Landsat 9 Thermal Infrared Sensor 2 Pre-Launch Characterization: Initial Imaging and Spectral Performance Results

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SPIE
San Diego, CA
August 21, 2018
TIRS-2 Project Overview

- TIRS-2 will fly on the LandSat 9
  - 16 day re-visit cycle
  - 2 bands: 10.8 μm & 12 μm
- Like TIRS on Landsat 8, TIRS-2 will produce radiometrically calibrated, geo-located thermal image data
- Risk Class C for Landsat 8 to Class B for Landsat 9
  - Increased redundancy to satisfy Class B reliability standards
  - Improved stray light performance through improved telescope baffling
  - Improved position encoder for scene select mirror to address problematic encoder on Landsat 8 TIRS
- USGS will be responsible for operations
- TIRS-2 development:
  - NASA GSFC TIRS-2 team formed in 2015
  - TIRS-2 completed Critical Design Review in Feb. 2017
  - Instrument in fabrication at NASA GSFC
  - Initial pre-launch imaging and spectral characterization Nov. 2017 – March 2018
  - On target for August-2019 delivery to spacecraft

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Increase in pivot irrigation in Saudi Arabia from 1987 to 2012 as recorded by Landsat. The increase in irrigated land correlates with declining groundwater levels measured from GRACE (courtesy M. Rodell, GSFC)
Stray Light Issue from TIRS

- Non-uniform banding and absolute calibration error found in TIRS imagery post-launch – suspected stray light
- Characterized on-orbit using a raster-scan of the moon around the out-of-field-view

Moon is ~ 0.5 deg. wide
TIRS detector arrays

Stray light source roughly 13° from optical axis

Lunar locations where a stray light signal appeared anywhere on the detectors

The baffles at Lens 3 and Lens 2 locations address scattered light paths at 13° and 22° off-axis, respectively.

FPA made up of three separate quantum well infrared photodetector arrays each filter covering ~30 pixel rows and 1850 total pixel columns (185 km swath width)

[Reuter et al Remote Sens. 2015
Montanaro et al IGARSS 2018]
Initial performance tests at “almost” instrument-level (Telescope/focal plane arrays/focal plane electronics, no scene select mirror)

- **Focus test**
  - Determine focus position of FPA/telescope, determine proper shims, & verify

- **Spatial response test - Initial characterization**

- **Scatter survey test**
  - Only opportunity to measure far-field scattering (due to config of test article and CGSE in the chamber)

- **Spectral response test - Initial characterization**

- **Characterize cryoshell performance**
TIPCE Configuration

**Focus, Scatter, & Spatial**

- 16-pixel circular target
- 1- and 2-pixel circular targets
- 1-degree target

Diagram showing:
- Calibration Ground Support Equipment (Cal GSE)
- Off-Axis Parabolic Mirror
- Blackbody (not installed)
- Blackbody
- Steering Mirror
- Front End Baffle Simulator
- TIRS-2 telescope & FPAs
- Baffles added to reduce stray light
Focus Test Methodology

• The Focus Test is used to determine the optimal focus position of the TIRS-2 focal plane assembly (FPA) relative to the optical telescope.

• Optimal focus is determined by minimizing the full-width, half-maximum (FWHM) of a Gaussian-based model fit to the image created by an input two-pixel source.

• *This focus map is then reported to the instrument team so that proper shims can be fabricated and installed.*

• These measurements are first performed at the telescope-FPA assembly (TIPCE level) to find best focus, then repeated at the full instrument level to validate consistency and characterize focus as function of telescope temperature.
Focus Test Results

- Full focus survey collected during TIPCE with telescope at nominal temperature
  - *Shims calculated, manufactured, and installed*
- Full focus survey for verification collected during another phase of TIPCE at nominal telescope temperature and at nominal +5 K.
  - Found average piston defocus of +90 microns of CGSE z-axis
  - shim deltas to be only: +0.0003", +0.0002", -0.0002"
  - Decided on NO shim adjustment
  - Decided on NO telescope temperature adjustment
Spatial Response Test Methodology

• Processing follows the same methodology as used for TIRS1
  – Using ‘hockey puck’ target collect frames as target is moved in incremental sub-pixel (1/5) steps across-track and along-track over 3 pixels in each direction.
  – 16 pixel diameter circle target (“Hockey Puck”)
  – Large square for flat field
  – Blank for background correction
  – Repeat at different locations on FPA

Each circular image frame has a background-correction and flat field applied at pixel level

\[ \text{dn}(i,j) = \frac{\text{DN}_P(i,j) - \text{DN}_{BKG}(i,j)}{\text{DN}_{FF}(i,j) - \text{DN}_{BKG}(i,j)} \]

Horizontal cross section through center of puck normalized to maximum value
Spatial Response Test Methodology

All 80 cross sections shifted to common reference point

Metrics for evaluating spatial performance -- edge slope, edge extent -- derived from each edge response plot.

Spatial Response Results:
Edge Slope

**10.8 μm - Across Track**

- Edge Slope: 0.004, 0.005, 0.006, 0.007
- Column #: 0, 500, 1000, 1500

**10.8 μm - Along Track**

- Edge Slope: 0.004, 0.005, 0.006, 0.007
- Column #: 0, 500, 1000, 1500

**12.0 μm - Across Track**

- Edge Slope: 0.004, 0.005, 0.006, 0.007
- Column #: 0, 500, 1000, 1500

**12.0 μm - Along Track**

- Edge Slope: 0.004, 0.005, 0.006, 0.007
- Column #: 0, 500, 1000, 1500

TIPCE-2
TIPCE-3
Spatial Response Results: Edge Extent

10.8 µm - Across Track

10.8 µm - Along Track

12.0 µm - Across Track

12.0 µm - Along Track

TIPCE-2
TIPCE-3
Scatter Survey Test Methodology

- Optical modeling reveals residual scattering at 13-deg and at 22-deg with the baffles.
- Wanted to scan the azimuthal extent of the 22-deg feature in TIPCE.
- Each dot represents the center of the 0.7-deg blackbody square target.
Scatter Results: Target @ -28 deg

Blackbody square target is here

Frame of signal corresponding to the grid location

Units are percent of the signal when the target is directly illuminated on the detectors
Scatter Results:
Target @ -22 deg and @ -13 deg
Scatter Results: Total Scattering

- Combine scattering data from TIPCE2 and TIPCE3. Red boxes where source was when signal observed on any detector.
Scatter Results:
TIPCE Scattering Sum

Angles relative to FPA center

Percent signal

Signal profile through each filter

- Blue: 10.8 um
- Red: 12.0 um

Detector number: 0 200 400 600 800 1000 1200 1400 1600 1800

SCA-A
SCA-C
SCA-B
Scatter Results:
TIPCE3 Scatter vs. Optical Model

Optical model from June Tveekrem for SCA-B, 12 um band

- TIPCE angles do not encompass entire out-of-field but can use TIPCE results to scale optical model to same units.
- Use sum of TIPCE signal here and sum of model signal here to derive scale factor.
- Scale entire optical model using scale factor and sum up signal for each SCA/band.
Scatter Results: Total Scatter Sum

Sum using optical model:

<table>
<thead>
<tr>
<th></th>
<th>10.8 um</th>
<th>12.0 um</th>
</tr>
</thead>
<tbody>
<tr>
<td>SCA-A</td>
<td>0.69 %</td>
<td>1.11 %</td>
</tr>
<tr>
<td>SCA-B</td>
<td>0.76 %</td>
<td>1.01 %</td>
</tr>
<tr>
<td>SCA-C</td>
<td>0.24 %</td>
<td>0.21 %</td>
</tr>
</tbody>
</table>

Preliminary look at science impact:

SCA-A, 12.0 um, 1.11%

Out-of-field Temperature is:

<table>
<thead>
<tr>
<th>In-field Temperature is:</th>
<th>200</th>
<th>240</th>
<th>260</th>
<th>270</th>
<th>280</th>
<th>290</th>
<th>300</th>
<th>320</th>
<th>330</th>
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</thead>
<tbody>
<tr>
<td>240</td>
<td>-2.06</td>
<td>-1.36</td>
<td>-0.83</td>
<td>-0.52</td>
<td>-0.18</td>
<td>0.19</td>
<td>0.59</td>
<td>1.48</td>
<td>1.97</td>
</tr>
<tr>
<td>260</td>
<td>-1.40</td>
<td>-0.92</td>
<td>-0.56</td>
<td>-0.35</td>
<td>-0.12</td>
<td>0.13</td>
<td>0.40</td>
<td>1.00</td>
<td>1.33</td>
</tr>
<tr>
<td>270</td>
<td>-1.18</td>
<td>-0.77</td>
<td>-0.47</td>
<td>-0.30</td>
<td>-0.10</td>
<td>0.11</td>
<td>0.34</td>
<td>0.84</td>
<td>1.12</td>
</tr>
<tr>
<td>280</td>
<td>-1.00</td>
<td>-0.66</td>
<td>-0.40</td>
<td>-0.25</td>
<td>-0.09</td>
<td>0.09</td>
<td>0.29</td>
<td>0.72</td>
<td>0.96</td>
</tr>
<tr>
<td>290</td>
<td>-0.86</td>
<td>-0.57</td>
<td>-0.35</td>
<td>-0.22</td>
<td>-0.08</td>
<td>0.08</td>
<td>0.25</td>
<td>0.62</td>
<td>0.82</td>
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<tr>
<td>300</td>
<td>-0.75</td>
<td>-0.49</td>
<td>-0.30</td>
<td>-0.19</td>
<td>-0.07</td>
<td>0.07</td>
<td>0.21</td>
<td>0.54</td>
<td>0.72</td>
</tr>
<tr>
<td>310</td>
<td>-0.66</td>
<td>-0.43</td>
<td>-0.26</td>
<td>-0.17</td>
<td>-0.06</td>
<td>0.06</td>
<td>0.19</td>
<td>0.47</td>
<td>0.63</td>
</tr>
<tr>
<td>320</td>
<td>-0.58</td>
<td>-0.38</td>
<td>-0.23</td>
<td>-0.15</td>
<td>-0.05</td>
<td>0.05</td>
<td>0.17</td>
<td>0.42</td>
<td>0.55</td>
</tr>
<tr>
<td>330</td>
<td>-0.52</td>
<td>-0.34</td>
<td>-0.21</td>
<td>-0.13</td>
<td>-0.05</td>
<td>0.05</td>
<td>0.15</td>
<td>0.37</td>
<td>0.49</td>
</tr>
<tr>
<td>360</td>
<td>-0.38</td>
<td>-0.25</td>
<td>-0.15</td>
<td>-0.10</td>
<td>-0.03</td>
<td>0.03</td>
<td>0.11</td>
<td>0.27</td>
<td>0.36</td>
</tr>
</tbody>
</table>

TIRS-2 estimated to have more than an order of magnitude lower stray light impact than TIRS-1

Numbers in table are the percent radiance that the condition is high or low when an out-of-field radiance of 285 K is assumed and removed from the calibration.
Spectral Response Test Methodology

- Data collect with TIRS from the monochromator bracketed by collects with the MCT reference detector.

- Cal GSE in “monochromator mode” where collimated beam from the setup outside the chamber is focused and then re-collimated.

\[
\frac{dn_{corr}(\lambda, pix)}{dTIRS(\lambda, pix) \times \tau_{ref path}} = \frac{dn_{TIRS}(\lambda, pix) \times \tau_{TIRS path} \times V_{ref}}{\tau_{TIRS path} \times V_{ref}}
\]

\[
RSR_{TIRS}(\lambda, pix) = \frac{dn_{corr}(\lambda, pix)}{\max_{\lambda}(dn_{corr}(\lambda, pix))}
\]
• Data was collected for three or four locations on each SCA.
• The monochromator slits were 2 mm (~150 nm).
• TIRS data is collected using the monochromator shutter to provide background measurement. MCT data is collected between channels/SCAs.
• Optimization of the linear stage is run before each collect.
• Optimized for integration time
Spectral Response Results

SCA-A, 10.8 μm

SCA-B, 10.8 μm

SCA-C, 12.0 μm

SCA-A, 12.0 μm

SCA-B, 12.0 μm

SCA-C, 12.0 μm
Spectral Response Results: Comparison to Component-Level

The shading represents the standard deviation over the per pixel RSRs averaged at each location.
Spectral Response Results: Center Wavelength & Band Edges

10.8 µm

12.0 µm
Spectral Response Results: Uniformity

10.8 µm

12.0 µm
Summary

• The results show that TIRS-2 performance is expected to meet all of its performance requirements with few waivers and deviations.
  – Initial TIRS-2 performance testing set and verified the focus of the instrument.
  – Spectral response results show good agreement with component-level measurements accounting for the angular dependence of the detector spectral response.
  – The scatter survey showed improved stray light rejection compared to TIRS-1 the total stray light effect of 1% or less (TIRS-1 – 8%).

• Current preparations for instrument-level thermal vacuum in the fall testing are now underway and delivery is expected Aug 2019.
Backup
• Used NIST wavelength standard (1921b) to calibrate the monochromator wavelength scale using absorption lines closest to the TIRS-2 bands
• The adjustment was programmed into the monochromator to correct an 120 nm offset before TIPCE
• The wavelength calibration was validated pre/post TIPCE phases
  – Monochromator wavelength < 10 nm from wavelength reference throughout TIPCE.

<table>
<thead>
<tr>
<th>Reference Wavelengths</th>
</tr>
</thead>
<tbody>
<tr>
<td>9.0</td>
</tr>
<tr>
<td>9.5</td>
</tr>
<tr>
<td>10.0</td>
</tr>
<tr>
<td>10.5</td>
</tr>
<tr>
<td>11.0</td>
</tr>
<tr>
<td>11.5</td>
</tr>
<tr>
<td>12.0</td>
</tr>
</tbody>
</table>

Table 1. Certified Band Centroid Wavelength Values (in Vacuum)

<table>
<thead>
<tr>
<th>Band Number</th>
<th>Band Wavelength (μm)</th>
<th>Expanded Uncertainty, U (μm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>18.3512</td>
<td>8.2 × 10^{-2}</td>
</tr>
<tr>
<td>2</td>
<td>11.3577</td>
<td>1.8 × 10^{-2}</td>
</tr>
<tr>
<td>3</td>
<td>11.0276</td>
<td>1.3 × 10^{-2}</td>
</tr>
<tr>
<td>4</td>
<td>9.7237</td>
<td>2.5 × 10^{-3}</td>
</tr>
<tr>
<td>5</td>
<td>9.3522</td>
<td>6.8 × 10^{-4}</td>
</tr>
<tr>
<td>6</td>
<td>8.6608</td>
<td>7.0 × 10^{-4}</td>
</tr>
<tr>
<td>7</td>
<td>6.3169</td>
<td>3.4 × 10^{-4}</td>
</tr>
<tr>
<td>8</td>
<td>6.2446</td>
<td>4.1 × 10^{-4}</td>
</tr>
<tr>
<td>9</td>
<td>3.50853</td>
<td>1.5 × 10^{-4}</td>
</tr>
<tr>
<td>10</td>
<td>3.33178</td>
<td>1.0 × 10^{-4}</td>
</tr>
<tr>
<td>11</td>
<td>3.30421</td>
<td>1.0 × 10^{-4}</td>
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<td>12</td>
<td>3.26782</td>
<td>9.0 × 10^{-4}</td>
</tr>
<tr>
<td>13</td>
<td>3.24442</td>
<td>1.0 × 10^{-4}</td>
</tr>
</tbody>
</table>
Spectral Shape - Optical Modeling

Simulated Image on TIRS focal plane

Measured Image on TIRS focal plane

Model and TIPCE show slit images with similar shapes & sizes
Thermal Radiance Detected by TIRS-2 from Surface and Atmosphere

\[ L_s = \frac{\int (B(T, \lambda) \cdot \tau(\lambda) + L_{atm}(\lambda)) \cdot R'(\lambda) \cdot d\lambda}{\int R'(\lambda) \cdot d\lambda} \]

- \( B(T, \lambda) \) • Emitted and reflected surface radiance
- \( \tau(\lambda) \) • Transmission of atmosphere
- \( L_{atm}(\lambda) \) • Emitted and scattered radiance of atmosphere
- \( R'(\lambda) \) • Spectral response of pixel

\( L_s \) • Pixel integrated radiance

Two channel “split window” techniques correct for atmosphere and improve retrieved surface temperature
TIPCE Chamber Configuration

- Test article consists of major TIRS-2 components (except scene select mirror)
- Front end baffle simulator (FEBSim) forward of telescope to simulate entrance apertures of the optical system
- Test article positioned close to the calibration ground support equipment (Cal GSE) to allow for angular range needed for scatter survey.
## TIRS-2 (TIPCE-3) TIRS Pre-launch

<table>
<thead>
<tr>
<th>Channel</th>
<th>Direction</th>
<th>TIRS-2 (TIPCE-3) Mean</th>
<th>TIRS Pre-launch Mean</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>σ</td>
<td>σ</td>
</tr>
<tr>
<td><strong>Edge Slope (pixel⁻¹)</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>10.8 µm</td>
<td>Cross</td>
<td>0.0059</td>
<td>0.0059</td>
</tr>
<tr>
<td>10.8 µm</td>
<td>Along</td>
<td>0.0058</td>
<td>0.0053</td>
</tr>
<tr>
<td>12.0 µm</td>
<td>Cross</td>
<td>0.0059</td>
<td>0.0061</td>
</tr>
<tr>
<td>12.0 µm</td>
<td>Along</td>
<td>0.0060</td>
<td>0.0063</td>
</tr>
<tr>
<td><strong>Edge Extent (m)</strong></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>10.8 µm</td>
<td>Cross</td>
<td>215.6</td>
<td>202.8</td>
</tr>
<tr>
<td>10.8 µm</td>
<td>Along</td>
<td>222.8</td>
<td>234.0</td>
</tr>
<tr>
<td>12.0 µm</td>
<td>Cross</td>
<td>214.9</td>
<td>197.6</td>
</tr>
<tr>
<td>12.0 µm</td>
<td>Along</td>
<td>207.5</td>
<td>184.3</td>
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