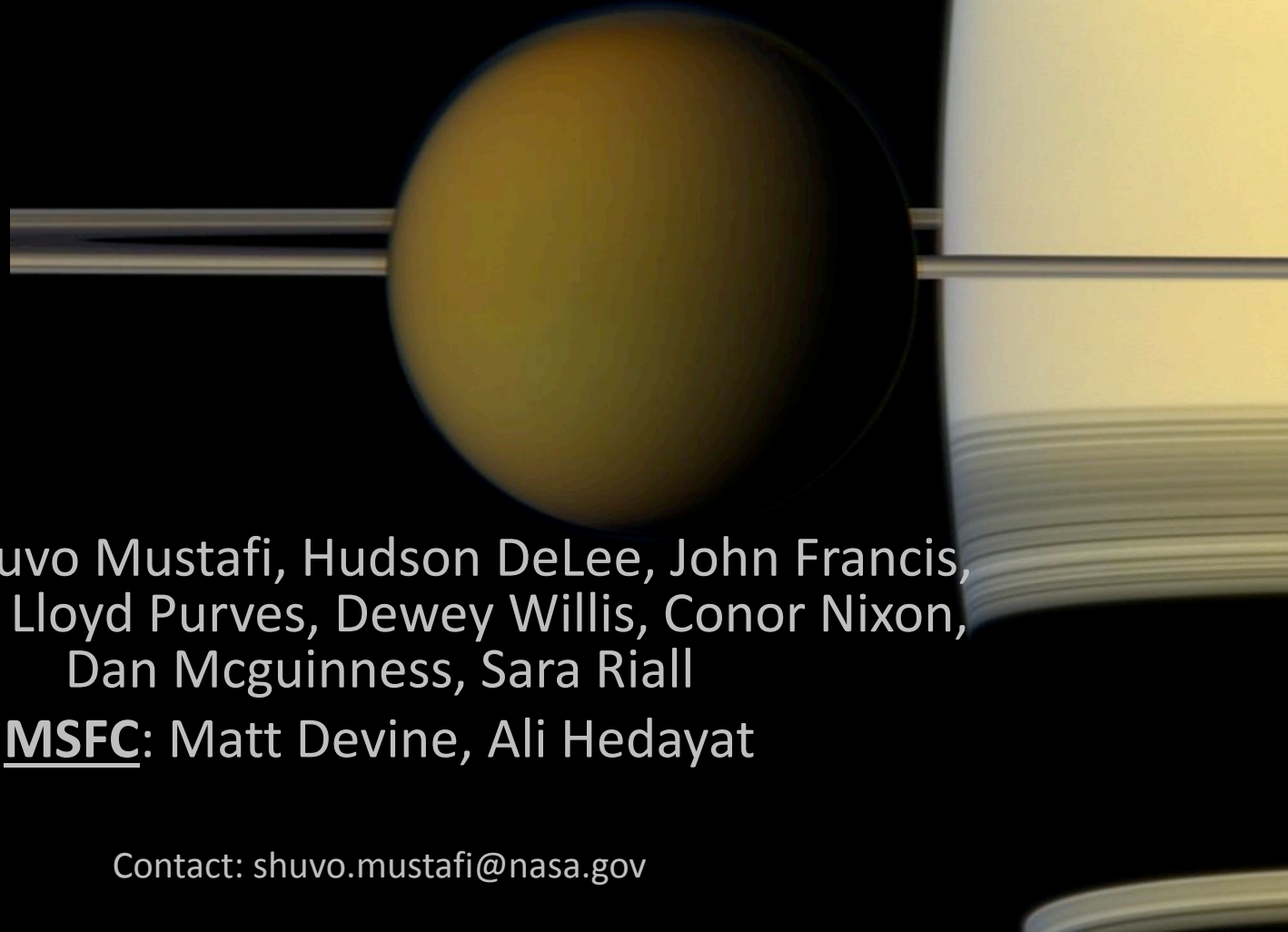


Cryogenic Propulsion for the Titan Orbiter Polar Surveyor

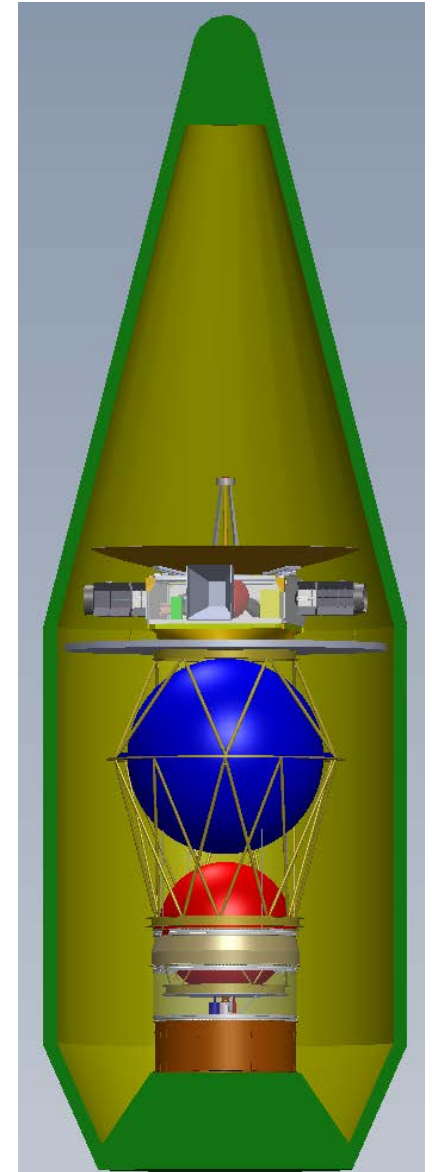


GSFC: Shuvo Mustafi, Hudson DeLee, John Francis,
Xiaoyi Li, Lloyd Purves, Dewey Willis, Conor Nixon,
Dan Mcguinness, Sara Riall

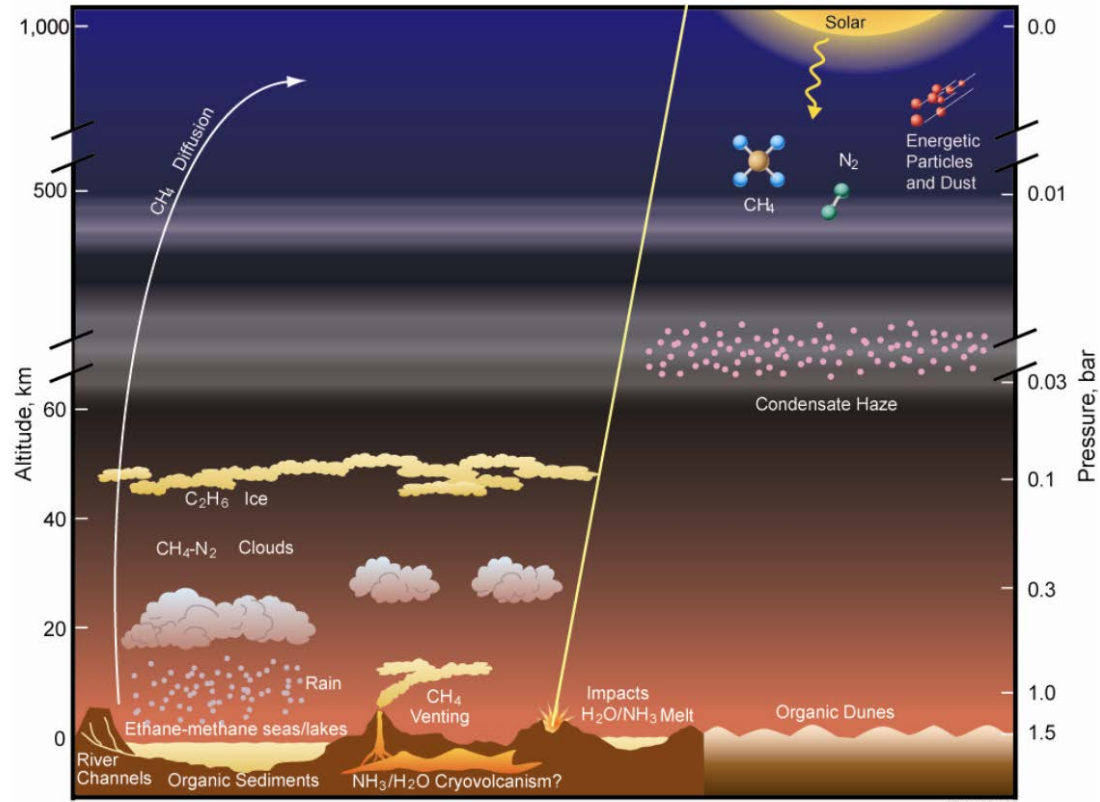
MSFC: Matt Devine, Ali Hedayat

Contact: shuvo.mustafi@nasa.gov

- TOPS Science Goals
- TOPS Spacecraft
- Thermal Design and Analysis
- Conclusions



- Titan's has similarities to Earth
 - 95% N₂ and 1.5 bar pressure at surface
 - Evaporation and Precipitation of Methane similar to Water Vapor Cycle
 - Methane is source of active photochemistry that produces haze and net greenhouse effect of 12K
- Differences
 - Surface Temperature 93K
 - Precipitation of Methane
 - Ethane/Methane seas and lakes
- TOPS Orbit
 - TOPS would place the first spacecraft in polar orbit around Titan
 - First global multi-spectral and radar maps of the surface
- TOPS Science Goals
 - Complete crater counts, yielding surface age estimates for different terrains
 - Lake composition and morphology studies
 - Search for volcanic/endogenic/tectonic activity
 - Meteorology – Clouds and Haze



NASA/JHU/APL, from "Titan Explorer" Mission Study, Lorenz et al., 2008

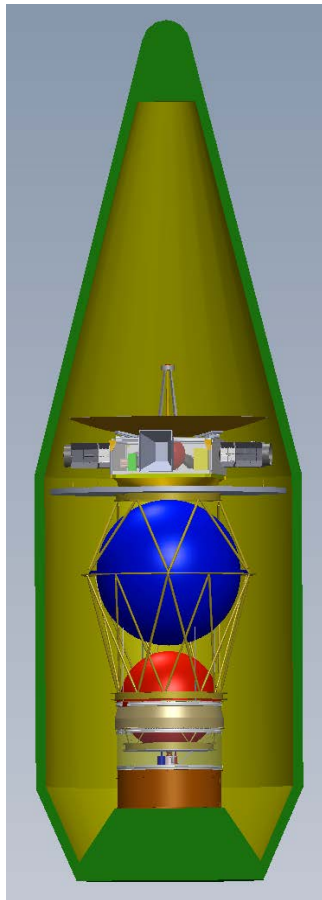


TOPS Mission Parameters

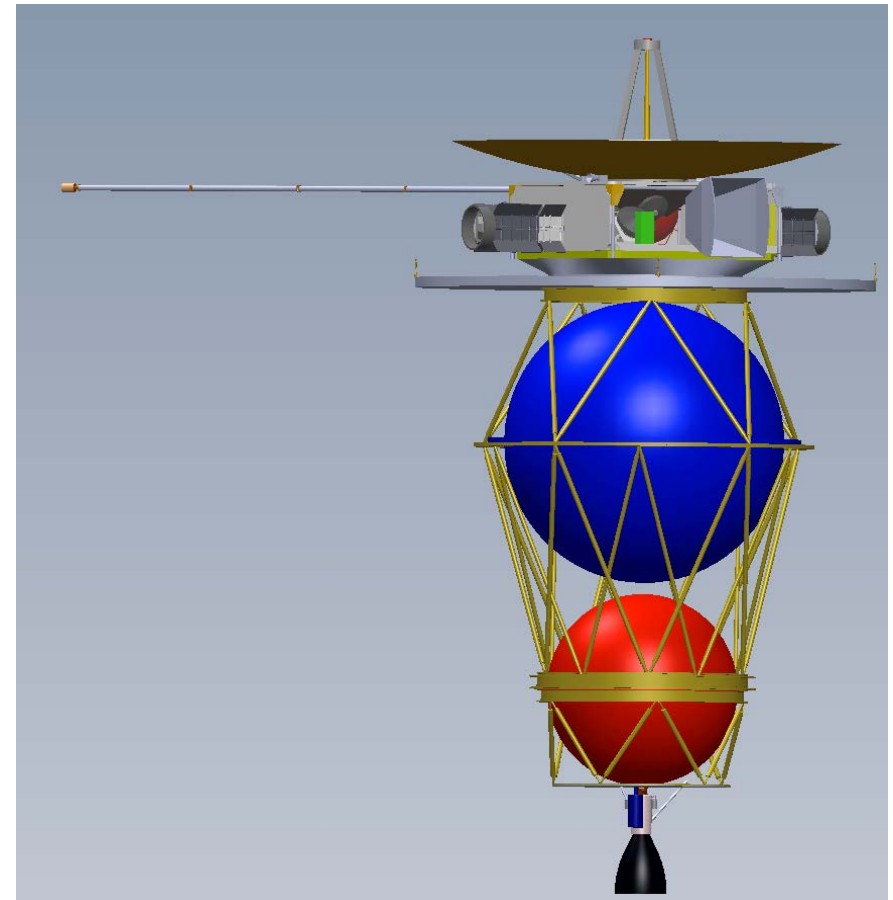


- Mission Duration: 10.5+ years
- Cryogenic Propellant Storage Mission: 8.5+ Years
- Launch in 2022
 - Jupiter not available for gravity assist
- $\Delta V = 5887$ m/s
- 7 Engine Burns
 - Shortest Burn = 2.2 min.
 - Longest Burn = 56 min.
- Launch on an existing Atlas Launch Vehicle
- Science Payload Mass = 53.3 kg
- No Active Cooling during Mission

TOPS Spacecraft

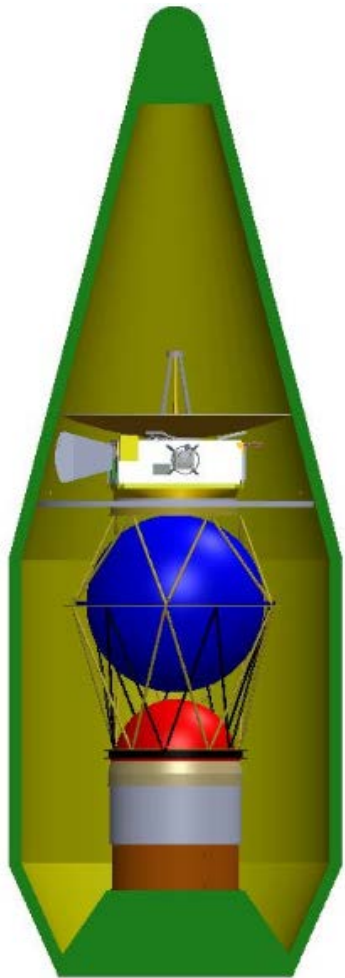


TOPS Spacecraft
Stowed in Atlas AV 551

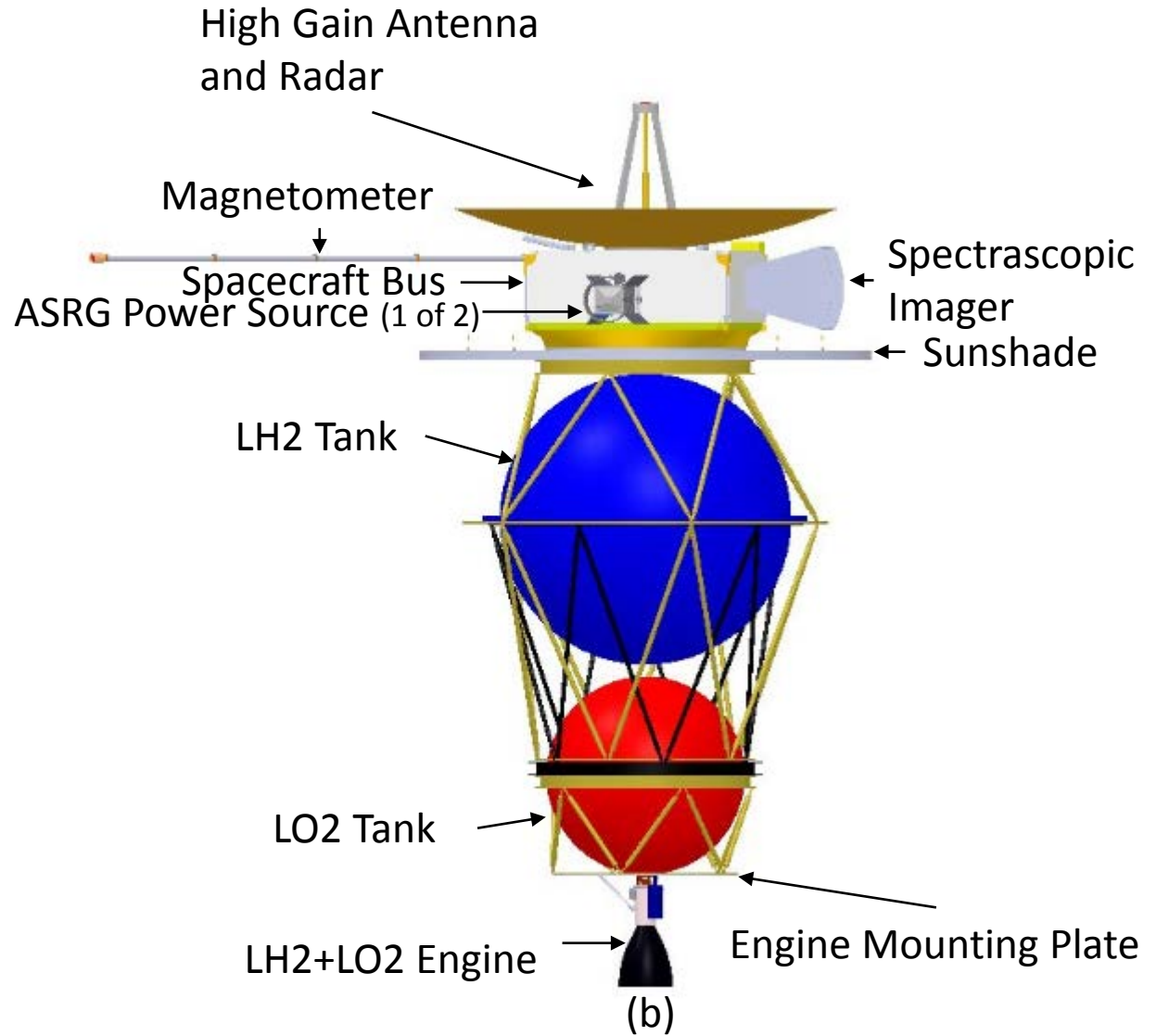


TOPS Spacecraft Deployed

TOPS Spacecraft



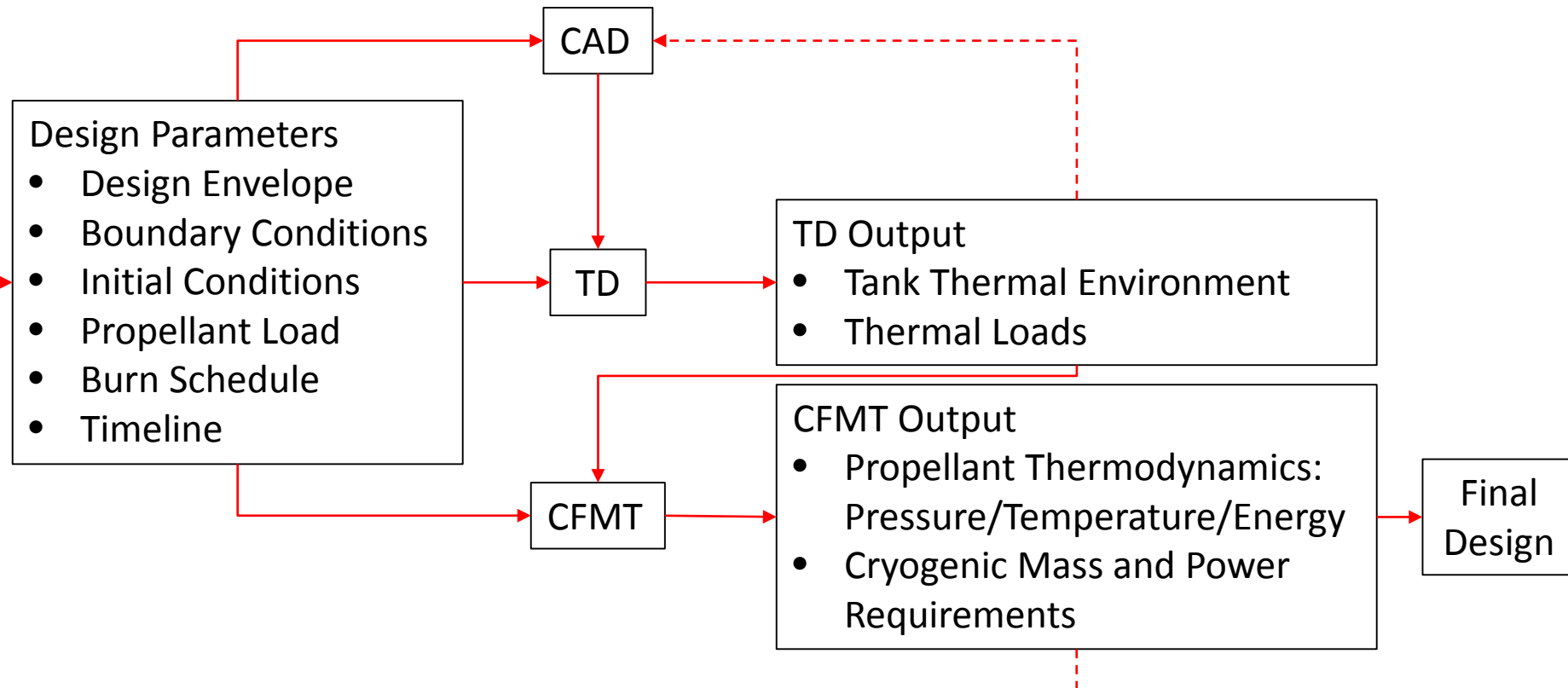
(a)



(b)

Thermal Analysis

- CAD: Creo and Solid Works
- Heat Transfer: Thermal Desktop (TD)
- Fluid Condition: Cryogenic Fluid Management Tool (CFMT) - GSFC Spreadsheet and REFPROP Based Tool



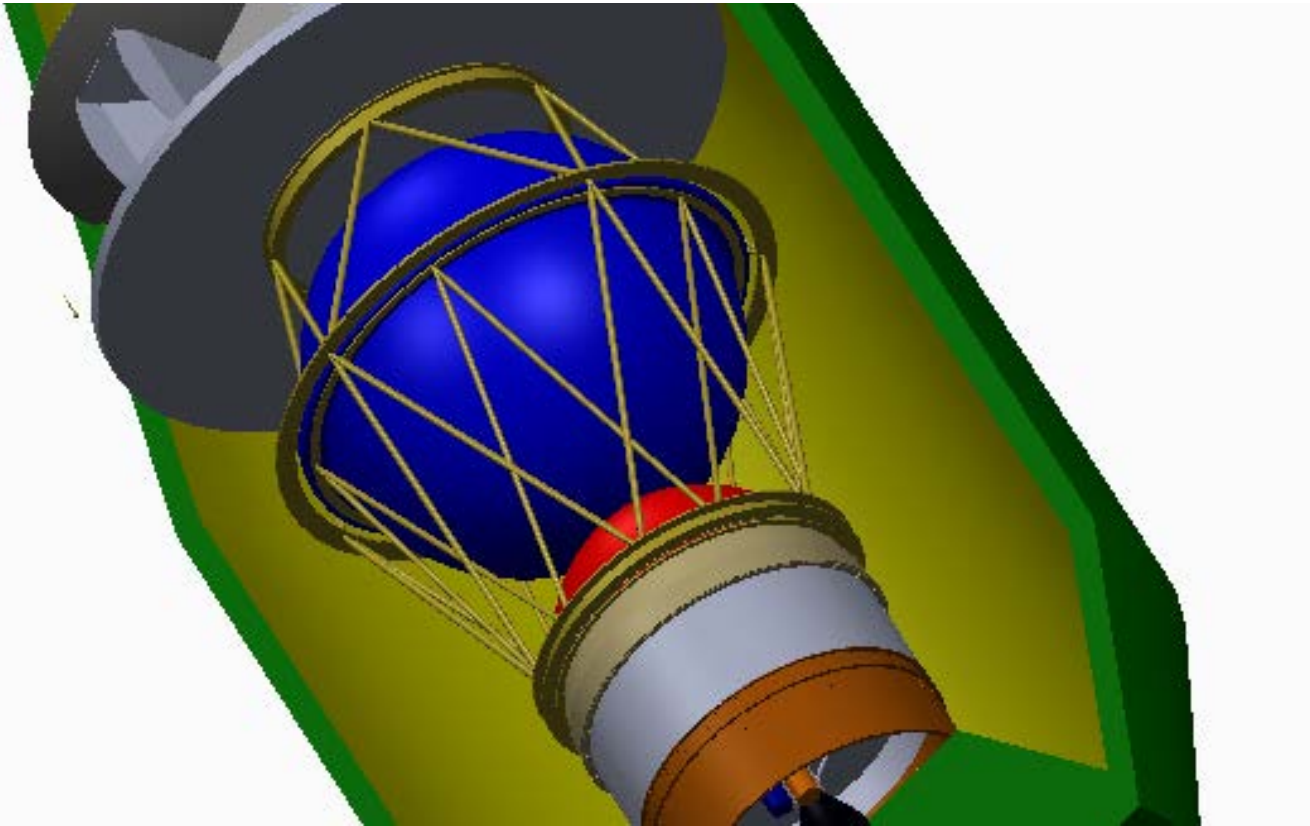


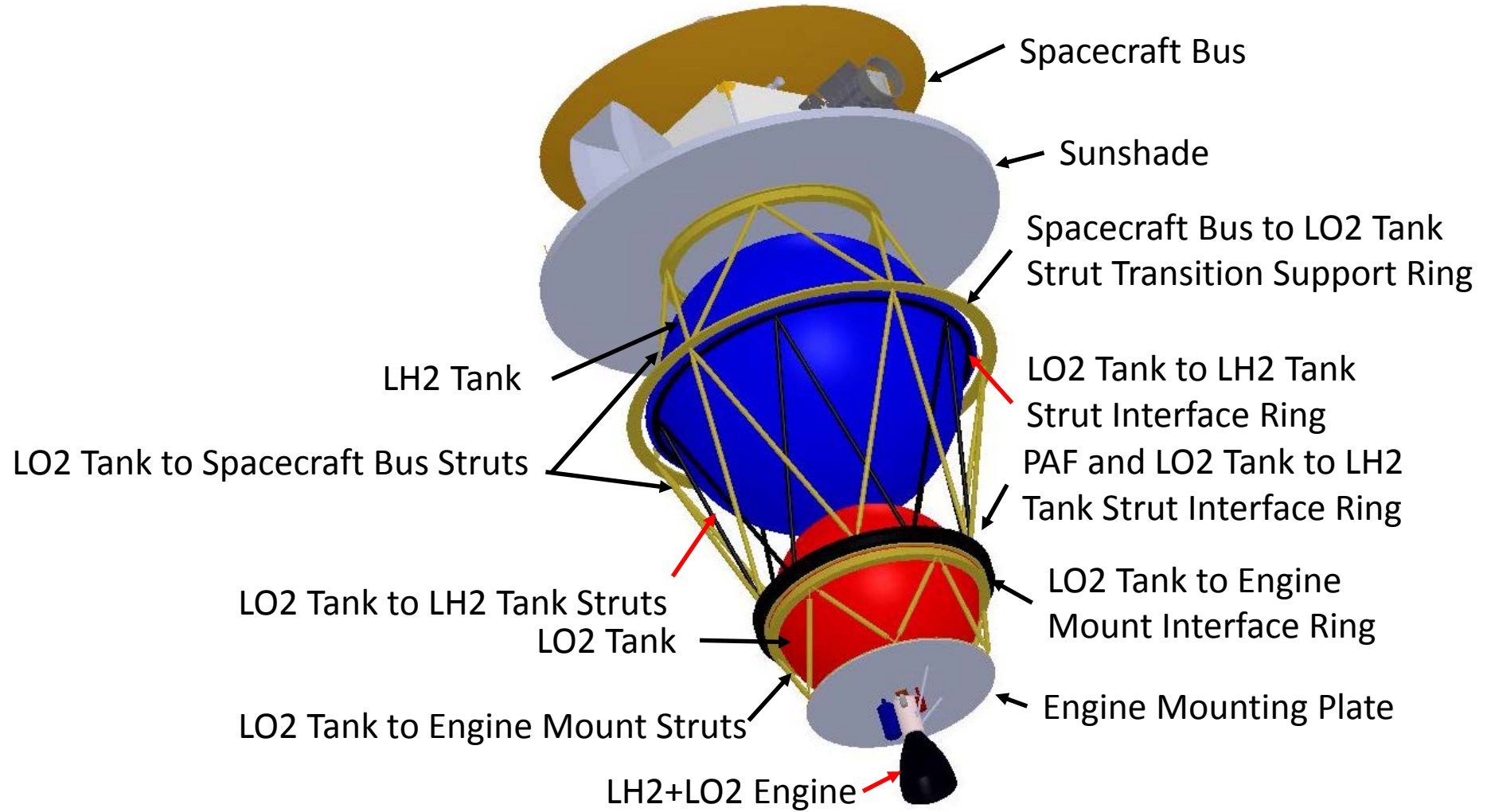
Cryogenic Storage Strategies



- Struts:
 - T300 with low emissivity Aluminum Tape
 - Struts Implemented to have LH2 Tank at Maximum Conductive Isolation via LO2 Tank Stage to Spacecraft Bus or Launch Vehicle Payload Adapter Fairing
- LOx and LH2 Tank
 - 5 layer Load Responsive MLI (LRMLI) for Convective Isolation on the Launch Pad
 - 40 layer Integrated MLI (IMLI) for Radiative Isolation
 - LRMLI and IMLI manufactured by Quest Thermal Group
- Sunshield and Orientation:
 - Multi-layer low solar absorptivity
 - Nominally spacecraft bus will point towards sun
 - Thermal design can accommodate short durations of increased heat input from sun views and engine burns during burn and communication maneuvers
- Fluid Condition
 - LO2: Launched normal boiling point. Densifies slowly during interplanetary phase of mission.
 - LH2: Launched subcooled. Warms slowly during interplanetary phase of mission
 - LH2 subcooling can be provided by a launch pad cryocooler
 - Eg. Turbo-Brayton Cryocooler 400W@15 K Cooler: Estimated Mass: 780 kg Estimated Power: 32kW

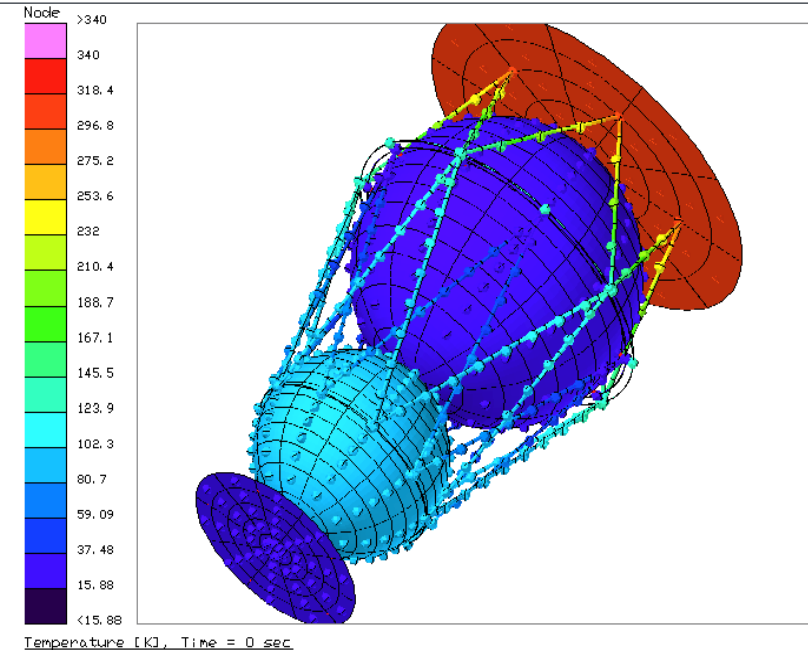
TOPS Truss Structure





Thermal Loads

- Duration of Propellant Storage Mission >8.5+ Years
- LOx Tank
 - Deep Space Nominal Heat Loss: 42 mW
- LH2 Tank
 - Deep Space Nominal Heat Gain = 71 mW
 - Maximum Heat Input During Burns = 191 W
 - Duration of Longest Burn < 57 min.



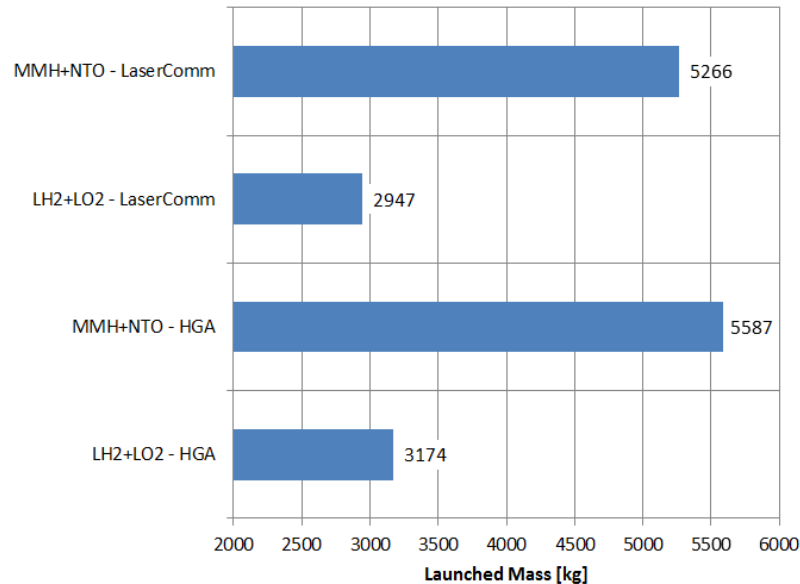


TOPS Launch Vehicle Performance



	LH2+LOX - HGA	MMH+NTO - HGA	LH2+LOX - LaserComm	MMH+NTO - LaserComm
Total ΔV	5887	5887	5887	5887
Dry Mass - Nominal [Kg]	739	878	685	828
Dry Mass with 25% Dry Mass Contingency [Kg]	880	1053	812	991
Launch Mass with 25% Dry Mass Contingency [Kg]	3174	5587	2947	5266
AV 431 - Separated Launch Limit [Kg]	2922	2922	2922	2922
AV 431 - Separated Launch Mass Margin [%]	-8	-48	-1	-45
AV 541 - Separated Launch Limit [Kg]	3200	3200	3200	3200
AV 541 - Separated Launch Mass Margin [%]	1	-43	9	-39
AV 551 - Separated Launch Limit [Kg]	3525	3525	3525	3525
AV 551 - Separated Launch Mass Margin [%]	11	-37	20	-33

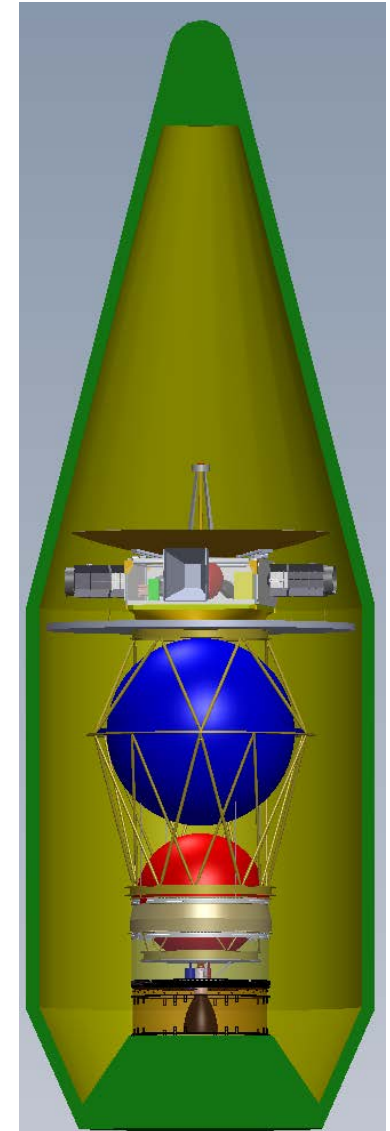
TOPS Launched Mass - Various Configurations



- **LH2+LOx provides the highest specific impulse of any practical chemical propulsion system.**
- For the TOPS Mission this means a 43% reduction in launched mass. This mission can be completed using an Atlas Launch Vehicle using LH2+LO2 but not with MMH+NTO.
- LH2+LOx can enable missions that deliver/recover substantially larger masses to/from the target destinations, or launch the mission on smaller and cheaper launch vehicles, or both.
- Subcooling saves a further 30 kg of boil-off H2 mass that can be directly used for payload.
 - 56.4% of Science Payload Mass of 53.3 Kg
 - Not including secondary mass savings from smaller tank, less insulation, less support structure, less propellant. Accounting for this leads to increased reduction in launched mass.

Summary: Cryogenic Propulsion for Planetary Science Missions

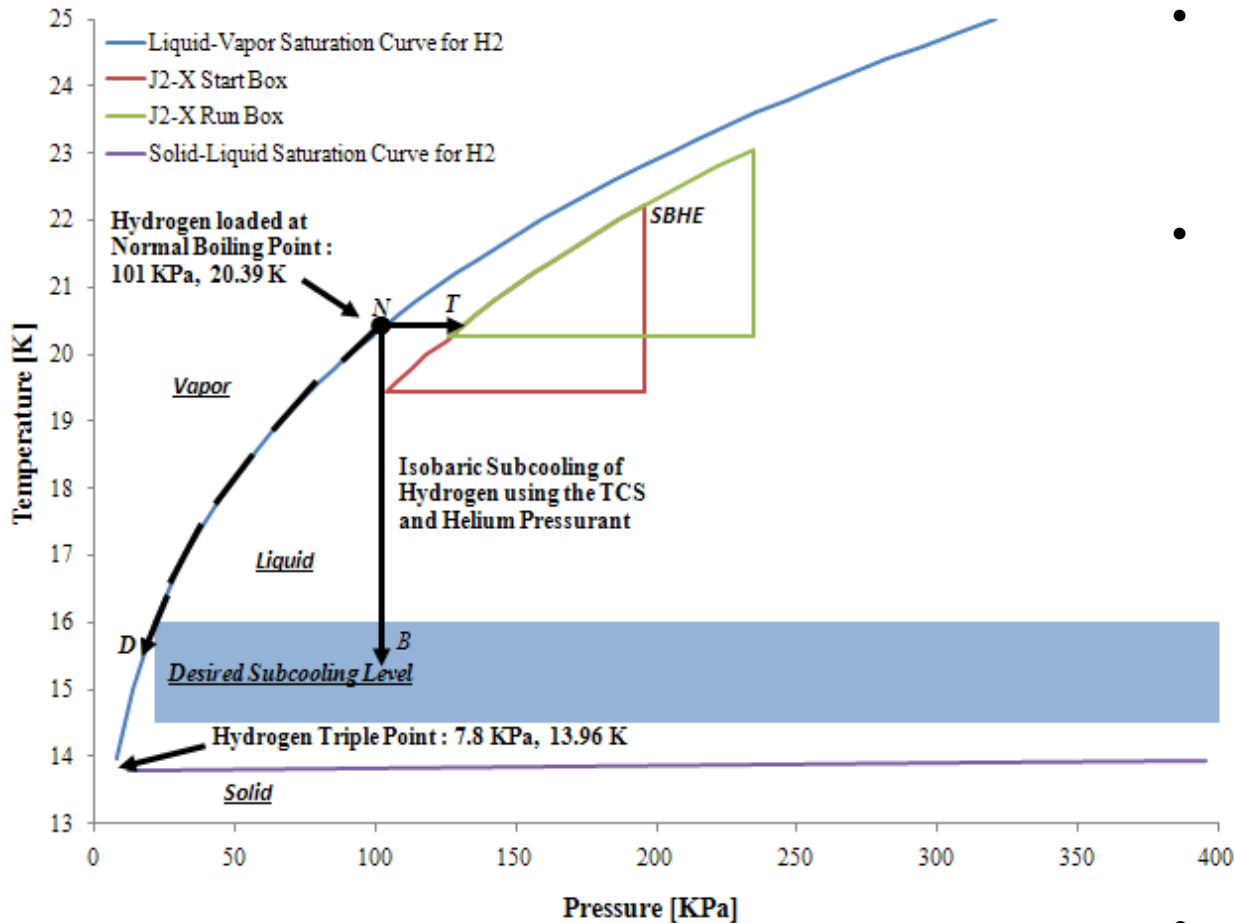
- Cryogenic LH₂+LO_x Propulsion provides high specific impulse chemical propulsion for planetary science exploration
- Provide high ΔV and high delivered and high returned mass to and from planets, moons, asteroids, comets with lower spacecraft wet mass.
- For the TOPS mission, passively cooled LH₂+LO_x reduces launched spacecraft mass by 43% and allows for launch on an Atlas launch vehicle. The same mission cannot be performed using a MMH+NTO propulsion and an Atlas launch vehicle.
- Subcooling cryogenic propellants on the launch pad using a cryocooler enables multi-year storage of LH₂ without adding launched mass. For the TOPS Mission Subcooling saved LH₂ boil-off mass that amounts to 56% of science payload mass.
- LH₂+LO_x Propulsion Development Required:
 - 890 N LH₂+LO_x Engine
 - Implementation of LRMLI and IMLI on 5500 to 6500 L Tanks.
 - Launchpad Subcooling of LH₂
- TOPS Mission and other planetary science missions can be accomplished using without any in-space active cooling.





Backup Slides

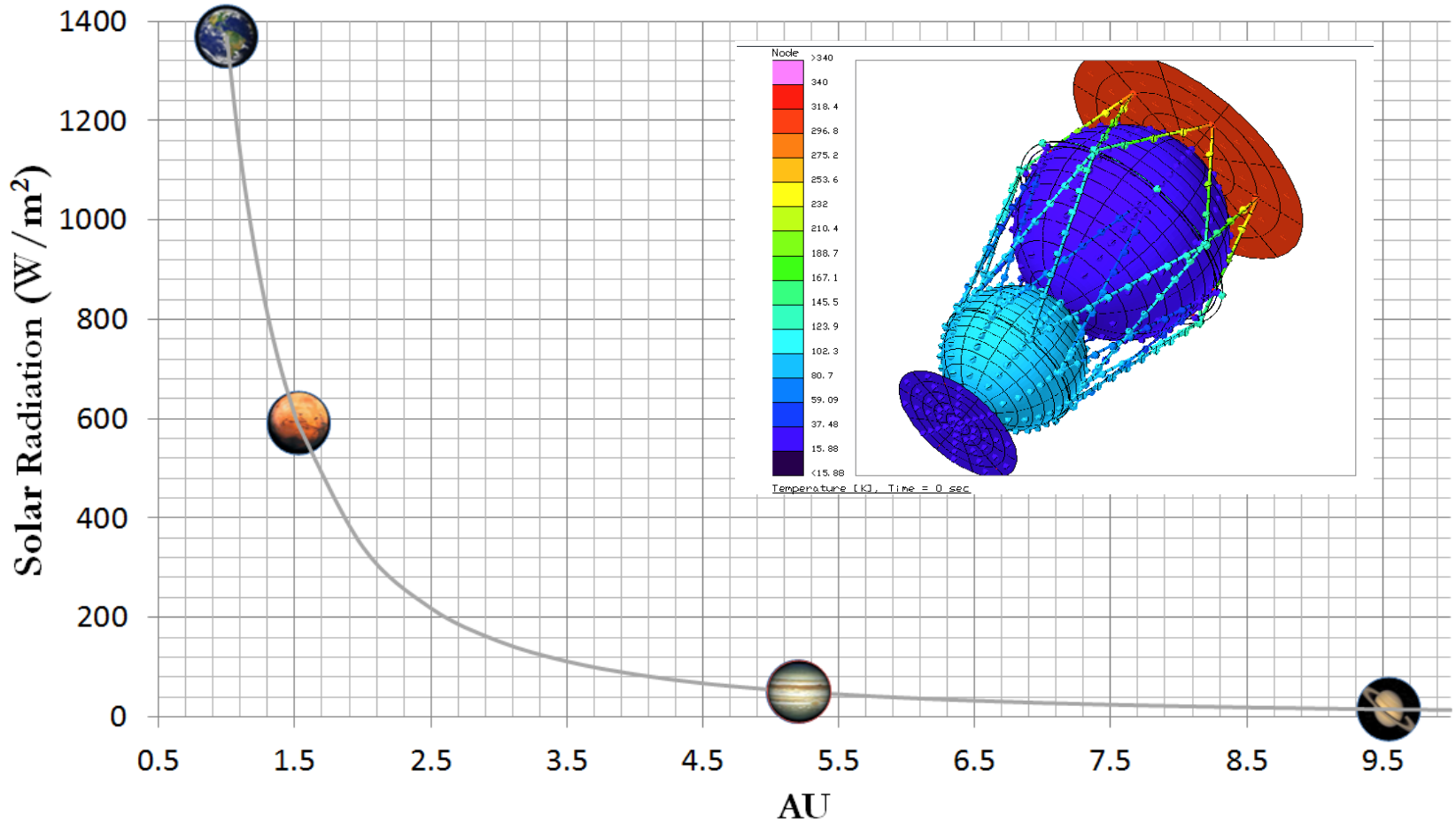
Pre-Launch Isobaric Subcooling for Storage



- RL-10s operated with densified hydrogen
- Other Engines would have to be qualified

- **Objective:** Delay venting of the cryogen as long as possible.
- **Fluid Conditioning**
 - Engine Start Box High End (SBHE)
 - Fluid at Normal Boiling Point (N)
 - Isobaric Subcooling (B)
 - Proposed fluid conditioning method
- **Physics**
 - Substantially lower heat flux in-space than in-atmosphere exploited or enhanced
 - Dominant in-space load < 0.25 W/m²
 - Dominant in-atmosphere load > 63 W/m²
 - Available heat capacity of the stored cryogen - Unexploited
 - Heat Capacity from N to SBHE = 18.2 KJ/Kg
 - Heat Capacity from B (@ T=16 K) to SBHE = 55.0 KJ/Kg
 - Isobaric Subcooling to 16 K allows hydrogen to absorb ~ 3x the energy before venting has to be initiated => hold time before venting for isobaric subcooling is ~ 3x
- Pre-launch Subcooling using launch pad subcoolers or a thermodynamic cryogen subcooler

LH2+LO2 Storage



Combination of Smart Cryogenic Design with Subcooling and Lowering Solar Flux (artificially and naturally) allows long term storage of LH2+LO2 for Planetary Science propulsion

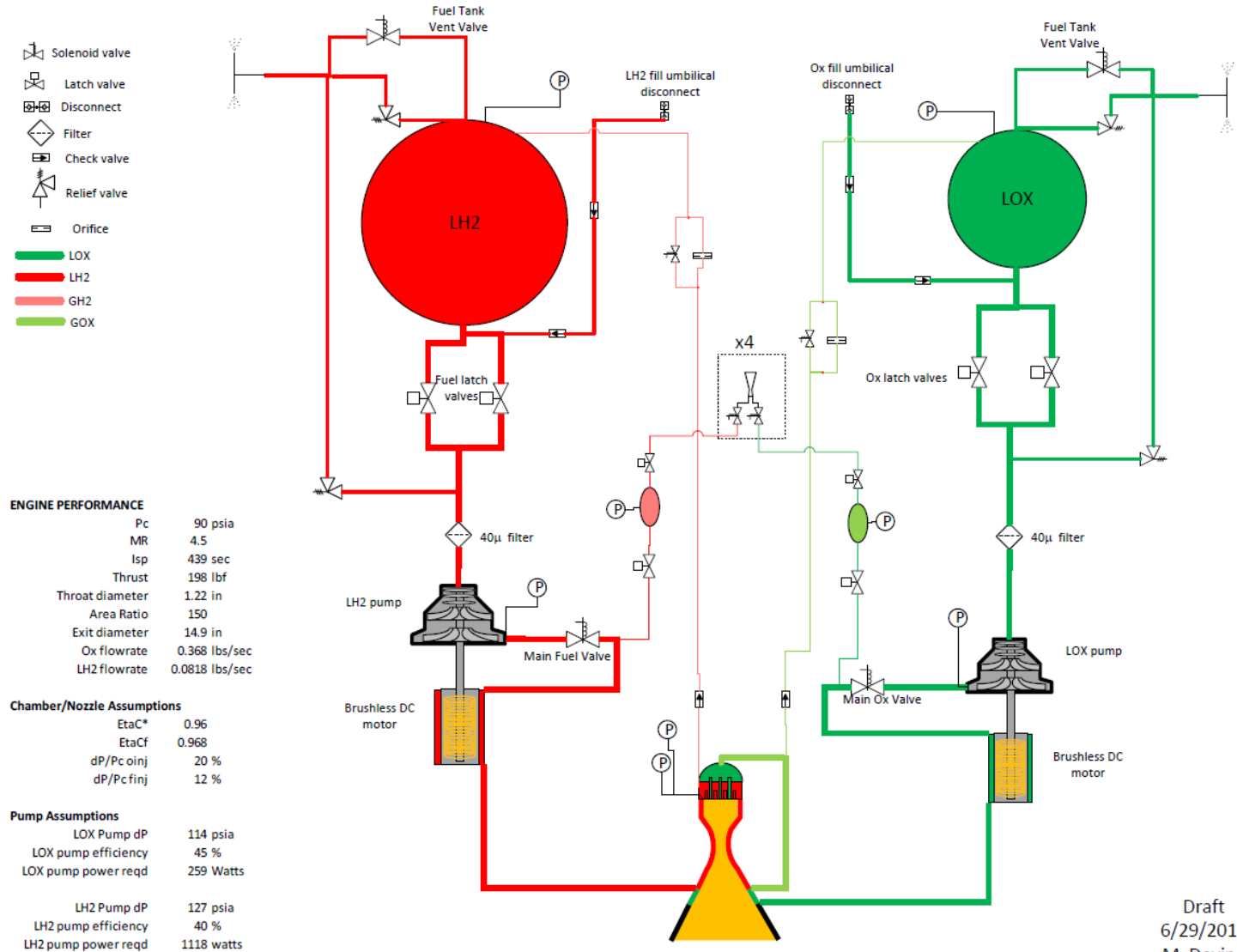
LH2+LOx Main Engine

LH2 + LOx Main Engine Needs to be developed

- Thrust: 890 N
- 440 s Isp
- Area Ratio: 150:1
- Chamber Pressure: 621 kPa
- Mixture Ratio: 4.5
- 7 Burns
- Longest Burn 56+ Minutes.
- Pump Fed
 - Brushless DC Motor
- Active Cooling Circuits for autogenous repres
- Gimballed for Thrust Vector Control



TOPS Main Propulsion System



- Solenoid valve
- Latch valve
- Disconnect
- Filter
- Check valve
- Relief valve
- Orifice
- █ LOX
- █ LH2
- █ GH2
- █ GOX

ENGINE PERFORMANCE

Pc	90 psia
MR	4.5
Isp	439 sec
Thrust	198 lbf
Throat diameter	1.22 in
Area Ratio	150
Exit diameter	14.9 in
Ox flowrate	0.368 lbs/sec
LH2 flowrate	0.0818 lbs/sec

Chamber/Nozzle Assumptions

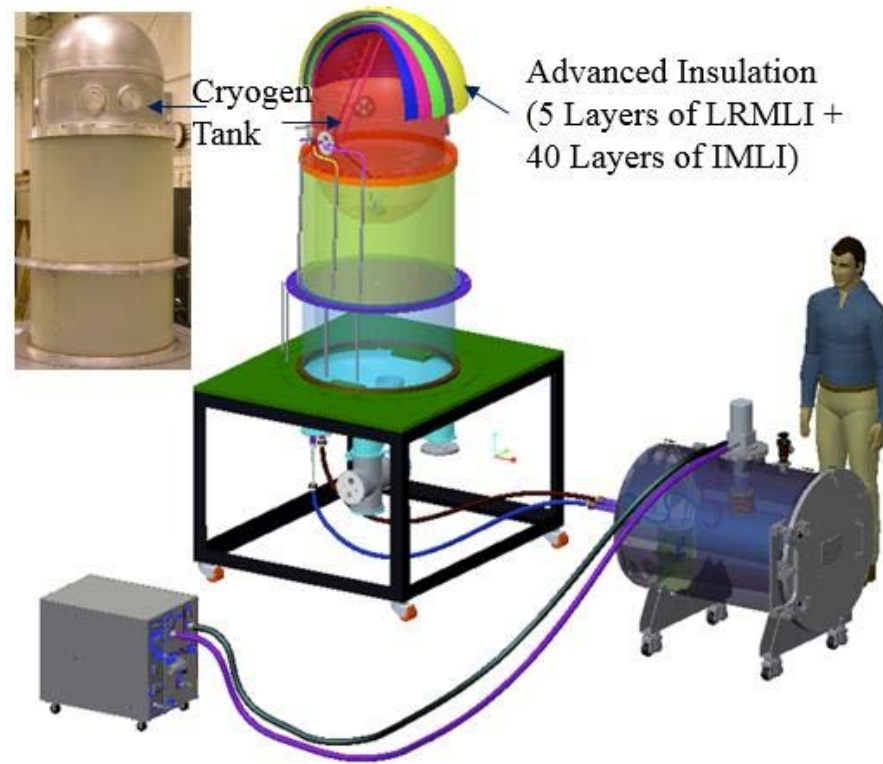
EtaC*	0.96
EtaCf	0.968
dP/Pc oinj	20 %
dP/Pc finj	12 %

Pump Assumptions

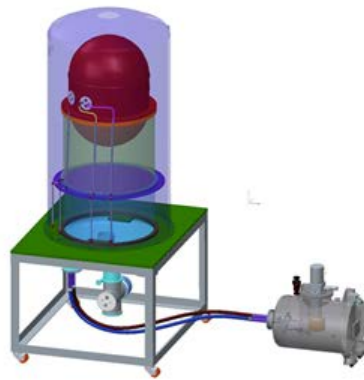
LOX Pump dP	114 psia
LOX pump efficiency	45 %
LOX pump power reqd	259 Watts
LH2 Pump dP	127 psia
LH2 pump efficiency	40 %
LH2 pump power reqd	1118 watts

Draft
6/29/2014
M. Devine

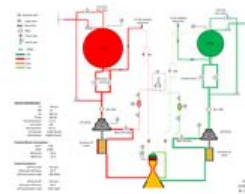
Subcooling Demonstration



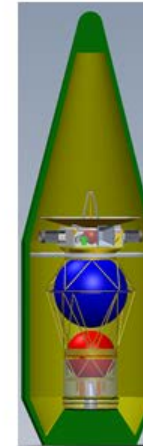
Roadmap



2015: TRL 5



2017: TRL 6



2022: TRL 9