Fuel Sensitivity of Gas Emissions, Lean Blowout and Combustion Dynamics for a 9-point LDI Combustor

Zhuohui J. He, Derek P. Podboy and Clarence T. Chang NASA Glenn Research Center, Cleveland, Ohio, 44135





Introduction

Pratt & Whitney, Axially Controlled Stoichiometry (ACS)

- NASA has been investigated the using synthetic fuel on aircraft combustor for decades.
 Advanced Air Transport Technology (AATT) Program
 - 50%/50% alternative fuel/ jet-a blended
 - 80% NOx emissions reduction of ICAO CAEP 6.

Environmentally Responsible Aviation (ERA)

- **75% NOx reductions**
- 50%/50% Rentech / Jet-A blended.
- Alterative fuels tested recently:
 - hydrotreated tallow (HRJ),
 - direct sugar fermentation (Amyris AMJ-710)
 - Fishcher-Tropsch processes (Rentech).



General Electric, twin-annular pre-mixing swirler





National Jet Fuels Combustion Program (NJFCP)

- highly-coordinated, involving several government agencies, universities, industry partners and international collaborations
- focused on the impacts of fuel compositions and physical properties on aviation engine combustor operability
 - lean blowout
 - high altitude ignition
 - cold start
- The fuels under investigation
 - Category A fuels are petroleum base fuels, (JP-8 (A1), JP-A (A2), or JP-5 (A3))
 - Category C fuels are bended fuels, with unconventional properties, composition or distillation curves



OBJECTIVE

- Compare behavior of test fuels C1 and C3 to average Jet A (A2)
- A lean-burn combustor
 - 9-point Lean Direct Injection (LDI)
 - Short fuel-air mixture preparation time
- High pressure and high temperature conditions (T3 = 575 K to 825 K, P3 = 689 to 1723 kPa)
- Gas emissions and combustion dynamics
 - Near Lean blow-out, NO_x emissions, combustion dynamics, ignition.





Experimental Set Up

- NASA Glenn Research Center's CE-5 test facility
- Ceramic liners, rectangular cuboid, (7.6 cm X 7.6 cm X 46 cm)
- Inlet air temperature up to 830 K and inlet air pressure up to 2400 kPa or 24 bar.
- Standard gas-analysis procedure, SAE-ARP1256D
- Three dynamic pressure sampling locations





Test Hardware

- Two 9-point Swirl-Venturi Lean Direct Injection (SV-LDI) injector configurations
- A lean burn concept
 Three fuel circuits
- Local fuel air equivalence ratios were similar among the nine fuel air mixers for most conditions





b) Cross-sectional drawing



2015 test

- Fuel:
 - random batch of Jet-A, A2, C1,C3.
- Injector configuration:
 - Co-rotating pilot



2016 test

Fuel:

- A2 and C1
- Injector configuration,
 - Counter-rotating pilot





Fuels Properties

- A2, (POSF 10325), "average/nominal" Jet-A
- C1, (POSF 11498)
 - high molecular weight duel-component iso-paraffin
 - low cetane number
 - long ignition delay time
 - 80% fuel distillated at a temperature of 35°C lower, faster vaporazation rate.
- C3, (POSF 12341)
 - high viscosity (upper specification limit at -20C)
 - look at the effect of atomization

Properties	A2	C1	C3		
Overall composition	Petroleum Jet A	Gevo ATJ; C12/C16	64% A-3; 36% Amyris		
	(w/ average properties)	highly-branched iso-	farnesane (C15 iso-paraffin)		
		paraffins			
Viscosity, -20 C (cSt)	4.5	4.9	8.0		
Cetane number	48.3	17.1	47		
Distillation (°C), 90%	244	228	245		
80%	230	195	243 NAS		
50%	205	182	230		

Results-NO_x emissions

- A random batch of Jet-A, C3 about the same as A2.
- C1 lower NOx emissions
 - 12% El lower at T3 of 725 K,
 - 5% El lower at T3 of 825 K.
- Possible explanation for Lower NOx with C1
 - Longer ignition delay time, low cetane number
 - faster vaporization rate.
- NOx emissions do not appear to correlate with Cetane Number.
 - Current testing shows similar NOx emissions for C1 (DCN=16) and A2 (DCN=48)
 - Previous HRJ (Cetane Index =69) testing showed similar NOx emissions as Jet-A



Results-ignition

- The C1 fuel was hard to ignite.
- Auto-ignition temperature for A2 is about 700k.
- One successful C1 ignition (P3=1379 kPa, T3=810 K, phi=0.49)
- Also tried fueling the center (pilot) mixer with A2 (instead of C1) at lower T3 and P3 conditions, but no successful ignition.

Fuel used	P ₃	T ₃	DP%	Φ	Φ	Φ	Φ	Successful
	(kPa)	(K)		(Pilot)	(Main1)	(Main2)	(total)	ignition
C1 only	1723	727	2	0.96	0.37	0.37	0.43	NO
C1 only	1034	727	2	0.96	0.36	0.36	0.42	NO
C1 only	1379	810	3	0.97	0.37	0.37	0.44	NO
C1 only	1379	810	3	0.97	0.43	0.43	0.49	YES
Pilot A2/	862	672	2	1.05	0.37	0.37	0.44	NO
Main C1								
Pilot A2/	862	672	2	1.67	0.37	0.37	0.51	NO
Main C2								



Results-Near lean blow-out

2016 test data



- The C1 flame blows out at a calculated adiabatic flame temperature 25 K higher than the A2 fuel.
- Near LBO results are independent of T3, inlet air temperature



- CO curves vary with combustor design
 - Rich burn or lean burn with relatively higher pilot fuel air ratio tend to stay lite even at lower fuel air ratio and at high CO emissions conditions
- C3 has higher CO emissions than C1 and A2 at similar adiabatic flame temperature.
 - high viscosity property of C3
 - the fuel injector may produce larger fuel drop sizes relative to A2 and C1

Low power conditions, high PILOT Φ OF 0.68



Combustion Dynamics







Conclusion

Two tests series were completed

- Used a 9-point LDI combustor
- Measured gaseous emissions and combustion dynamics
- Iong ignition delay time. faster vaporization rate than A2
- promotes better fuel air mixing and lower NO_x emissions
- C1 blows out at a flame temperature 25 K higher than A2
- **C**3

C1

- high in viscosity. larger size fuel droplets and slower vaporization rate
- no NO_x emissions differences observed
- At low power, higher CO emissions observed

No combustion dynamics difference observed between the three fuels.



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Questions and Comments

