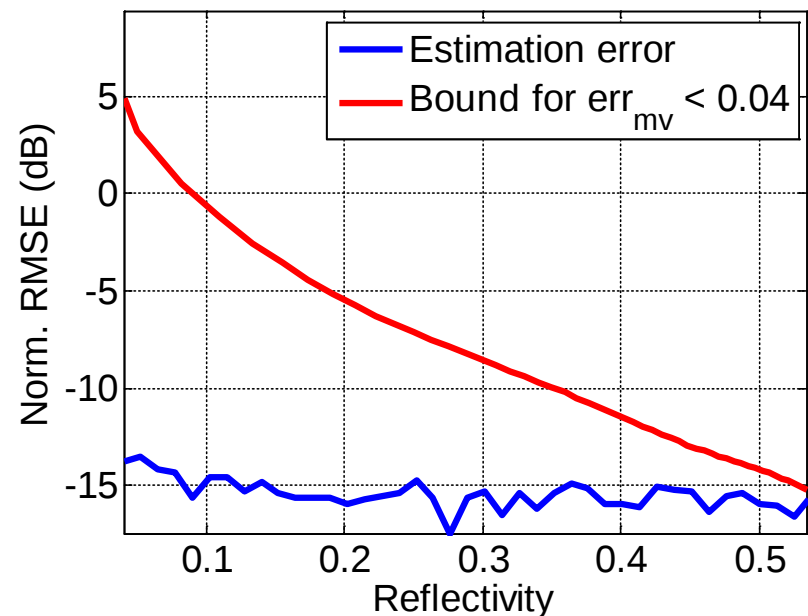
Modelling Results

Results including limited antennas directivities, interference from a second milsat satellite, uncertainty on aircraft position and attitude, 14dBW EIRP, and using 4 samples per correlation, 1s integration time. **Good margin on measurement requirements so far.**

Monte Carlo Results



EKF Results



$$NRMSE_{dB} = 10\log_{10} \left(\frac{1}{\Gamma} \sqrt{\frac{1}{n} \sum_{i=1}^n (\hat{r}_i - \Gamma)^2} \right)$$

Next Steps

- Continue Model Refinement
- Perform I&T at GSFC this Summer
- Field campaign using a tower
- Aircraft campaign