



**TFAWS**  
JSC • 2018

## CO<sub>2</sub> Cryofreezer Coldhead and Cycle Design Insights for Mars ISRU

Jared Berg (GRC LTT)  
Malay Shah (KSC NE-XY)

Presented By

**Jared Berg**

[jared.j.berg@nasa.gov](mailto:jared.j.berg@nasa.gov)

Thermal & Fluids Analysis Workshop

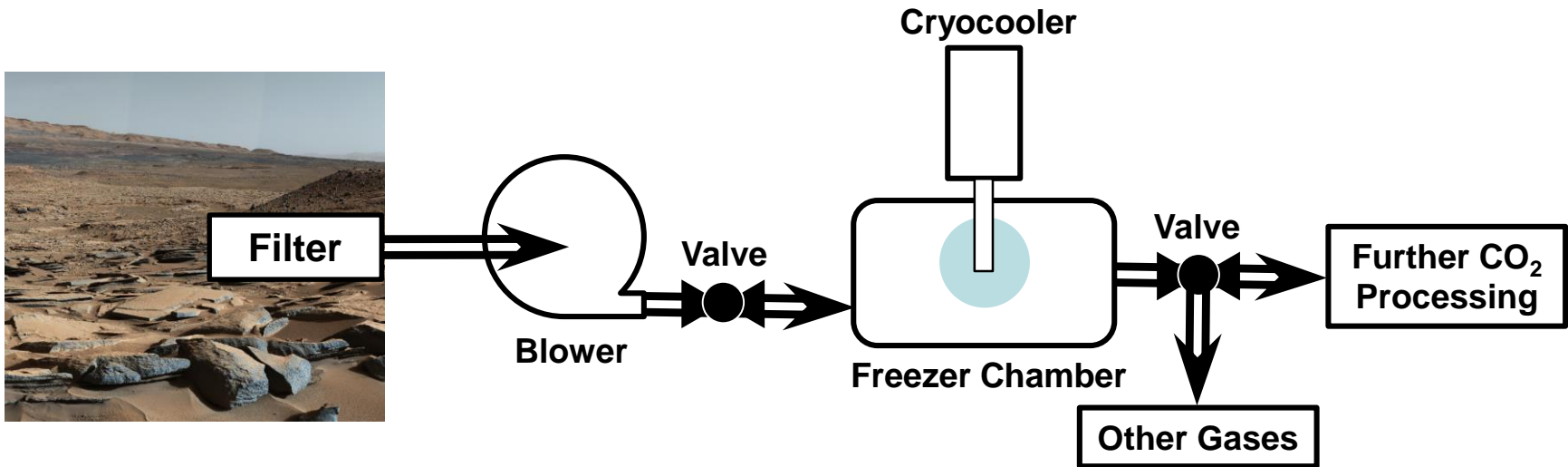
TFAWS 2018

August 20-24, 2018

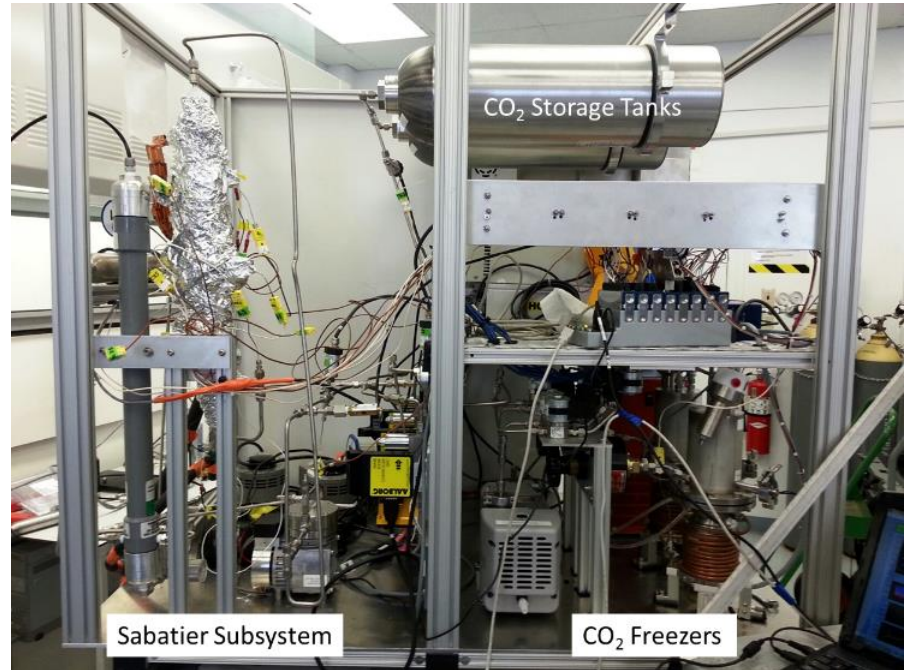
NASA Johnson Space Center

Houston, TX

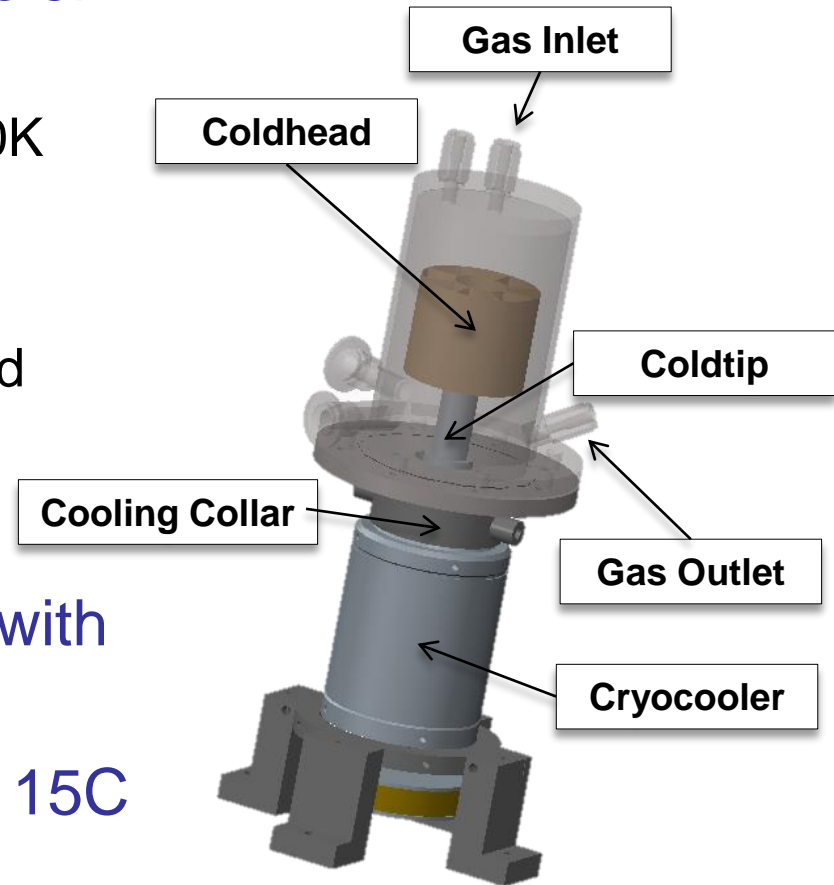
- In Situ Resource Utilization (ISRU) on Mars
  - Create propellant from Mars atmosphere
    - Must separate and compress CO<sub>2</sub> to utilize
      - Mars ~7 Torr (~0.1 psi), 95% CO<sub>2</sub>, 3% N<sub>2</sub>, 2% Ar
      - Approaches include direct compression, sorption pumps, freezer
  - Cryofreezer concept for ISRU discussed in 90s literature
    - Clark, Payne, and Trevathan experiment in 2001 (LM+JSC)
      - Describes basic configuration and tested simple coldheads



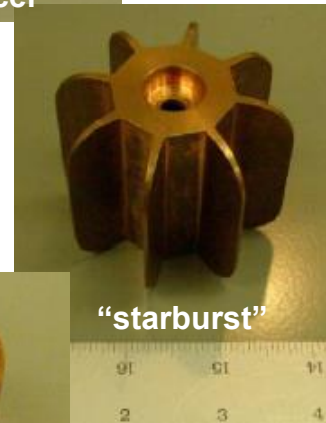
- Mars ISRU Pathfinder project APM (KSC)
  - CO<sub>2</sub> Freezer – Twin units
  - Sabatier reactor – Combine with H<sub>2</sub> to make CH<sub>4</sub>



- Sunpower CryoTel GT cryocooler
  - ~37 W lift @ 150 K
  - ~20% of Carnot efficiency @ 150K
  - 240 W input
  - External water cooling loop
  - Stirling cycle, helium working fluid
- Coldtip protrudes into freezing chamber
- Coldhead mounted on coldtip with thermal grease, securing nut
- External chiller loop maintains 15C rejection temperature



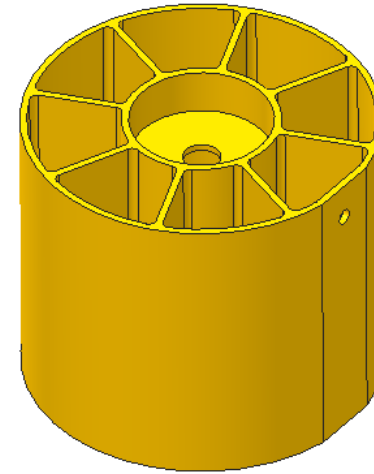
- Initial sizing of cryocooler based on target production rate
  - How many Watts to cool gas and change phase?
  - Coldhead adds additional mass (launch and thermal) to increase collection performance
- Accretion insulates coldtip
  - Solid CO<sub>2</sub> ~0.1 W/m/K (Cook et al)
- Previous work explored some shapes
  - Muscatello and Zubrin SBIR used metal foams
  - Clark et al. tested bare coldtip and simple coldhead geometry
  - Muscatello et al. tried three other shapes with mixed results



Muscatello et al geometries

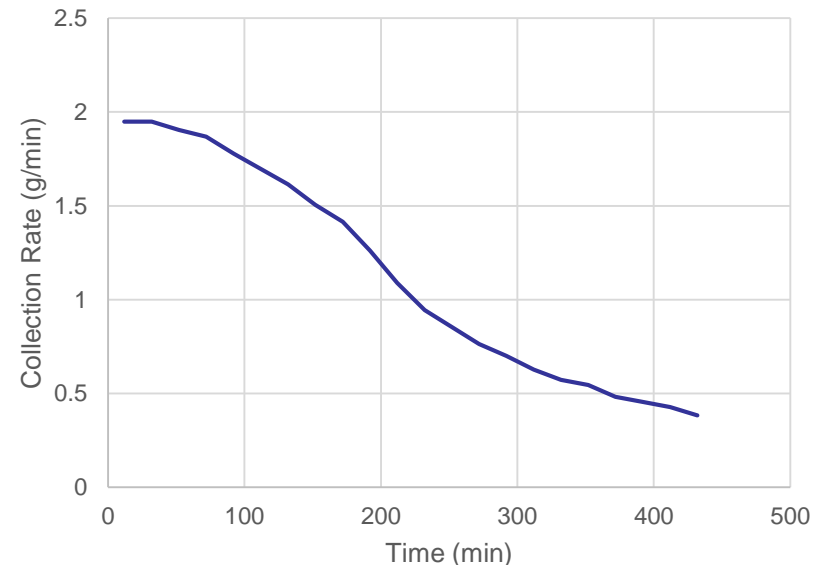
- Heat sinks – well explored area, but phase change and accretion typically absent, mass-production design constraints
  - Dede et al study of 3D printed, flat plate, air-cooled heat sink, gradient-based optimizer
  - Iga et al study of 2D heat sink topology, continuous material distribution interpolated with finite element method
  - These and other approaches (genetic algorithms) yield “spikey,” “natural-looking” designs
- Phase change energy storage – liquid-solid transition, different density and convection regimes, cycling between states
  - Sparrow et al study with paraffin freezing on finned tubes
    - Fin area / temperature boundary condition / time correlation with collected mass
  - Pizzolato et al study of topology for phase change storage, acknowledges high physics complexity and design limitations of previous work
    - Density-based optimization, conduction dominated
    - Defined time minimization and steadiness maximization metrics

- Based on previous experimental paradigm
  - Ferris wheel coldhead
  - Long freezing cycles (~8 hrs) going to “steady state” accretion levels
  - Temperature based cryocooler control (150K setpoint)
  - 1.2 SLPM CO<sub>2</sub> flow rate
- Steady state goal was attempt to correlate with CFD models
- Question assumptions
  - Why run so long?
  - Why use temperature control of cryocooler?
  - Why care about final collected mass?



“Ferris Wheel”

Ferris Wheel Performance (150K Fixed)

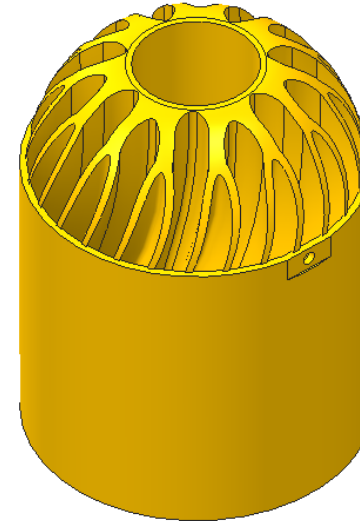


- **CFD**
  - STAR-CCM+ Melting and Solidification toolbox, volume of fluid method
  - Flow / no flow configurations
  - Single compound, solid / gas density change
    - Questionable accretion patterns, pseudotime
- **Thermal Desktop**
  - ACCRETE routine (basically reverse of ablation)
    - Stacked-layer technique not great for complex geometry
      - New feature, tricky to implement
    - Assumes energy is only limit on accretion rate





- **Goals**
  - Distribute metal more efficiently
    - “Biomimetic” branching shape
    - Curved top edge
  - Increase surface area
    - Increased diameter and length
    - Lattice-like surrounding belt
  - Flatten and extend collection performance curve
  - Demonstrate 3D printing with GRCop-84

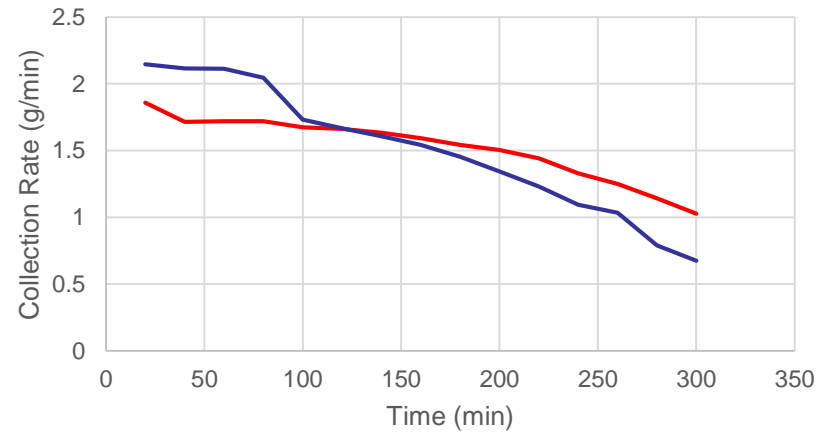


“Branching”

- **Results**
  - Lower initial performance
    - Heat leaks
  - Superior late-cycle performance
  - 45 min to cool to 150K vs. 13 min for Ferris Wheel

- **Success, but failure...**

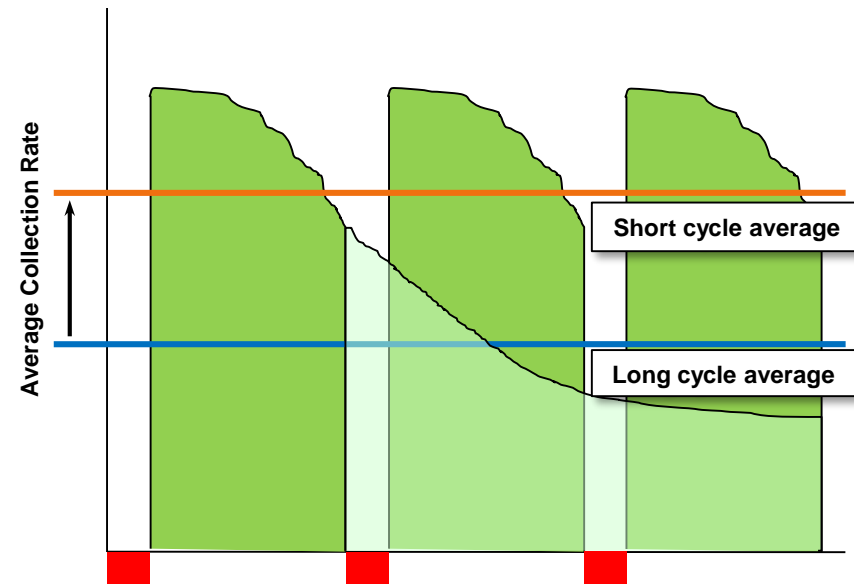
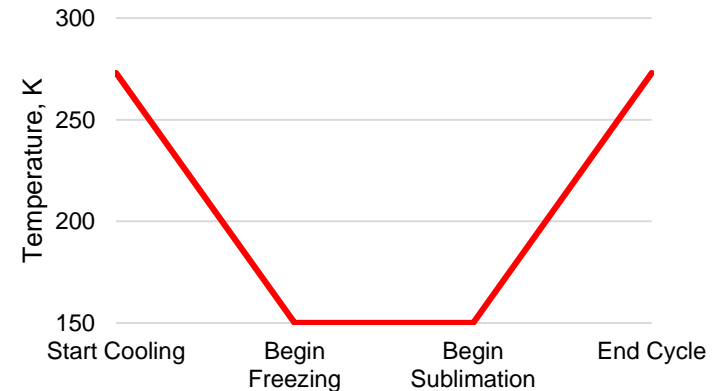
Branching Performance (Max Power)



— Branching — Ferris Wheel

- Collection performance is a complicated function of surface area, conductive material distribution, etc.
- Because of temperature swing, any design must have sufficient performance to “pay off” time spent cooling 270K -> 150K
  - Minimize total mass of coldhead
  - Specific heat / conductivity
  - Scale up limit?
- Parasitic heat leaks from chamber
  - Radiation, convection to hot wall, bypass flow heating
- Early cycle performance is most critical
  - When has performance degraded sufficiently to stop and restart cycle?
    - Much shorter than we thought
  - How do the cycle and coldhead geometry interact?
- Simple optimization needed to determine ideal length of cycle and compare designs

Freezer Cycle Schematic

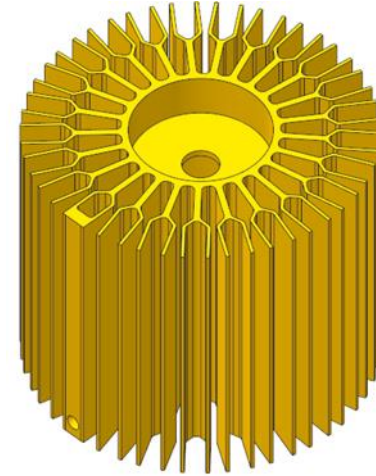


- **Goals**

- Minimize mass to shorten cooling cycle
- Increase surface area, but limit size to reduce heat leaks
- Target early-cycle performance only

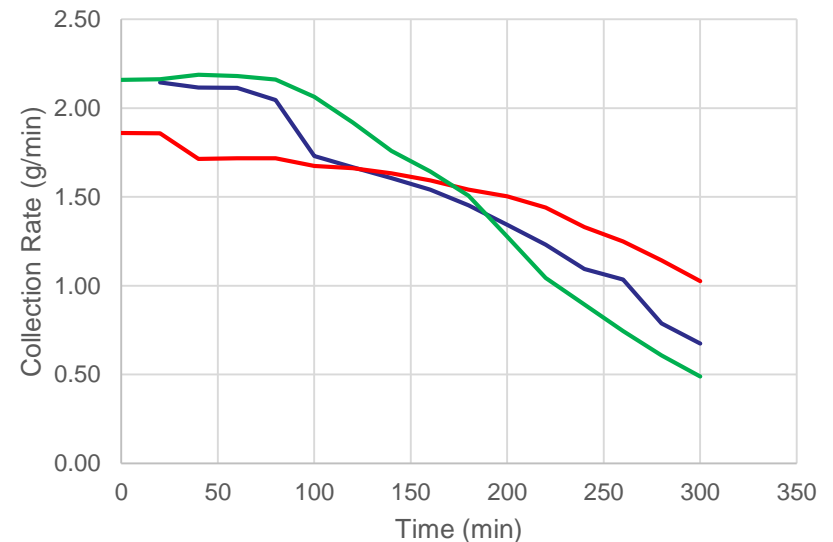
- **Results**

- Max performance at beginning of cycle
- Slow performance drop after peak
- Poor late-cycle performance



“Tuning Fork”

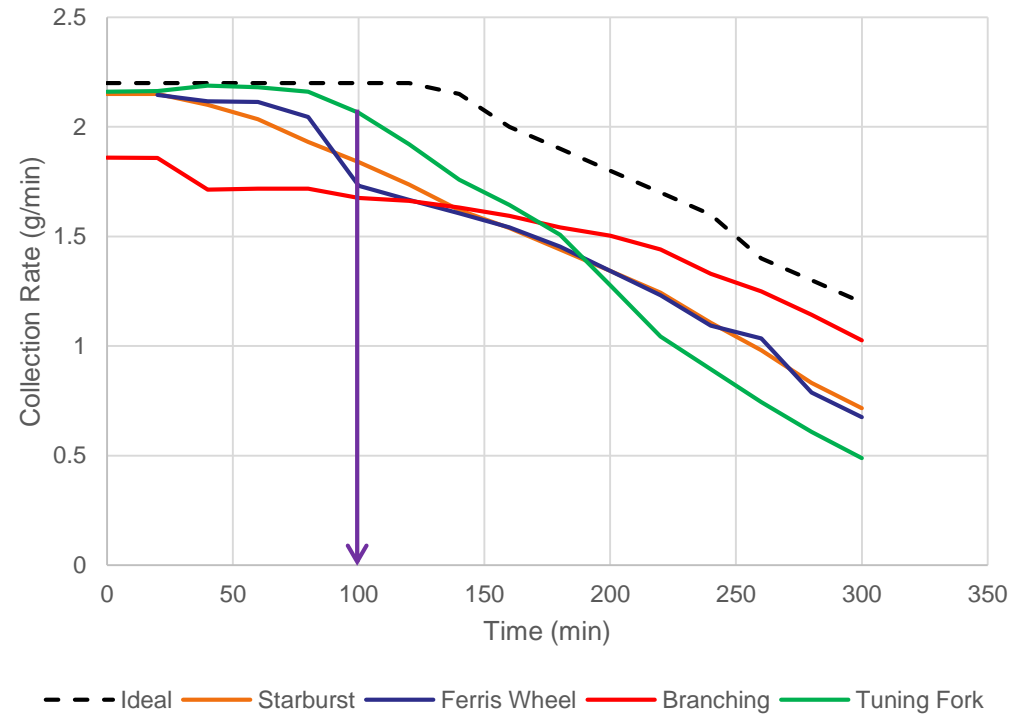
Tuning Fork Performance (Max Power)



— Ferris Wheel — Branching — Tuning Fork

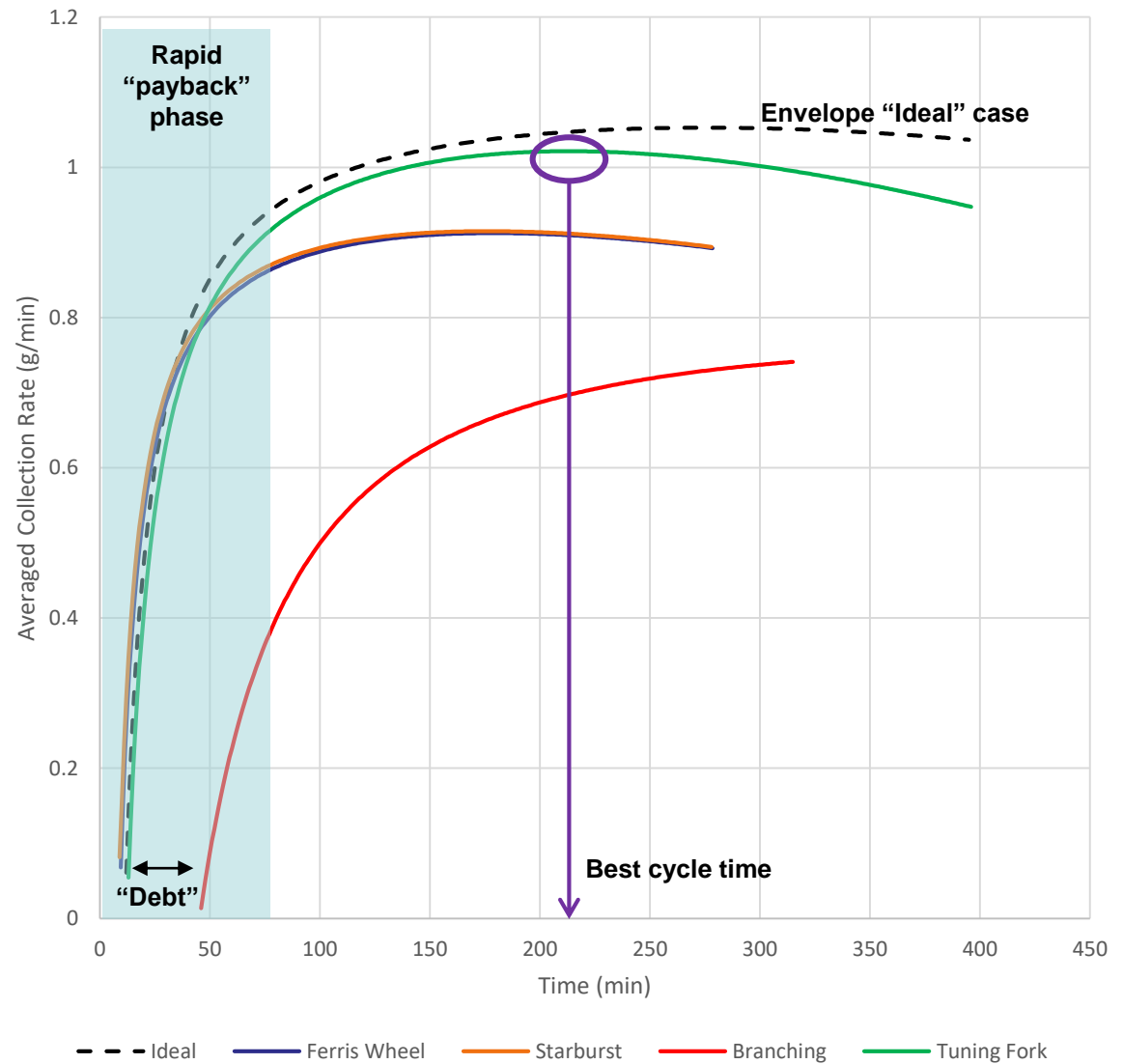
- Added data from legacy “Starburst” design
- Includes “Ideal” case meant to envelope possible designs
- Geometry can have measureable effect on collection performance
- Not a simple function of surface area

Coldhead Performance Comparison

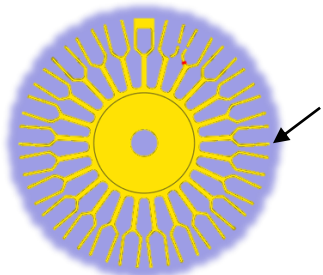
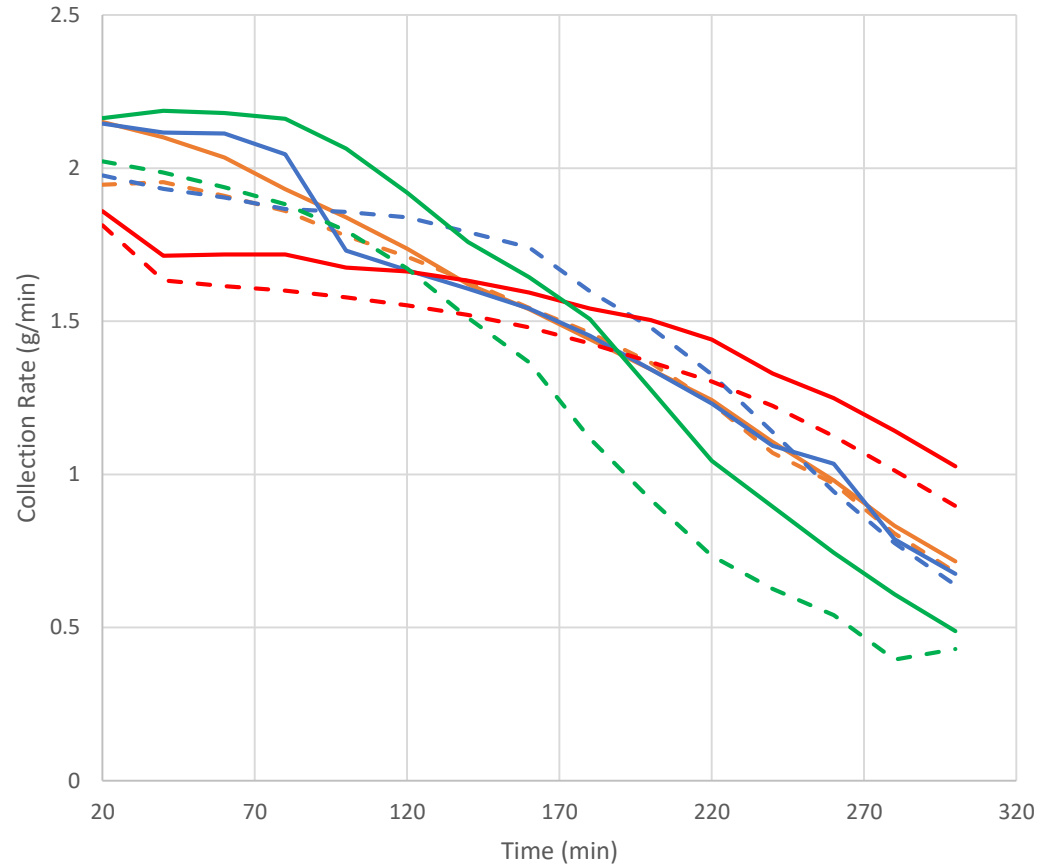


	Ferris Wheel	Branching	Tuning Fork
Volume [in <sup>3</sup> ]	1.74	6.67	2.37
Area [in <sup>2</sup> ]	64.35	157.38 (with lattice)	128.4

- Integrate collection performance curves
  - Assuming equal duration freezing / sublimation phases
    - Paired cryofreezer design
    - Sublimation rate determined by method
  - Starting offset determined by cool-down time
- Peak of curve indicates highest average collection rate
- Late cycle performance (Branching) never “pays back” initial time “debt”
- Best cycle times are much shorter than prior experiments
  - Given performance plateau, can trade collection rate vs. power efficiency, reduced on/off cycles, etc.
- Tuning Fork design superior
  - ~217 min cycle, ~100 min freezing



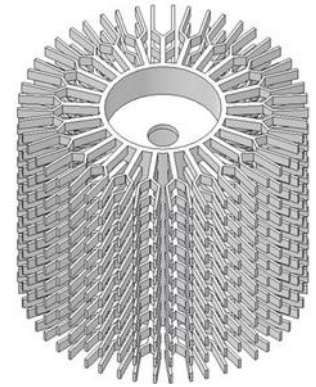
- Ar and N<sub>2</sub> remains after freezing, low temperatures and density limit diffusion rate
  - Previous work (Clark 2001) points this out and indicates importance of recirculation blower
- Differing impact on designs indicates geometry may be important
  - Tuning fork seemingly most affected
  - Ferris Wheel, Starburst most affected early in cycle
  - Branching least affected, likely due to lower overall rate
  - Additional cuts to open “pockets”?
  - More open fin spacing, larger size?



CO<sub>2</sub> depleted region

- Starburst
- Starburst Mars
- Ferris Wheel
- Ferris Wheel Mars
- Branching
- Branching Mars
- Tuning Fork
- Tuning Fork Mars

- Coldhead geometry does matter for performance
  - Tuning Fork ~11% improved cycle-averaged collection rate relative to Ferris Wheel / Starburst
    - But bounding “Ideal” case shows practical limitations
      - Only ~15% better than Ferris Wheel
      - Only 3% better than Tuning Fork
    - Worth trying harder?
- Cycle optimization is important
  - Impacts goals of coldhead geometry design
  - Allows trades with energy efficiency, system reliability, etc.
- Computational modeling is difficult
  - Multi-phase, multi-material, conduction and convection, 3D, transient, diffusion
  - Phase change energy storage analogy seems promising
- Novel concepts?
  - Self-cleaning / scraping coldhead
  - Other materials



Tuning Fork v2.0  
Concept

# References

- Clark, David. L., Payne, Kevin S., Trevathan, Joseph R. “Carbon Dioxide Collection and Purification System for Mars”, AIAA Space 2001 Conference and Exposition, Albuquerque, NM, Aug. 28-30, 2001.
- Muscatello, A., Devor, R., Captain, J. “Atmospheric Processing Module for Mars Propellant Production”. 2013.
- Sparrow, E. M., Larson, E. D., Ramsey, J. W. “Freezing on a finned tube for either conduction-controlled or natural-convection-controlled heat transfer”, Int. Journal of Heat Mass Transfer, Vol. 24, pp. 273-284, 1981.
- Dede, Ercan M., Joshi, Shailesh N., Zhou, Feng. “Topology optimization, additive layer manufacturing, and experimental testing of an air-cooled heat sink”, Journal of Mechanical Design, Vol. 137, Nov. 2015.
- Pizzolato, A., Sharma, A., Maute, K., Sciacovelli, A., Verda, V. “Topology optimization for heat transfer enhancement in latent heat thermal energy storage”, International Journal of Heat and Mass Transfer, Vol. 113, pp. 875-888, 2017.
- Cook, T., Davey, G. “The density and thermal conductivity of solid nitrogen and carbon dioxide”, Cryogenics, June 1976, pp 363-369.
- Iga, A., Nishiwaki, S., Izui, K., Yoshimura, M. “Topology optimization for thermal conductors considering design-dependent effects, including heat conduction and convection”. International Journal of Heat and Mass Transfer, Vol. 52, 2009., pp. 2721-2732.