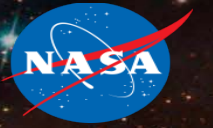




# **NASA Cryocooler Technology Developments and Goals to Achieve Zero Boil-Off and to Liquefy Cryogenic Propellants for Space Exploration**

**D. Plachta, J. Stephens, W. Johnson, NASA Glenn Research Center  
M. Zagarola and D. Deserranno (Creare, LLC)  
July 7, 2017**



- The history of Zero Boil-Off (ZBO) cryocooler integration to cryogenic propellant tanks is described to provide a context for distributed cooling and present cryocooler investments
  - History of ZBO
    - 1998, 2001, 2003 testing
    - Evolution of distributed cooling
      - Analysis at GRC
      - Analysis and testing at ARC
      - 2009 test at Ball
      - Trade study in 2011
      - Reduced boil-off tests in 2012
      - Zero boil-off tests in 2013
- Present ZBO requirements
  - ZBO is required for Nuclear Thermal Propulsion (NTP) concepts in support of human missions to Mars
  - ZBO is required for NASA's Mars Study Capabilities Team, for LOX production and in-space storage
- 20K cryocooler development
- 90K cryocooler development
- Related developments described
- Summary



# 1998 LH2 ZBO Test; 2001 ZBO Test



## 1998 test at GRC

- Condenser at tank top removed heat, along with copper leaves within MLI
- Thermal gradient btw cryocooler and tank was high--8K
- Heat removal relied on buoyancy of LH<sub>2</sub>

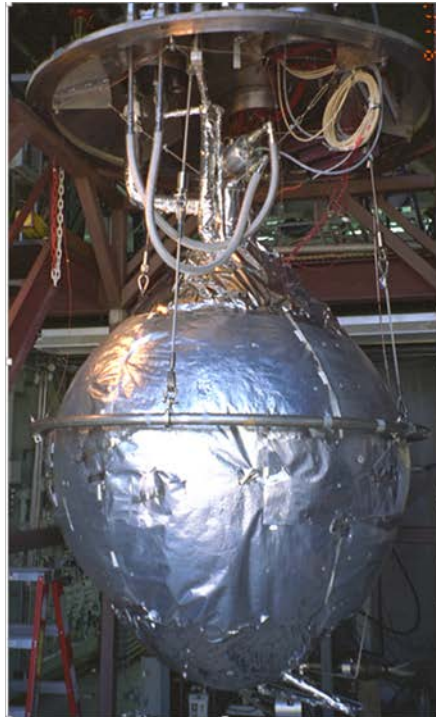


Figure 1. First LH2 ZBO test, 1998, NASA GRC.

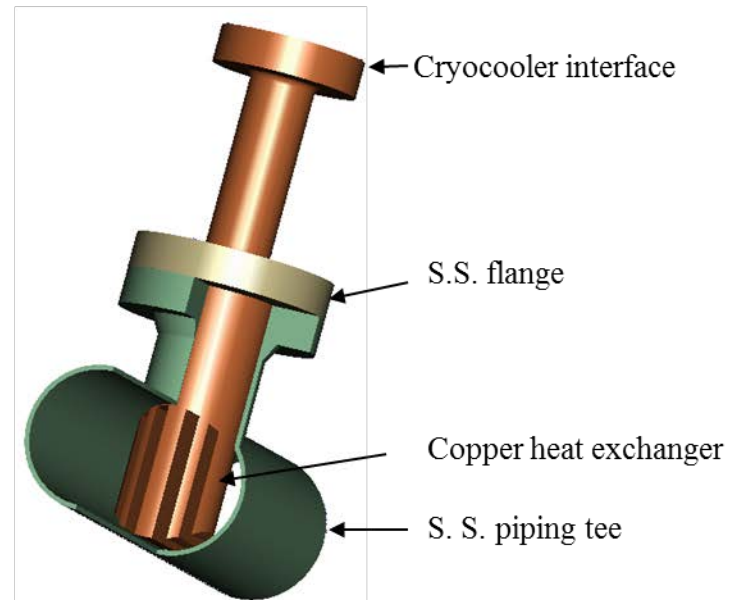


Figure 2. MSFC LH2 ZBO test heat exchanger design.

## 2001 test at MSFC

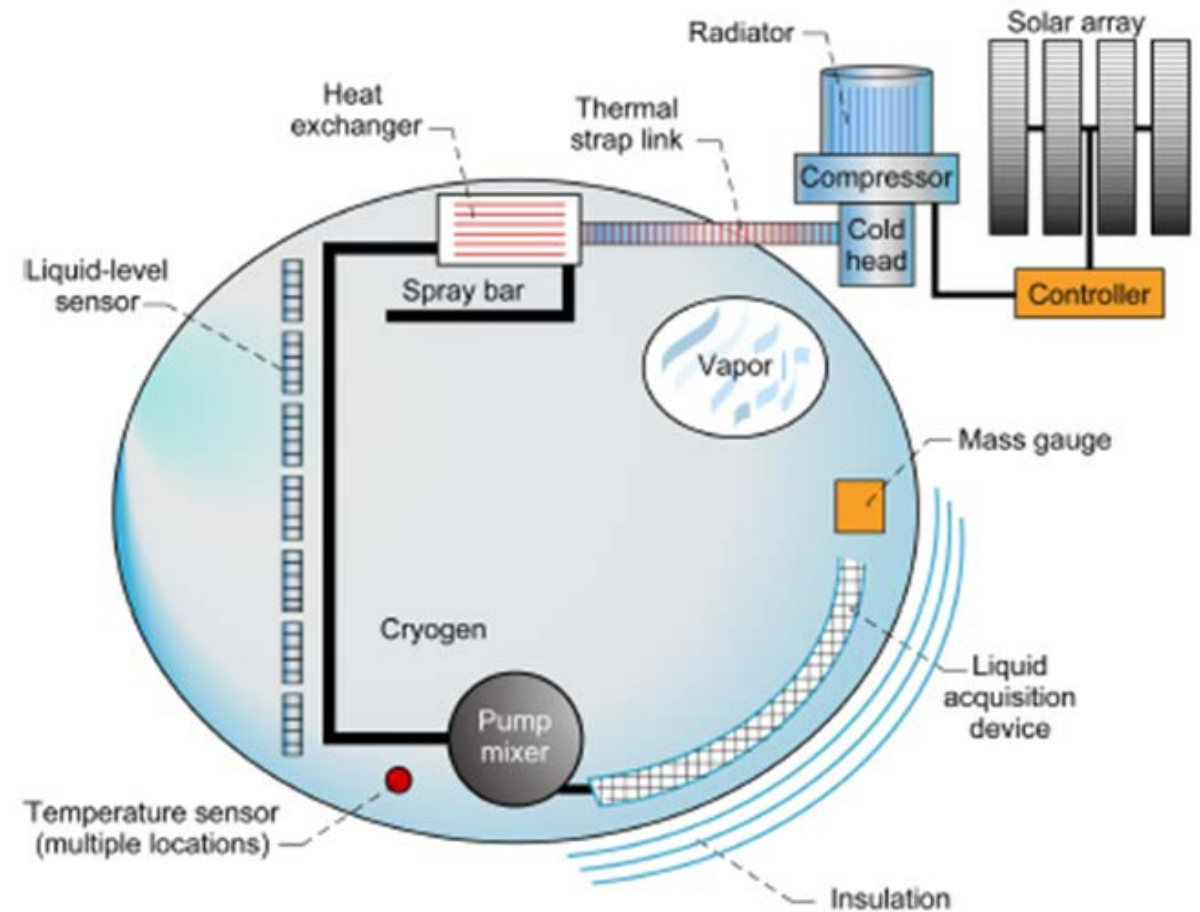
- Heat removed in recirculation loop at tank bottom
- While concept was not sensitive to gravity, integration issues were added heat of recirculation loop and heat from mixer, which required continuous operation

- *These tests provided a foundation for future developments*

# 2003 Advanced Development Test



- Figure shows schematic representation of preferred flight ZBO concept in 2003
- 2003 test at GRC
  - Flight-type cryocooler integrated with heat pipe
  - Cryocooler located close to tank at top
  - Issues were:
    - High thermal gradient between tank top and cooler (6.9K); expected to increase when cooler placed further from tank, as expected
    - Pump operation added heat



# Distributed Cooling



- GRC design of distributed cooling began in 2007
  - Concept uses gas circulated across cryocooler heat exchanger and plumbed around tank and within MLI
- Ames analysis and bench testing proved heat exchanger designs
- 2009 test at Ball using broad area cooled shield, shown at right. Results showed:
  - High heat exchanger effectiveness
  - Insensitivity to slight flow imbalance in tubes
  - Temperature gradients between tubes were less than design indicated
    - MLI helped distribute cooling

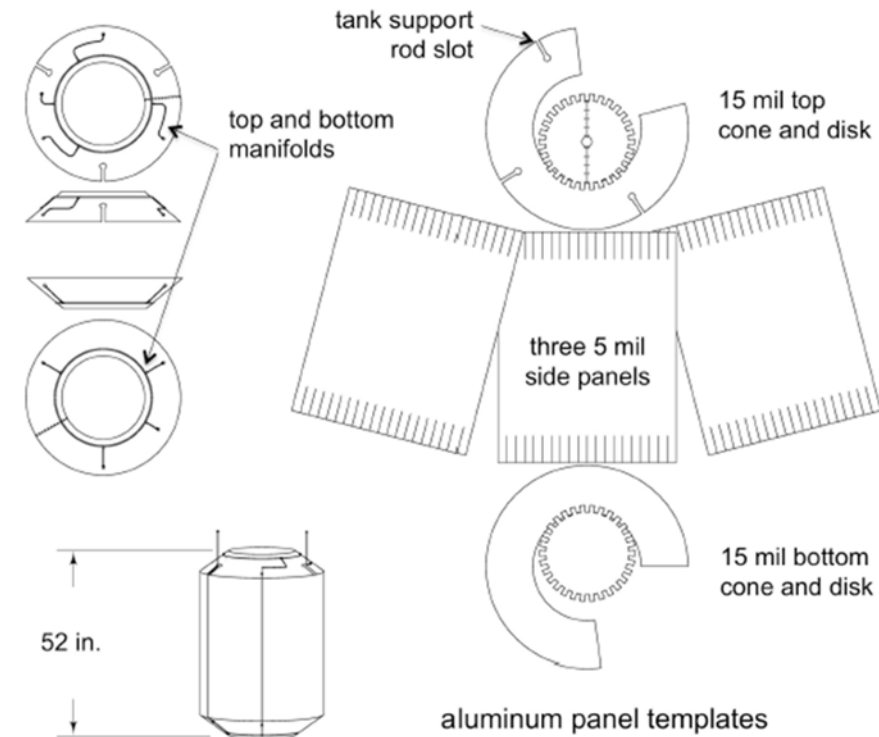
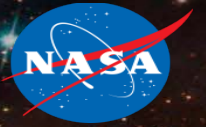


Figure 4. The broad area cooled shield, constructed from 1100 aluminum panels and cooled with three  $\frac{1}{4}$ " tubes.

# Distributed Cooling Trade Study



- Following Ball test, NASA pursued comprehensive trade study of cryocoolers and circulators for:
  - LOX ZBO/liquid hydrogen RBO demonstration under CPST
  - Extensibility for flight via scaling/sizing
- Reverse turbo-Brayton cycle (RTBC) was selected
  - Working fluid could be used to directly cool tank
  - Cryocooler specific mass and power improves with larger lifts, critical to ZBO application
  - RTBC includes very efficient circulator
    - Circulator options considered (see table)
    - Heat leak to fluid and anticipated heat exchanger loss from integration of cold finger to circulator were important factors

| Manufacturer                 | Mass, kg | TRL <sup>a</sup> | Input power, W | Heat Leak to fluid, W | Fluid          | Phase, Φ     | Motor temp., K | Flow, g/s | Press., atm |
|------------------------------|----------|------------------|----------------|-----------------------|----------------|--------------|----------------|-----------|-------------|
| CryoZone Ciezo               | N/A      | 5                | N/A            | 4                     | He             | Gas (cold)   | 85             | 0.6       | 21          |
| Sierra Lobo He blower        | 1        | 4                | 0.28           | .14                   | He             | Gas (cold)   | 85             | .57       | 20          |
| Creare NICMOS circulator     | 1        | 9                | .89            | .6                    | Ne             | Gas (cold)   | 80             | .75       | 3           |
| CryoZone Noordenwind CryoFan | N/A      | 5                | .6             | N/A                   | He             | Gas (hot)    | 300            | .57       | 21          |
| Aerojet He gas circulator    | 3.5      | 5                | 2.8            | 2.0                   | He             | Gas (cold)   | 150            | .8        | 20          |
| Barber-Nichols               | N/A      | 4                | 71             | 44.9                  | He             | Gas (cold)   | 90             | 41.8      | 27          |
| Sierra Lobo piston           | 1        | 3                | .01            | .001                  | N <sub>2</sub> | Liquid (2-Φ) | 85             | .13       | 2           |
| Lawrence Lab bellows linear  | 4.5      | 3                | 16.5           | 5.0                   | He             | Liquid (2-Φ) | 4.5            | 40        | 4           |
| Mikrosysteme 2-phase         | N/A      | 4                | .1             | .0                    | Ar             | Liquid (2-Φ) | 120            | .3        | 12          |

<sup>a</sup>Technology readiness level.



# Reduced Boil-Off Tests (RBO) Conducted



- Using Creare RTBC cryocooler with distributed cooling on tank, NASA MSFC, Ames, and GRC combined efforts to complete Reduced Boil-Off LH2 tests and ZBO LN2 tests
  - Tube on shield heat exchanger used
  - Where cooled was used, boil-off was reduced 60%
  - MLI heat leak under 90K shield was higher than expected
    - Cause of issue remains unsolved
  - Penetration conduction (plumbing and struts) heat was reduced by 67%



Figure 5. The NASA SMiRF test rig used in RBO and ZBO testing.

# Zero Boil-Off (ZBO) Tests Conducted

- Same cryocooler was used to achieve robust tank pressure control of LN<sub>2</sub> without venting
- Tube-on-tank heat exchange used
- RTBC Cryocooler cycle is shown on right
- Cryocooler achieve ZBO at high and low fill levels
- Cryocooler (at ZBO condition) dropped thermal gradient in fluid from 10.2 to 3.8K
- As power to cryocooler was increase, cryocooler decreased tank pressure
  - Graph shows that pressure rise/decay rates vs. net heat
  - Data agrees with homogenous model, showing distributed cooling effectively de-stratified cryogen
  - Testing validated Cryo Analysis Tool and Scaling Study

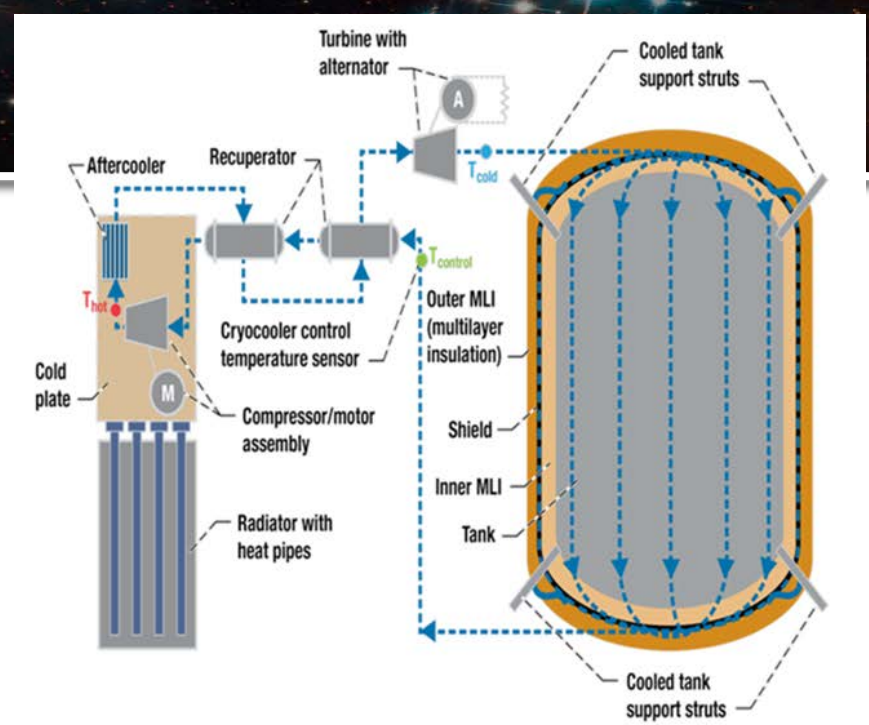


Figure 6. Schematic of the reverse turbo-Brayton cycle cryocooler

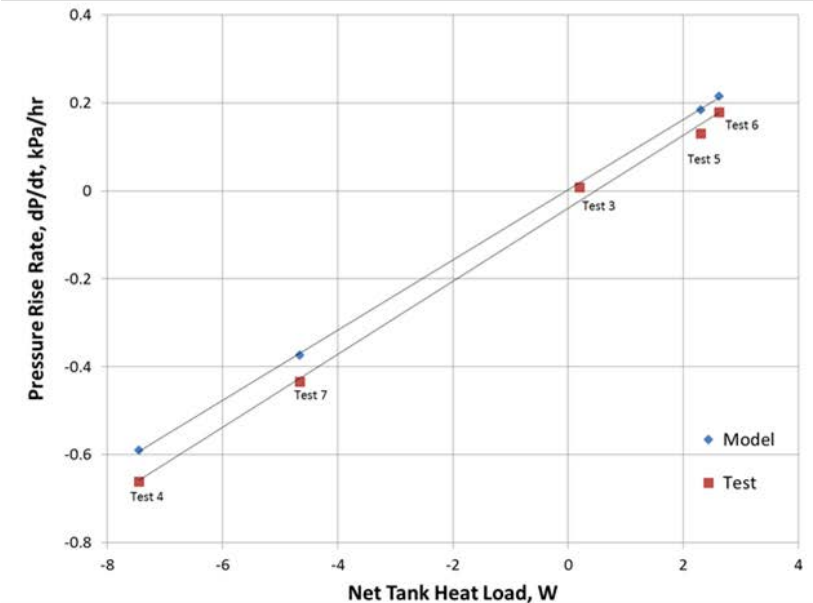


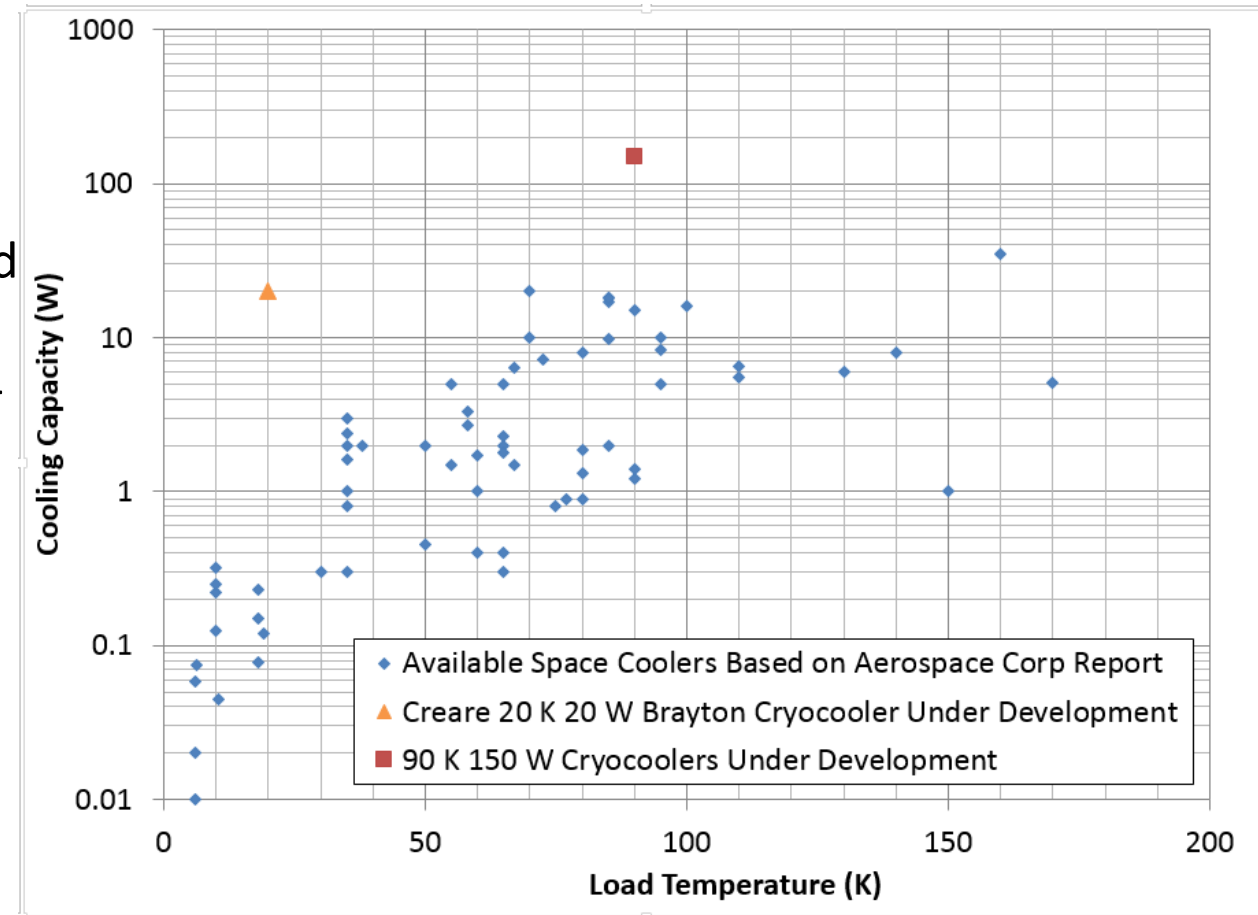
Figure 7. Tank pressurization sensitivity to net tank heat.



# Extension to NASA's Missions



- NASA's Mars Study Capabilities Team is studying propulsion options for human missions to Mars
- Applications for ZBO are:
  - Nuclear Thermal Propulsion Stages
  - In-space chemical propulsion stages, LO<sub>2</sub> and LCH<sub>4</sub>
  - Liquefaction of LO<sub>2</sub> on Mars surface from In-Situ Resources
- Cryocooler requirements are over 20W at 20K and ~150W at 90K
  - Both requirements are substantially greater than that available
  - NASA is directing technology investments to advance the state-of-art through the SBIR program



# 20K-20W Program

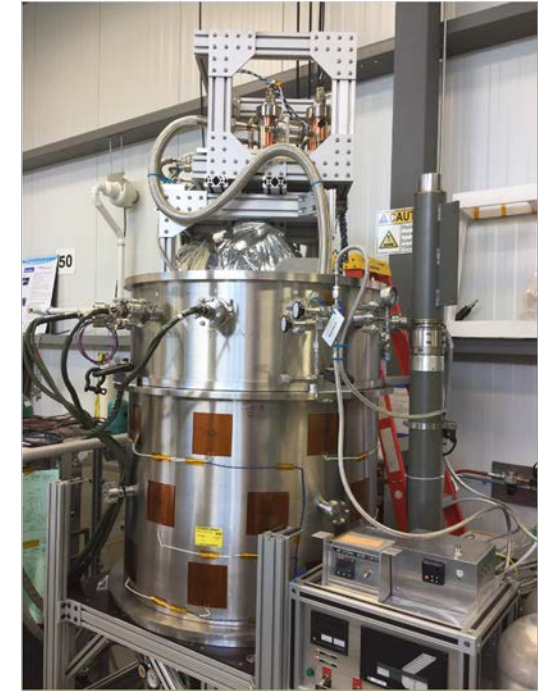
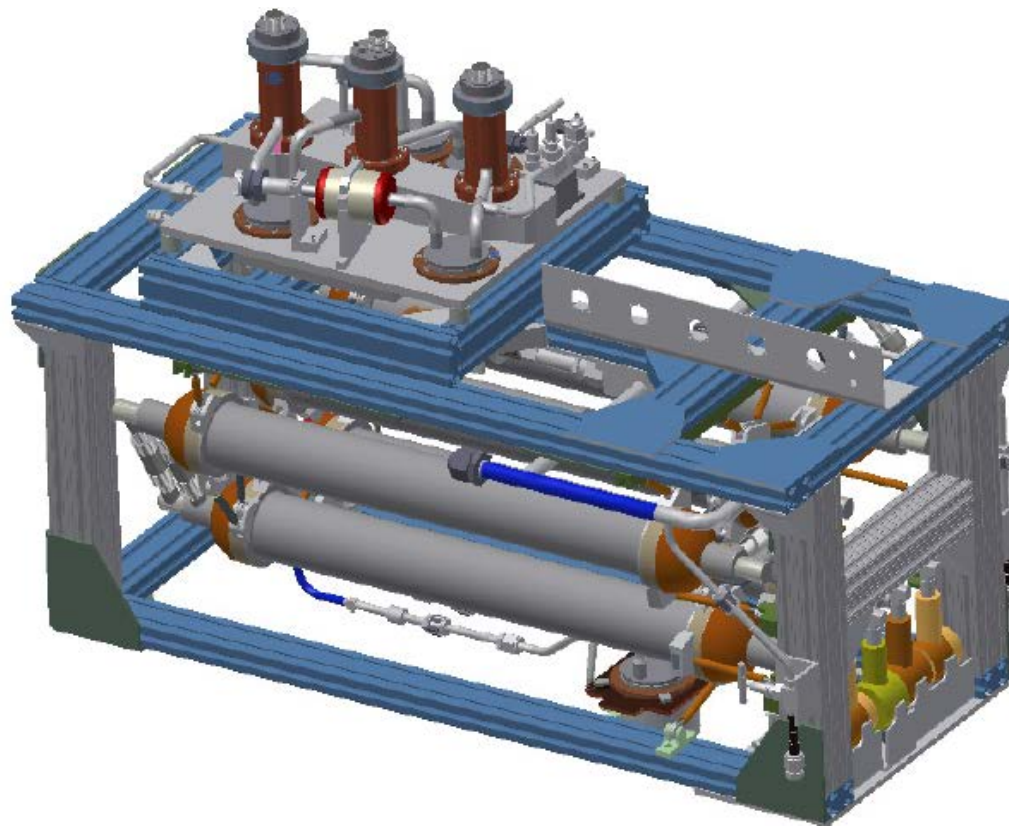


Figure 9. The assembled 20K-20W cryocooler installed into the bottom section of the vacuum bell jar, in preparation for testing.

| Key Performance Parameter     | State-Of-The-Art | Contract Threshold | Contract Goal | As-Delivered | Flight      |
|-------------------------------|------------------|--------------------|---------------|--------------|-------------|
| Cryocooler Lift at 20 K       | 1 W              | 17 W               | 20 W          | 20 W         | 20 W        |
| Compressor Speed              | N/A              | N/A                | N/A           | 6,600 rev/s  | 6,380 rev/s |
| Cryocooler Input Power        | N/A              | N/A                | N/A           | 1,800 W      | 1,420 W     |
| Specific Power                | 370 W/W          | 80 W/W             | 60 W/W        | 90 W/W       | 71 W/W      |
| Cryocooler Mass (flight like) | N/A              | N/A                | N/A           | N/A          | 106 kg      |
| Specific Mass (flight like)   | 18.7 kg/W        | 5.5 kg/W           | 4.4 kg/W      | N/A          | 5.3 kg/W    |

- Two Phase II SBIRs are underway
  - Converter Source
  - Creare
- Results of Phase I concept development

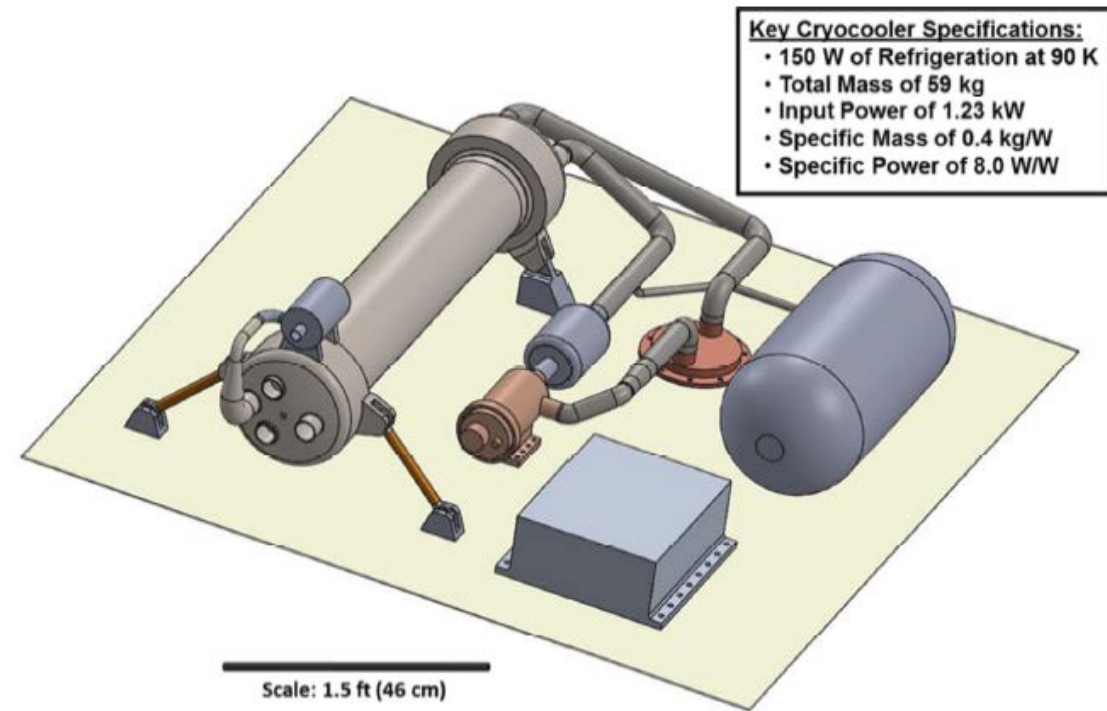
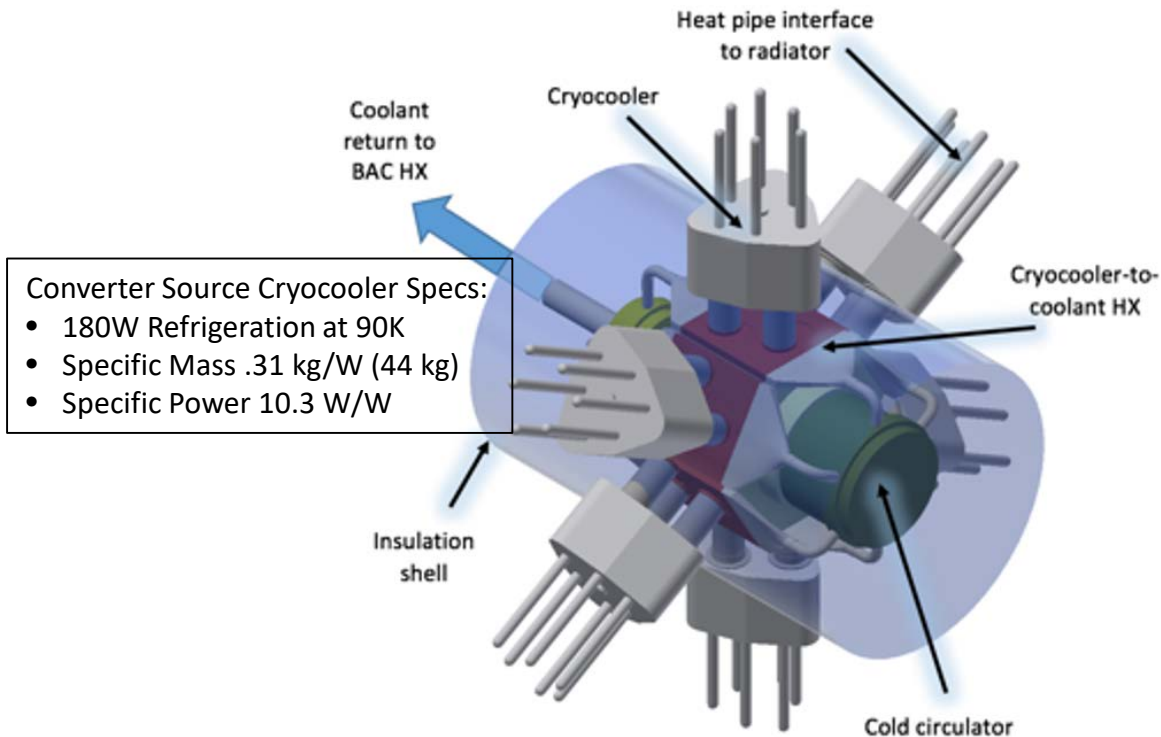


Figure 2. Creare's Preliminary Design of a 90 K, 150 W Cryocooler for Liquid Oxygen Storage



# Recommended Related Developments



- Optimized thermal/structural design of NTP stage
  - Structural heat leak for tank skirt remains unknown
  - Fluid system design must be configured, sized, and heat loads estimated
- Further development of high capacity 90 K cryocoolers
- Additional testing:
  - NASA characterization and endurance test of 20K-20W Cooler
  - Vibration testing of 20K-20W
  - LH2 ZBO test with two stages of cooling
- Summary—NASA developments in ZBO technologies has evolved, with focus on distributed cooling, 20K and 90K coolers, and optimized vehicle design.