TFAWS Interdisciplinary Paper Session



Two-Phase Flow System Design Status of the Flow Boiling and Condensation Experiment Jesse deFiebre – GRC Monica Guzik - GRC

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ANALYSIS WORKSHOP

&

THERMAS

JSC • 2018

Thermal & Fluids Analysis Workshop TFAWS 2018 August 20-24, 2018 NASA Johnson Space Center Houston, TX





- Science Objectives
- System Overview
- Test Conditions
- Critical Components
 - Bulk Heater
 - Condenser
 - Accumulator
 - Degasser
 - Flight Functionality
- Current Status



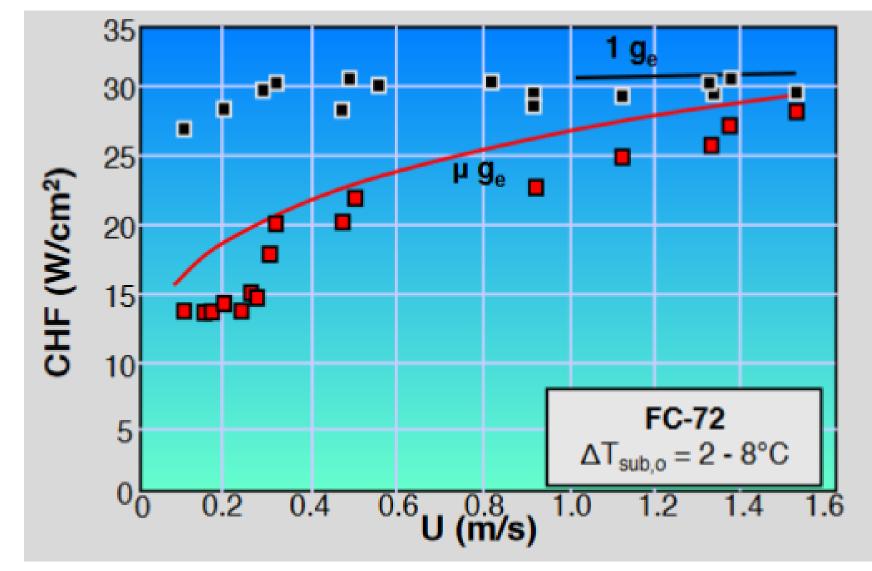




- 1. Develop an experimentally validated, mechanistic model for microgravity flow boiling Critical Heat Flux (CHF) with dimensionless criteria to predict minimum flow velocity required to ensure gravity independent CHF.
 - Obtain flow boiling data (heat flux, wall temperature difference, etc.) in long duration microgravity environments for a well characterized heating surface as functions of liquid inlet mass velocity and sub-cooling.
- 2. Develop an experimentally validated, mechanistic model for microgravity annular condensation with dimensionless criteria to predict minimum flow velocity required to ensure gravity independent annular condensation.
 - Obtain flow condensation data (heat flux, wall temperature difference, etc.) in long duration microgravity environments for a well-characterized condensing surface as functions of inlet quality and flow rate of condensing vapor.



Science Objectives





Relevance

Storage



UNIVERSIT

Vapor Compression Heat Pump for Future Space Vehicles **Planetary Bases**

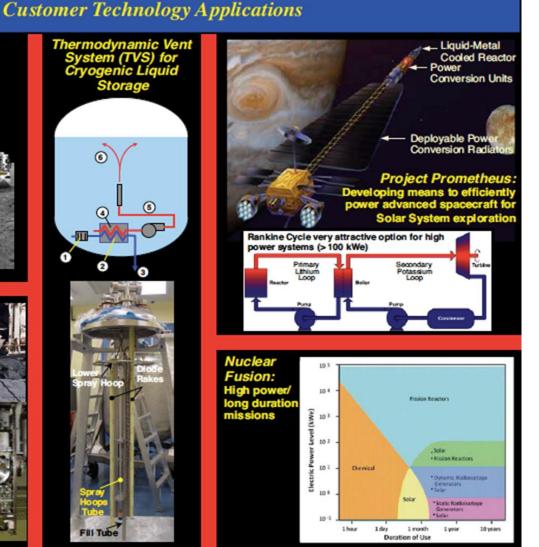




Thermal Control Systems and Advanced Life Support Systems

- Thermal Control System TCS) to control temperature and humidity
- Refrigerator/freezer components
- Advanced water recovery systems

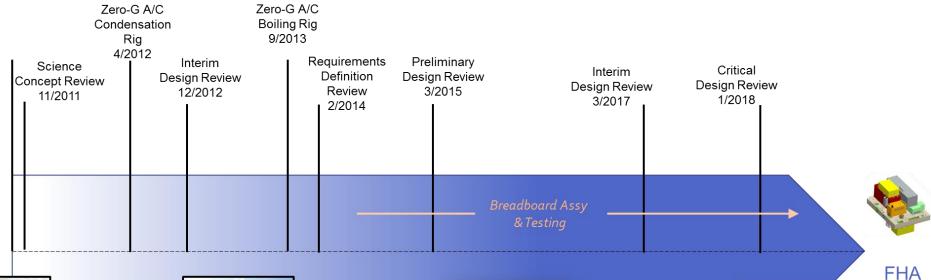






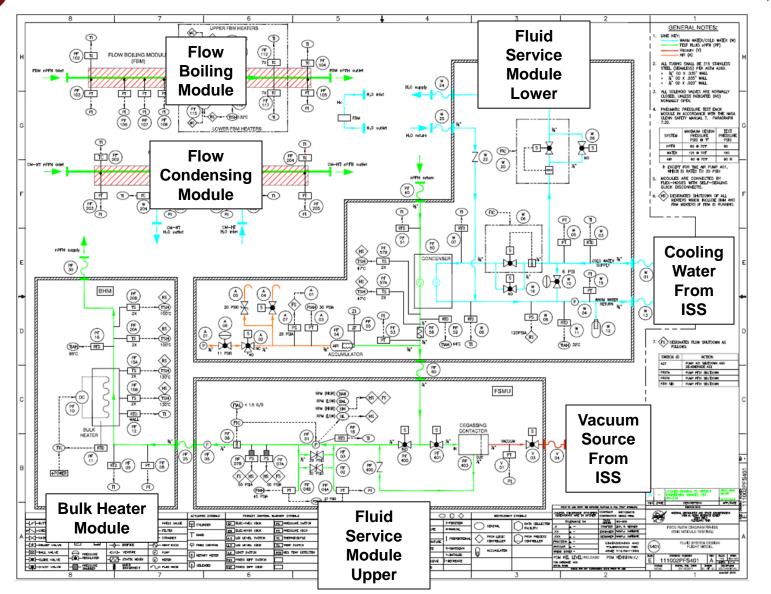
Project Timeline



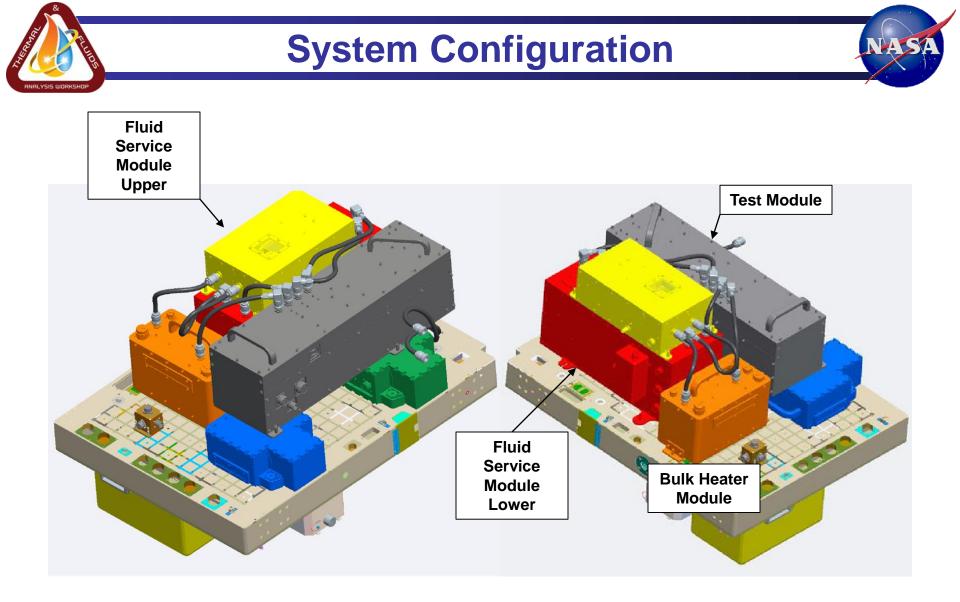




Flight System Overview

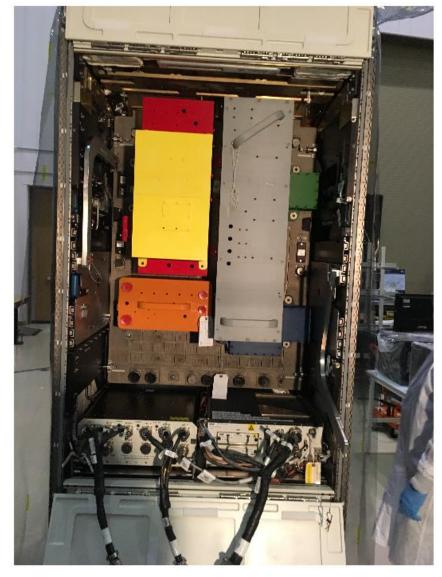


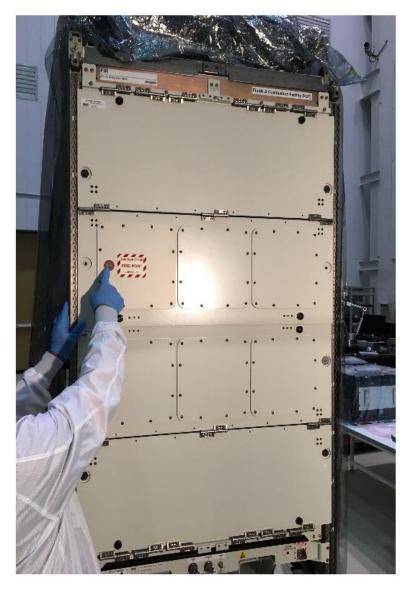
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Fluids Integration Rack







Operations



• Operations will be completely controlled from the Telescience Support Center at NASA GRC







- **Coolant**: nPFH (normal-Perfluorohexane, C₆F₁₄)
- Inlet quality: 0 0.4
- Inlet pressure: $100 150 \pm 20kPa$
- Liquid inlet velocity:

 $U = 0.1 - 2.0 \frac{m}{s}$ for liquid inlet conditions

Mass velocity:

 $G = 180 - 3,200 \frac{kg}{m^2 s}$ for two phase inlet conditions

Inlet subcooling:

$$DT_{sub,i^*} = 0 - 54^{\circ}F (0 - 30^{\circ}C)$$

FBM heater heat flux:

$$q'' = 0 - 60 \frac{W}{cm^2}$$

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- Condensing fluid: nPFH
- Cooling fluid: Water
- **Condensing fluid inlet pressure**: 100 150 kPa
- Cooling water inlet temperature: $68^{\circ}F(20^{\circ}C)$
- Mass flow rate of nPFH:

$$m_{nPFH} = 1 - 14 \frac{g}{s}$$

Mass flow rate of cooling water:

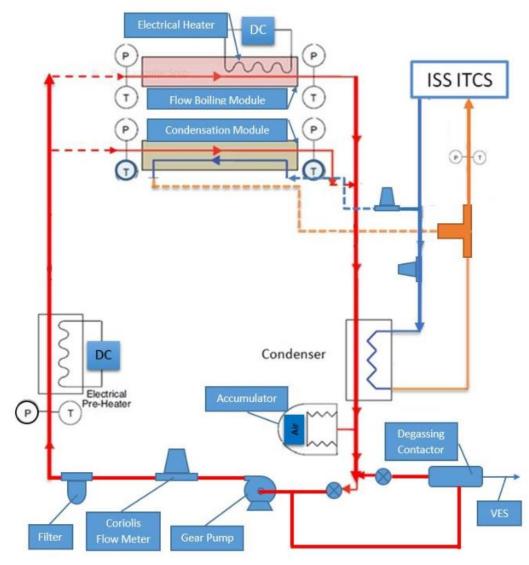
$$m_{water} = 10 - 40 \frac{g}{s}$$

Temperature rise of cooling water:

$$\Delta T_{water} = 9 - 54^{\circ}F (5 - 25^{\circ}C)$$

NAS

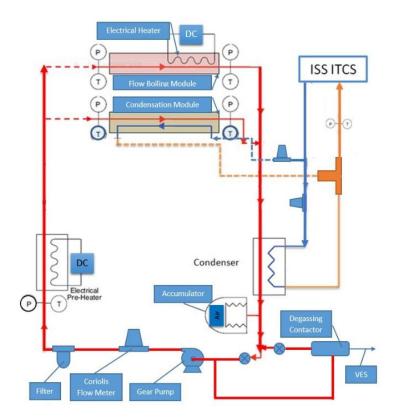
Simplified Fluid Diagram







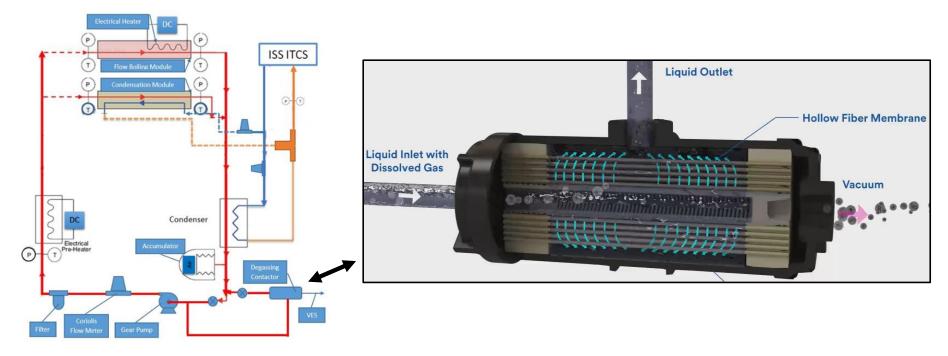
- Accumulator
- Condenser
- Pump/ Mass Flow Controller
- Mass Flow Meters
- Test Module Assemblies
- Heater
- Temperature Control

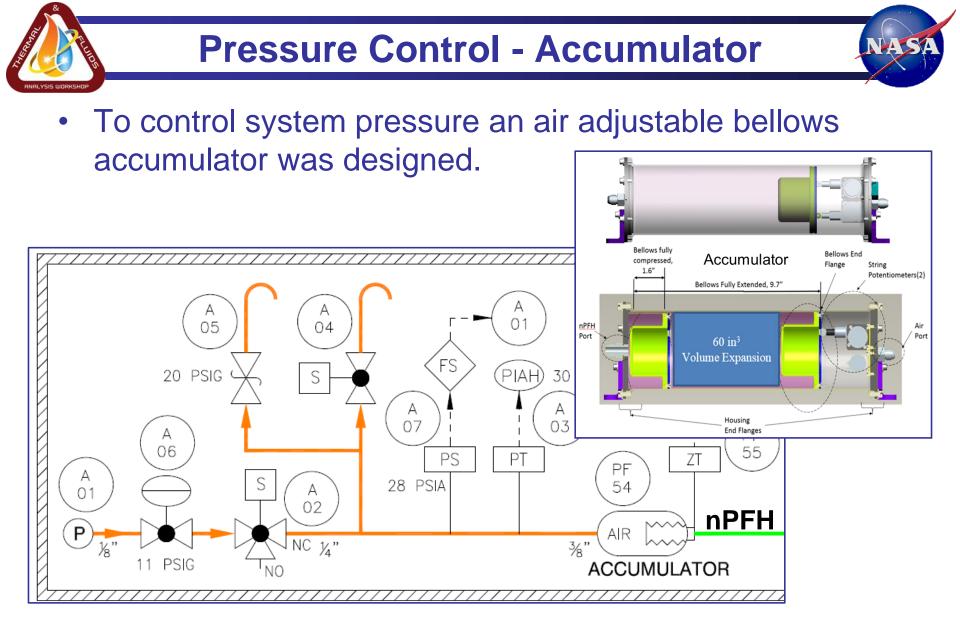




Degassing

- NASA
- The test fluid, normal-perfluorohexane (nPFH) has a high affinity for the absorption of oxygen and nitrogen. Small system leaks will cause build up over time of these noncondensable gases causing degradation in heat transfer. The degasser loop removes them.









- The Bulk Heater heats the nPFH to provide the temperature needed at the inlet of the test module.
- Designed based on Lessons Learned from previous flight experiment to avoid direct contact of heaters with the nPFH fluid as a safety hazard mitigation
- Construction
 - Coiled stainless steel tubing
 - Cast aluminum thermal mass
 - Embedded heaters and temperature sensors.



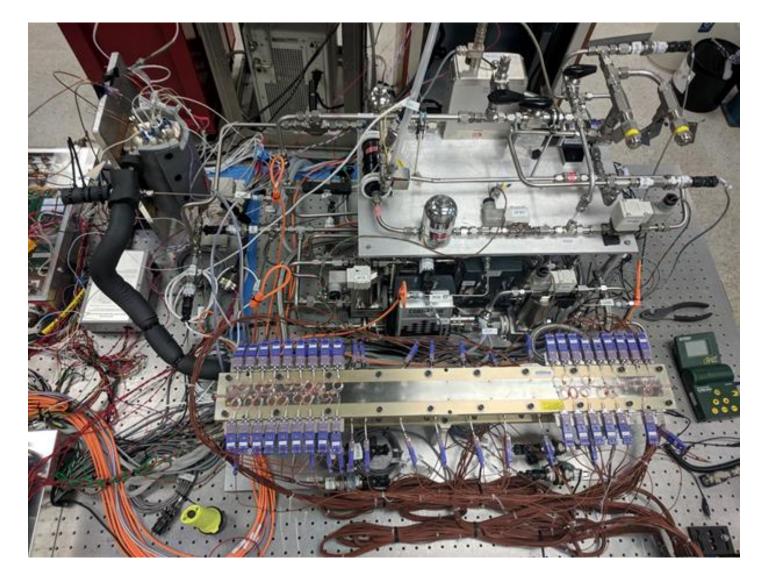


- Original breadboard condenser material was copper
 - Great thermal conductivity properties
- Flight unit cannot be copper due to incompatibility with ISS coolant water
- Stainless steel was chosen for flight unit
 - Thermal conductivity < copper
 - Resulted in increased size/ decreased thermal performance
- During brassboard testing, bubbles
 were observed in the condenser outlet
 - Theorized that slug flow through condenser combined with decreased performance resulted in some noncondensed vapor
- - Opposing theories suggest noncondensable gas presence due to incomplete degassing operations or transient heating



Brassboard





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- NASA
- Precise control of conditions (temp, pressure, quality) at a given location in a closed two-phase flow loop is difficult and requires control of multiple variables (heater power, system pressure, flow rate)
 - Test matrix should be informed by analysis during requirements development to avoid having to make late changes to the design and/or requirements
- Essential to have flight-like hardware in an engineering brassboard as early as possible (i.e. condenser material change being a bigger issue than expected, etc.)
- Try to implement automated controls into an engineering brassboard as early as possible – transient response of a two-phase flow loop can cause surprises when switching from manual to automated control or anticipate transients when designing control loops





- All fluid procurements have been made.
 - Most have been delivered.
- Tube assemblies are being manufactured.
- The accumulator is being assembled.





- Currently in hardware assembly phase
- System level testing scheduled to begin in January 2019
- Still targeting FHA of August 2019
- Anticipate test start aboard ISS in early 2020

Questions?

