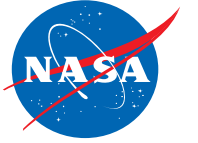


2018 Spring Technical Meeting  
Central States Section of the Combustion Institute



# Chemiluminescence measurements in a combustor using a 7-point lean direct injector array configuration for gas turbine engine applications

Tyler G. Capil, NASA Glenn Research Center  
Kathleen M. Tacina, NASA Glenn Research Center  
Yolanda R. Hicks, NASA Glenn Research Center

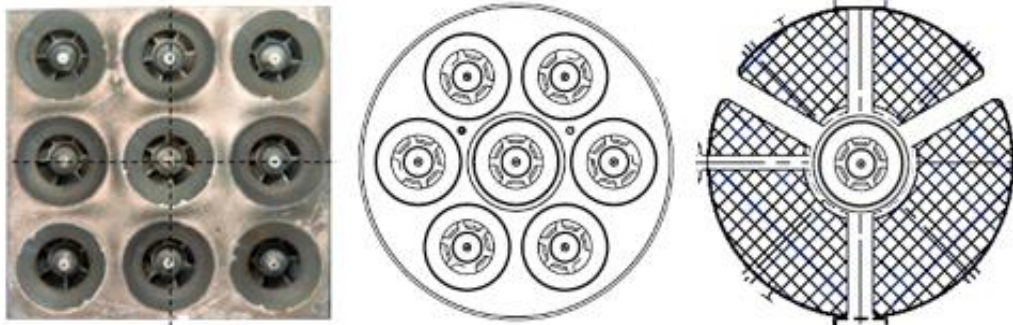
Minneapolis, Minnesota  
May 20-22, 2018

# Outline

- Motivation
- LDI hardware
- Objectives for present work
- Recent history
- Optical diagnostics setup
- Results from LDI

# The motivation for Lean Direct Injection (LDI) was proposed as a technique to reduce aircraft NOx emissions

- Fuel directly injected into combustor
- Fine atomization and rapid fuel-air mixing
- Multiple, smaller fuel injectors instead of single injector



Performs well at high power but sometimes suffers unstable flame at low power conditions

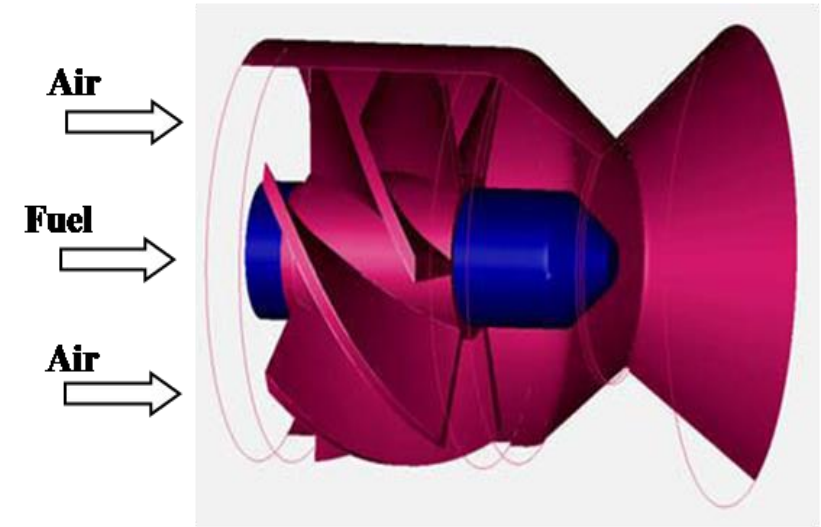
Lean combustion prone to pressure dynamics leading to instabilities

# LDI Hardware

The baseline element of the LDI hardware consists of a converging-diverging venturi throat

Simplex fuel nozzle placed at tip of venturi throat

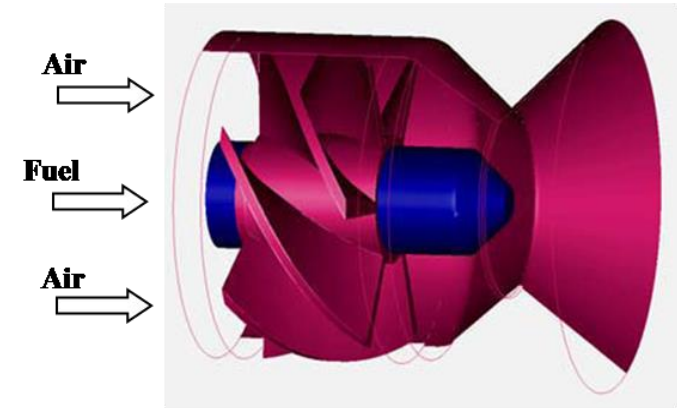
Six helical blades guide the air flow path  
Typical swirlers used are  $45^\circ$ ,  $52.5^\circ$ ,  $60^\circ$



# LDI Hardware

Seven elements arranged to form 7-point array where spacing between elements is 23.8 mm

Center element acts as pilot and injector tip can be offset in upstream direction



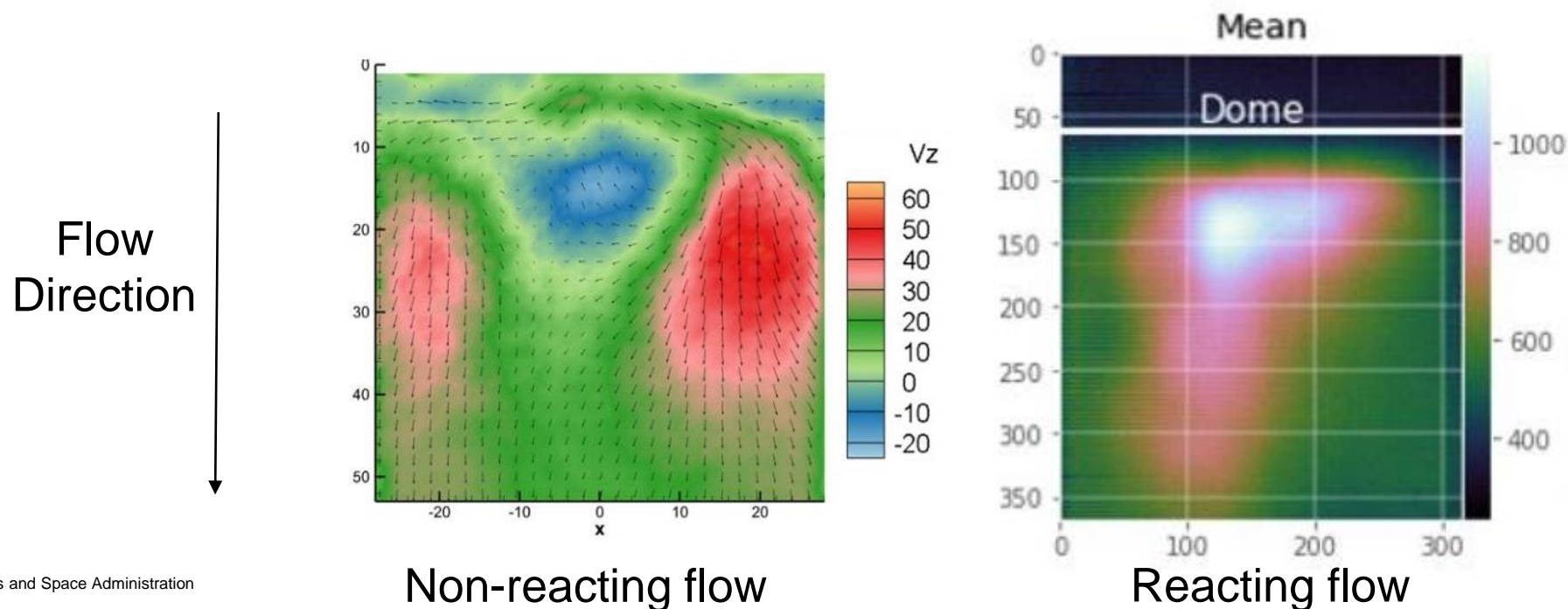
# Objective of this work was to provide a comparison of flame structure from two different configurations of the 7-point LDI hardware

1. Co-swirling configuration  
Center pilot swirler: RH  $60^\circ$   
Outer swirler: RH  $52^\circ$
2. Counter-swirling configuration  
Center pilot swirler: LH  $60^\circ$   
Outer swirlers: RH  $52^\circ$



# Recent studies reported for 7-point LDI for both non-reacting and reacting conditions

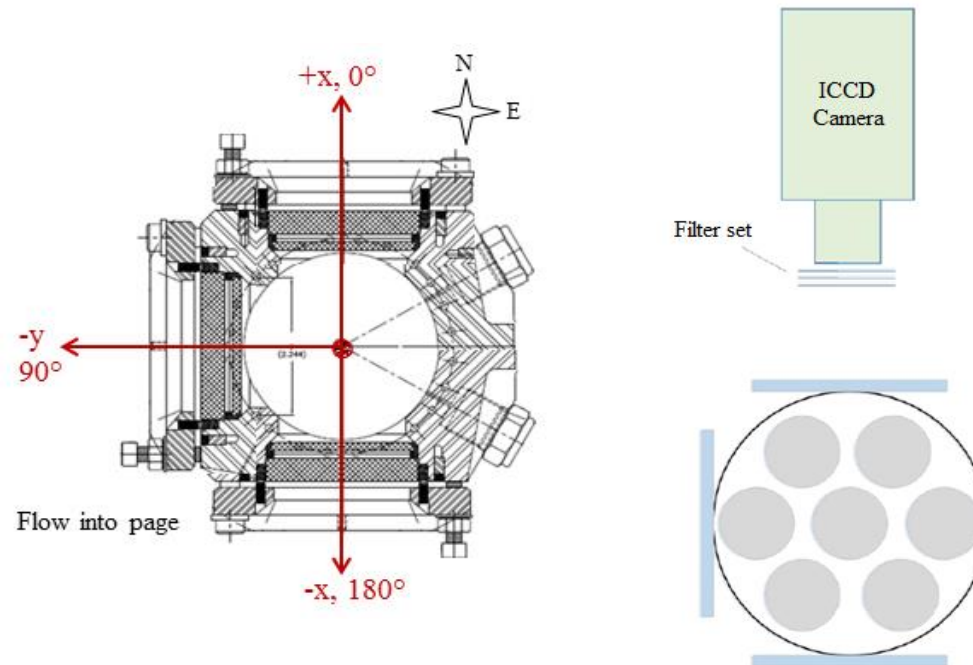
- Parametric studies to observed effect of swirler angle, clocking, and center offset
- Non-reacting cases studied formation of recirculation zones
- Combustion tests examined flame structure and combustion dynamics



# Optical measurements for combustion were acquired through chemiluminescence

Combustion tests captured chemiluminescence through intensified CCD (ICCD) camera, PI-Max 3, at 25 Hz frame rate

Chemiluminescence species of  $C_2^*$  and  $CH^*$  spectrally isolated using narrow bandwidth filters





Several inlet test conditions were used to observe the effect of varying equivalence ratio and reference velocity

$P_3$ psia	$T_3$ °F	$u_{ref}$ m/s	$\Phi$	$\Phi_c$	$\Phi_o$
75	800	10.7	0.450	0.450	0.450
75	800	10.7	0.480	0.480	0.480
75	800	10.7	0.500	0.500	0.500
75	800	12.2	0.450	0.450	0.450

# Optical measurements for non-reacting flows were acquired through water-seeded PIV

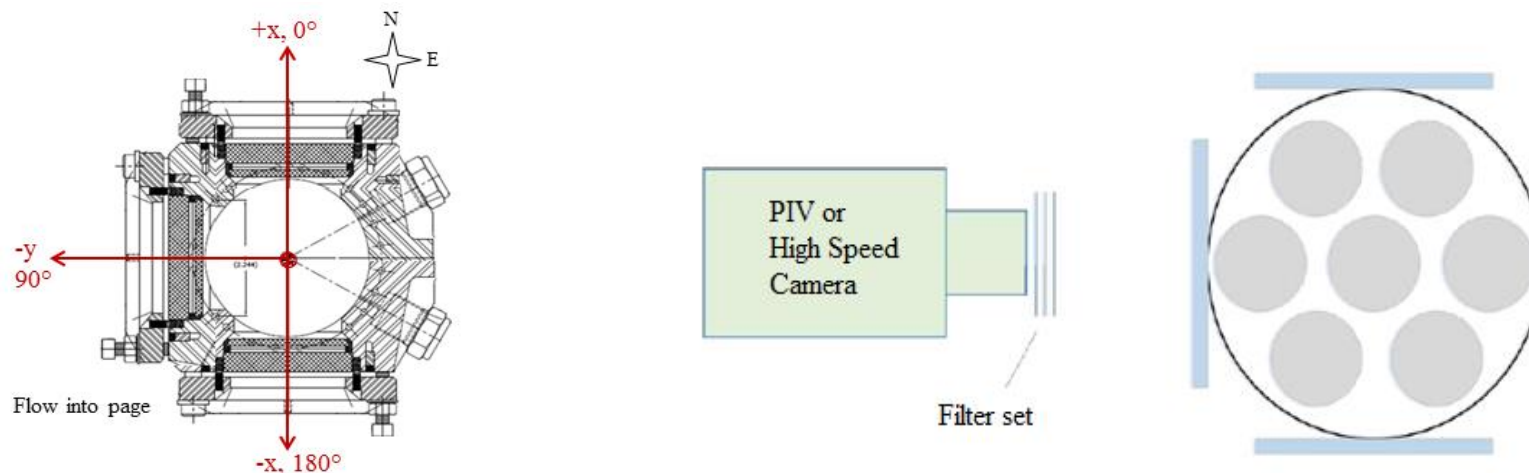
Cold flow testing was done by spraying water into the center nozzle

15 Hz, dual head, Nd:YAG laser was used to scatter light off water droplets

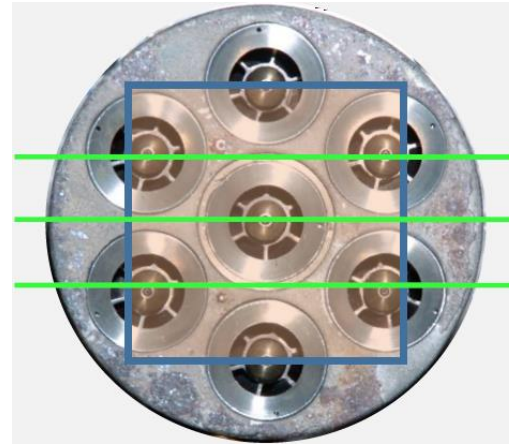
500 image pairs captured by interline transfer, CCD camera

Traverse laser sheet along y-coordinate from -24 mm to 24 mm

Inlet air conditions: 75 psia, 800 F, 22.9 m/s



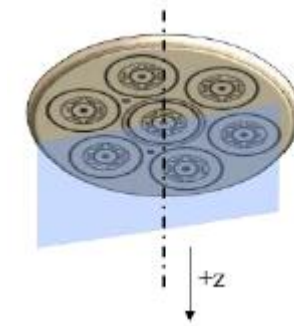
# Average x-z velocity field for non-reacting, co-swirl showed an elongated central recirculation zone (CRZ)



$Y = +12$

$Y = 0$

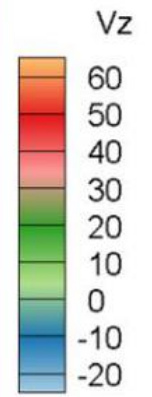
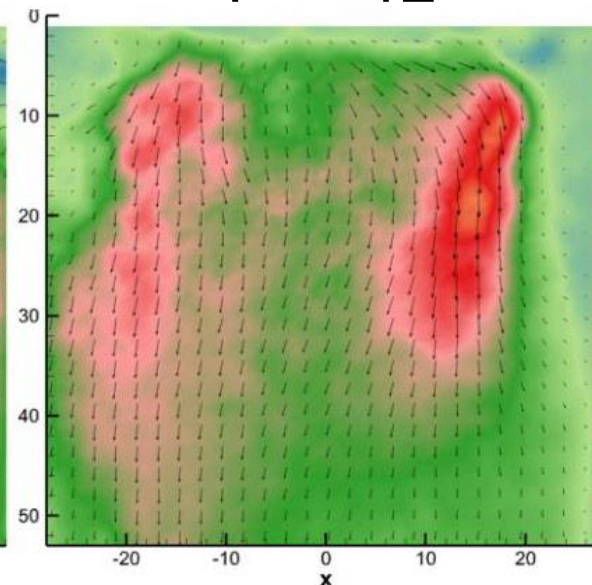
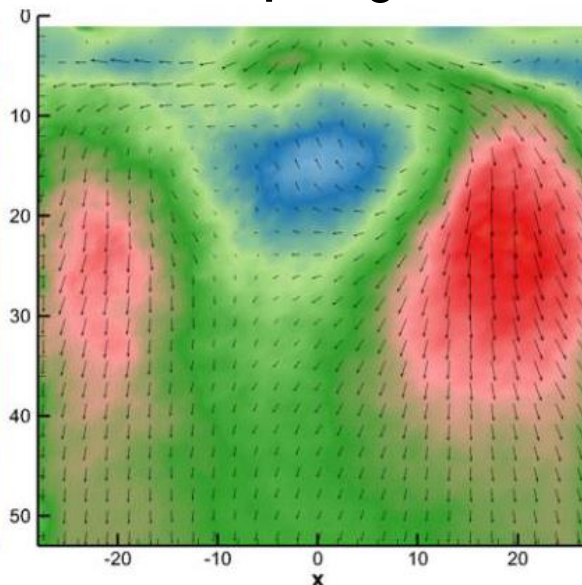
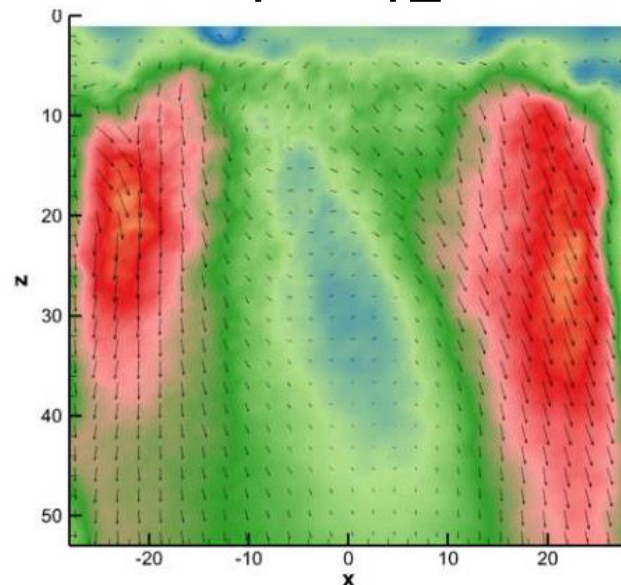
$Y = -12$



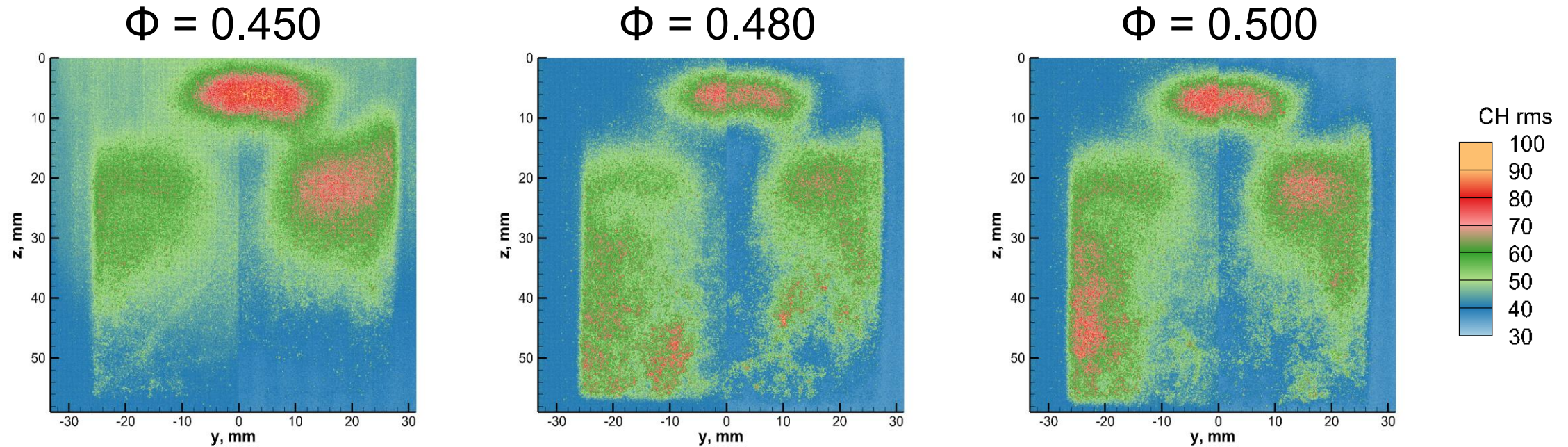
$Y = -12$

$Y = 0$

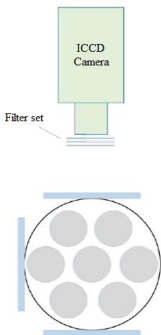
$Y = +12$



# Co-swirl $\text{CH}^*$ chemiluminescence showed flat shape near pilot and rough symmetry from outers

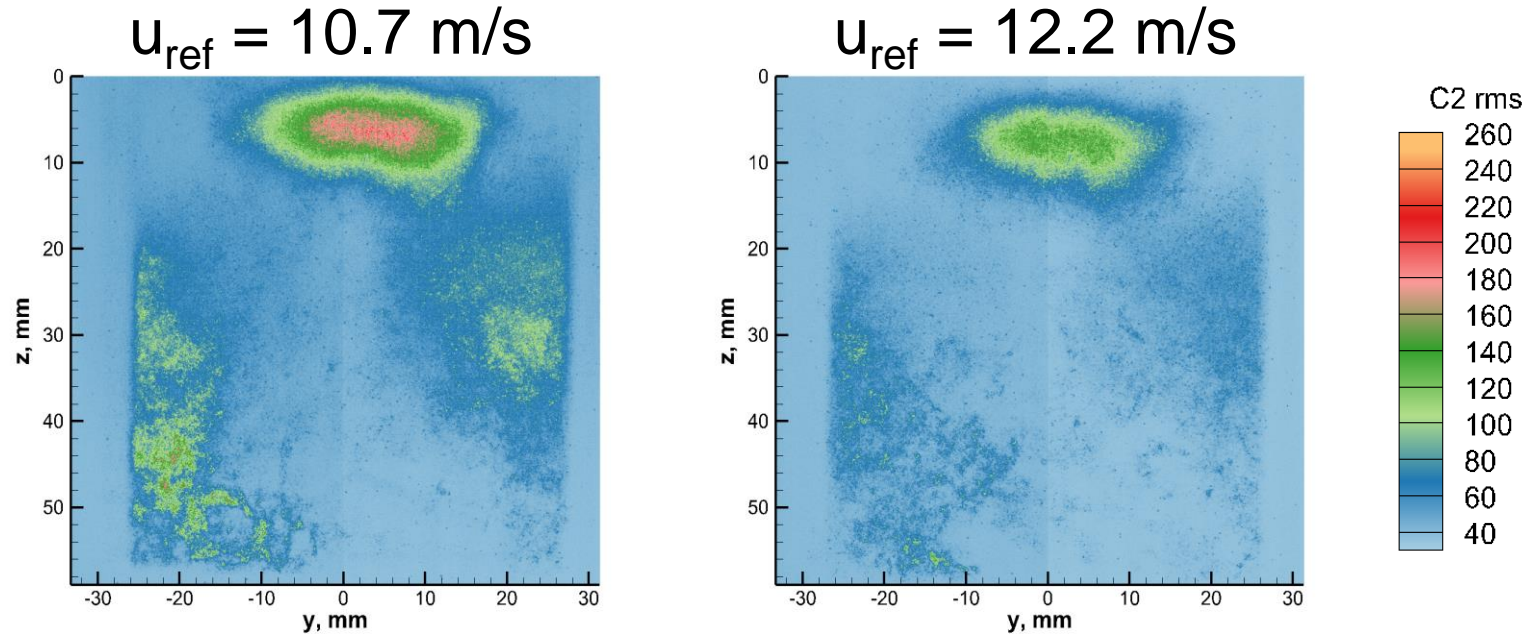


$\text{CH}^*$  tended to increase as equivalence ratio increased  
Hollow region of lower  $\text{CH}^*$  downstream of pilot similar shape to CRZ



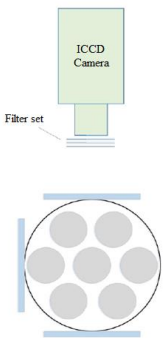
# Co-swirling $C_2^*$ chemiluminescence decreased as reference velocity increased

$\Phi = 0.450$

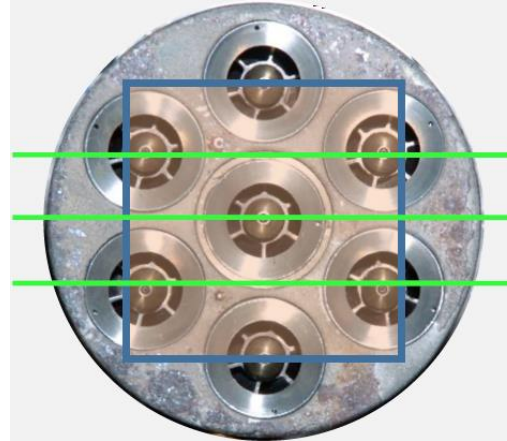


Increased reference velocity means:

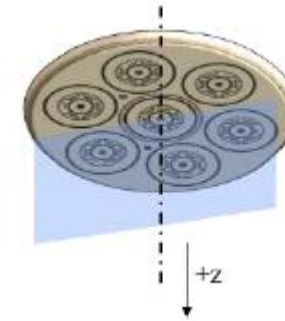
- Higher pressure drop across nozzle results in finer atomization
  - Smaller fuel drops vaporize better
  - Increased turbulence with higher velocity means enhanced mixing
- $\therefore$  Weaker chemiluminescence



# Average x-z velocity for non-reacting, counter-swirl hints at weak recirculation zone



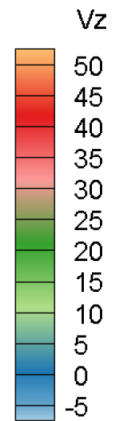
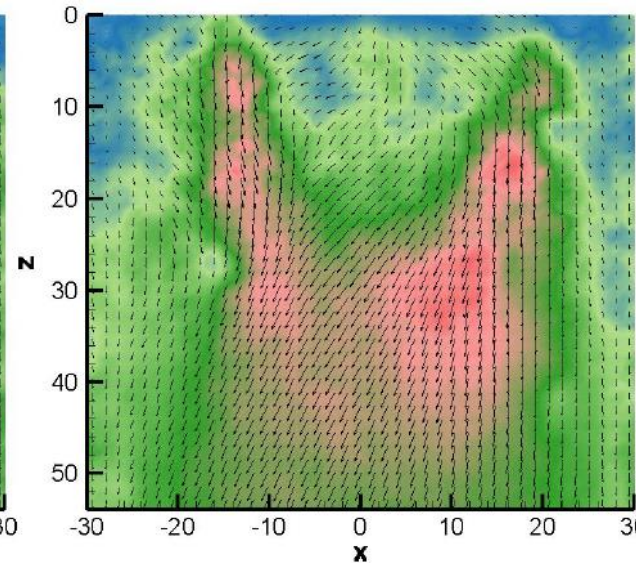
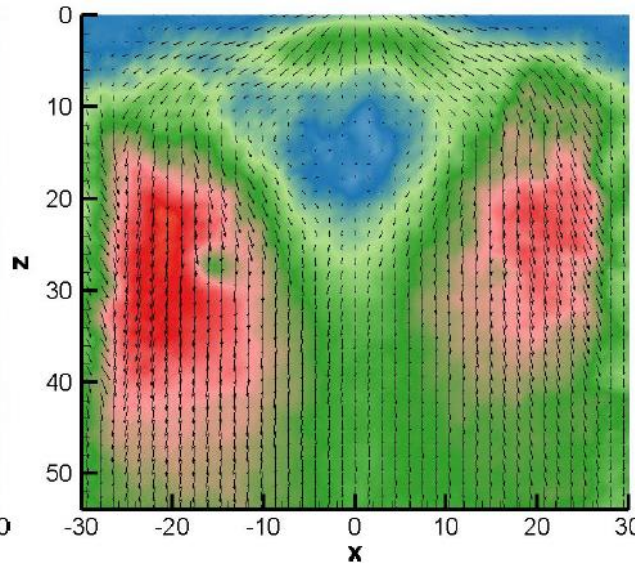
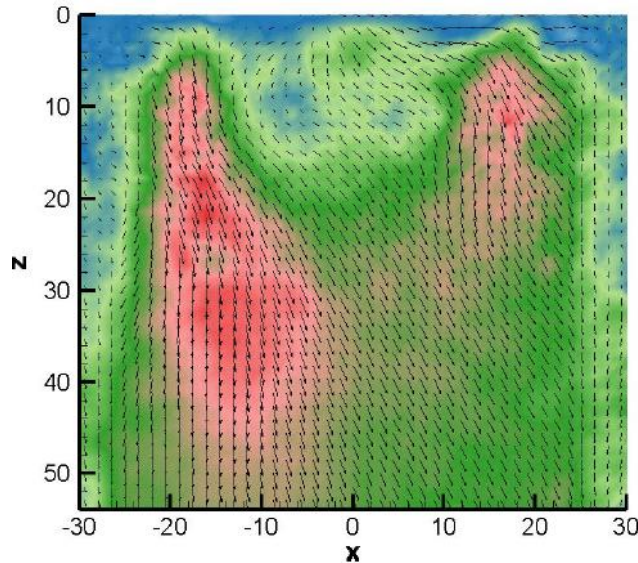
$Y = +12$   
 $Y = 0$   
 $Y = -12$



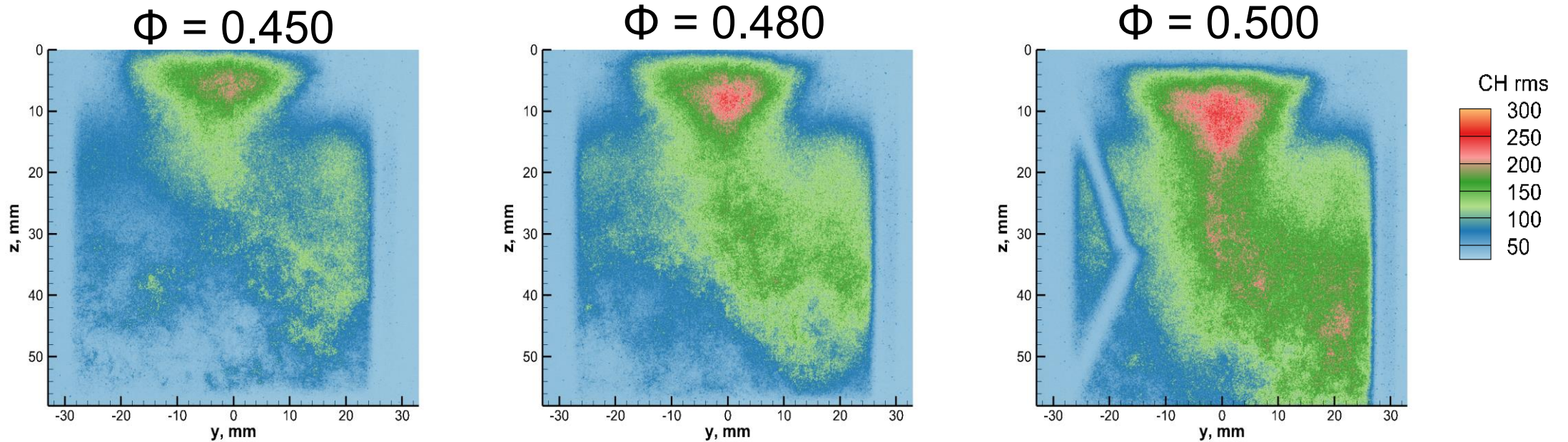
$Y = -12$

$Y = 0$

$Y = +12$



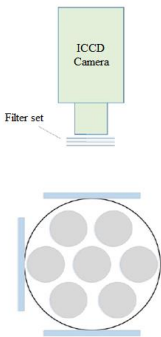
# Counter-swirl $\text{CH}^*$ chemiluminescence displayed a triangular shape from pilot and overall asymmetry



Triangular shaped pilot similar in shape to weak CRZ

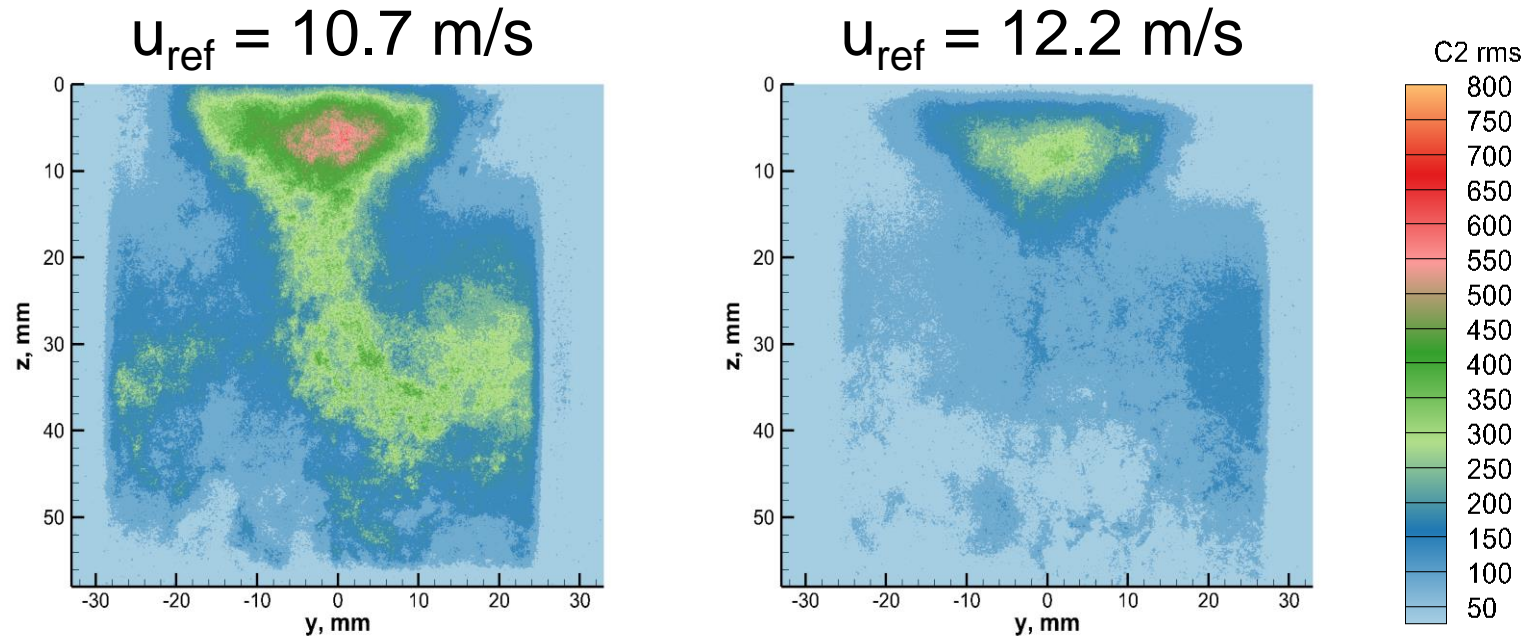
Asymmetry could be result of downstream swirl

Chemiluminescence approaching camera could “forward scatter”



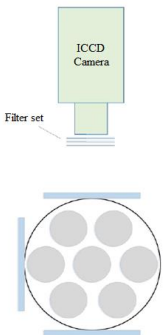
# Counter-swirl $C_2^*$ chemiluminescence also showed weaker chemiluminescence with increased velocity

$\Phi = 0.450$



Increased reference velocity means:

- Higher pressure drop across nozzle results in finer atomization
- Smaller fuel drops vaporize better
- Increased turbulence with higher velocity means enhanced mixing
- ∴ Weaker chemiluminescence





# Summary

A comparison of co-swirling and counter-swirling configurations was examined

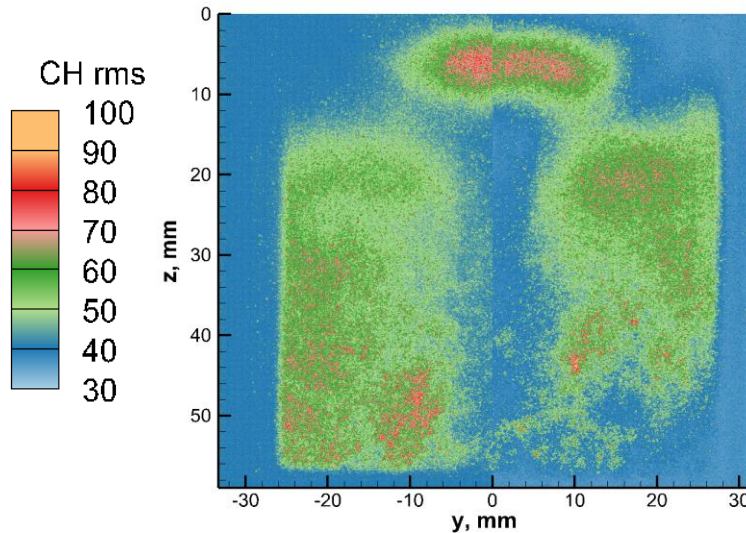
## Co-swirling configuration

- Flat, round pilot
- Symmetry observed with outers
- Weak region of CH\* seemed to coincide with CRZ

## Counter-swirling configuration

- Triangular, pilot
- Asymmetry showed most signal concentrated right-handed

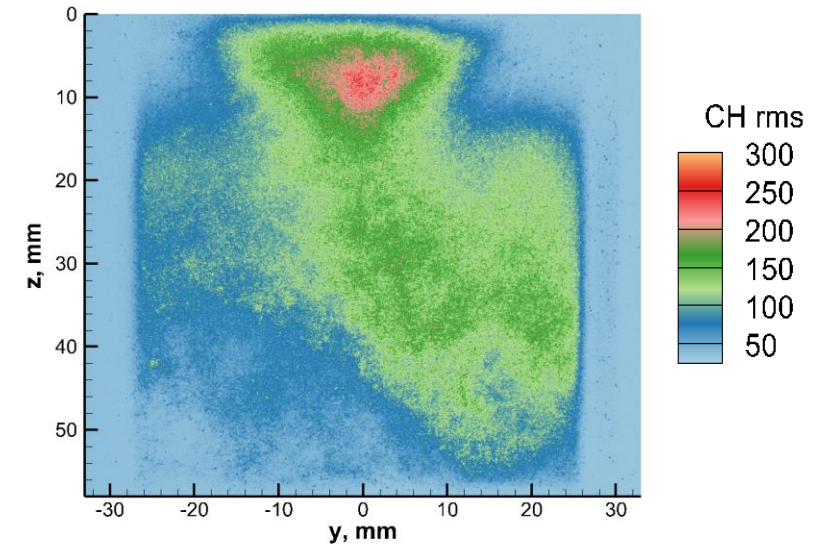
$\Phi = 0.480$



Both configurations showed:

- Increased chemiluminescence as equivalence ratio increased
- Decreased chemiluminescence as reference velocity increased

$\Phi = 0.480$



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