

Uncertainty in Inverted Pendulum Thrust Measurements

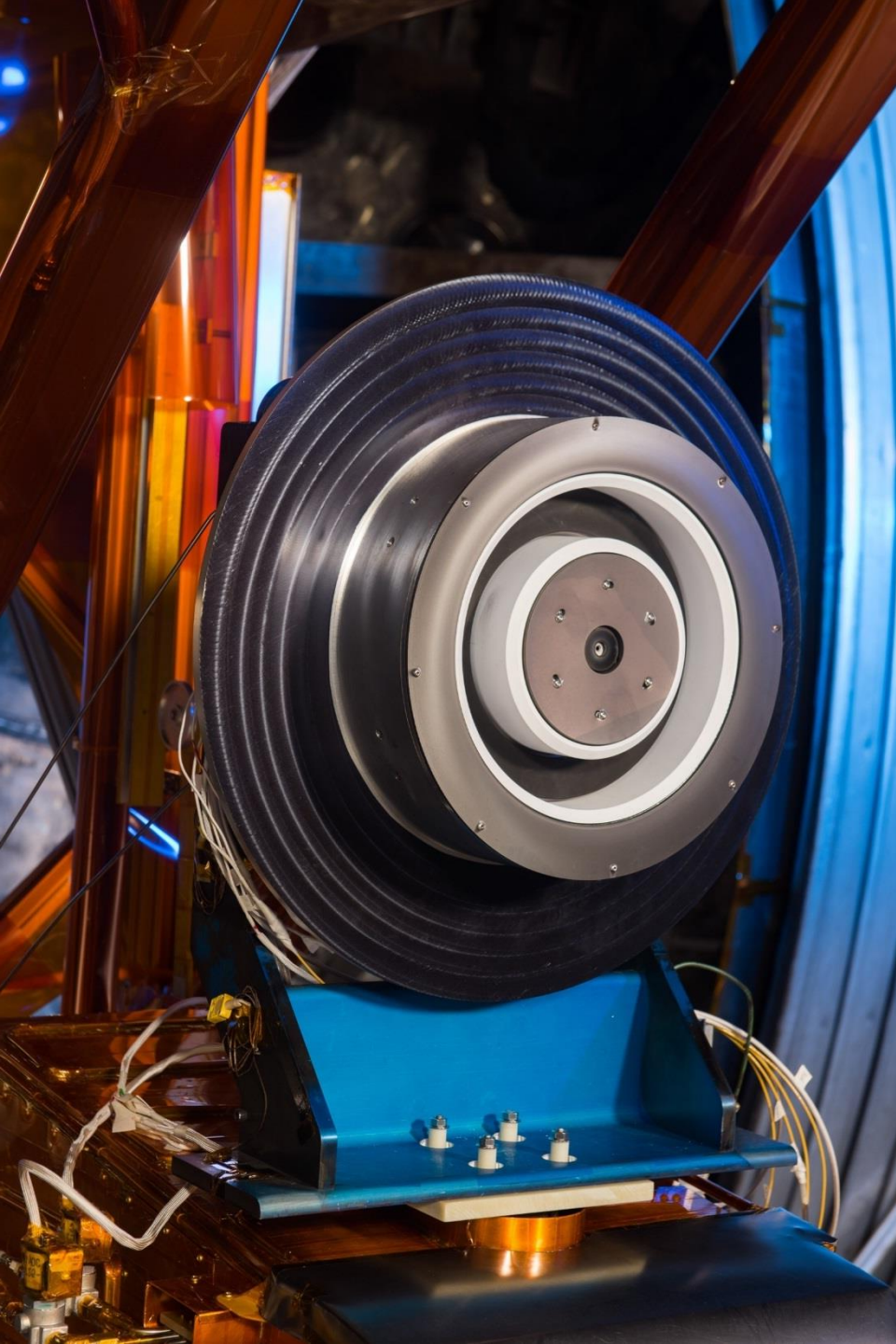
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S. Hall and P. Peterson

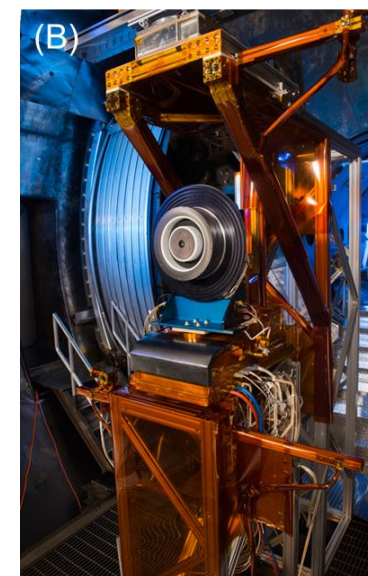
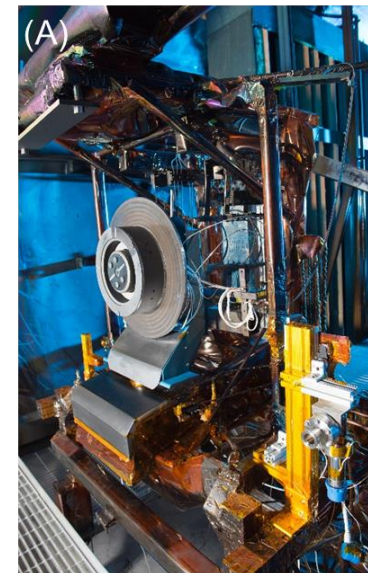
Vantage Partners LLC, Brook Park, Ohio 44142

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9 July 2018, Cincinnati, Ohio



Introduction

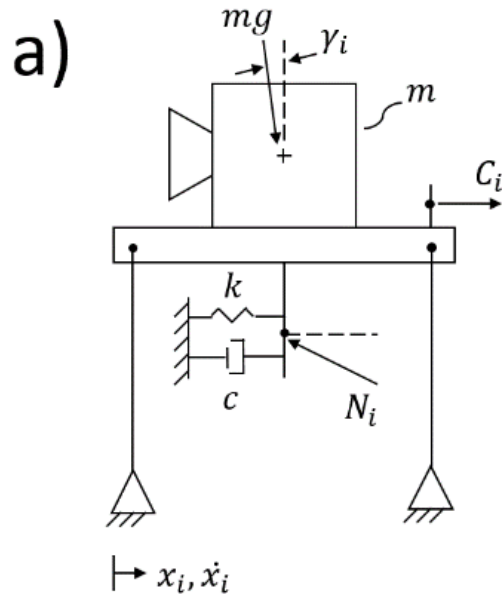
- Thrust measurement is critical to the characterization of electric propulsion (EP) systems.
 - Quantify: thrust, specific impulse, and efficiency.
 - Challenging because of low thrust to weight ratios of EP systems.
 - Sources of potential error must be well understood for reliable data.
 - Strong need for detailed uncertainty analysis.
- NASA GRC vacuum facility 5 (VF-5) and vacuum facility 6 (VF-6) have similar inverted pendulum thrust stands.
 - Several other NASA GRC thrust stands also exist with similar characteristics.



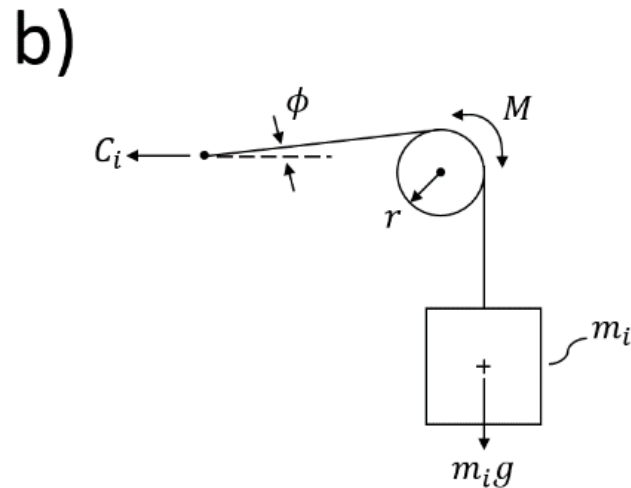
Model of an Inverted Pendulum Stand



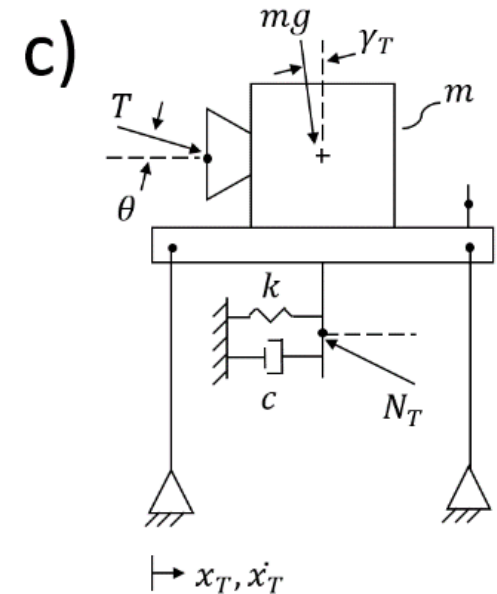
Calibration Mode



Calibration Details

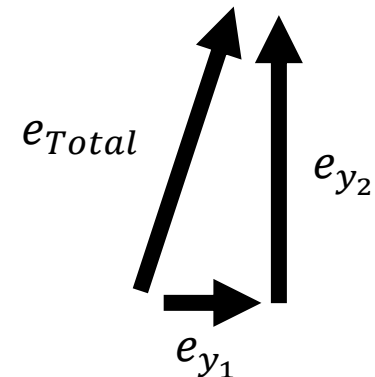
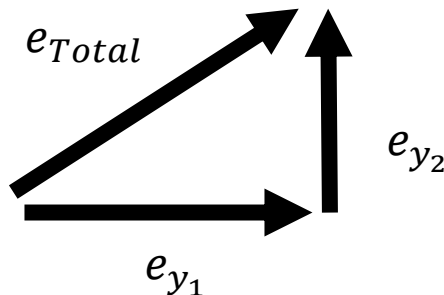
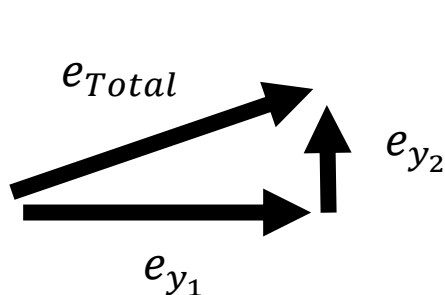
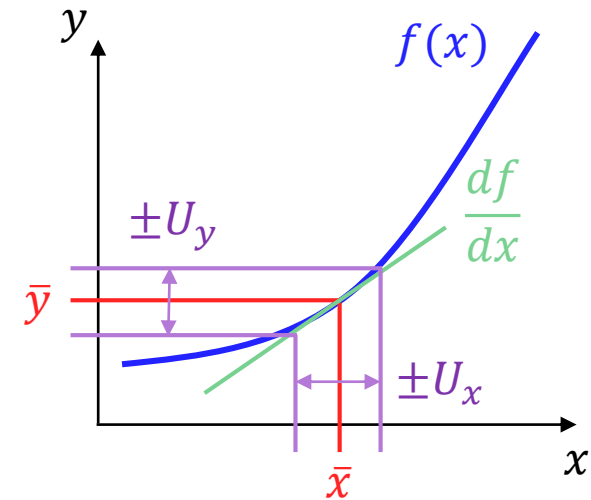


Thruster Mode



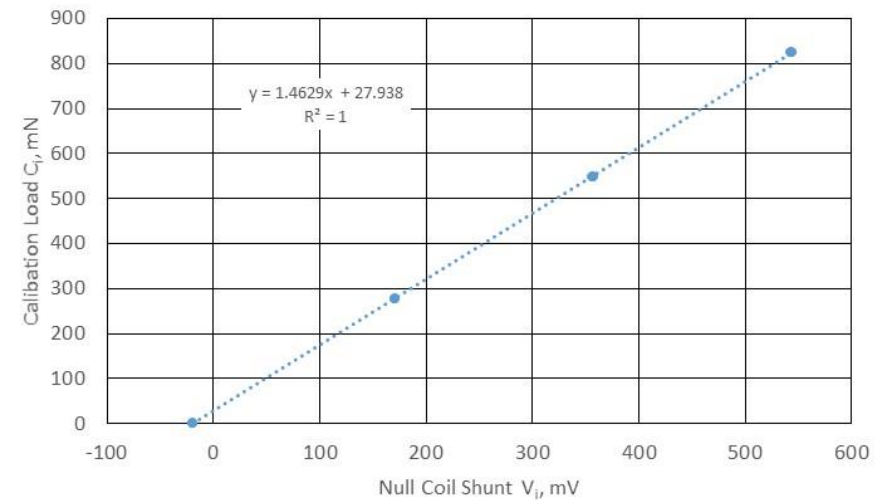
Methodology

- Classic approach of Figliola and Beasley, Abernethy et al., or Moffat.
 - Design-stage, single-measurement
- Propagate error of independent sources using a truncated Taylor Series expansion.
- Combine normalized error sources using a root sum of squares (RSS) type norm.



Methodology (cont.)

- Thrust stands can be operated in one of two modes:
 - Displacement mode
 - » Load vs. deflected position
 - Null coil mode
 - » Position held constant with a restoring force provided by a “null coil”
 - » Load vs. null coil current
- Example calibration dataset (right) can be reliably fit with a linear regression.
- Thrust can be estimated from calibration regression parameters and null coil shunt voltage.
- Objective of this work is to quantify the possible difference between a “measured” thrust and the “actual” thrust to some confidence level.



$$T = a + b V_T \pm U_T$$

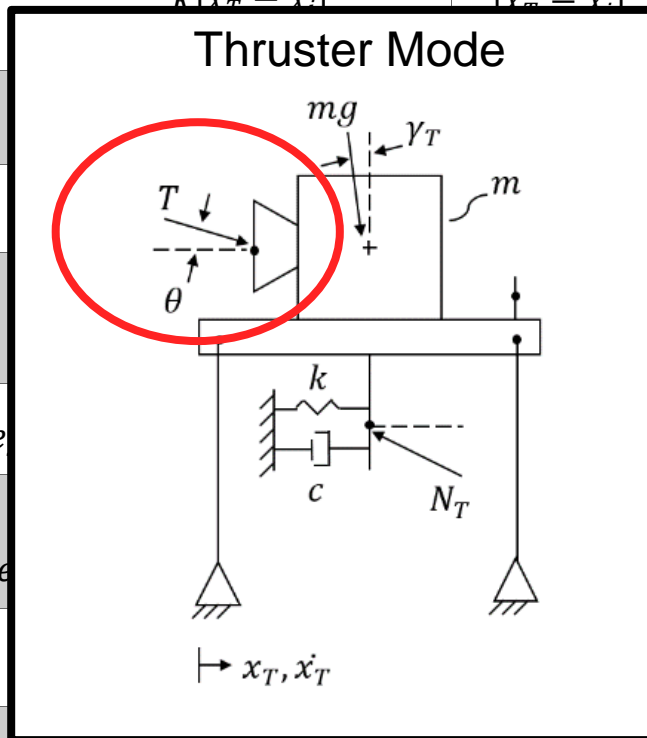
U_T 95% Confidence

Sources of Uncertainty

| Source | Relative Uncertainty | Parameters of Interest | Parameter Description |
|---|---|--|--|
| Thrust vector | $e_{\theta} = 1 - \cos(\theta)$ | θ | Thrust vector angle |
| Stand displacement drift | $e_x = \frac{k x_T - \tilde{x}_i }{\bar{T}}$ | $ x_T - \tilde{x}_i $, $k = \omega_n^2 m$ | Stand position drift, Stiffness |
| Stand velocity drift | $e_{\dot{x}} = \frac{c \dot{x}_T - \tilde{\dot{x}}_i }{\bar{T}}$ | $ \dot{x}_T - \tilde{\dot{x}}_i $, c | Stand velocity drift, Damping coefficient |
| Stand inclination drift | $e_{\gamma} = \frac{mg \sin \gamma_T - \tilde{\gamma}_i }{\bar{T}}$ | $ \gamma_T - \tilde{\gamma}_i $, mg | Stand inclination drift, Thruster weight |
| Shunt thermal drift | $e_{shunt} = \frac{\alpha t_T - \tilde{t}_i }{\bar{R}_{shunt}}$ | $ t_T - \tilde{t}_i $, α , \bar{R}_{shunt} | Temperature drift, Thermal sensitivity, Nominal resistance |
| Calibration slope repeatability | $e_{slope} = \frac{S_b \bar{V}_T}{\bar{T}} = S_b \left(\frac{1}{b} - \frac{a}{b\bar{T}} \right)$ | S_b | Calibration gain standard deviation |
| Calibration regression correlation | $e_{s_{xy}} = \frac{\sqrt{\frac{\sum (C_i - [a + bV_i])^2}{n - 2}}}{\bar{T}}$ | C_i , $a + bV_i$ | Calibration force, Calibration regression |
| DAQ uncertainty | $e_{V_i} = \frac{U_{V_i}}{\bar{V}_T} = U_{V_i} \frac{\bar{T} - a}{b}$ | U_{V_i} | Data acquisition uncertainty |
| Calibration uncertainty | $e_{C_i} = \frac{1}{\bar{T}} \frac{\partial T}{\partial C_i} U_{C_i}$ | U_{C_i} | Calibration uncertainty, see table 2 |

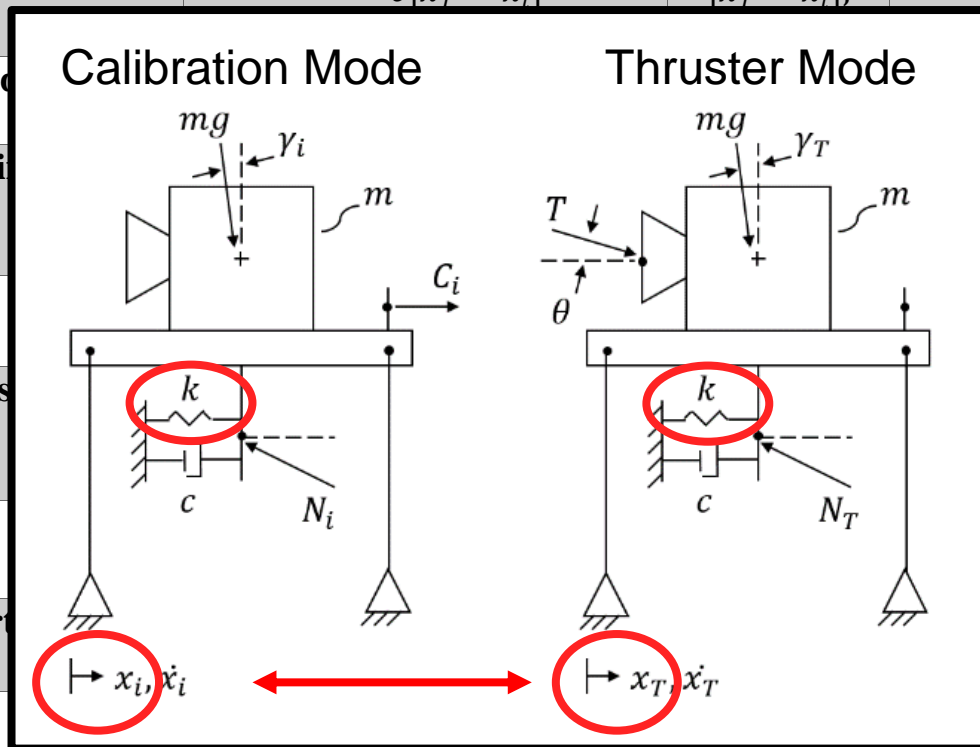
Sources of Uncertainty

| Source | Relative Uncertainty | Parameters of Interest | Parameter Description |
|------------------------------------|---|------------------------|--|
| Thrust vector | $e_\theta = 1 - \cos(\theta)$ | θ | Thrust vector angle |
| Stand displacement drift | $k x_m - x_c $ | $ x_m - x_c $ | Stand position drift, Stiffness |
| Stand velocity drift | | | Stand velocity drift, Damping coefficient |
| Stand inclination drift | | | Stand inclination drift, Thruster weight |
| Shunt thermal drift | | | Temperature drift, Thermal sensitivity, Nominal resistance |
| Calibration slope repeatability | e | | Calibration gain standard deviation |
| Calibration regression correlation | e | | Calibration force, Calibration regression |
| DAQ uncertainty | | | Data acquisition uncertainty |
| Calibration uncertainty | $e_{c_i} = \overline{\overline{T}} \frac{\partial C_i}{\partial C_i} U_{C_i}$ | e_i | Calibration uncertainty, see table 2 |



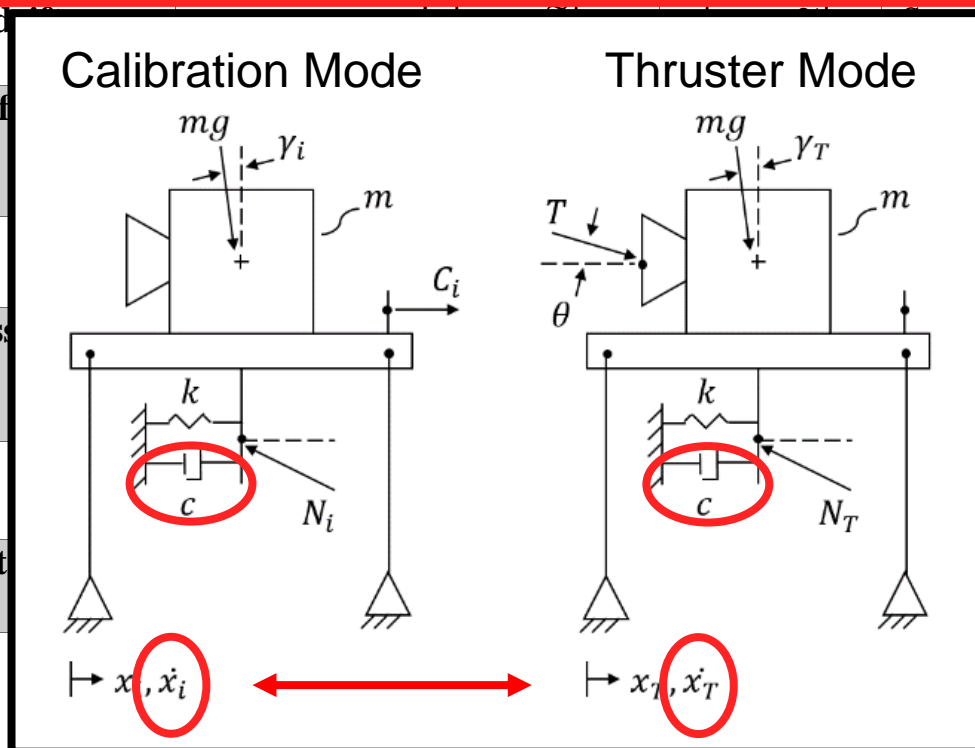
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| Stand velocity drift | $c \dot{x}_T - \tilde{\dot{x}}_i $ | $ \dot{x}_T - \tilde{\dot{x}}_i $ | Stand velocity drift, Damping coefficient |
| Stand inclination drift | | | Stand inclination drift, Center weight |
| Shunt thermal drift | | | Temperature drift, Thermal sensitivity, Thermal resistance |
| Calibration slope repeatability | | | Calibration gain Standard deviation |
| Calibration regression correlation | | | Calibration force, Calibration regression |
| DAQ uncertainty | | | Data acquisition Uncertainty |
| Calibration uncertainty | | | Calibration uncertainty, Table 2 |



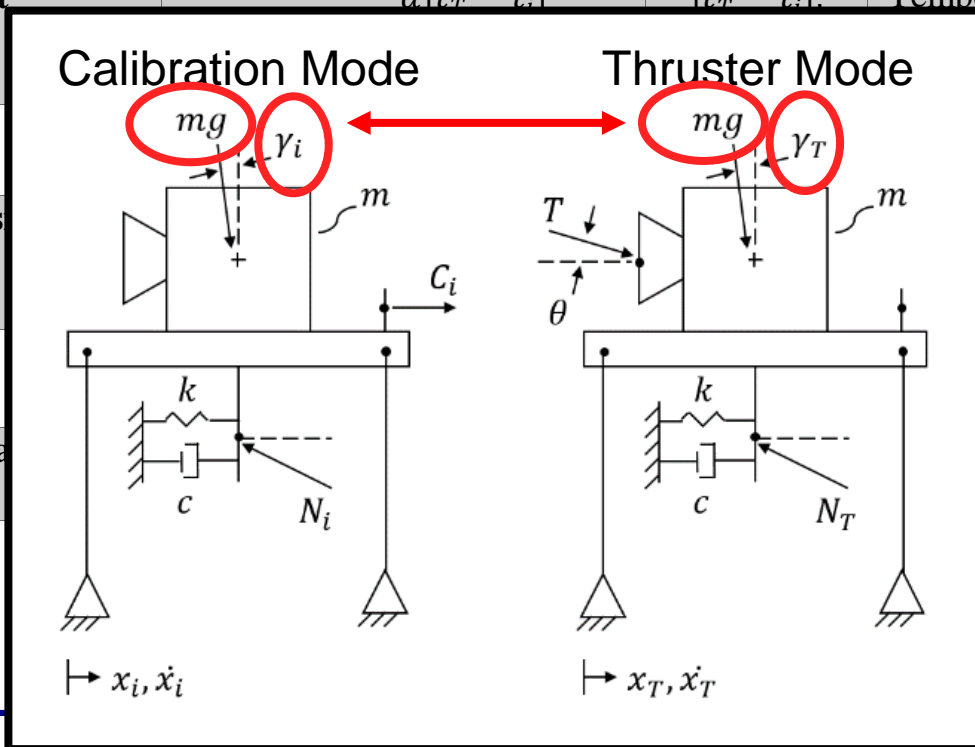
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Sources of Uncertainty

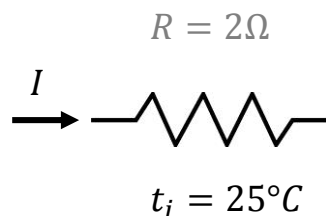
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| Stand inclination drift | $e_\gamma = \frac{mg \sin \gamma_T - \tilde{\gamma}_i }{\bar{T}}$ | $ \gamma_T - \tilde{\gamma}_i $, mg | Stand inclination drift, Thrust weight |
| Shunt thermal drift | $\alpha t_T - t_i $ | $ t_T - t_i $ | Temperature drift, Thermal sensitivity, Thermal resistance |
| Calibration slope repeatability | | | Calibration gain Standard deviation |
| Calibration regression correlation | | | Calibration force, Calibration regression |
| DAQ uncertainty | | | Acquisition uncertainty |
| Calibration uncertainty | | | Calibration uncertainty, Equation 2 |



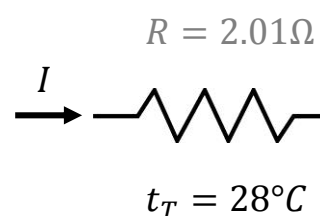
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| Stand inclination drift | $e_\gamma = \frac{mg \sin \gamma_T - \tilde{\gamma}_i }{\bar{T}}$ | $ \gamma_T - \tilde{\gamma}_i $, ma | Stand inclination drift, Thrust weight |
| Shunt thermal drift | $e_{shunt} = \frac{\alpha t_T - \tilde{t}_i }{\bar{R}_{shunt}}$ | $ t_T - \tilde{t}_i $, α , \bar{R}_{shunt} | Temperature drift, Thermal sensitivity, Nominal resistance |
| Calibration slope repeatability | $S_b V_T$ | $(1 - a)$ | S_b |
| Calibration regression correlation | | | Standard deviation Calibration force, Calibration regression |
| DAQ uncertainty | | | Acquisition uncertainty |
| Calibration uncertainty | | | Calibration uncertainty, Example 2 |

Calibration Mode

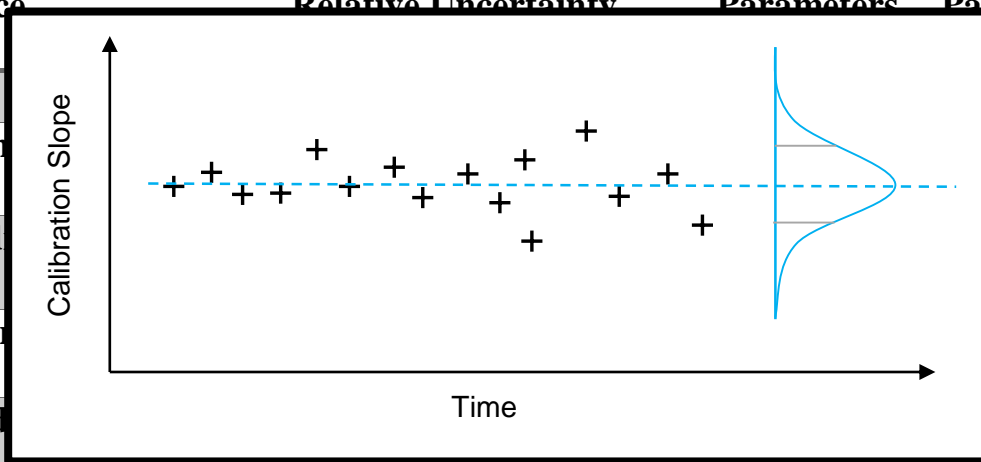


Thruster Mode

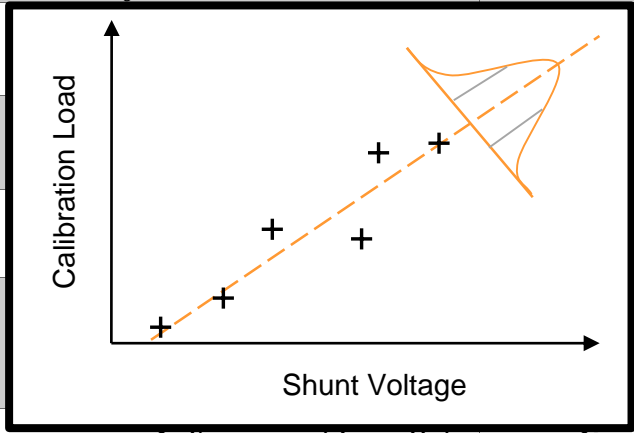


Sources of Uncertainty

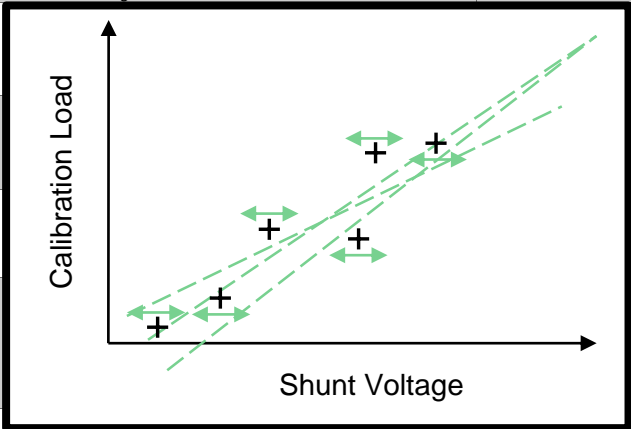
| Source | Relative Uncertainty | Parameters | Parameter Description |
|------------------------------------|---|-----------------|--|
| Thrust vector | | | Thrust vector angle |
| Stand displacement | | | Stand position drift, stiffness |
| Stand velocity drift | | | Stand velocity drift, damping coefficient |
| Stand inclination | | | Stand inclination drift, cluster weight |
| Shunt thermal drift | | | Temperature drift, thermal sensitivity, Nominal resistance |
| Calibration slope repeatability | $e_{slope} = \frac{S_b \bar{V}_T}{\bar{T}} = S_b \left(\frac{1}{b} - \frac{a}{b\bar{T}} \right)$ | S_b | Calibration gain standard deviation |
| Calibration regression correlation | $e_{s_{xy}} = \frac{\sqrt{\frac{\sum (C_i - [a + bV_i])^2}{n - 2}}}{\bar{T}}$ | $C_i, a + bV_i$ | Calibration force, Calibration regression |
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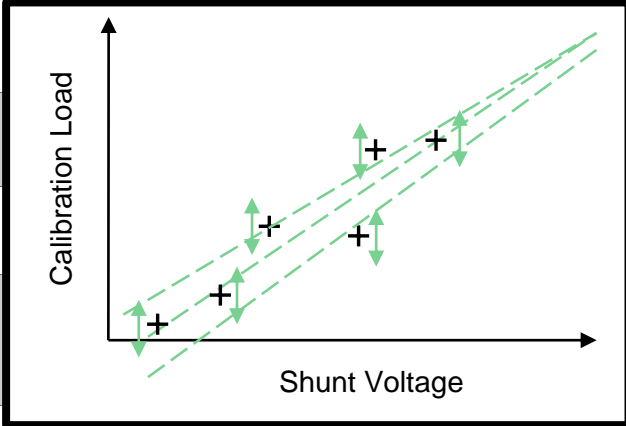
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| Stand displacement drift |  | C_i, m | Stand position drift, Stiffness |
| Stand velocity drift | | \dot{C}_i, \dot{m} | Stand velocity drift, Damping coefficient |
| Stand inclination drift | | $\theta, \dot{\theta}$ | Stand inclination drift, Thruster weight |
| Shunt thermal drift | | R, \dot{R} | Temperature drift, Thermal sensitivity, Nominal resistance |
| Calibration slope repeatability | | S_b | Calibration gain standard deviation |
| Calibration regression correlation | $e_{s_{xy}} = \frac{\sqrt{\frac{\sum (C_i - [a + bV_i])^2}{n - 2}}}{\bar{T}}$ | $C_i, a + bV_i$ | Calibration force, Calibration regression |
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| Stand velocity drift | | θ , m | Stand velocity drift, Damping coefficient |
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| Calibration slope repeatability | | S_b | Calibration gain standard deviation |
| Calibration regression correlation | $e_{slope} = \frac{S_b V_T}{\bar{T}} = S_b \left(\frac{1}{b} - \frac{a}{b\bar{T}} \right)$ $e_{s_{xy}} = \sqrt{\frac{\sum (C_i - [a + bV_i])^2}{n - 2}} \cdot \frac{1}{\bar{T}}$ | C_i , $a + bV_i$ | Calibration force, Calibration regression |
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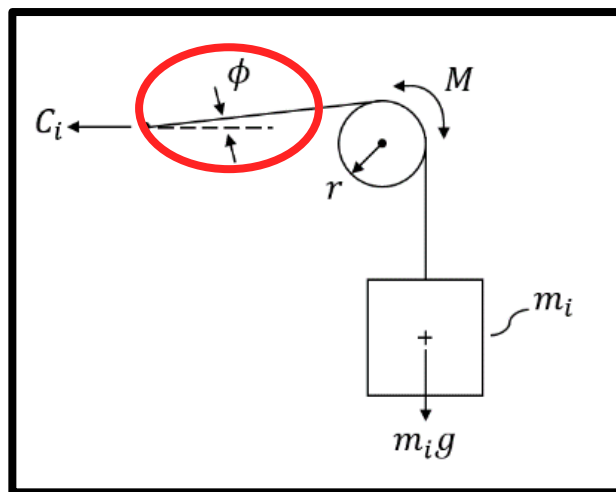
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Calibration Sources of Uncertainty

| Source | Relative Uncertainty | Parameters of Interest | Parameter Description |
|---------------------------------|--|------------------------|---------------------------------|
| Calibration alignment | $e_{\varphi} = 1 - \cos(\varphi)$ | φ | Calibration alignment angle |
| Calibration pulley moment | $e_M = \frac{M}{r\bar{C}_i}$ | M | Calibration pulley moment |
| Calibration mass uncertainty | $e_{m_i} = \frac{U_{m_i}g}{\bar{C}_i}$ | U_{m_i} | Calibration mass uncertainty |
| Calibration gravity uncertainty | $e_g = \frac{U_g}{g}$ | U_g | Calibration gravity uncertainty |

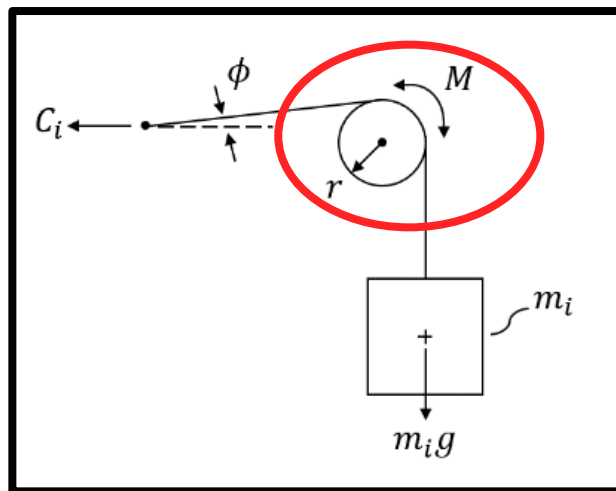
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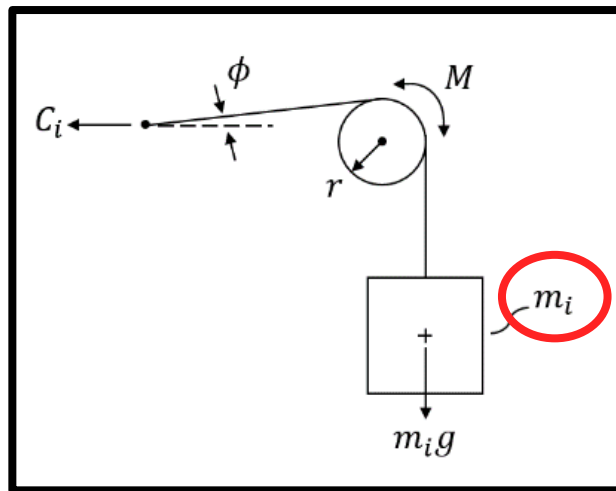
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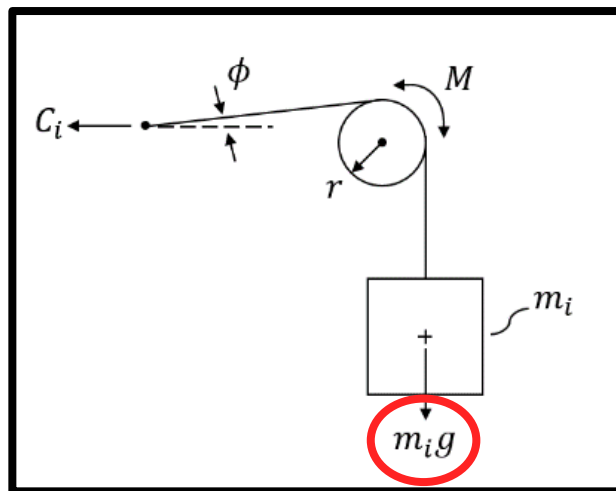
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Calibration Sources of Uncertainty

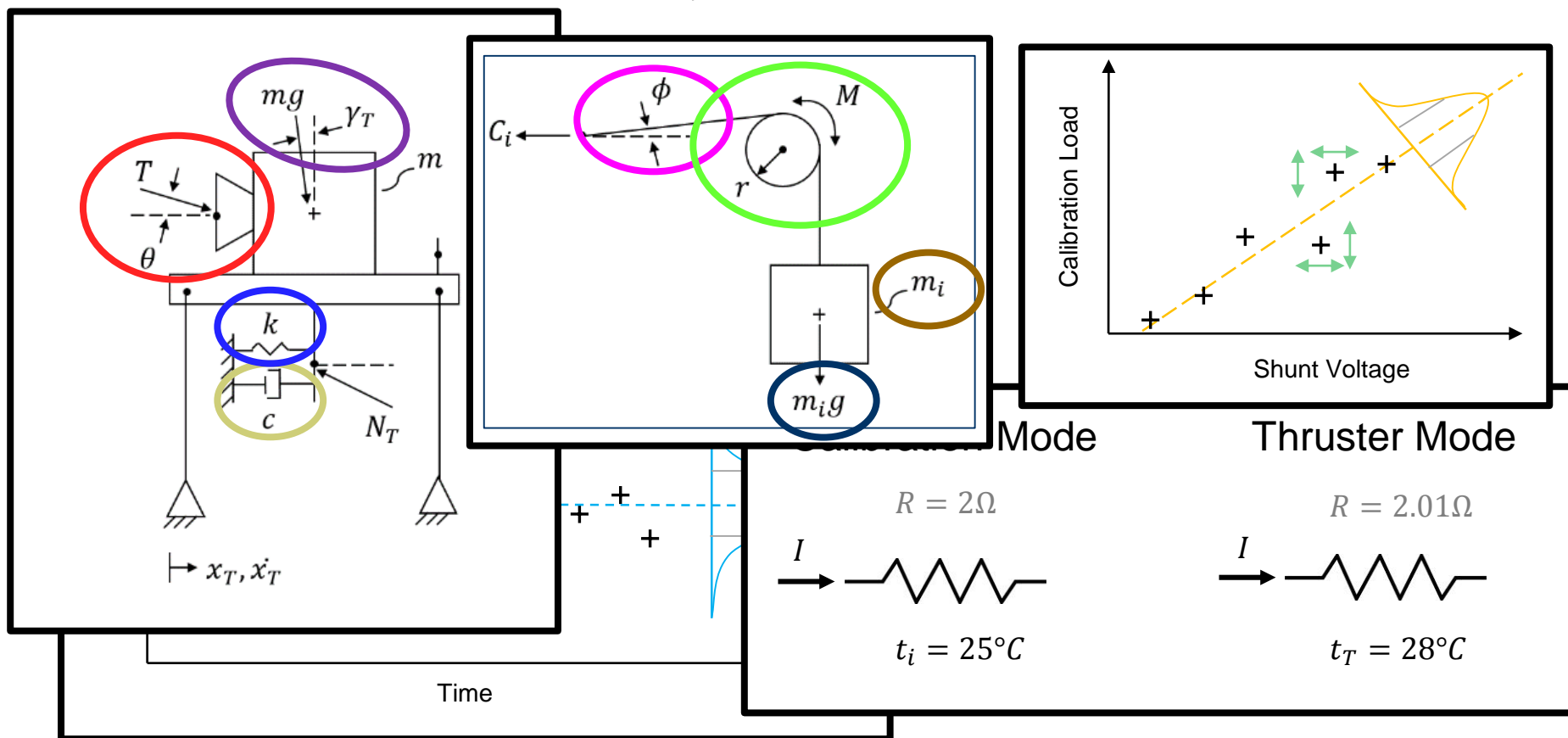
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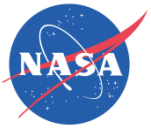
Combination of Sources

$$e_T = \frac{U_T}{\bar{T}} = \sqrt{e_{\theta}^2 + e_x^2 + e_{\dot{x}}^2 + e_{\gamma}^2 + e_{shunt}^2 + e_{slope}^2 + e_{S_{xy}}^2 + e_{V_i}^2 \sqrt{n} + e_{C_i}^2 \sqrt{n}}$$

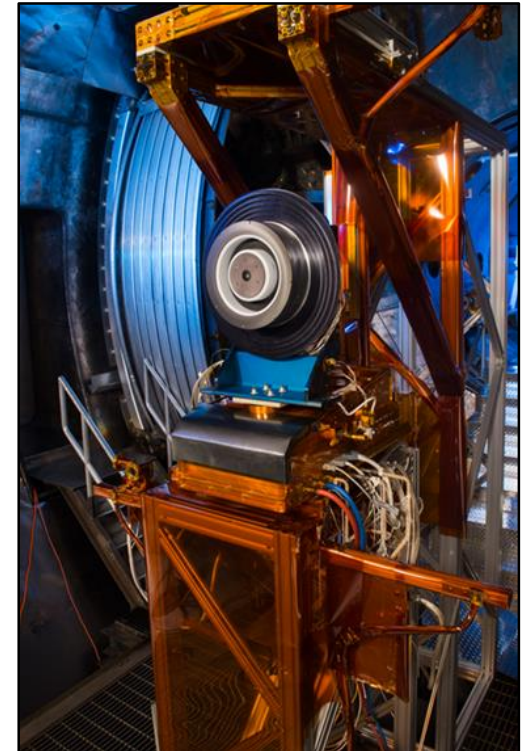
$$U_{C_i} = \bar{T} \sqrt{e_{\phi}^2 + e_M^2 + e_{m_i}^2 + e_g^2}$$



Case Study NASA VF-6 Thrust Stand



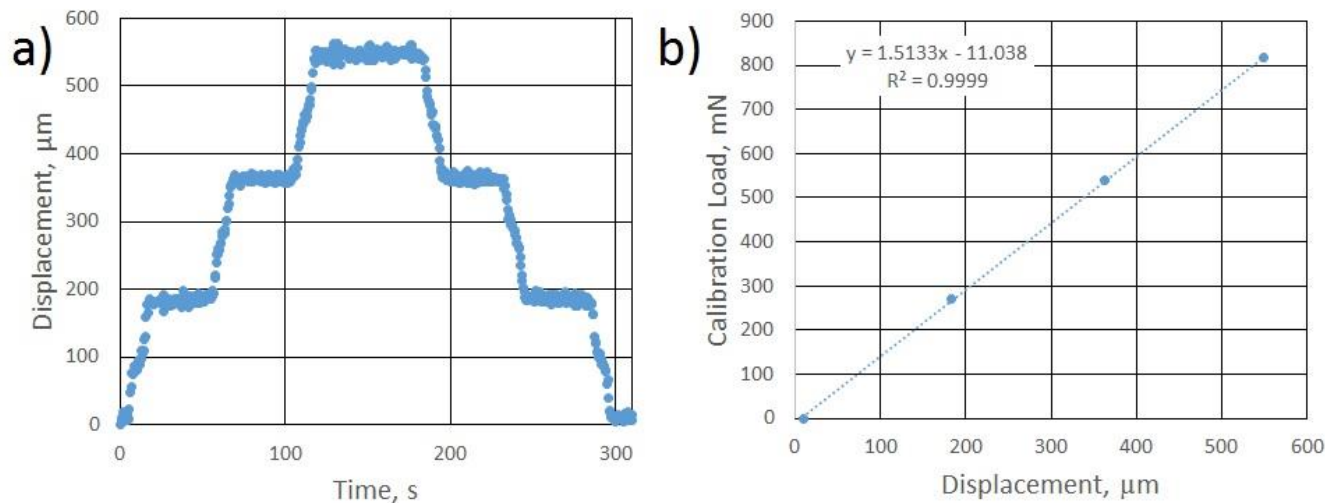
- VF-6 inverted pendulum thrust stand has been recently constructed with uncertainty quantification in mind.
 - Technology Development Unit (TDU) 12.5 kW Hall thruster for Advanced Electric Propulsion System (AEPS).
- Null and damper coils on PID feedback loops.
- Inclination control on PID feedback loop.
- Linear variable differential transformer (LVDT) position measurement for PID feedback.
- Laser triangulation sensor as secondary position measurement.
- Electrolytic inclinometer tilt sensor for PID feedback.
- Inertial inclinometer tilt sensor for secondary inclination measurement.
- In-situ calibration mechanism.
- Protective thermal/environmental shroud.



Stand Characterization

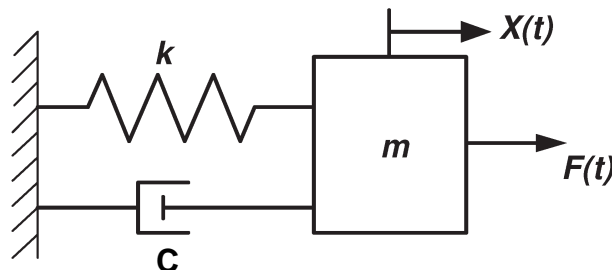
- Stand stiffness, damping coefficient, and total dynamic mass were calculated.
 - May change with different thrusters, different thrust stands, and different setup configurations.

Displacement Mode Operation

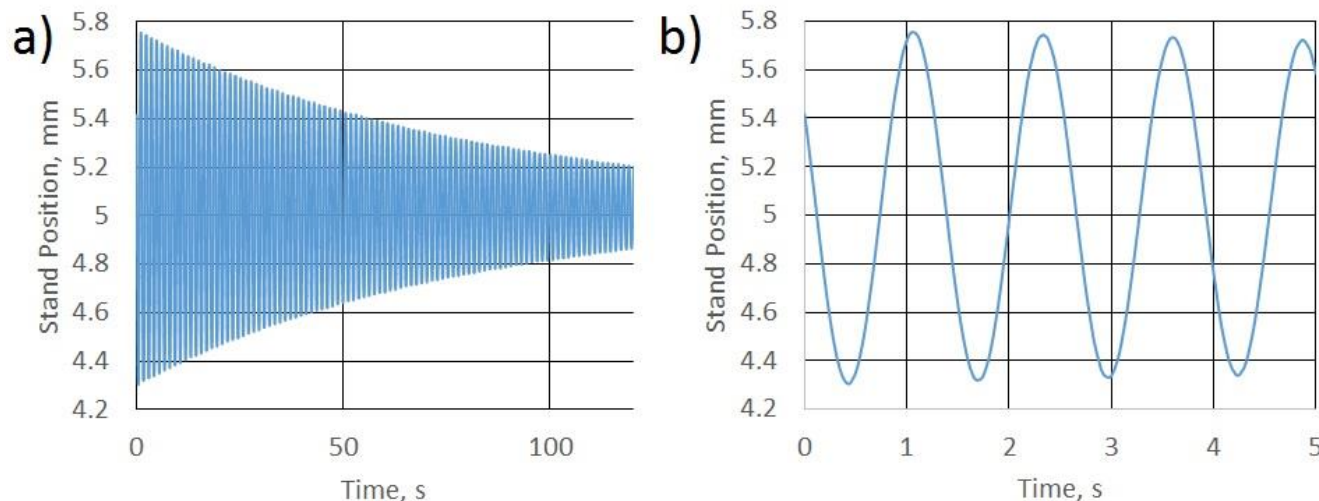


Stand Stiffness $k=1.5 \text{ mN}/\mu\text{m}$

Stand Characterization (cont.)



“Free” Response to Impulse, No Active Coils

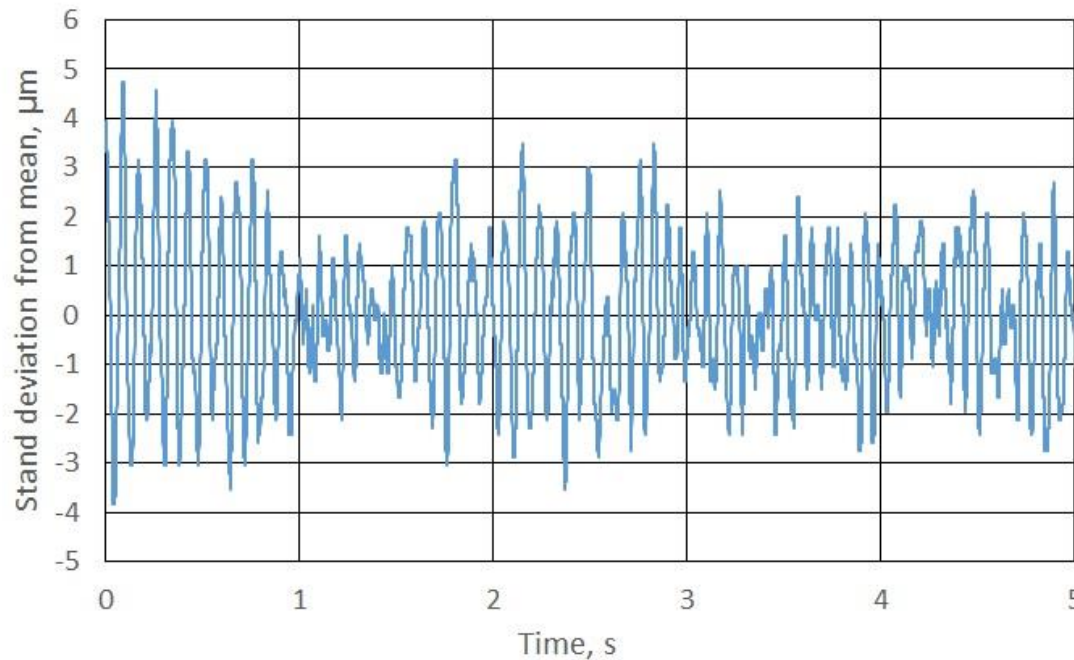


Stand Damping Coefficient $c=1.5$ kg/s ($\xi=2.5e-3$)

Stand Natural Frequency $\omega_n=0.788$ Hz

Stand Characterization (cont.)

Nominal Quiescent Operation



Stand Velocity $\dot{x}=0.3$ mm/s

Total Mass $m_{stand} + m_{thruster}=(14.9+46.7)$ kg

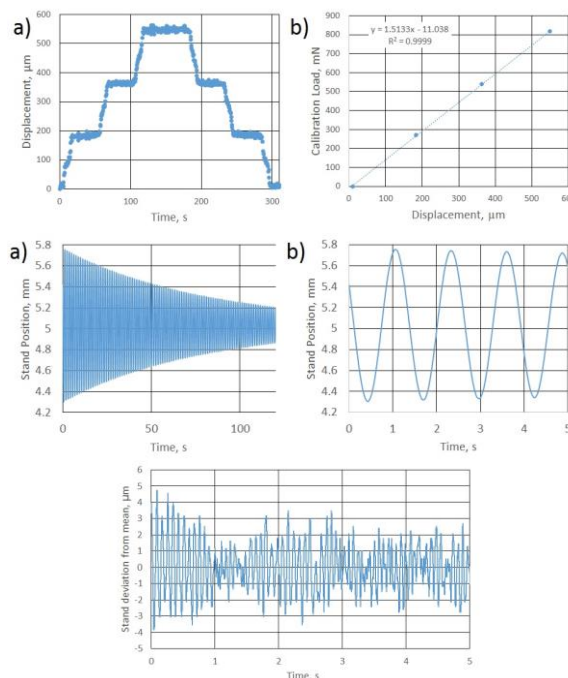
Summary of Assumed Values

| Parameter | Term | Assumed Value |
|--|-----------------------------------|-----------------------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{Stand} | 14.9 kg |
| Total Weight | mg | 604 N |
| Stand natural frequency | ω_n | 0.788 Hz |
| Stand damping coefficient | c | 1.5 kg/s |
| Stand position drift | $ x_T - \tilde{x}_i $ | 2.4 μm |
| Stand velocity drift | $ \dot{x}_T - \tilde{\dot{x}}_i $ | 0.3 mm/s |
| Stand inclination drift | $ \gamma_T - \tilde{\gamma}_i $ | 2.0 arc seconds |
| Shunt thermal sensitivity | α | 100 ppm/ $^{\circ}\text{C}$ |
| Shunt thermal drift | $ t_T - \tilde{t}_i $ | 10 $^{\circ}\text{C}$ |
| Thrust vector alignment angle | θ | 2.0 $^{\circ}$ |
| Calibration slope repeatability | S_b | 1.54 mN/V |
| DAQ uncertainty | U_{v_i} | 600 μV |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | φ | 2.0 $^{\circ}$ |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s 2 |

Summary of Assumed Values

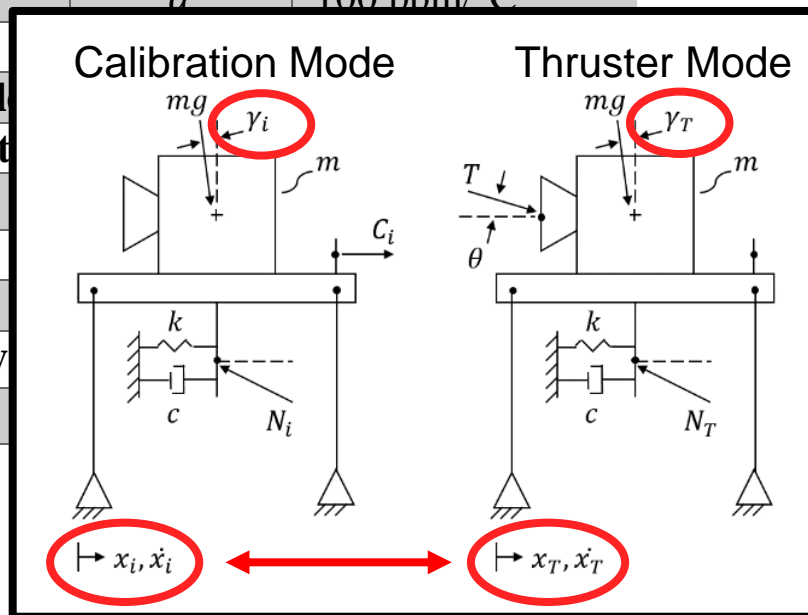
| Parameter | Term | Assumed Value |
|---------------------------|-------------------|-------------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{Stand} | 14.9 kg |
| Total Weight | mg | 604 N |
| Stand natural frequency | ω_n | 0.788 Hz |
| Stand damping coefficient | c | 1.5 kg/s |
| Stand position drift | $ x - \tilde{x} $ | 2.4 μm |

Characterization Results



Summary of Assumed Values

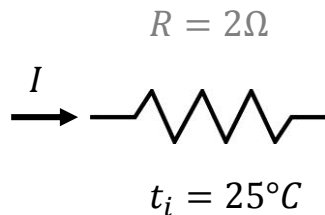
| Parameter | Term | Assumed Value |
|---------------------------------|-----------------------------------|-----------------------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{Stand} | 14.9 kg |
| Total Weight | mg | 604 N |
| Stand natural frequency | ω_n | 0.788 Hz |
| Stand damping coefficient | c | 1.5 kg/s |
| Stand position drift | $ x_T - \tilde{x}_i $ | 2.4 μm |
| Stand velocity drift | $ \dot{x}_T - \tilde{\dot{x}}_i $ | 0.3 mm/s |
| Stand inclination drift | $ \gamma_T - \tilde{\gamma}_i $ | 2.0 arc seconds |
| Shunt thermal sensitivity | α | 100 ppm/ $^{\circ}\text{C}$ |
| Shunt thermal drift | | |
| Thrust vector alignment angle | | |
| Calibration slope repeatability | | |
| DAQ uncertainty | | |
| Calibration pulley moment | | |
| Calibration alignment angle | | |
| Calibration mass uncertainty | | |
| Gravity uncertainty | | |



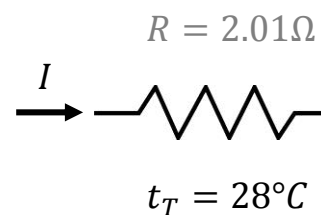
Summary of Assumed Values

| Parameter | Term | Assumed Value |
|---------------------------|-----------------------------------|-----------------------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{Stand} | 14.9 kg |
| Total Weight | mg | 604 N |
| Stand natural frequency | ω_n | 0.788 Hz |
| Stand damping coefficient | c | 1.5 kg/s |
| Stand position drift | $ x_T - \tilde{x}_i $ | 2.4 μm |
| Stand velocity drift | $ \dot{x}_T - \tilde{\dot{x}}_i $ | 0.3 mm/s |
| Stand inclination drift | $ \gamma_T - \tilde{\gamma}_i $ | 2.0 arc seconds |
| Shunt thermal sensitivity | α | 100 ppm/ $^{\circ}\text{C}$ |
| Shunt thermal drift | $ t_T - \tilde{t}_i $ | 10 $^{\circ}\text{C}$ |

Calibration Mode



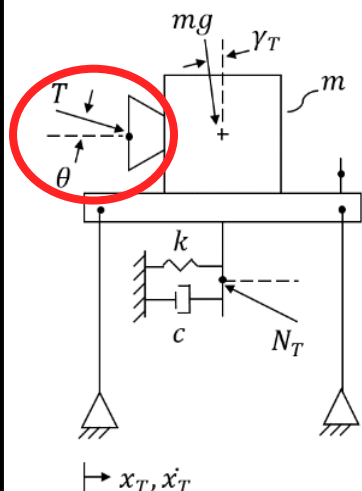
Thruster Mode



| Type | Power Rating Heatsink ¹ Free Air ² | Thermal Resistance | Resistance Range ³ Min Max | Tolerances | Temperature Coefficients |
|--------|---|---------------------------------|--|---|---|
| PF2205 | 50W 1W | 2.3 $^{\circ}\text{C}/\text{W}$ | 0.02 Ω 51K Ω | $\pm 1\%$ ($R \geq 0.1\Omega$) $\pm 5\%$ | $\pm 50\text{ppm}/^{\circ}\text{C}$ ($R \geq 10\Omega$) $\pm 100\text{ppm}/^{\circ}\text{C}$ ($0.1\Omega \leq R < 10\Omega$) $\pm 250\text{ppm}/^{\circ}\text{C}$ ($R < 0.1\Omega$) |
| PF2203 | 35W 1W | 3.3 $^{\circ}\text{C}/\text{W}$ | 0.01 Ω 51K Ω | 1% ($R \geq 0.1\Omega$) $\pm 5\%$ | $\pm 50\text{ppm}/^{\circ}\text{C}$ ($R \geq 10\Omega$) $\pm 100\text{ppm}/^{\circ}\text{C}$ ($0.1\Omega \leq R < 10\Omega$) $\pm 250\text{ppm}/^{\circ}\text{C}$ ($R < 0.1\Omega$) |
| PF2202 | 20W 1W | 5.9 $^{\circ}\text{C}/\text{W}$ | 0.02 Ω 51K Ω | 0.1%, 0.25%, 0.5%, ($R \geq 10\Omega$) $\pm 1\%$ ($R \geq 0.1\Omega$) $\pm 5\%$ | $\pm 50\text{ppm}/^{\circ}\text{C}$ ($R \geq 10\Omega$) $\pm 100\text{ppm}/^{\circ}\text{C}$ ($0.1\Omega \leq R < 10\Omega$) $\pm 250\text{ppm}/^{\circ}\text{C}$ ($R < 0.1\Omega$) |

Summary of Assumed Values

Thruster Mode



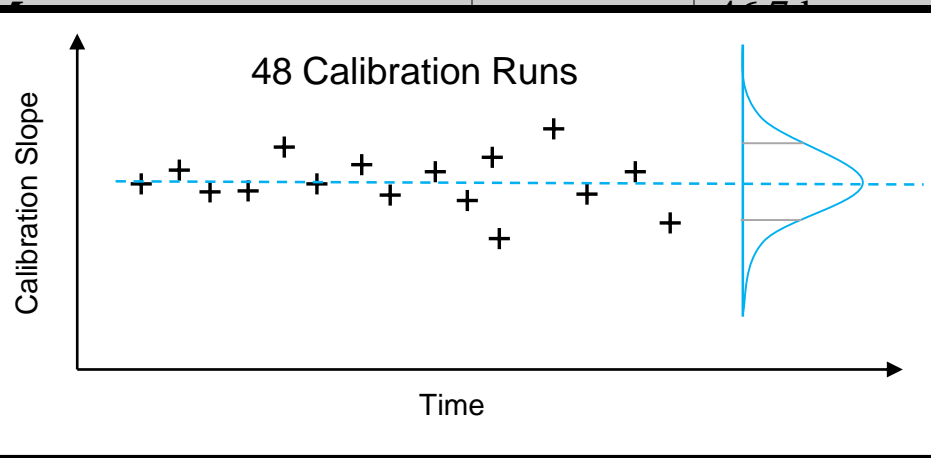
Diagnostic for Verifying the Thrust Vector Requirement of the AEPS Hall-Effect Thruster and Comparison to the NEXT-C Thrust Vector Diagnostic

Gabriel F. Benavides¹, Jonathan A. Mackey², Drew M. Ahern³, and Robert E. Thomas⁴
NASA Glenn Research Center, Cleveland, OH, USA 44135

| | | |
|---------------------------------|-----------------------|-----------------------|
| Shunt thermal drift | $ t_T - \tilde{t}_i $ | 10°C |
| Thrust vector alignment angle | θ | 2.0° |
| Calibration slope repeatability | S_b | 1.54 mN/V |
| DAQ uncertainty | U_{v_i} | 600 μ V |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | φ | 2.0° |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s ² |

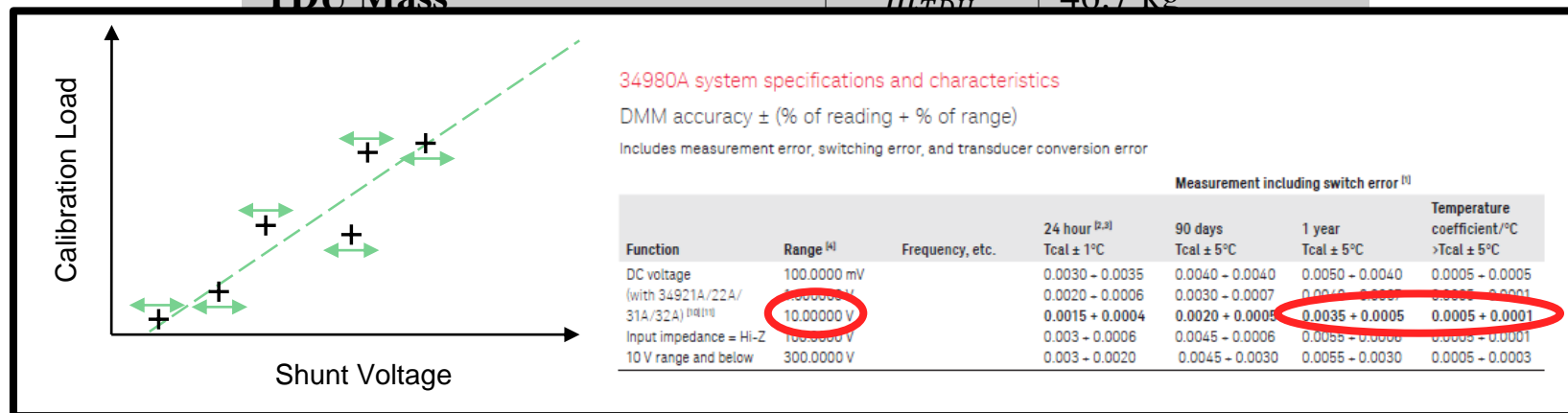
Summary of Assumed Values

| Parameter | Term | Assumed Value |
|---------------------------------|-----------------------|-----------------------|
| TDU | | |
| Stand | | |
| Total | | |
| Stand | | |
| Stand | | |
| Stand | | |
| Stand | | |
| Stand | | |
| Shunt | | |
| Shunt thermal drift | $ t_T - \tilde{t}_i $ | 10°C |
| Thrust vector alignment angle | θ | 2.0° |
| Calibration slope repeatability | S_b | 1.54 mN/V |
| DAQ uncertainty | U_{v_i} | 600 μ V |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | φ | 2.0° |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s ² |



Summary of Assumed Values

| Parameter | Term | Assumed Value |
|-----------------|-----------|---------------|
| TDU Mass | m_{TDU} | 46.7 kg |

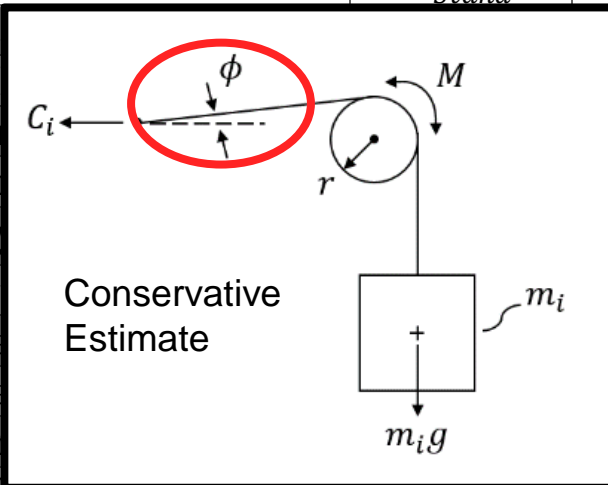


| | | |
|--|-----------------------|-----------------------|
| Shunt thermal drift | $ t_T - \tilde{t}_i $ | 10°C |
| Thrust vector alignment angle | θ | 2.0° |
| Calibration slope repeatability | S_b | 1.54 mN/V |
| DAQ uncertainty | U_{v_i} | 600 μ V |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | φ | 2.0° |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s ² |

Diagram illustrating a pulley system. A pulley of radius r is shown, with a mass m_i hanging from it. The pulley is rotating with angular velocity ω_o at time t_0 and ω_1 at time t_1 . The pulley is connected to a point C_i , which is at a distance r from the center of the pulley. The angle between the horizontal dashed line and the line connecting C_i to the center is ϕ . The pulley is highlighted with a red oval.

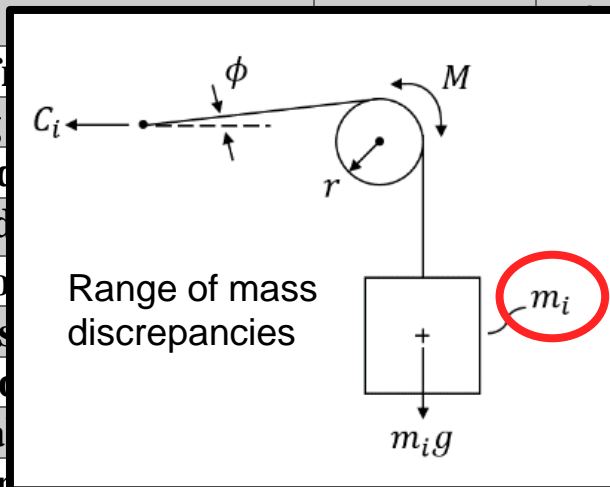
Summary of Assumed Values

| Parameter | Term | Assumed Value |
|---------------------------------|-------------|-----------------------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{Stand} | 14.9 kg |
| Total Weight | | 104 N |
| Stand natural frequency | | 788 Hz |
| Stand damping | | 5 kg/s |
| Stand position | | 4 μm |
| Stand velocity | | 3 mm/s |
| Stand inclination | | 10 arc seconds |
| Shunt thermal sensitivity | | 100 ppm/ $^{\circ}\text{C}$ |
| Shunt thermal offset | | 0 $^{\circ}\text{C}$ |
| Thrust vector | | 0 $^{\circ}$ |
| Calibration slope repeatability | S_b | 1.54 mN/V |
| DAQ uncertainty | U_{v_i} | 600 μV |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | ϕ | 2.0 $^{\circ}$ |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s 2 |



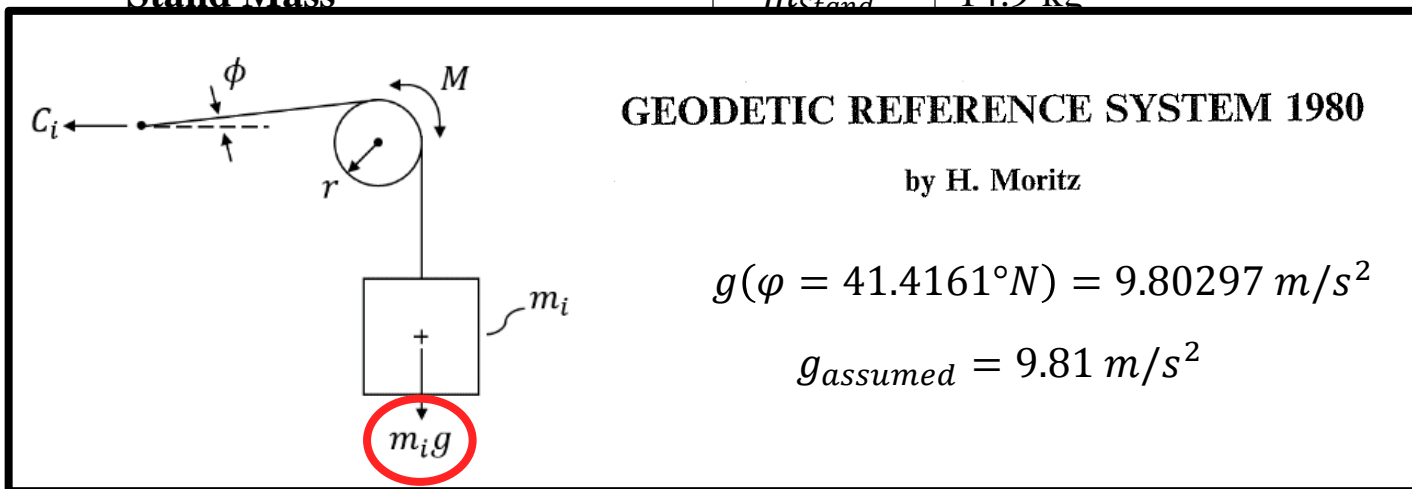
Summary of Assumed Values

| Parameter | Term | Assumed Value |
|---------------------------------|-------------|-----------------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{Stand} | 14.9 kg |
| Total Weight | | N |
| Stand natural frequency | | 8 Hz |
| Stand damping | | kg/s |
| Stand position | | mm |
| Stand velocity | | mm/s |
| Stand inclination | | arc seconds |
| Shunt thermal sensitivity | | ppm/°C |
| Shunt thermal coefficient | | C |
| Thrust vector angle | | |
| Calibration slope repeatability | | mN/V |
| DAQ uncertainty | U_{v_i} | 600 μ V |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | ϕ | 2.0° |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s ² |



Summary of Assumed Values

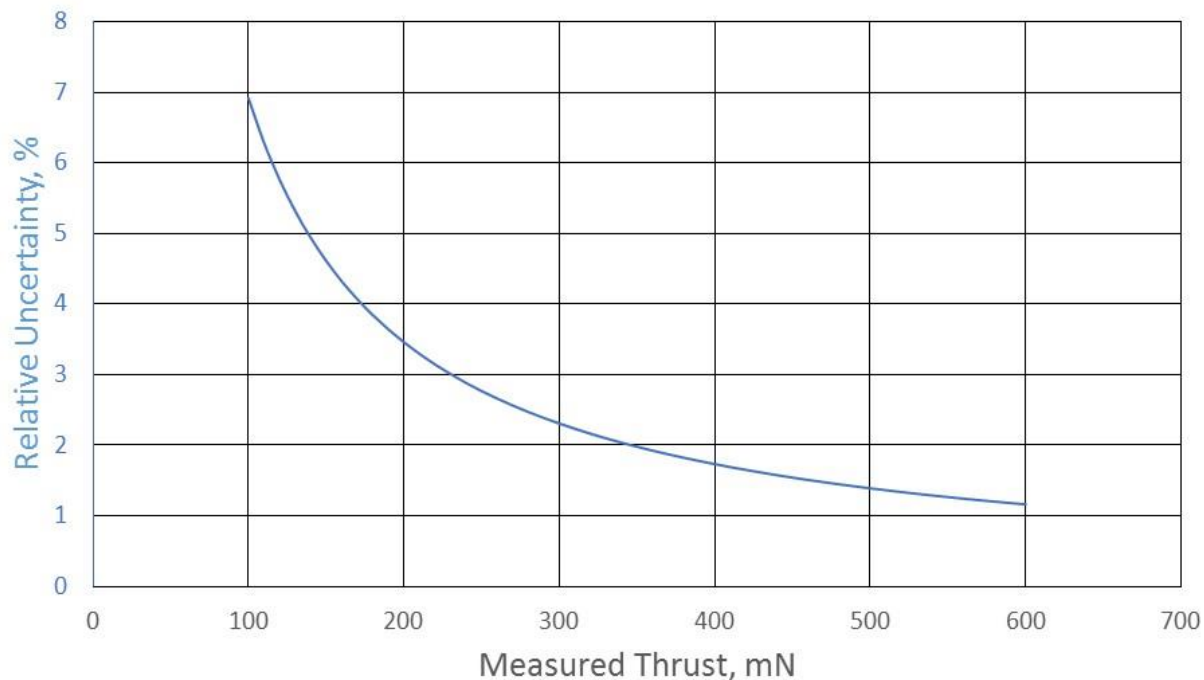
| Parameter | Term | Assumed Value |
|------------|-------------|---------------|
| TDU Mass | m_{TDU} | 46.7 kg |
| Stand Mass | m_{stand} | 14.9 kg |



| | | |
|---------------------------------|-----------|-----------------------|
| Calibration slope repeatability | S_b | 1.54 mN/V |
| DAQ uncertainty | U_{v_i} | 600 μV |
| Calibration pulley moment | M | 2.7e-6 Nm |
| Calibration alignment angle | φ | 2.0° |
| Calibration mass uncertainty | U_{m_i} | 0.1 g |
| Gravity uncertainty | U_g | 0.01 m/s ² |

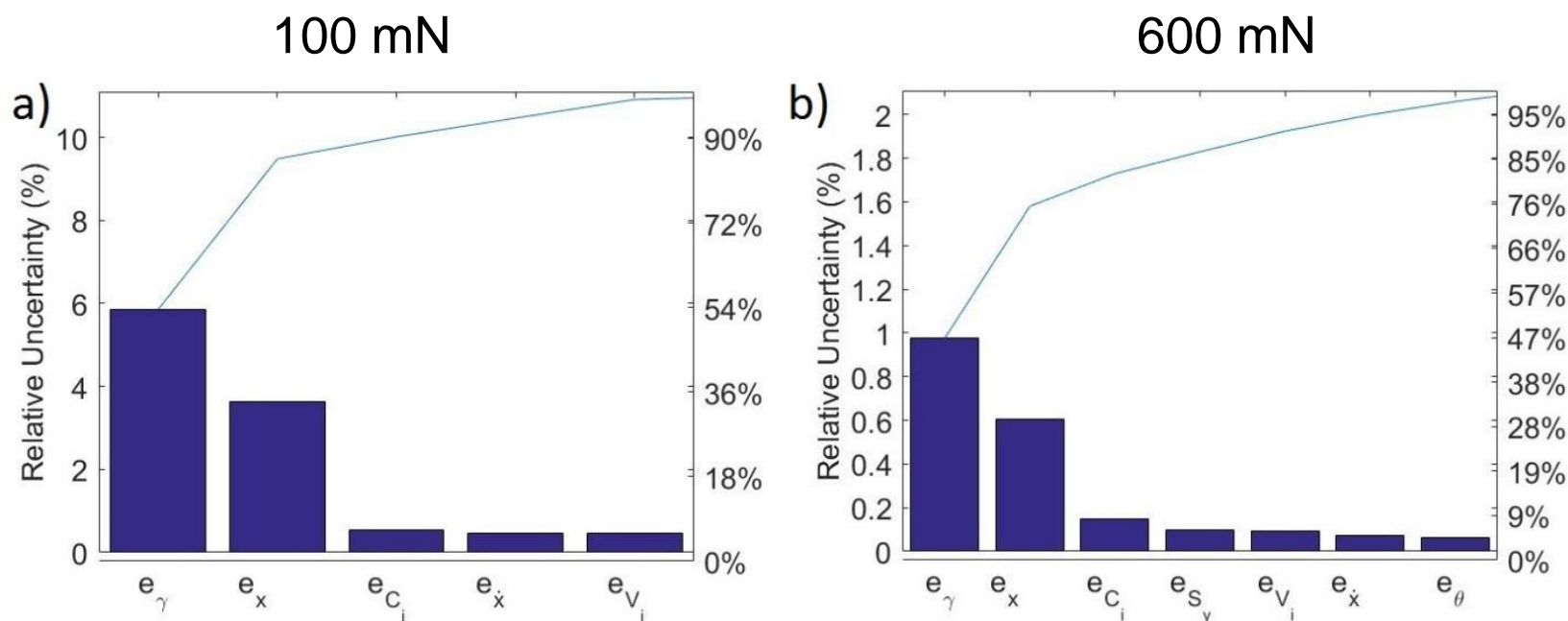
Uncertainty Results

- Relative uncertainty ranges from 7 to 1% depending on thrust level.
 - TDU generally operates 400 to 600 mN, so realistic uncertainty is between 1 to 2%.
 - Higher thrust has lower relative uncertainty.
- Absolute uncertainty (also full scale uncertainty) is fairly constant over full range, ~6.9 mN.



Uncertainty Sources

- Pareto plots highlight the leading sources of uncertainty for two cases of nominal thrust (100mN and 600mN).
- Inclination drift and displacement drift account for >70% of the uncertainty.
- Calibration uncertainty, slope repeatability, velocity drift, and DAQ uncertainty are the remaining significant sources.



Scaling Parameters

- Scaling results to other thrust stands, thrusters, and configurations will depend primarily on three scaling factors:
 - TDU in VF-6 stiffness to thrust ratio $k/T = 2.54 \text{ mm}^{-1}$
 - TDU in VF-6 damping to thrust ratio $c/T = 2.54 \text{ s/m}$
 - TDU in VF-6 weight to thrust ratio $mg/T = 1023$
- Considering uncertainty only, it is advisable to minimize these terms.
 - Temporal resolution of the stand may suffer for low stiffness ratio.
 - Structural integrity of the stand may suffer for low weight ratio.

Conclusions

- A 95% confidence uncertainty of $\pm 6.9\text{mN}$ has been established for TDU in VF-6.
- The leading sources of uncertainty are stand inclination drift and stand displacement drift.
- A stand characterization method and a set of scaling parameters have been established and calculated for the case study.
- Future Work:
 - Various thrusters on VF-6 thrust stand, other inverted pendulum thrust stands, torsional thrust stands, and quantification of additional sources.



Acknowledgements

- Space Technology Mission Directorate in support of the Solar Electric Propulsion Technology Demonstration Mission Project for funding the joint NASA GRC and JPL development of the Advanced Electric Propulsion System.

Questions?

