

# Estimation of Heatshield Mass Loss for Mars2020 Entry Vehicle

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12th AIAA/ASME Joint Thermophysics and Heat Transfer Conference

2018-06-25

# Outline



- Mars2020 entry vehicle and heatshield
- Motivation for estimating heatshield mass loss
- MSL approach for estimating heatshield mass loss
- Higher-fidelity approach for Mars2020
  - Analysis process and assumptions
  - Mass loss results
  - Comparison of temperature response to MSL Flight Data
- Application of mass loss analysis results in entry vehicle design

### Mars2020/MSL Entry Vehicle



- Mars2020 EDL sequence and entry vehicle design is very similar to MSL
  - Build-to-print with minor changes in vehicle design and descent sequence
  - Cruise Balance Mass (CBM) jettisoned prior to entry to offset CG such that the vehicle flies at a trim angle of attack hypersonically and generates lift for hypersonic guidance
  - Entry Balance Mass (EBM) jettisoned prior to parachute deploy to return vehicle's CG to its axis of symmetry to be aligned with parachute deployment direction
  - Heatshield ablates and loses mass during the heat pulse



#### MSL/Mars2020 Heatshield

- Turbulent transition leads to peak heating occurring on the vehicle's leeside
- Heatshield made of PICA tiles with RTV gap fillers
  - Instrumented with thermocouple plugs (MISP sensors)
- Measured recession from PICA shear testing was significantly higher than model predictions (FIAT)
  - Led to inclusion of a 150% recession lien in MSL heatshield analysis and sizing
  - Later proved to be due to test coupon design
- MSL Flight data confirmed that nominal recession predictions are conservative at MSL conditions











- Entry vehicle mass properties requirements
  - Entry vehicle CG should be within +/-15 mm (ideally at 0 mm) radially from axis of symmetry at parachute deploy, (x,y)=(0,0) – Heatshield ablated
    - Off-center CG leads to vehicle oscillations under parachute (wrist mode)
  - Entry vehicle CG should be offset by EBMs from entry until shortly before parachute deployment to meet a hypersonic L/D requirement (AoA) – heatshield ablating during this time)
- Vehicle balancing analysis process
  - Unbalanced entry vehicle CG is determined on a spin table
    - Nominal heatshield mass loss distribution is included by analysis
  - Static balance mass is added to shift the CG to axis of symmetry (0,0)
  - EBMs are calculated for unablated EV to offset CG to achieve a target L/D (AoA)
  - CBMs are calculated to balance the vehicle to the desired CG location for cruise
- Monte Carlo analysis is performed by varying many performance parameters (including heatshield mass loss) to ensure that the dispersed vehicle state meets the requirements
- Accurate estimates of heatshield mass; its spatial distribution and its uncertainty are important for vehicle balancing throughout entry
  - Also important for heatshield separation and re-contact analysis

### **MSL Approach**



- Recession was estimated at multiple points along the centerline based on margined design environments and including the recession lien
- Interpolations schemes were used to create full-heatshield recession map based on heating distribution (shown in bottom right)
- Integration of mass loss over heatshield produced a total mass loss of 56.6 kg
- To provide a measure of variability, 3 scenarios were assumed (table below)
  - 1. Recession occurs as predicted for the entire heatshield
  - 2. Only top half (leeside) of the HS recessed
  - 3. Only top third (leeside) recessed
- For balancing and Monte Carlo analysis, heatshield mass loss and corresponding CG were varied linearly between these three scenarios

Scenario	Description	Max Ablated Mass	Ablated CM @ Max Ablated Mass (Spacecraft CSYS)		
			$x_c$	Уc	Zc
		kg	mm	mm	mm
1	Max ablated mass	56.6	-199	0	1828
2	Only top half of HS recessed	32.3	-1041	0	1820
3	Only top third of HS recessed (in terms of diameter)	21.0	-1405	0	1760



# Improvement Opportunities in MSL Approach



- MSL analysis did not include mass loss due to decomposition
  - Assumed to be negligible compared to recession mass loss
- Simplified approach to estimate spatial distribution of recession
  - TPS response simulations only done along centerline
- Conservative design assumptions lead to overestimation of mass loss and off-nominal balancing
  - Design environments used for heatshield sizing are conservative by nature (fully turbulent, supercatalytic, roughness augmentation, margins)
  - Recession lien (later investigation and flight data suggest that this lien is not required)
- Simplified approach for assessing variability
- For Mars2020, our goal is to improve upon MSL analysis and provide more accurate and realistic recommendations for total mass loss, its spatial distribution and variability
  - Reasonable fidelity within project resources

### Mars2020 Approach



- Use unmargined heating environments to be closer to nominal expected response
  - Still conservative (fully turbulent, supercatalytic and includes roughness augmentation)
- Don't apply a recession lien (confirmed by MSL flight data)
- Employ a more accurate approach for determining the spatial distribution of mass loss
- Analysis process:
  - Perform TPS response simulations at discrete points distributed on the heatshield to estimate mass loss due to decomposition and recession
  - Polar interpolation between the analysis points to come up with a finer distribution of mass loss over the entire heatshield
  - Integrate mass loss distribution to arrive at total mass loss
  - Calculate CG of lost mass
- Provide a recommendation for mass loss variability

### **Study Limitations**



- This study does not account for mass loss of RTV gap fillers
  - The impact on total heatshield mass loss and CG should be small
  - Less than 5% of overall heatshield mass
  - Does not recede or pyrolyze as much as PICA
- This study does not account for mass loss of the backshell TPS materials
  - No recession at Mars2020 conditions
  - Heating conditions are significantly lower on the backshell, meaning that decomposition mass loss on backshell should be small compared to heatshield ablation
  - Distribution of mass loss expected to be more symmetric than heatshield





### **TPS Simulation Points**



- Heating boundary conditions are extracted from CFD solutions at 109 points distributed along 9 spokes
  - Consider only half of the vehicle (symmetric heating across the pitch plane)
  - Environments are curve-fitted in time based on 9 CFD solutions
- FIAT simulations performed to estimate recession and decomposition mass loss at each point (integrated in time per unit area)



#### **Mass Loss Distribution**

- NASA
- Interpolated estimated mass loss at discrete points to a finer resolution
- Integrated across the heatshield (multiplied by 2 for the full heatshield)
  - Integrated mass loss due to recession (full-heatshield): 13.94 kg
  - Mass loss due to decomposition (full-heatshield): 5.32 kg
  - Total Mass Loss (full-heatshield): 19.26 kg



#### **Recession Overprediction**



- The equilibrium gas-surface chemistry model for PICA is known to overestimate recession at low heating conditions
  - Finite-rate regime
  - Recession map from mass loss analysis (shown here) is based on this model
- MSL heatshield was instrumented with PICA plugs containing 4 in-depth thermocouples at 7 locations (MISP plugs)
  - Shallowest thermocouple was at a nominal depth of 0.254 cm
- All shallow TCs survived indicating that MSL recession at MISP plug locations was less then 0.254 cm
- We can scale FIAT-calculated recession such that max recession at MISP locations is less than the depth of shallowest thermocouple
  - Max recession of 0.58 cm happens at MISP2-3 location
  - Scale the recession map by 0.254/0.58 = 0.438



Black Circles: MISP Sensors Location



#### Mass Loss Distribution (Scaled Recession)

NASA

- Mass loss due to recession (full-heatshield): 6.11 kg
- Mass loss due to decomposition (full-heatshield): 5.32 kg (no change)
- Total Mass Loss (full-heatshield): 11.43 kg



\*Different color scale than figures shown earlier

#### Comparison to MSL Flight Data (MEDLI)

- FIAT simulations were done at locations near MISP sensors
- As a sanity check, the in-depth temperatures from our Mars2020
   FIAT simulations can be compared with MSL flight data
  - No recession scaling in analysis results
- We should not expect a great match
  - Different trajectories (as-flown MSL vs. Mars2020 design)
  - Conservative heating assumptions in analysis
  - Overprediction of recession by PICA response model





#### **Comparison to MSL Flight Data**





### **Final Recommendations**

NASA

- Best-estimate total mass loss is 11.4 kg
  - Corresponds to the case where recession was scaled to depth of shallowest thermocouple on MSL heatshield
- For Monte Carlo analysis, vary mass loss due to recession from zero to max recession (no scaling)
  - Upper bound of 19.3 kg
  - Lower bound of 5.3 kg
- As recession is varied, CG of lost mass shifts
  - CG-y =0 due to symmetric heating
  - CG-z is not very sensitive to recession scaling
  - CG-x moves toward the leeside as mass loss due to recession becomes a bigger part of total mass loss



#### Change in Lost Mass CG due to Recession Scaling

### **CG Requirement at Parachute Deploy**

- Balance Mass that will be installed on EV is applied to all the unbalanced EV cases in uncertainty analysis to create an uncertainty cloud of possible EV CGs
- The large scatter in MSL analysis forced engineers to balance the vehicle to off-nominal CG
- Mars2020 data shows much more confidence that CG of the EV at parachute deployment meets requirements
  - Ample margin is available



#### MSL Uncertainty Analysis

Mars2020 Uncertainty Analysis



### L/D Requirement



- Since EBMs are calculated for non-ablated vehicle, non-ablated cases (blue) surround the nominal L/D req. while ablated cases end up off nominal
- On MSL, ablation uncertainty was so high that new L/D requirement was added (the very right line) to accommodate ablation uncertainty
- With M2020 mass loss analysis, we have more confidence that even ablated cases will fall close to Nominal L/D requirement

**MSL Uncertainty Analysis** Mars2020 Uncertainty Analysis 29.8 30.2 Nominal L/D ablated EV 29.6 30  $\frac{1}{2}$ spacecraft<sup>-znose</sup> × 100%  $\times 100\%$ Constraint ablated EV Constraint 2 (with ablation) 29.4 29.8 cspacecraft<sup>-znose
</sup> nstraint DHS DHS 29.2 29.6 29 29.4 Axial CG Axial CG non non-EV ablated 28.8 29.2 EV 28.6 29 2 2.1 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.7 2.8 2 2.1 2.2 2.3 2.4 2.5 2.6 spacecraft<sup>2+y</sup>spacecraft x<sub>spacecraft<sup>2+y</sup>spacecraft<sup>2</sup></sub> × 100% Radial CG D<sub>HS</sub> × 100% Radial CG D<sub>HS</sub> 18

### Summary



- Mars2020 analysis provides more accurate and realistic recommendations for total heatshield mass loss, its spatial distribution and variability compared to MSL analysis
- Uncertainty analysis showed that the CG requirement at parachute deploy and the L/D requirement can be satisfied with ample margin



#### **Questions?**

#### Flight Data Compared to MSL Predictions With and Without Recession





Solid Lines: MISP Flight Data **Dashed Lines: Model Predictions** 



#### Heatshield Material Can Lose Mass in <u>Two</u> Different Ways

#### **1. Recession**: mass loss due to removal of material from ablator's surface

- Chemical reactions between the ablator and boundary layer gases (ex. Carbon oxidation, primary mode of recession for PICA at MSL conditions)
- Material phase change (melting, sublimation)
- Mechanical removal of material under pressure/shear
- 2. **Decomposition**: as heat penetrates in-depth, certain components decompose and lose mass by releasing gases that permeate to surface

# **Common Misconception:** Ablation was almost <u>non-existent</u> on MSL vehicle according to measured data

- The only information available from flight data is that recession was less than 0.1" at MISP sensor locations
- Conservative design assumptions led to pre-flight recession predictions as high as 0.8"; however, more realistic assumptions lead to 0.14" of max recession at MISP sensor locations
- MSL might have had recession as high as 0.1" in addition to mass loss due to in-depth decomposition

#### Ablation = Recession + Decomposition

MSL had non-zero recession and decomposition



- 15-TPS-01 trajectory
- Unmargined environments based on LAURA/HARA simulations
  - Fully turbulent, supercatalytic, roughness augmentation
  - Includes radiative heating
  - No margins
- 1D thermal analysis of PICA using NASA Ames code FIAT

#### Substructure stack

- Using the same substructure stack for all analysis points
- Mass loss not very sensitive to substructure stack

#### Initial temperature of 3 C used for the entire heatshield

- Mass loss not very sensitive to initial temperature
- Performed the analysis using minimum TPS temperature from MSL flight data; mass loss sensitivity was on the order of 1-2%

#### Mass loss is calculated at heatshield separation

- Same results at parachute deploy
- Semi-automated analysis process allows quick turnaround of mass loss estimation at other trajectory times

### What Is Currently Done for M2020?



- From MSL flight data, we know that recession was overestimated
- Based on back-of-the-envelope calculations, heatshield mass loss was reduced for Mars2020 simulations
  - Scenario 3 mass loss estimate from MSL (~21 kg) was reduced to 7.6 kg based on a simple scaling of recession (removing recession lien)
- For downstream analyses (ex. balance mass calculations), mass loss is assumed to be between 0 and 7.6 kg with an average of 3.8 kg
  - This is probably too low. 7.6 kg was supposed to be the best-estimate
  - Mass loss of 0 kg is not physically possible
- Static balance mass is calculated to balance the vehicle at parachute deploy
- EBMs for every Monte Carlo case are found by balancing the non-ablated vehicle to nominal L/D target requirement



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# National Aeronautics and Space Administration



Ames Research Center Entry Systems and Technology Division