



# **The D8 aircraft: An Aerodynamics Study of Boundary Layer and Wake Ingestion Benefit**

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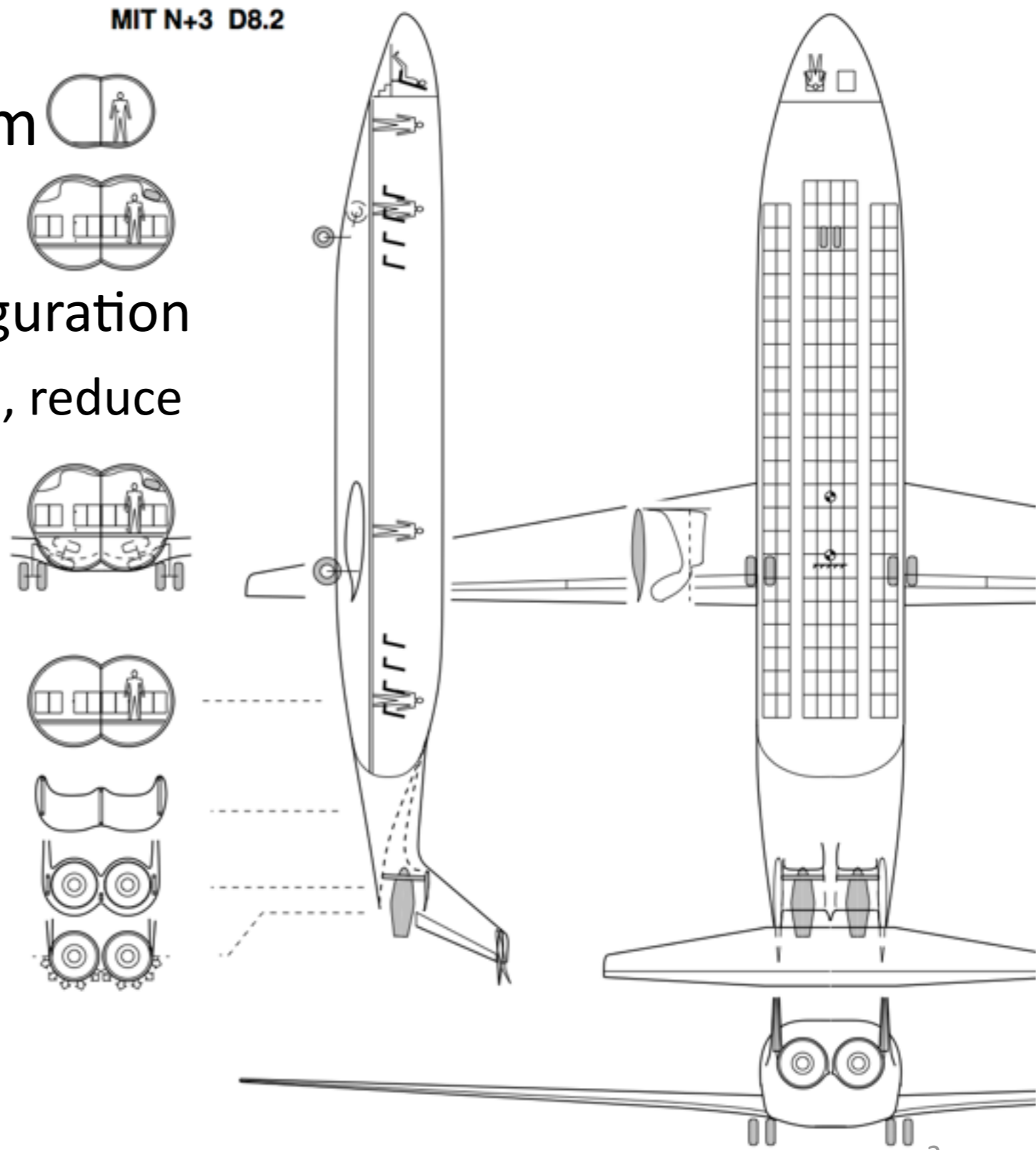
H. Dogus Akaydin and Shayan Moini-Yekta, Science and  
Technology Corporation

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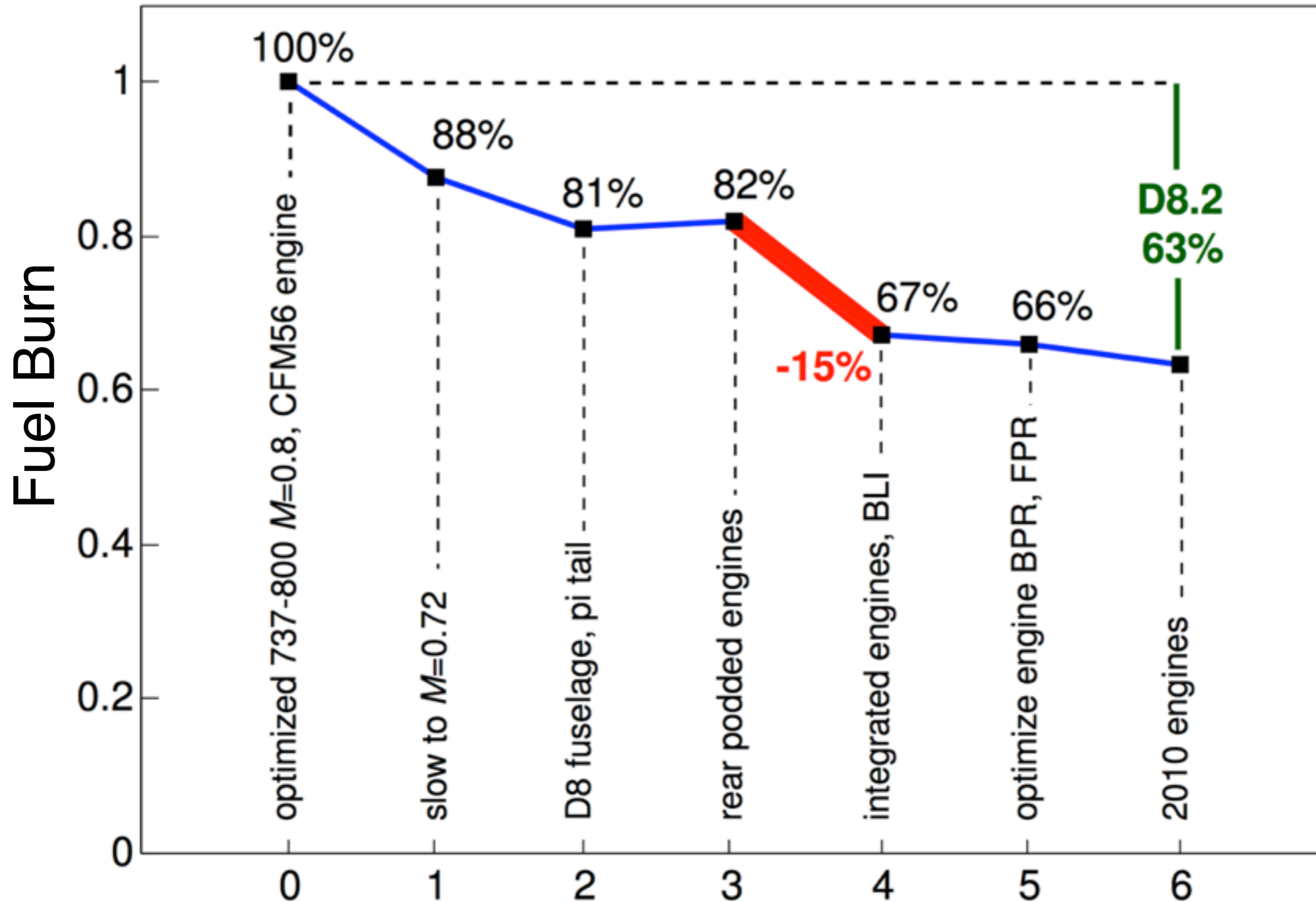
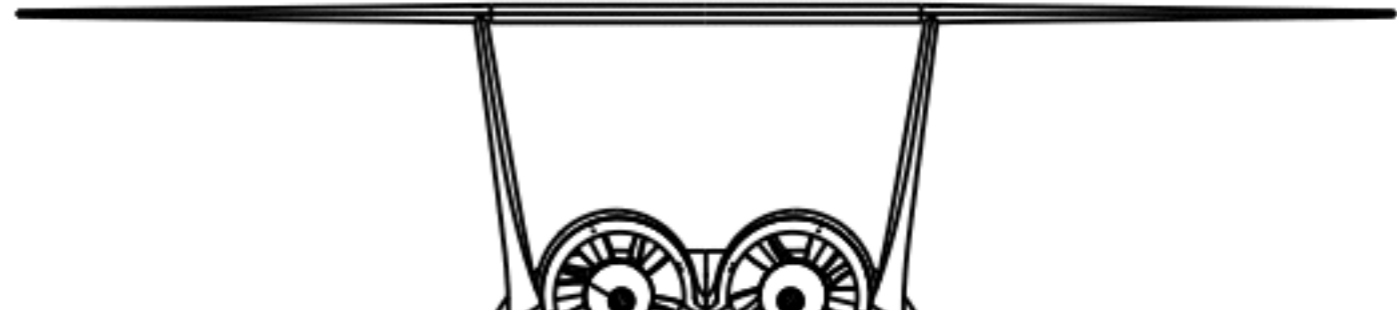
# The D8 Aircraft Concept

- Fundamental Aero program
  - Fixed-wing
  - N+3 advanced vehicle configuration
    - Lower fuel burn, lower noise, reduce emissions
- 180 passengers
- 3000 nmi range
- 118 ft span
- Boeing 737/A320 class
- Lifting fuselage, pi-tail
- Flush-mounted engines





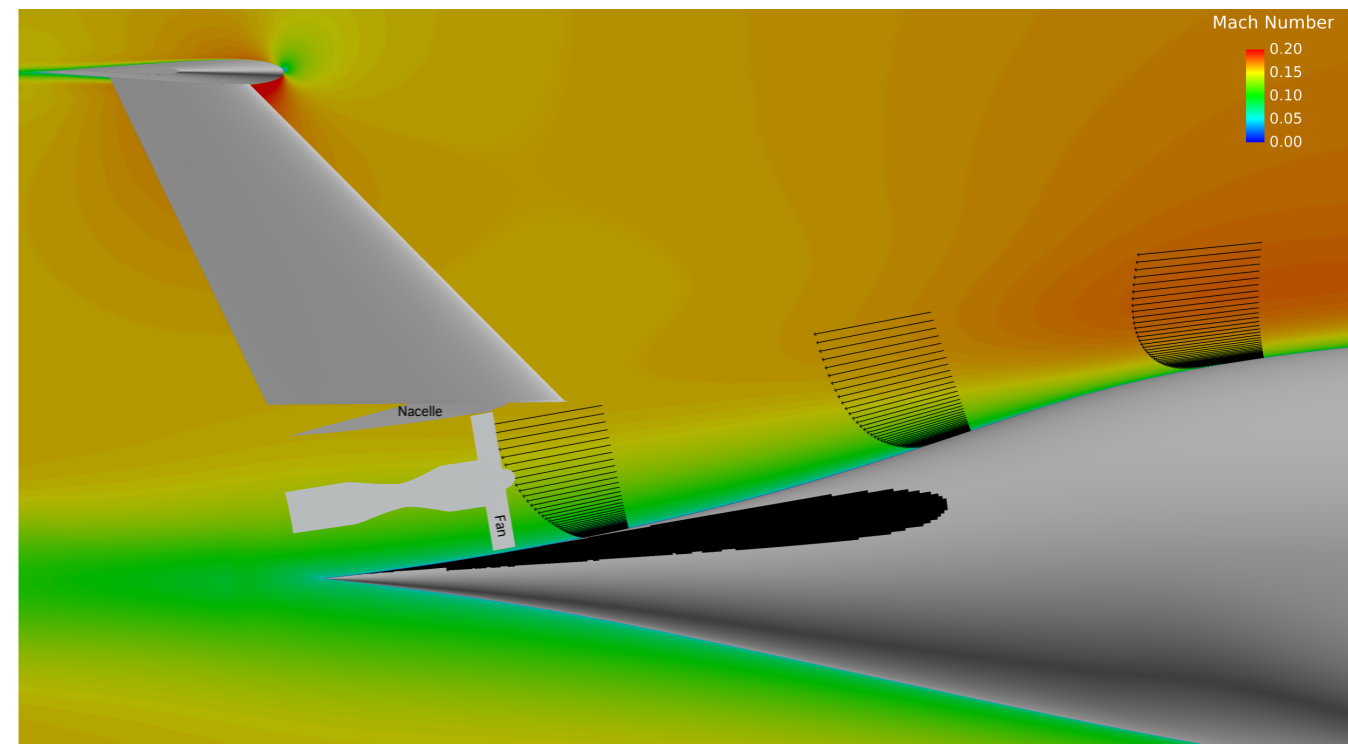
# B737-->D8





# Embedded Rear-Mounted Engines

- Boundary Layer Ingesting (BLI) engines for propulsive efficiency
  - Thicker boundary layer in the rear
  - Designed for  $M=0.6$  flow around engine inlet area
  - Distortion tolerant fan
  - High bypass ratio ( $\sim 20$ )
- Lower engine-out yaw
  - Reduced vertical tail size
- Noise shield





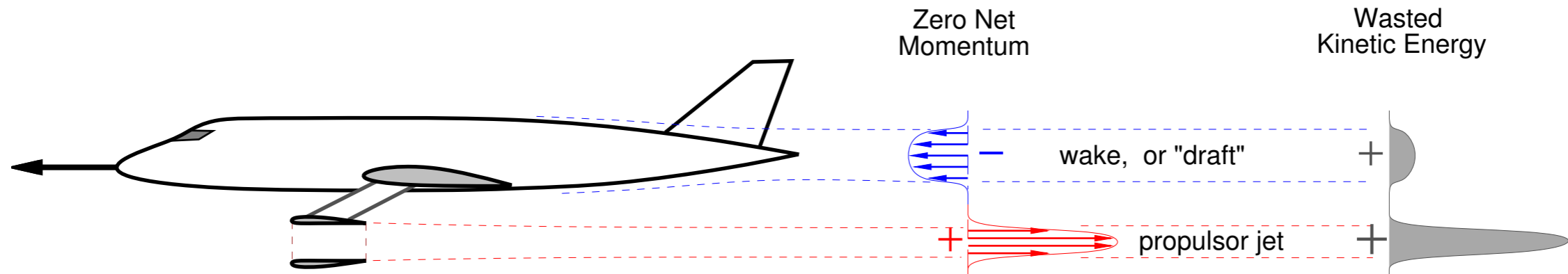
# Goals and Approach

- Goal: Quantify benefits of BLI and wake ingestion for the D8.
- Approach:
  - Overset CFD using CGT and Overflow-2.
  - CFD validation
    - NASA LaRC 14x22 WT data for a 1:11 scale model
  - Quantifying the BLI and wake ingestion benefit:
    - Direct Comparison between:
      - Efficient conventional (podded nacelle) configuration
      - BLI (integrated nacelle) configuration

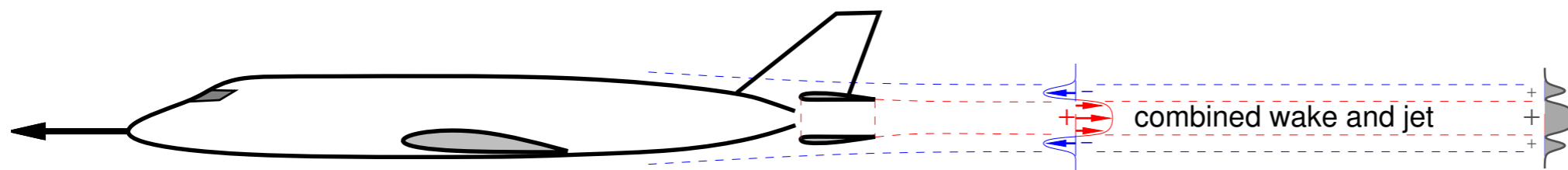


# BLI

- Conventional: wake/BL energy lost



- BLI: Fuselage boundary layer ingested by propulsor
  - Reduced viscous dissipation in combined wake + jet
  - Reduced flow power required from propulsor

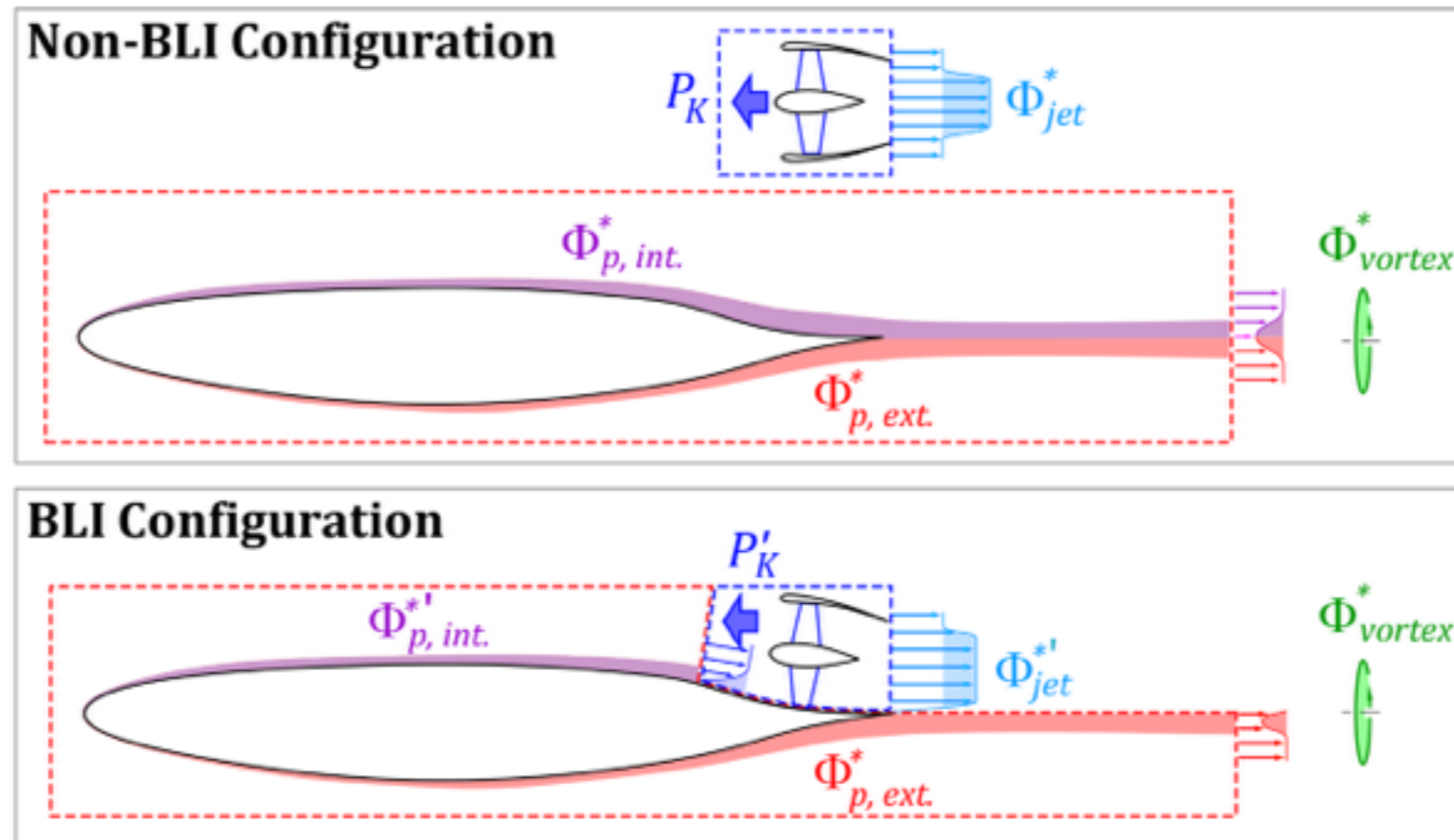


- Use Power-balance method



# Power Balance Method

- Mechanical energy sources and sinks



- Power-in = Dissipation



# BLI Benefit

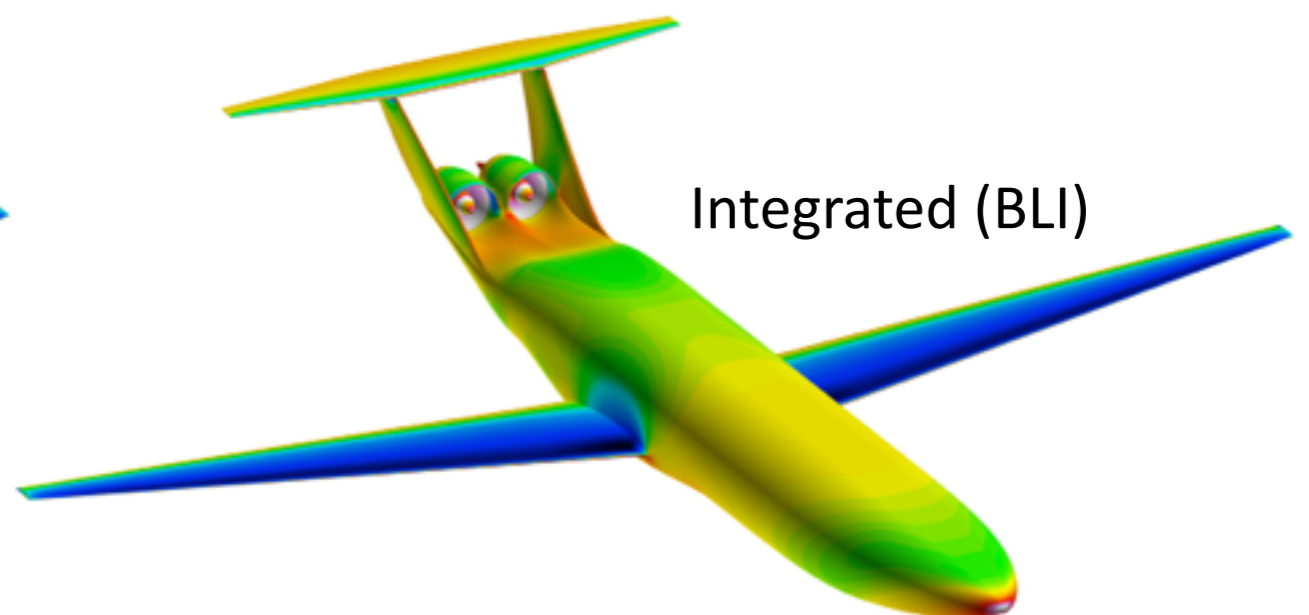
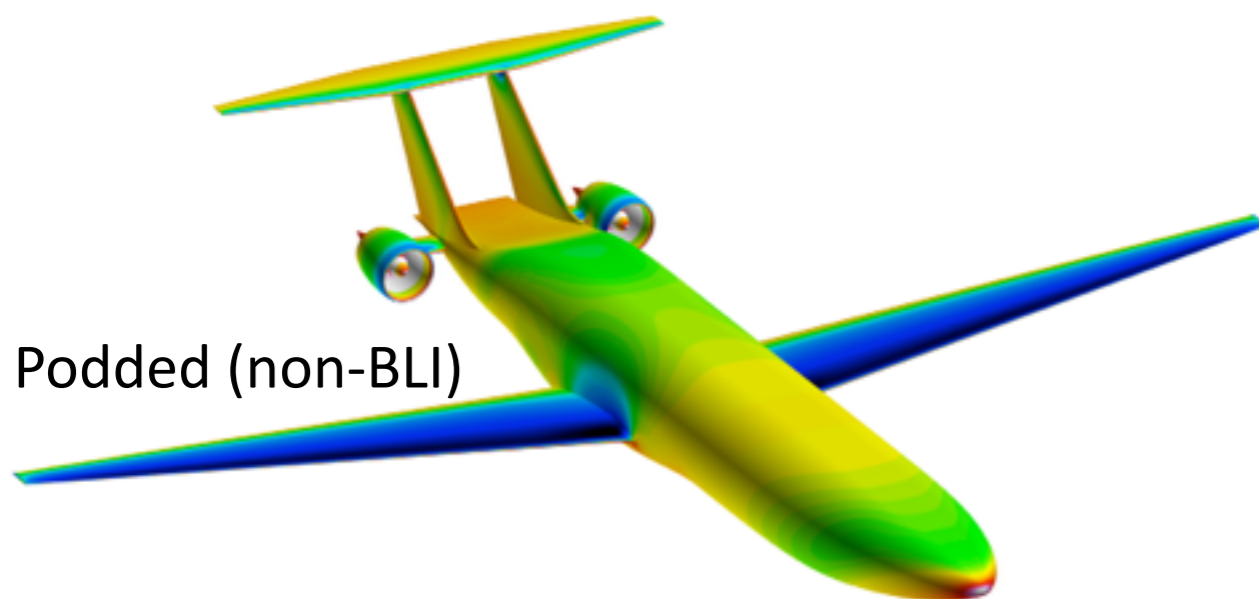
- Compare mechanical flow power

$$P_K = \oint_{propulsor} (p_{t,\infty} - p_t) (\mathbf{V} \cdot \hat{\mathbf{n}}) dA .$$

–Power transmitted by propulsor to the flow

- Savings in power required: integrated vs. podded

$$\text{BLI benefit} \equiv \frac{P_{K_{\text{non-BLI}}} - P_{K_{\text{BLI}}}}{P_{K_{\text{non-BLI}}}} \Bigg|_{\text{at given } F_X}$$







# WT Configurations



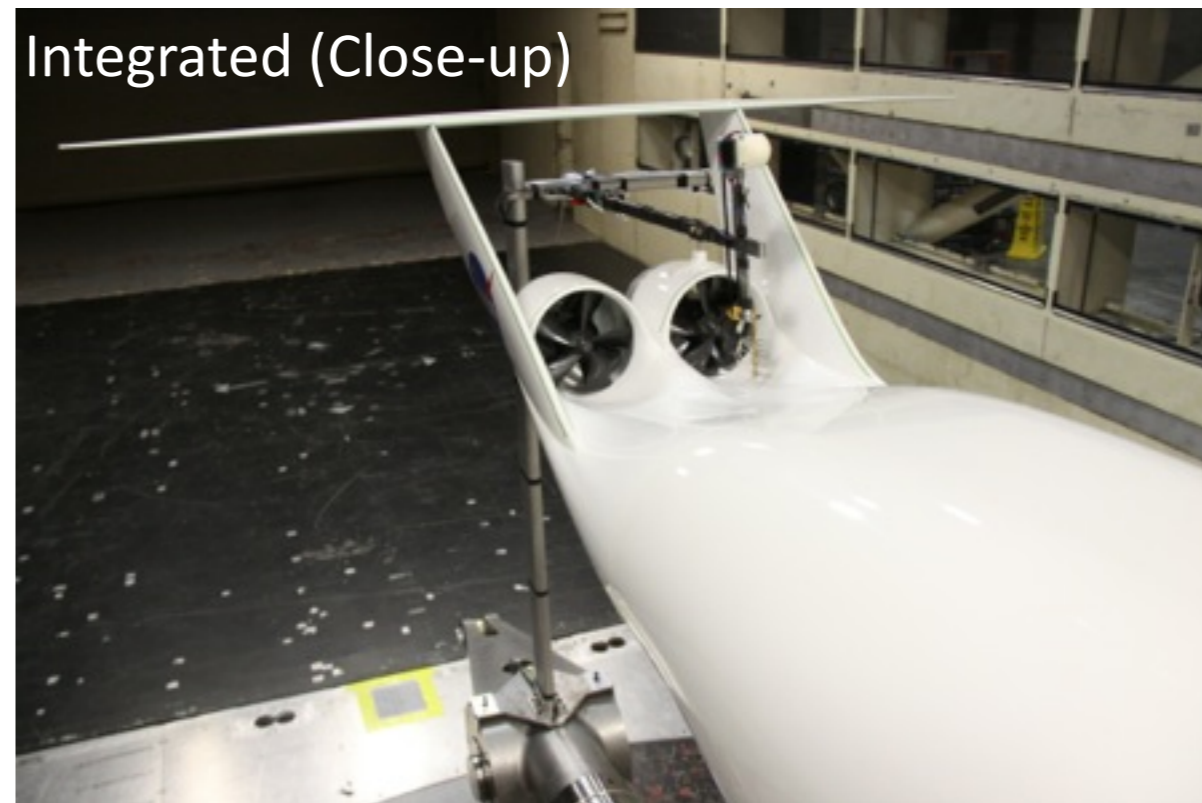
Unpowered



Podded



Integrated



Integrated (Close-up)

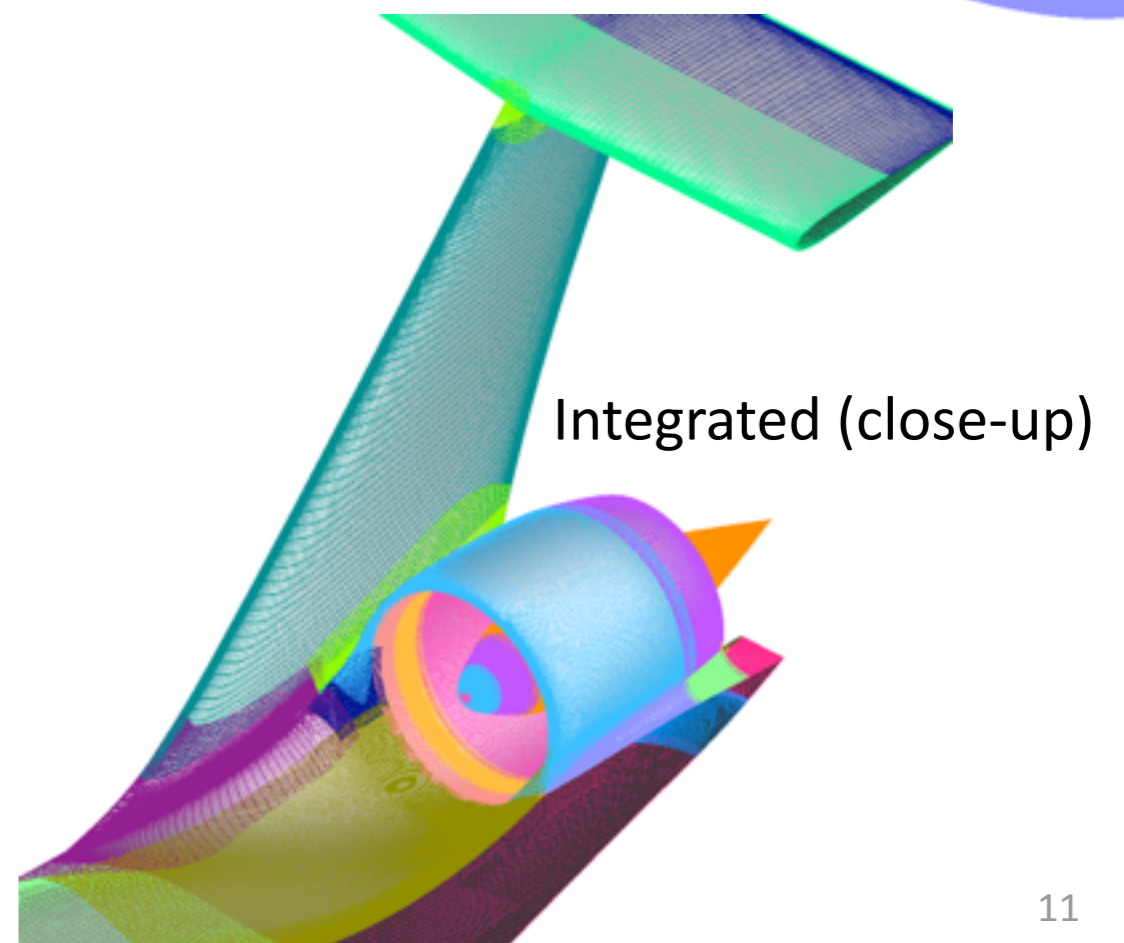
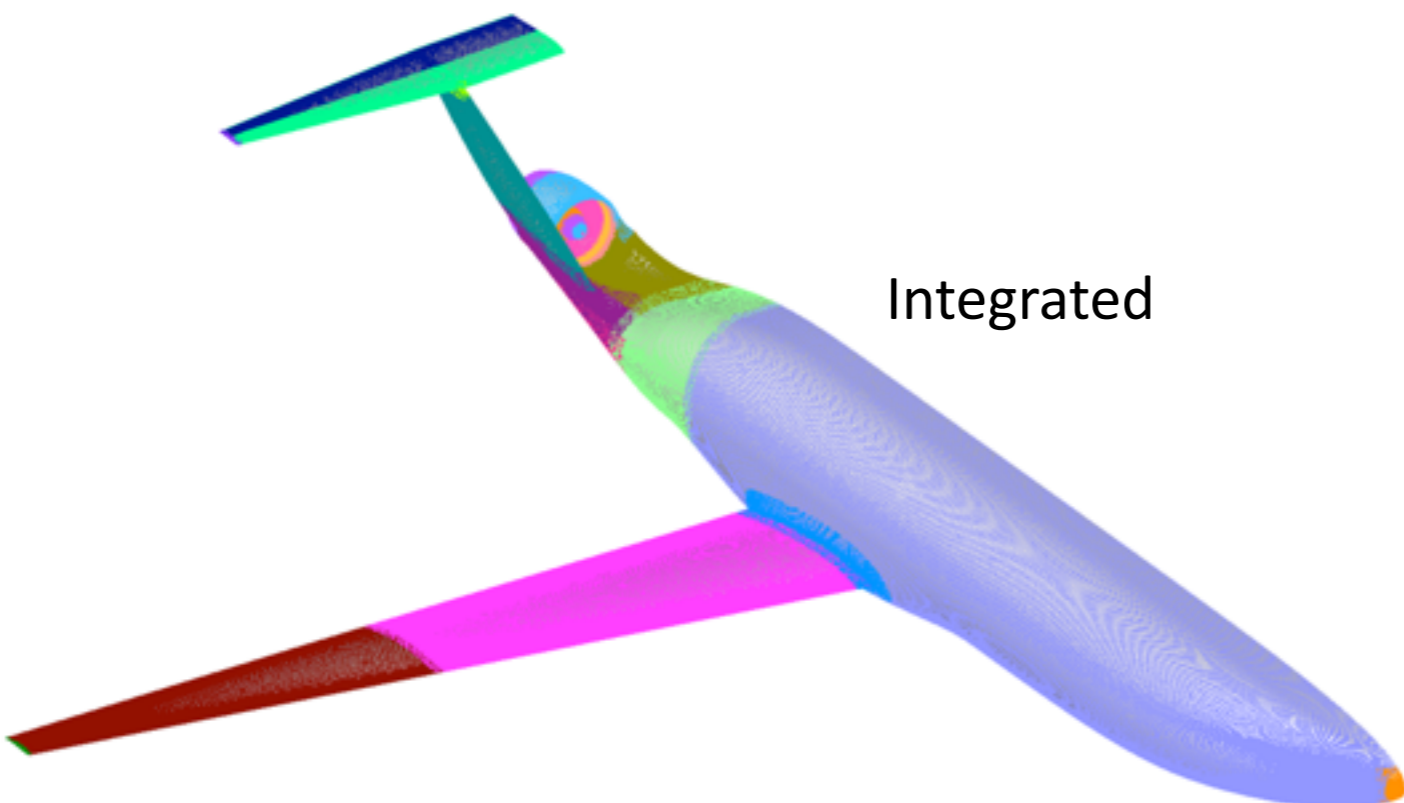
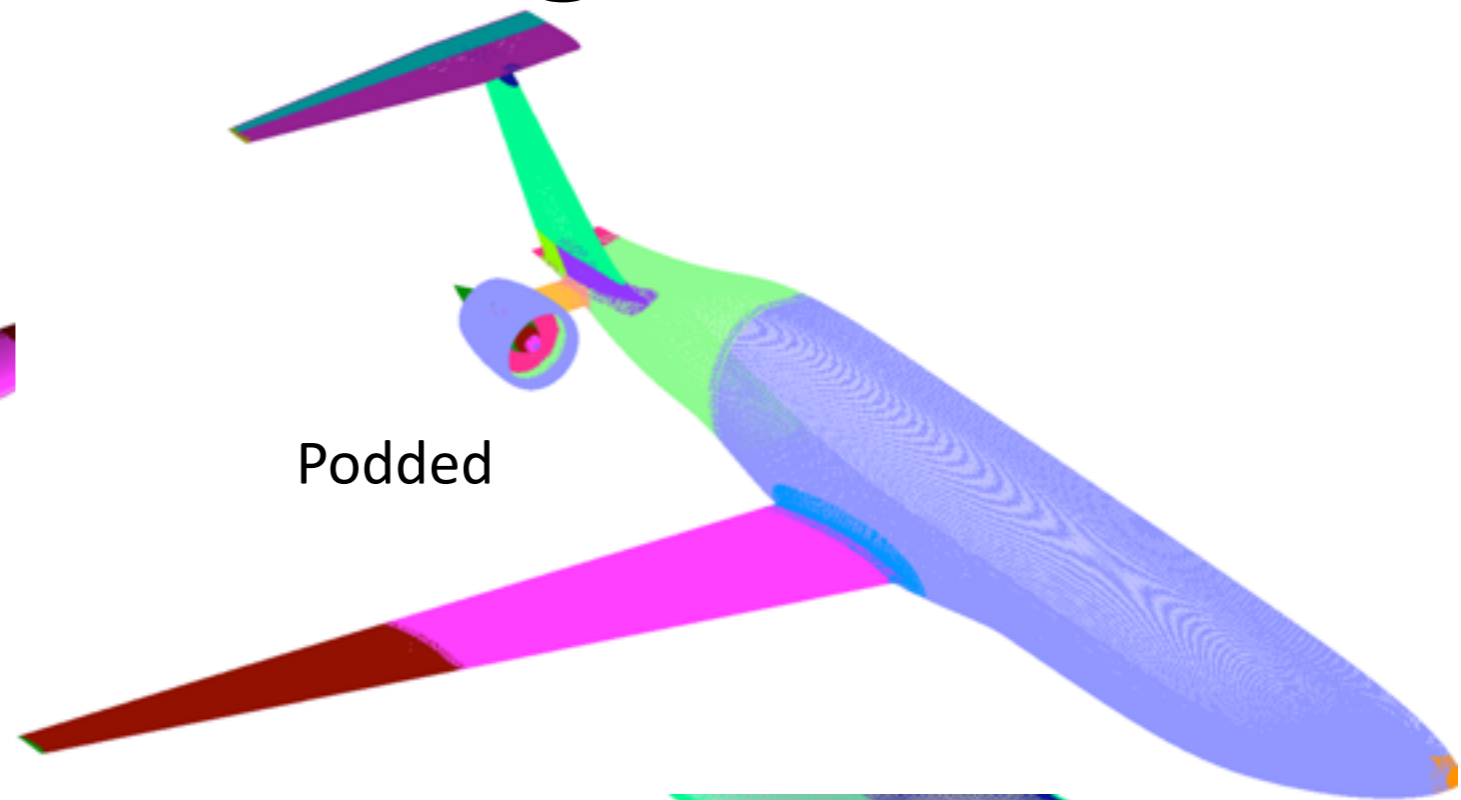
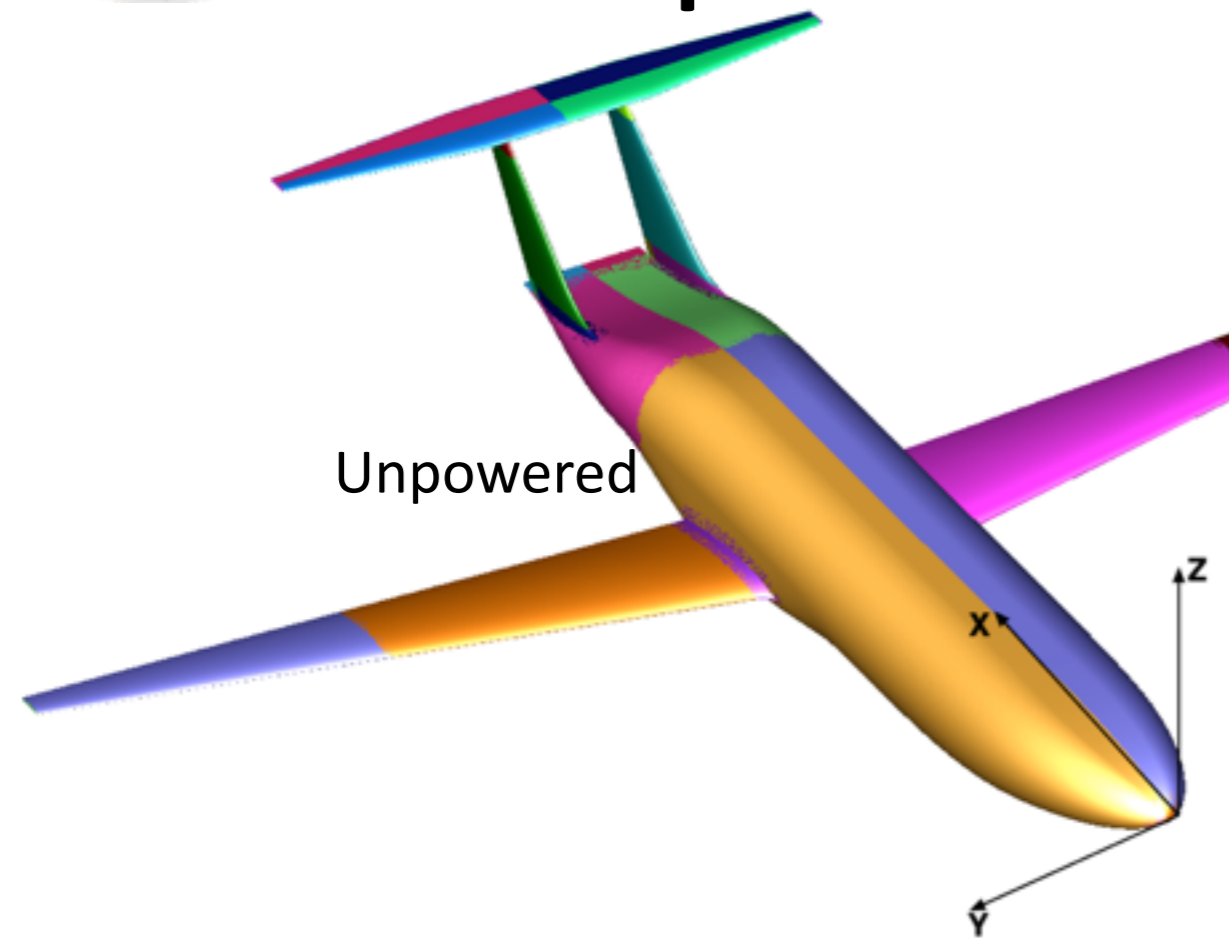


# Configuration Details

- WT runs at 70 mph,  $Re_c = 570,000$ 
  - lower-speed and Re compared to full-size at  $M=0.72$
- 1:11 Scale powered model
- Wing designed for low Mach, low Re
- Same wings
- Most of fuselage is the same
- Same propulsors plug into both podded and integrated configuration empennage sections



# Computational Configurations





# Computational Mesh

- Chimera Grid Tools

- Overset surface and volume mesh

- Same grids for forward fuselage, wing, and WT

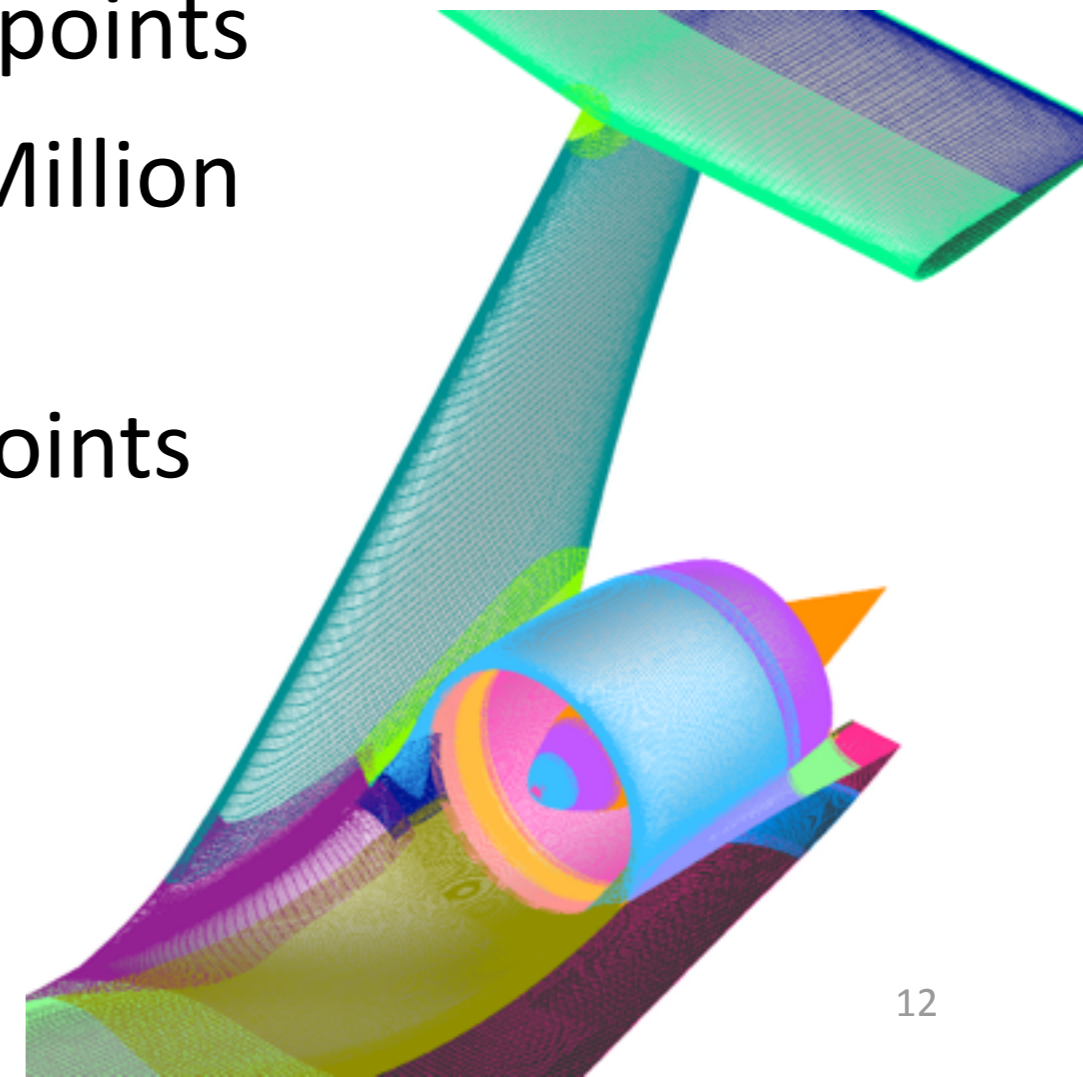
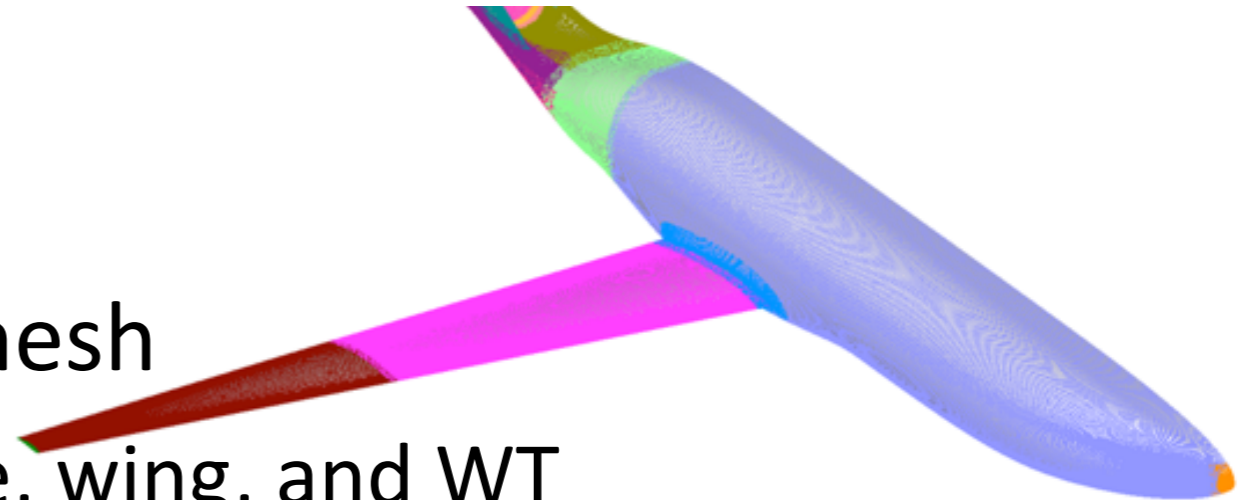
- Unpowered: 36 grids, 113 Million points

- Podded: 13 additional grids (~15 Million more points)

- Integrated: 64 grids, 135 Million points

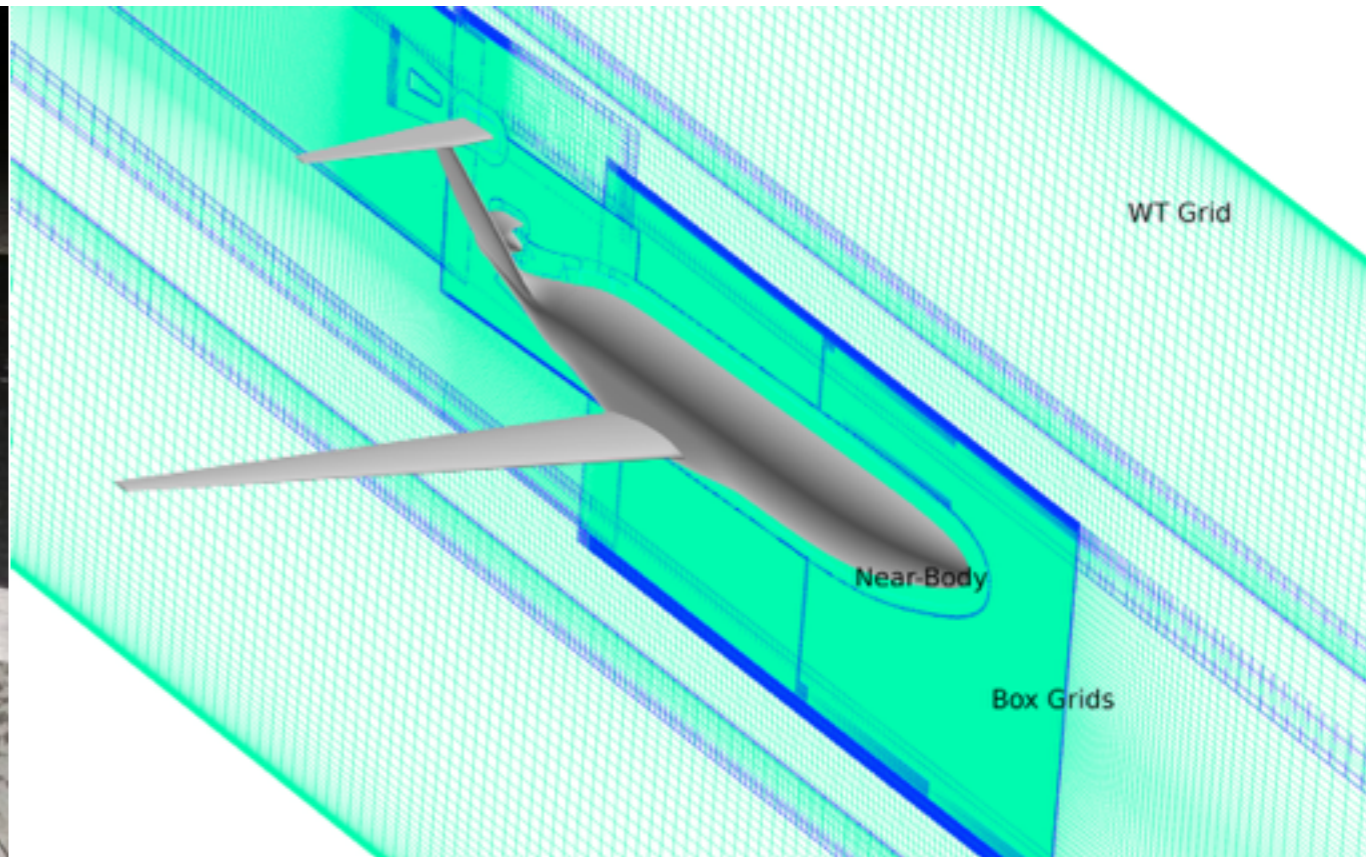
- No mounting hardware

- $y^+ \approx 0.7$





# D8 Model



Blue indicates regions of overlap

- Larc 14x22 WT model
  - 1:11 scale, Full body
  - Mounting hardware controls AoA

- Computational model
  - 1:11 scale, Half body
  - No mounting hardware
  - Inviscid walls



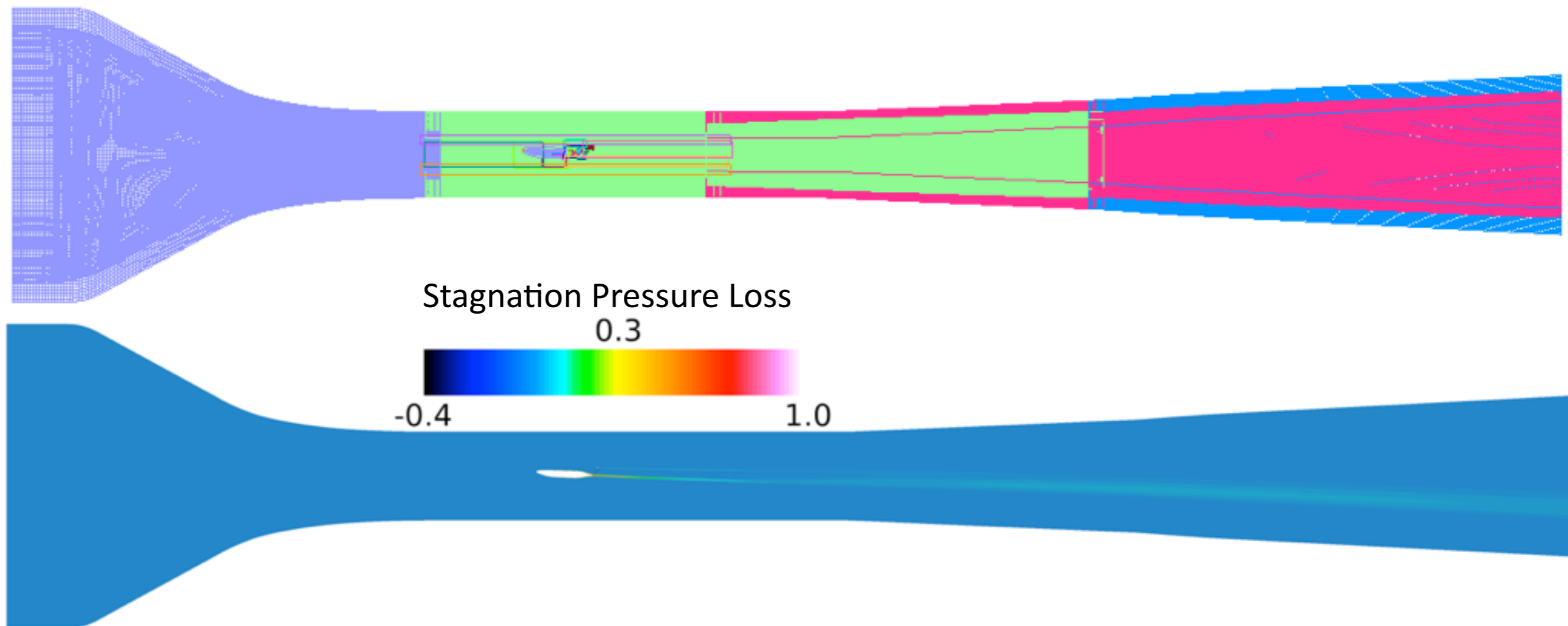
# CFD Solver

- **OVERFLOW**
  - 3D, RANS solver for overset structured grids
  - Diagonalized approximate factorization Scheme
  - 2nd order central difference + artificial dissipation
  - Matrix dissipation
  - RANS SST turbulence model
- **Flow Conditions**
  - Mach=0.088
  - Re = 44000/in.



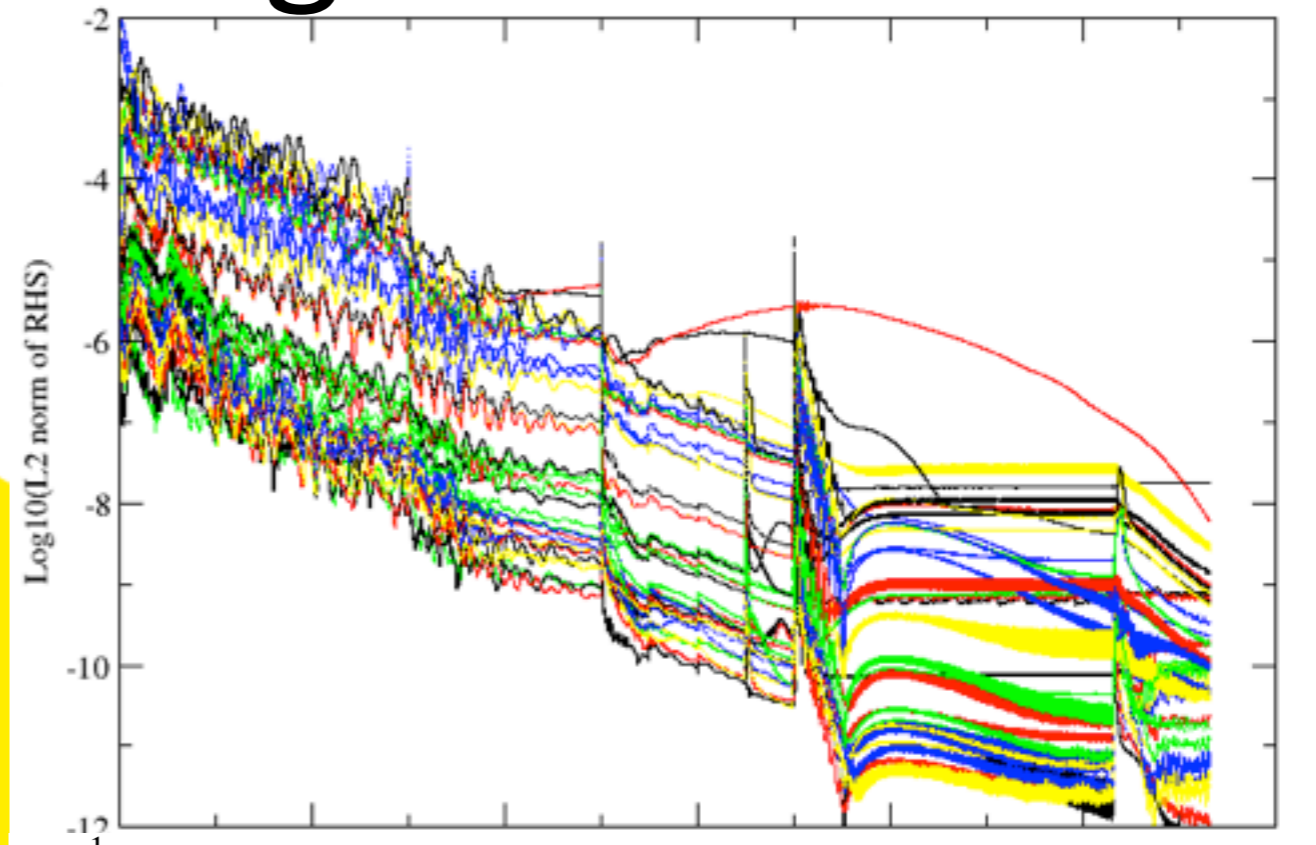
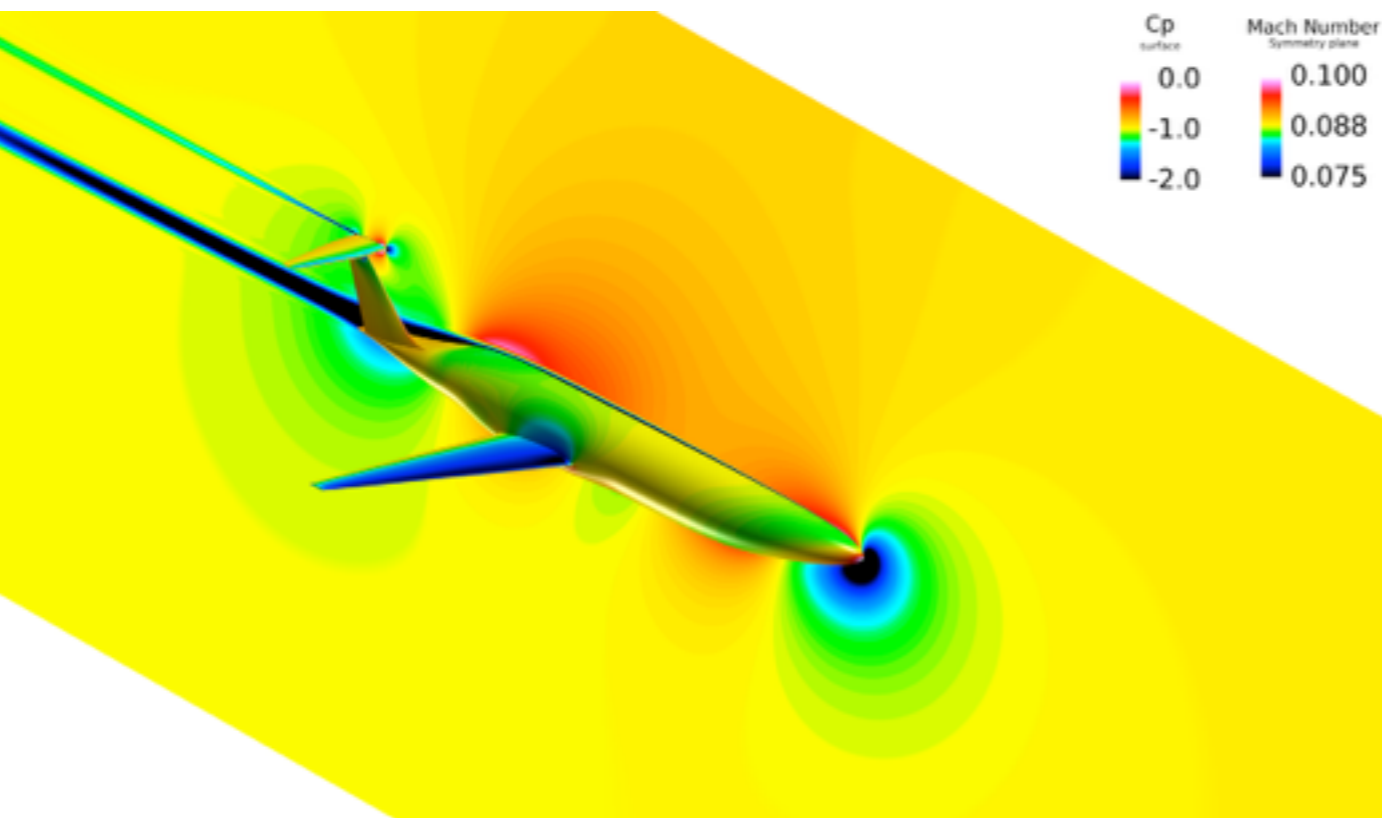
# Computational model for the WT

- Inviscid wall boundary condition
- 7 grids (4 wall grids, 3 core grids) + box grids
- Mach and Re number matched at pitot probe

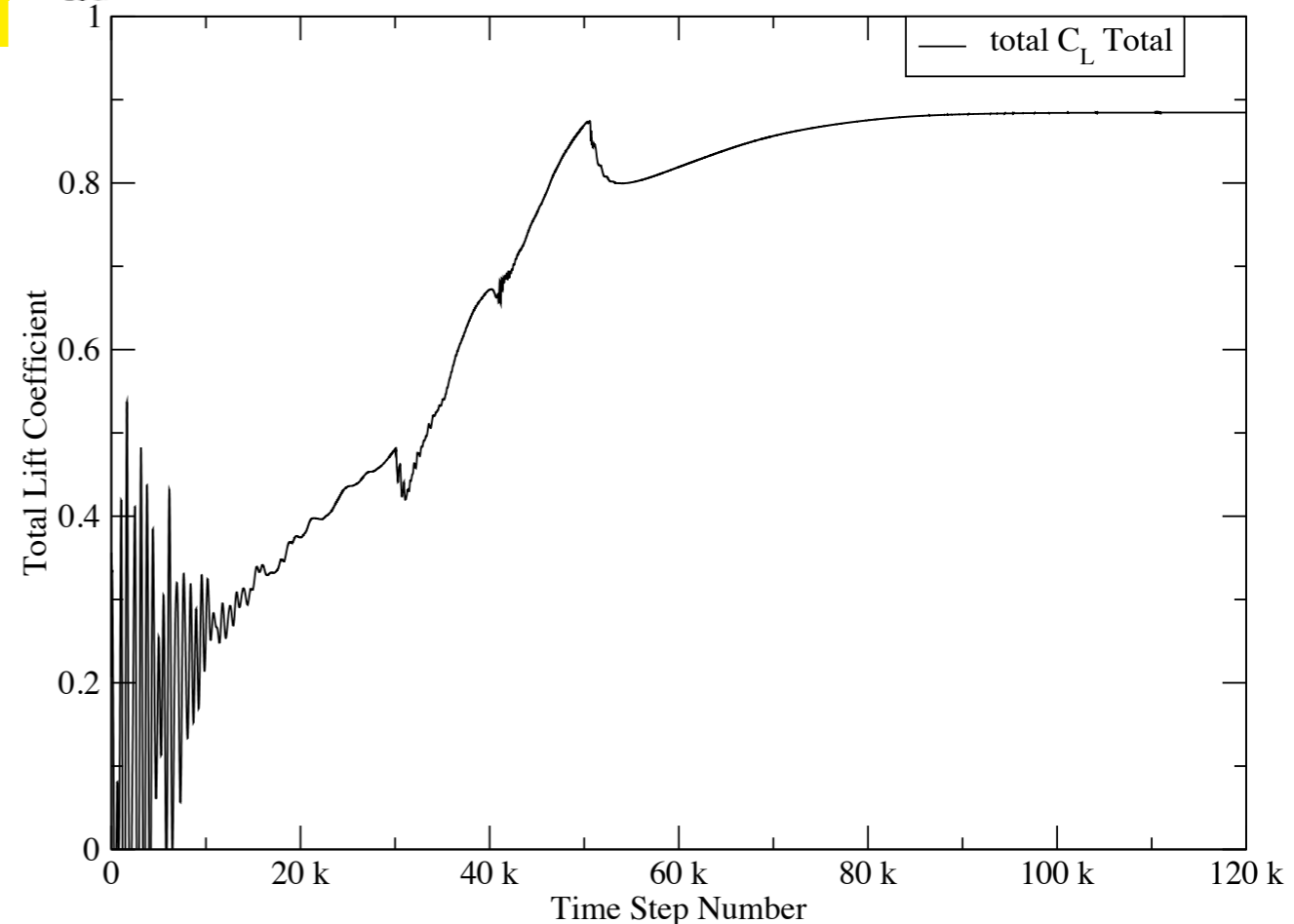




# Typical Convergence



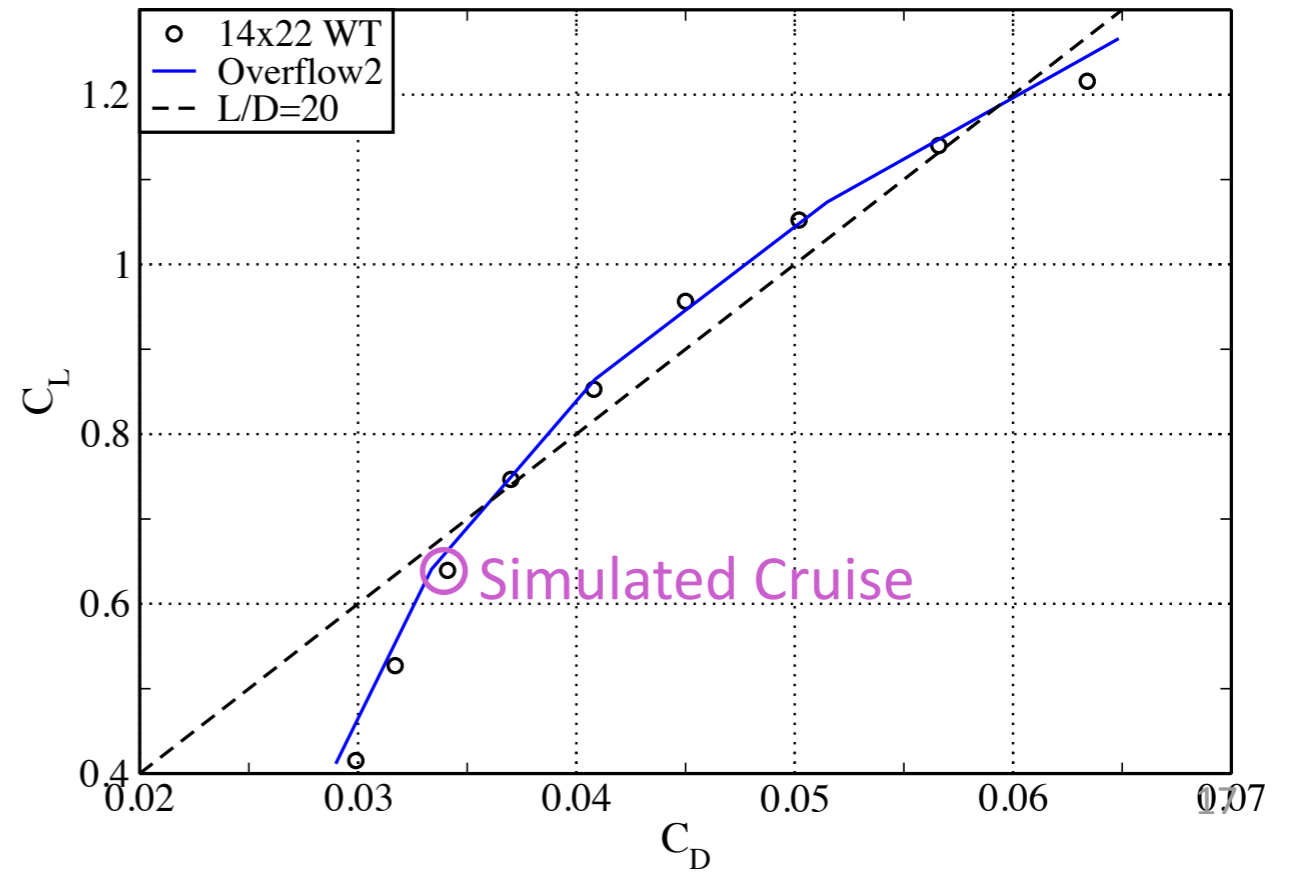
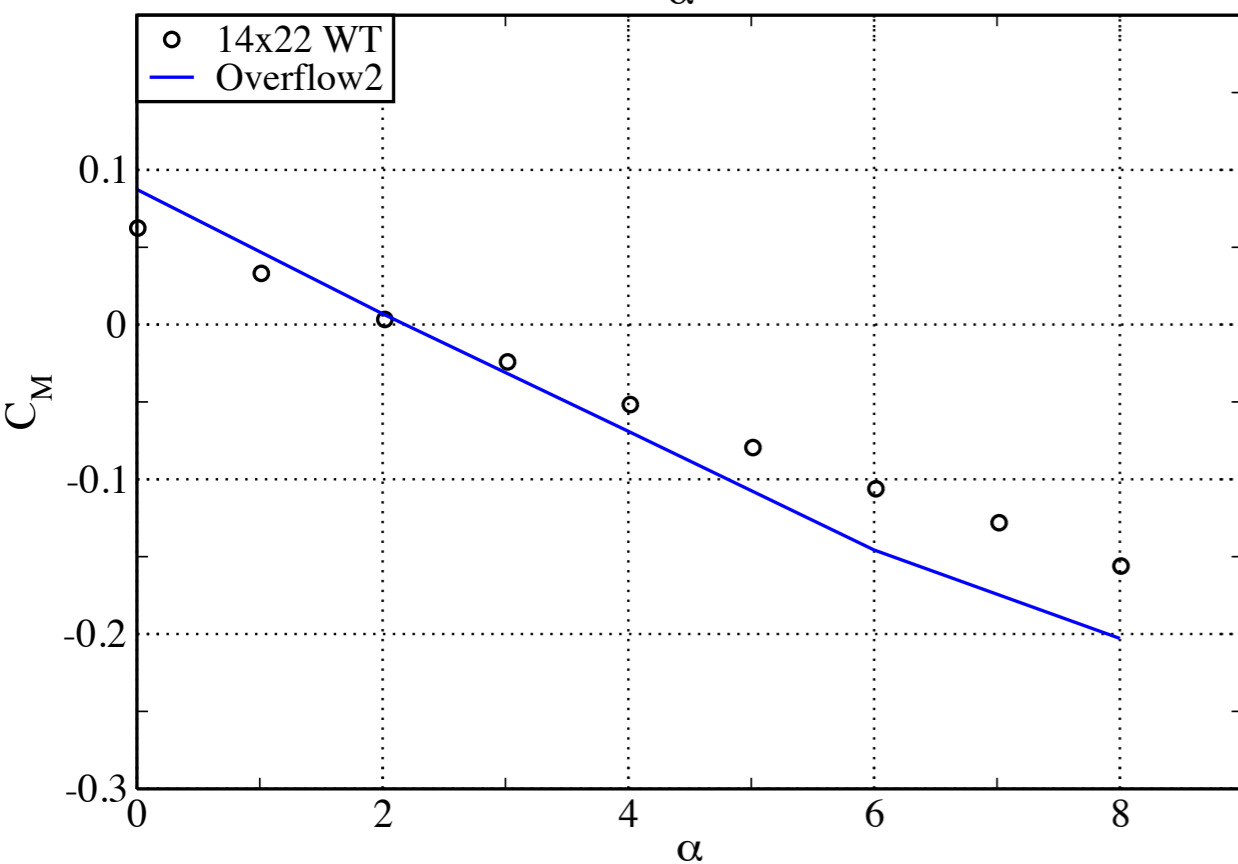
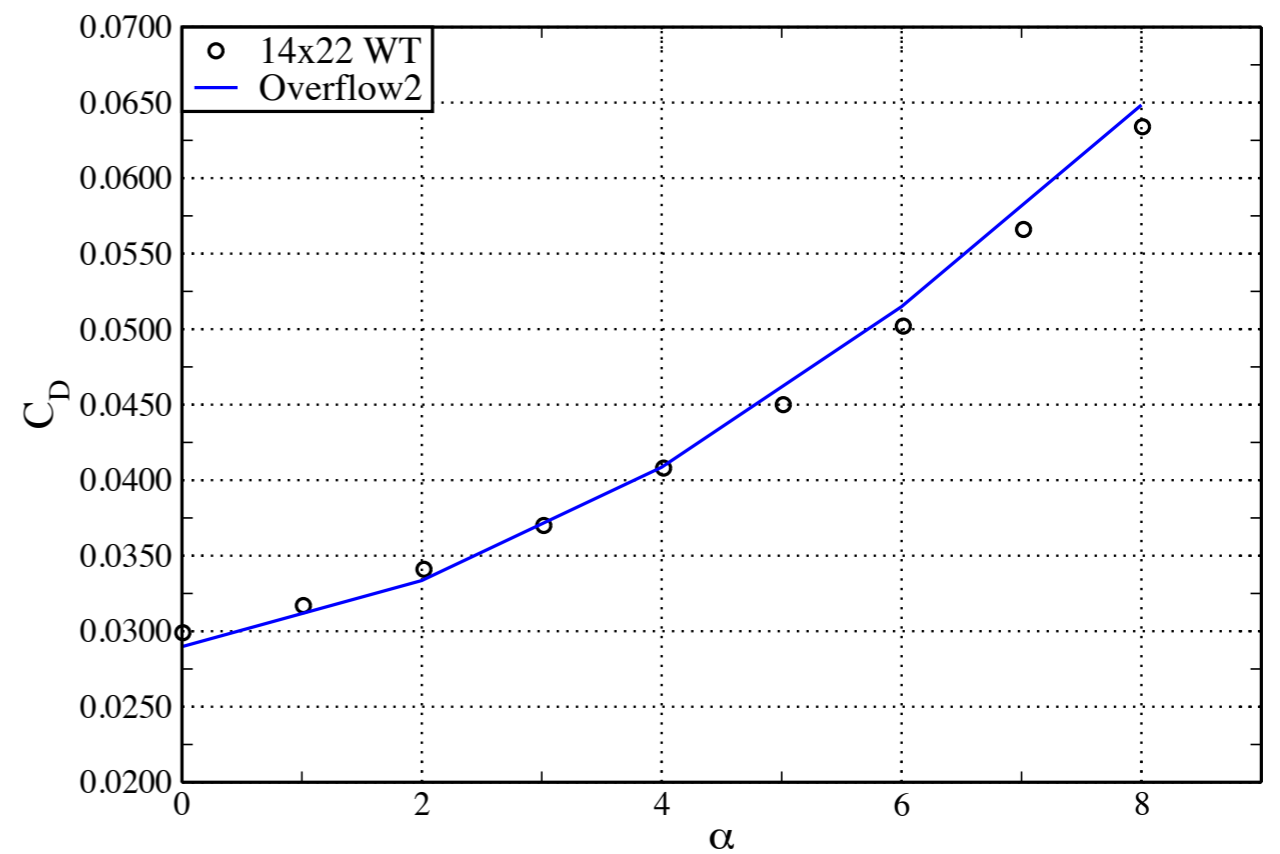
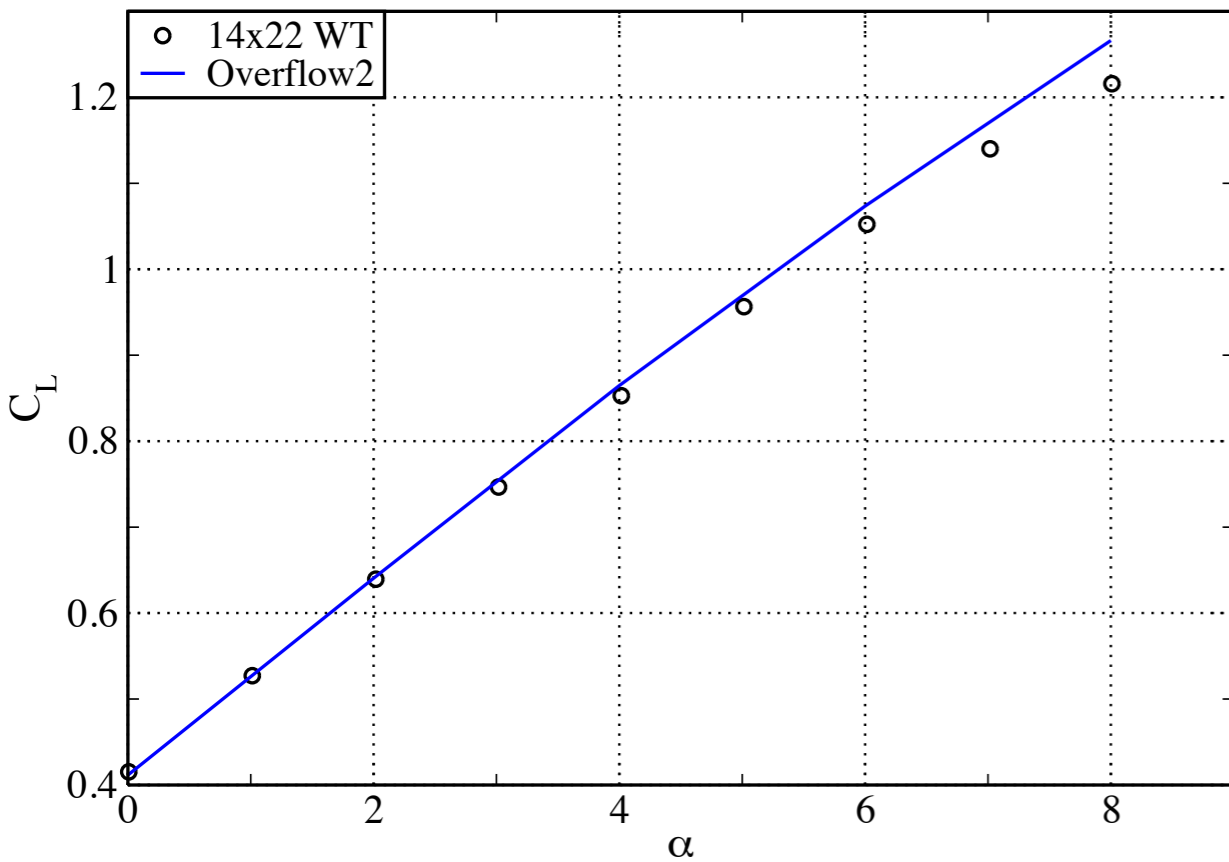
- Simulations without fans
- Alpha sweep
- Compare to Wind Tunnel (WT) test data
- Iterations to match Mach & Re at pitot probe







# Validation-unpowered





# Propulsor Inlet flow Comparison

$$\text{Total pressure coefficient } C_{p_t} = \frac{p_t - p_{t_\infty}}{q_\infty}$$

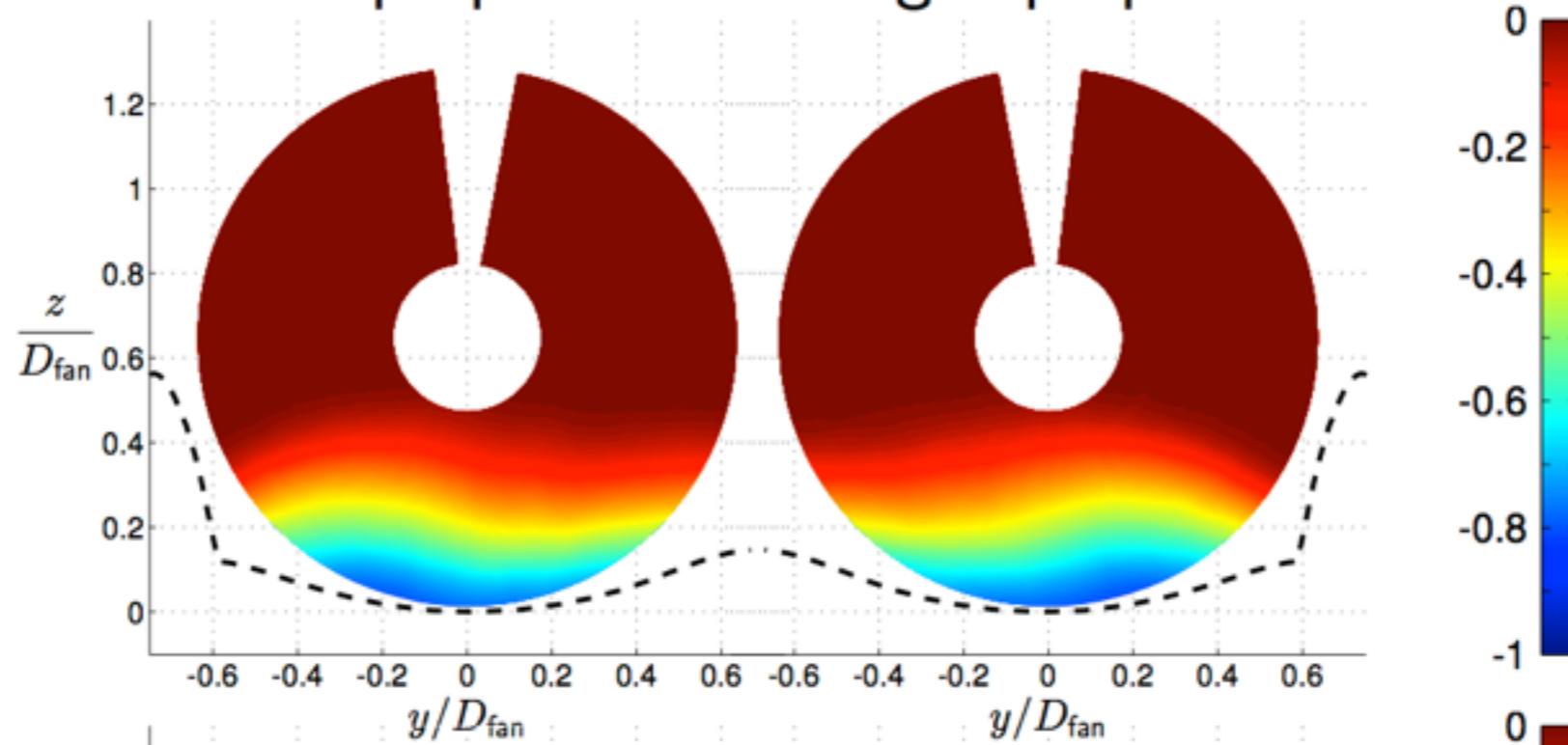
Integrated Configuration

AOA=2°

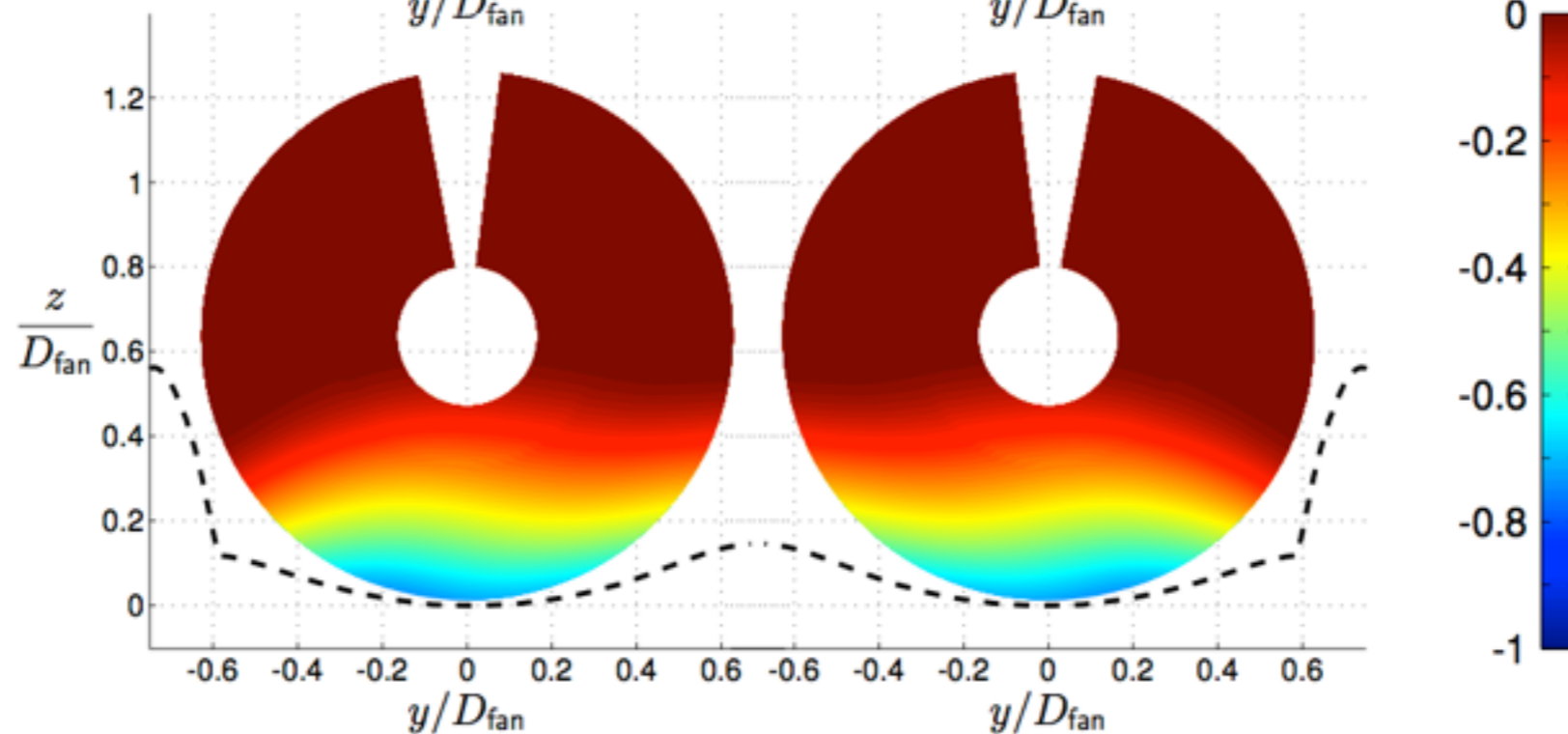
14x22 WT

Left propulsor

Right propulsor



Overflow





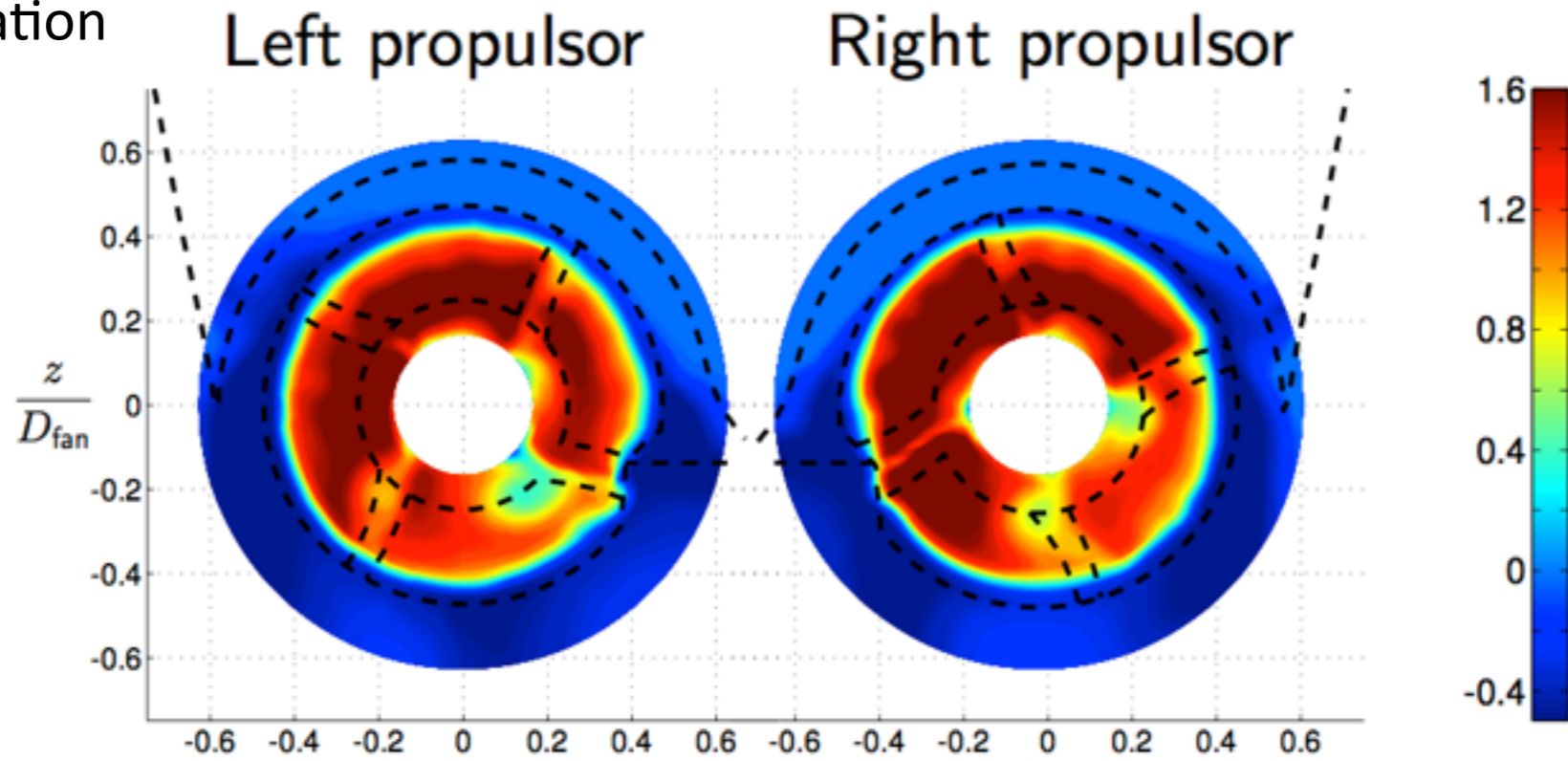
# Propulsor Exit flow Comparison

$$\text{Total pressure coefficient } C_{p_t} = \frac{p_t - p_{t_\infty}}{q_\infty}$$

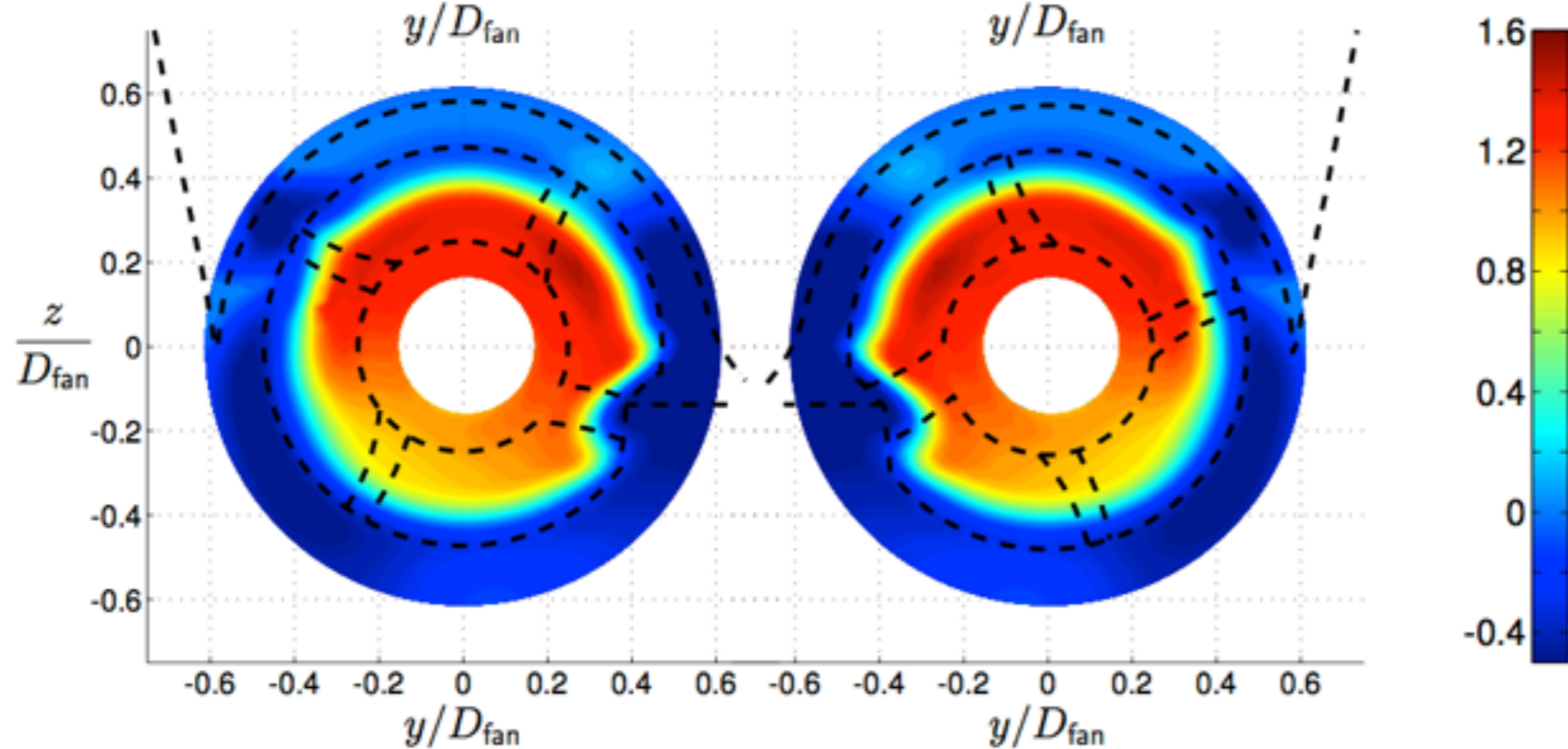
Integrated Configuration

AOA=2°

14x22 WT



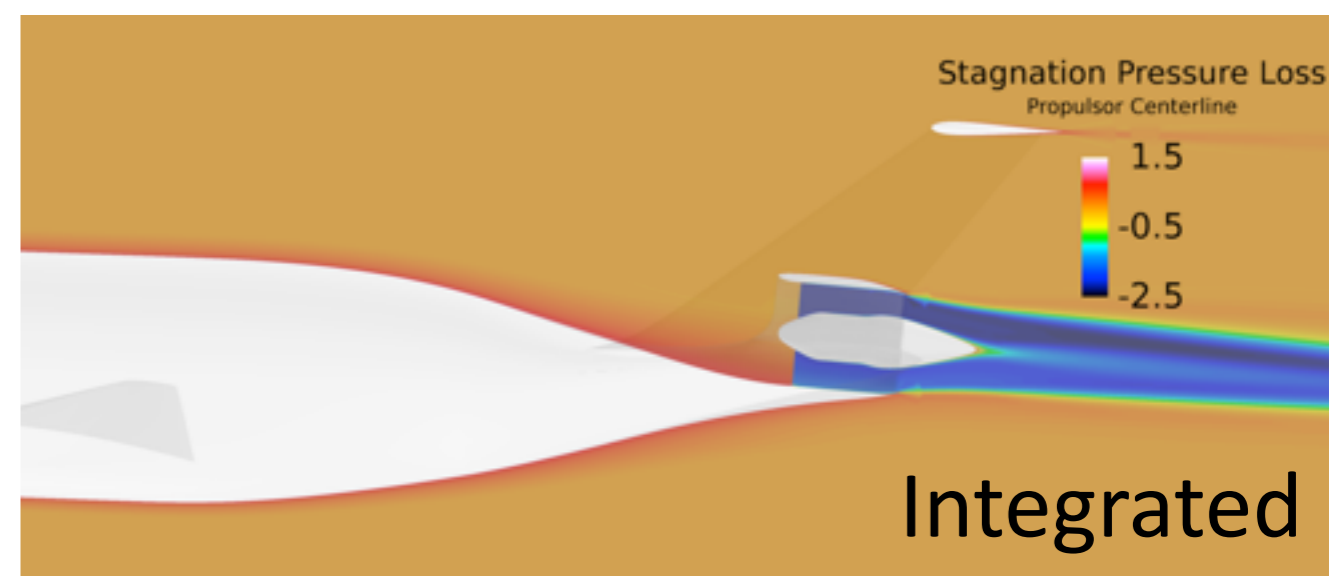
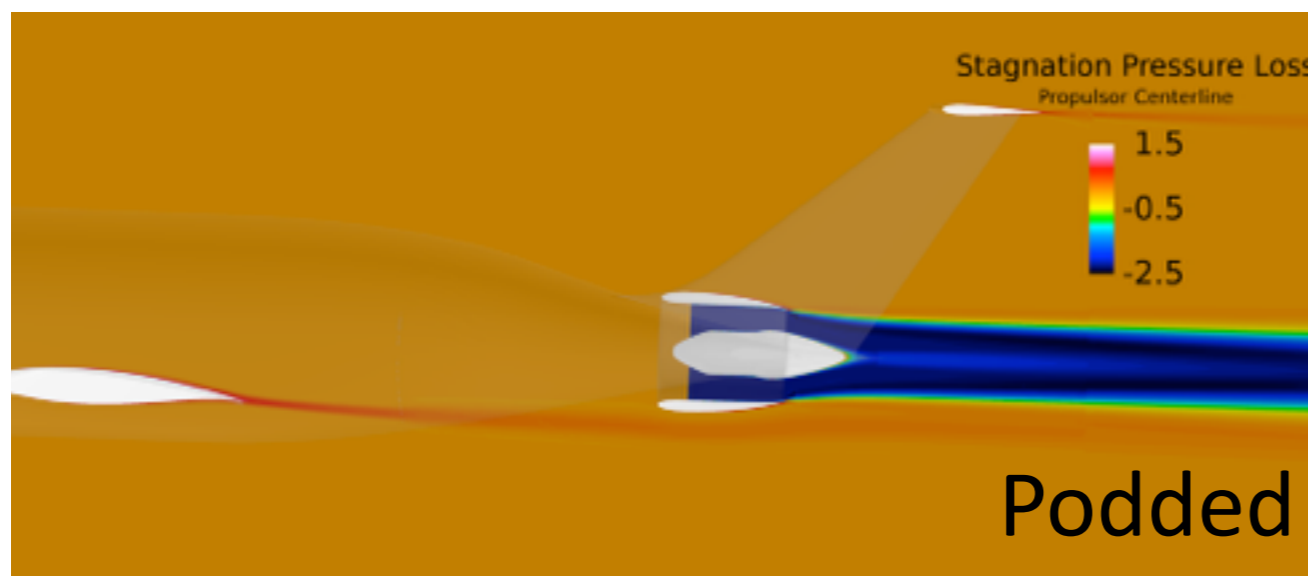
Overflow





# Fan Model and its Effect

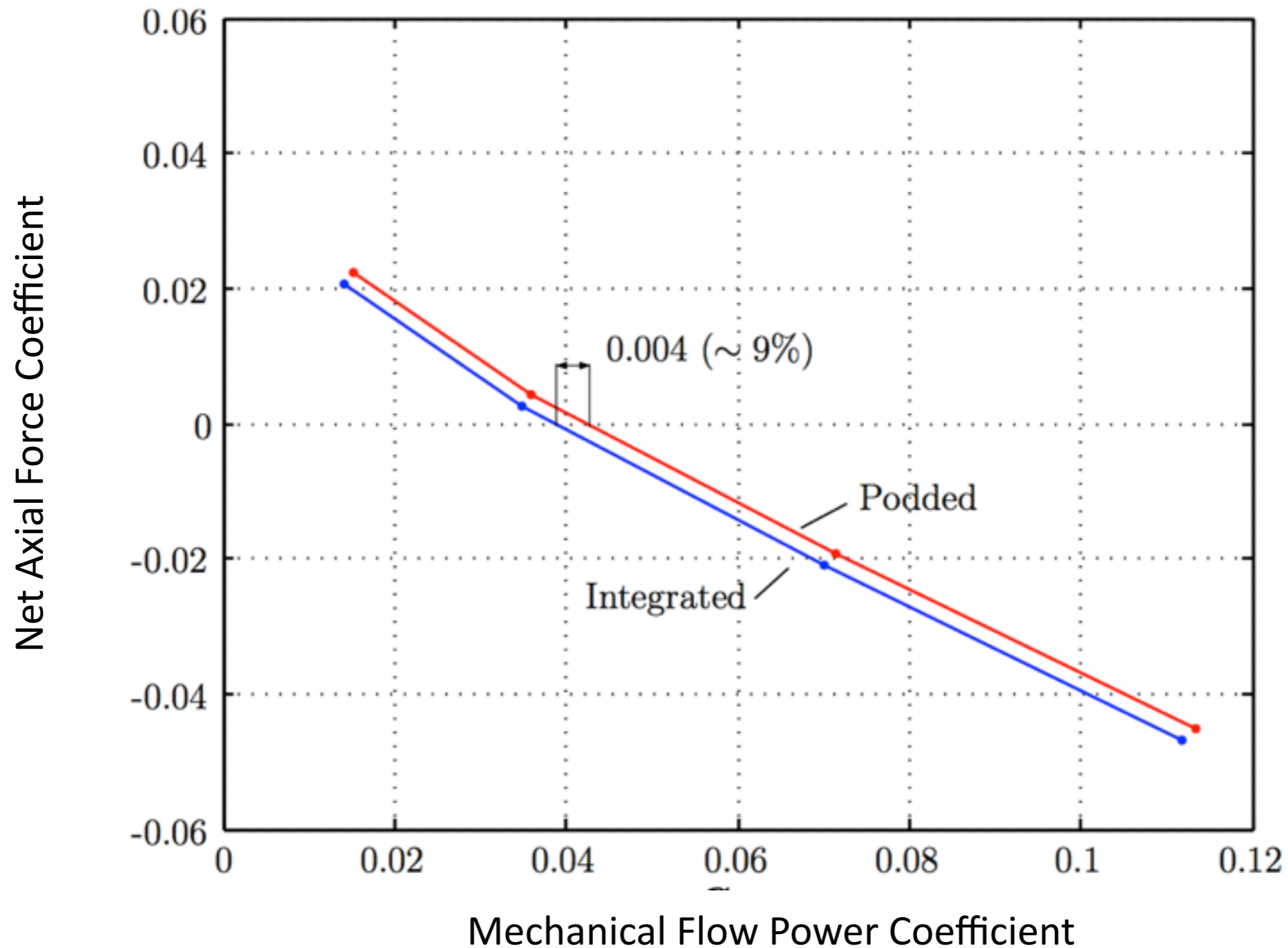
- Actuator disk
  - Uniform pressure jump
- Four cases with increasing pressure jump settings
  - For both podded and integrated
  - Integrated sees a lower mass flow



Cuts through propulsor centerline.

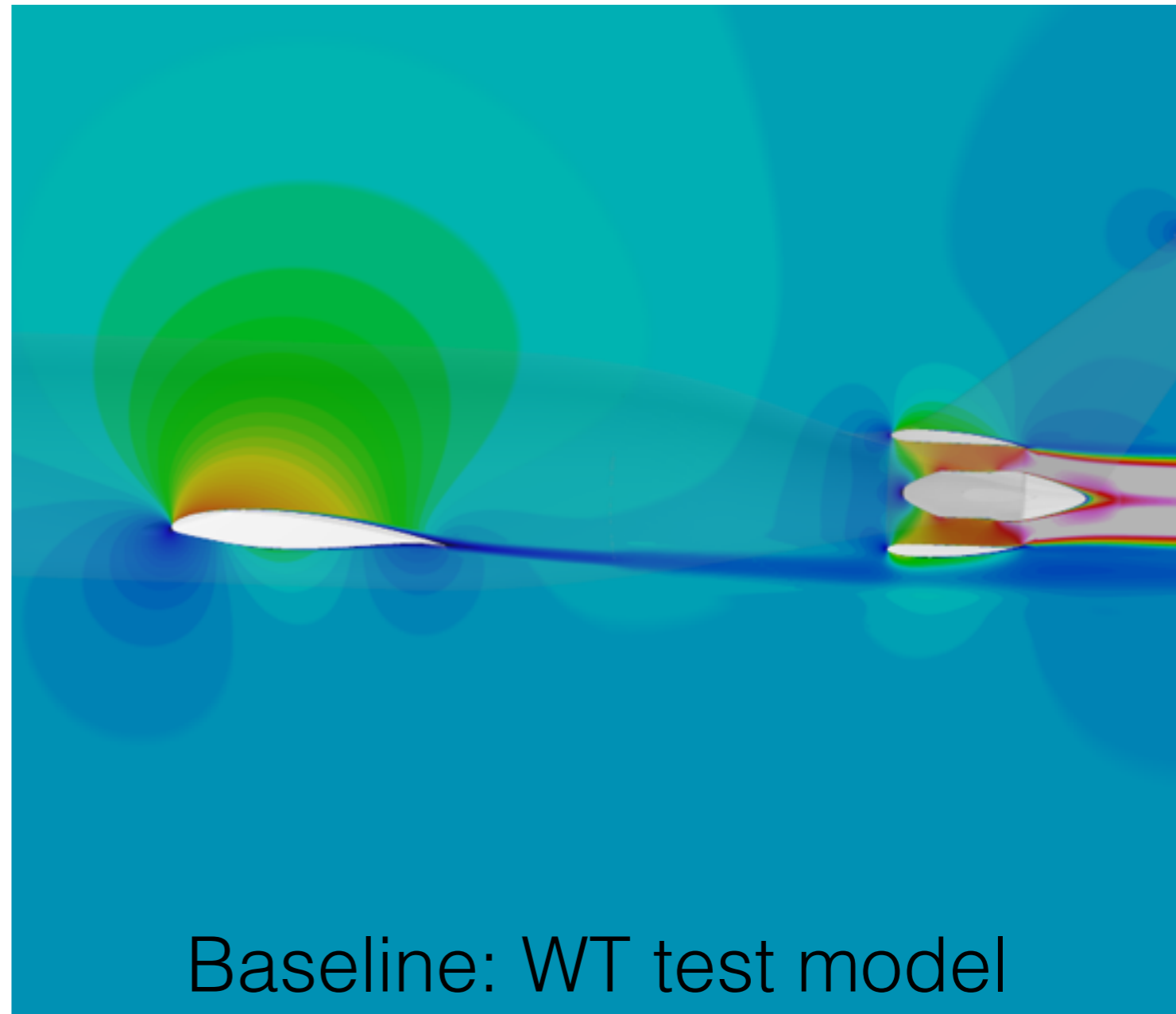


# Benefit of BLI (Computational)



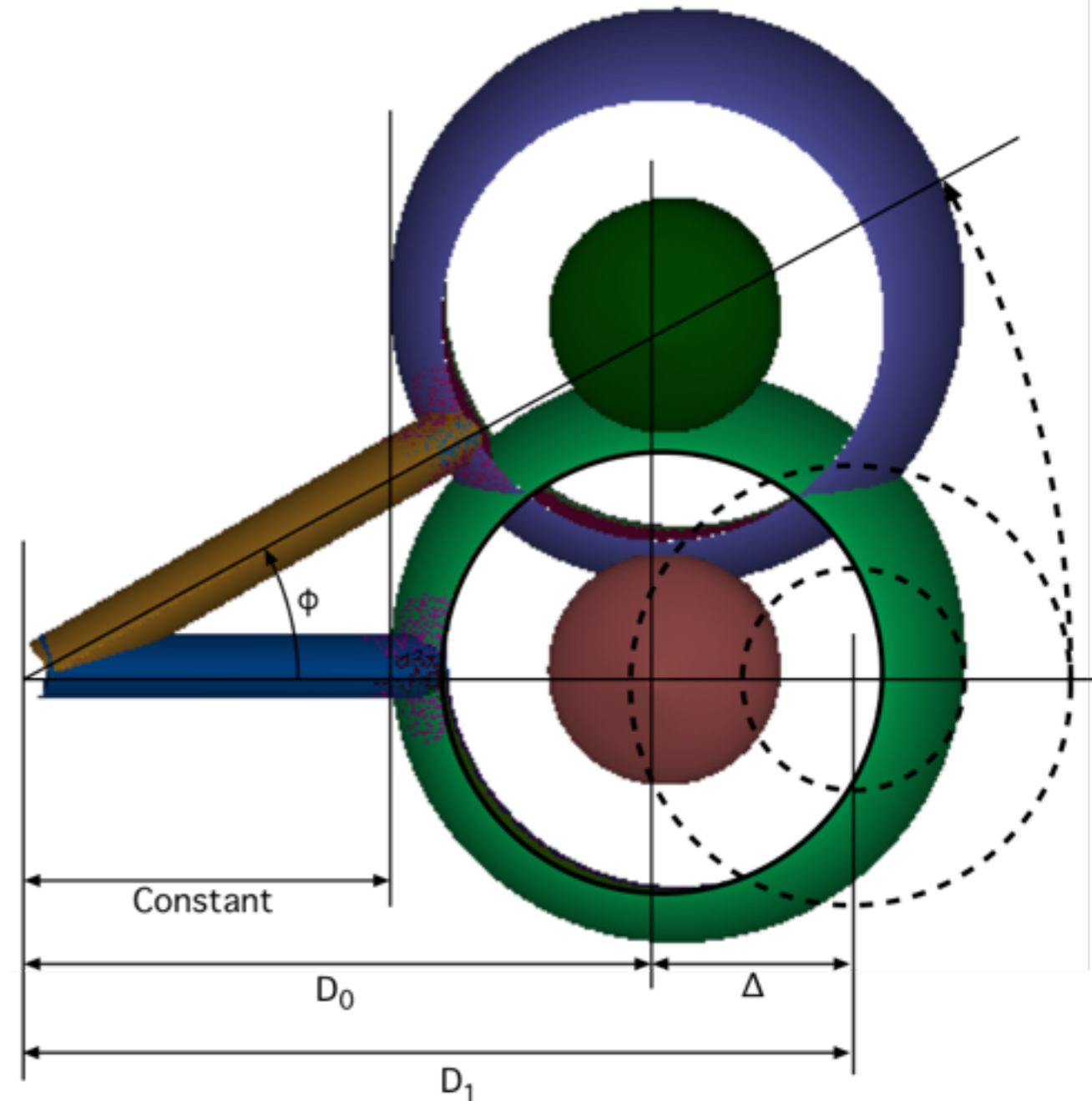
# Wake Ingestion

- Previous podded nacelle almost ingested the wing wake
- Can we move the nacelle out of the way?
- What is the effect of nacelle movement on BLI?

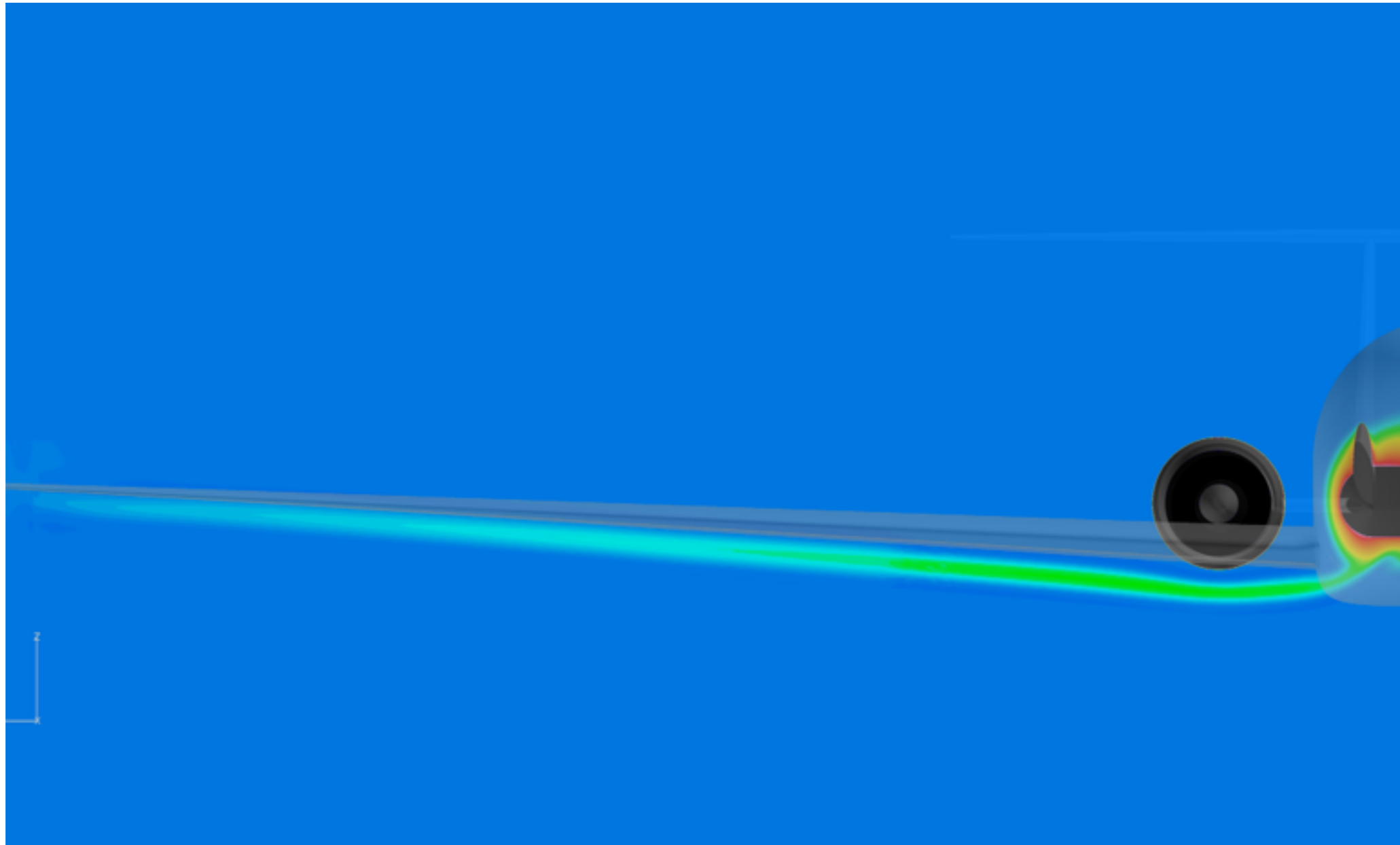


# Test Matrix

- Deflect the nacelle up and down ( $-20^\circ, -10^\circ, 0^\circ, 10^\circ, 20^\circ, 30^\circ$ )
- Power setting: closest to WT test setting
- Keep the outboard position and toe angle unchanged
- Compare to the baseline case
- $\Delta = D_1 - D_0 = D_0(1/\cos \theta - 1)$
- Translate by  $\Delta$ , then rotate by  $\theta$

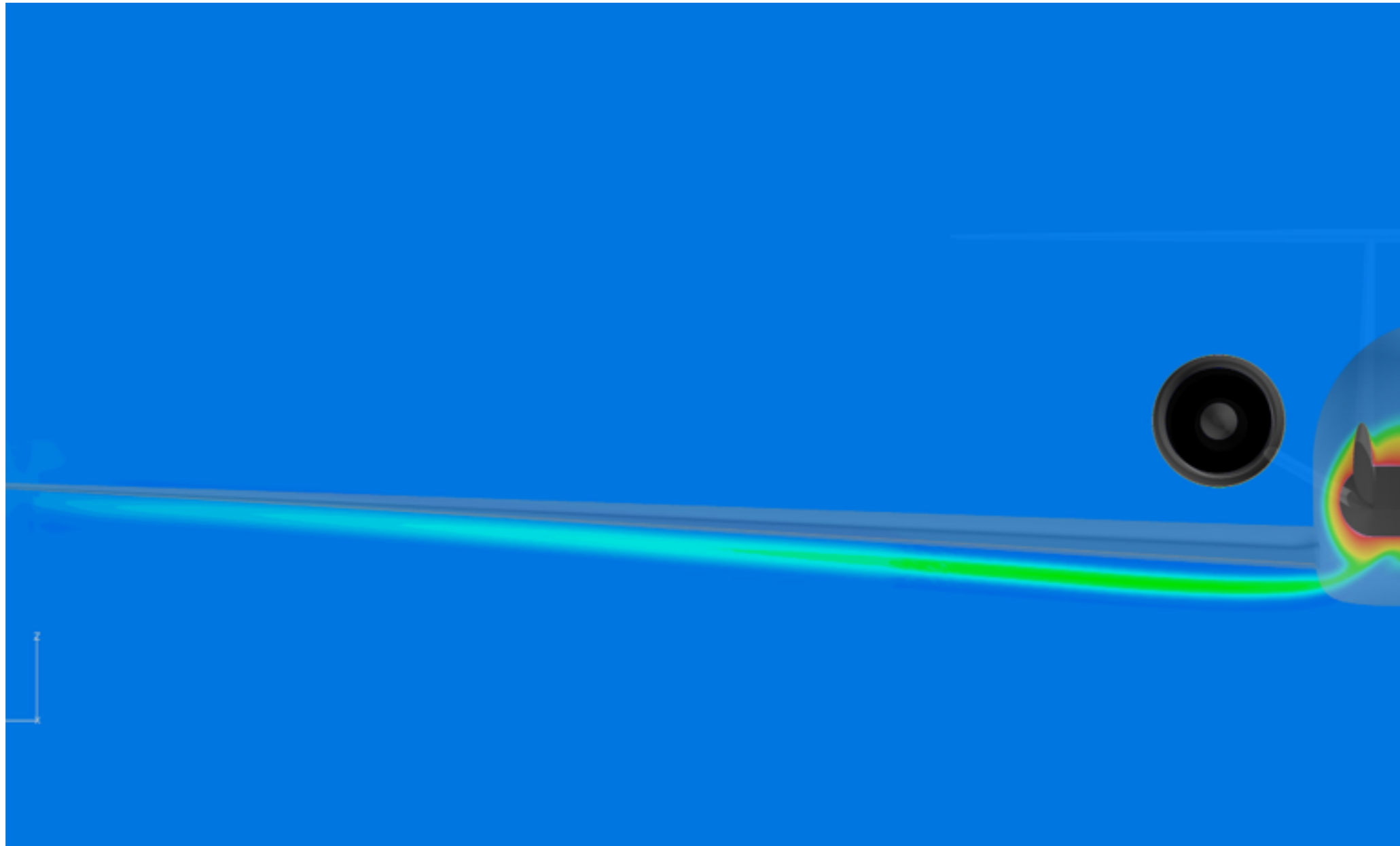


# Stagnation Pressure Loss ( $\phi=0^\circ$ ) prior to entering the nacelle

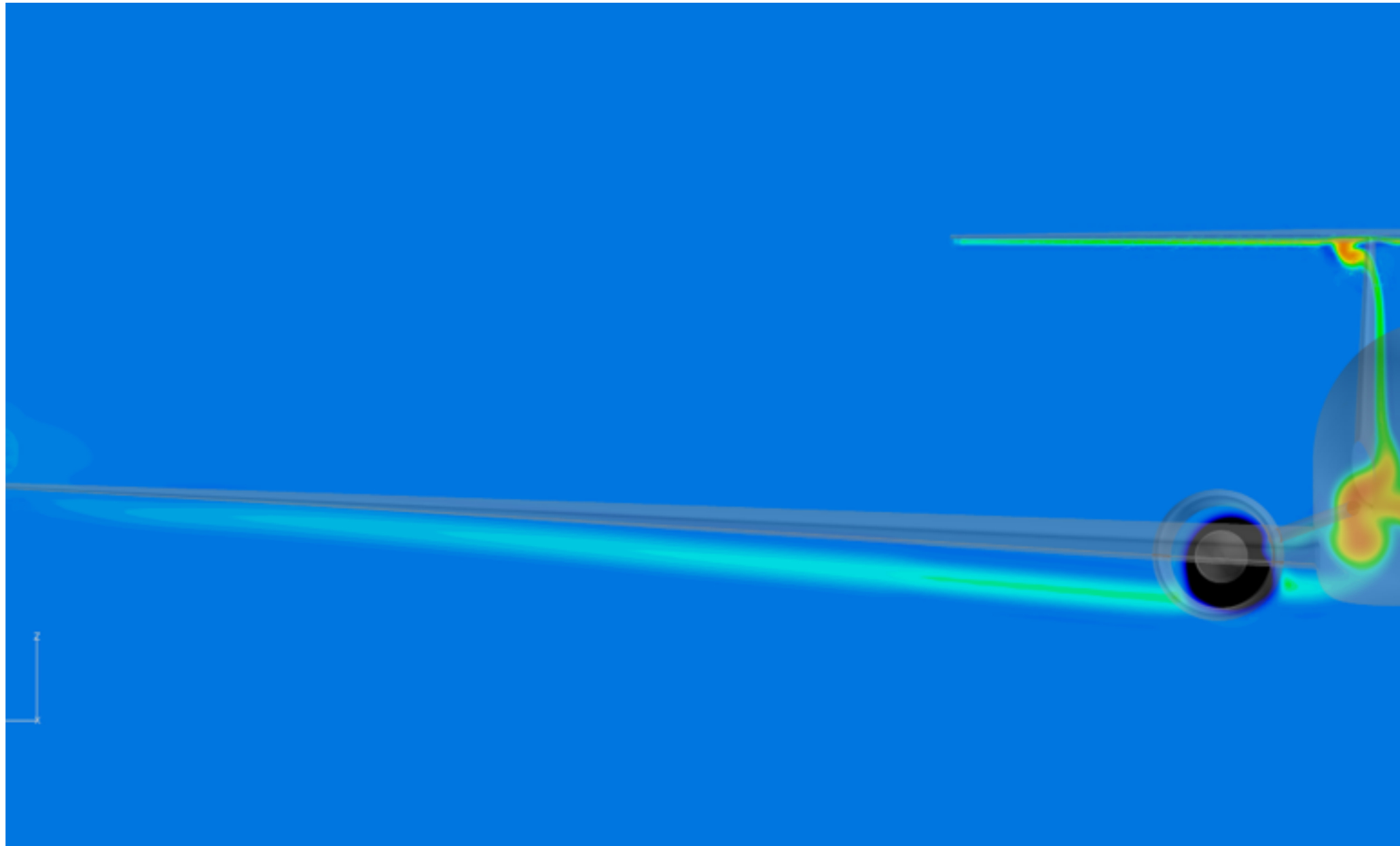


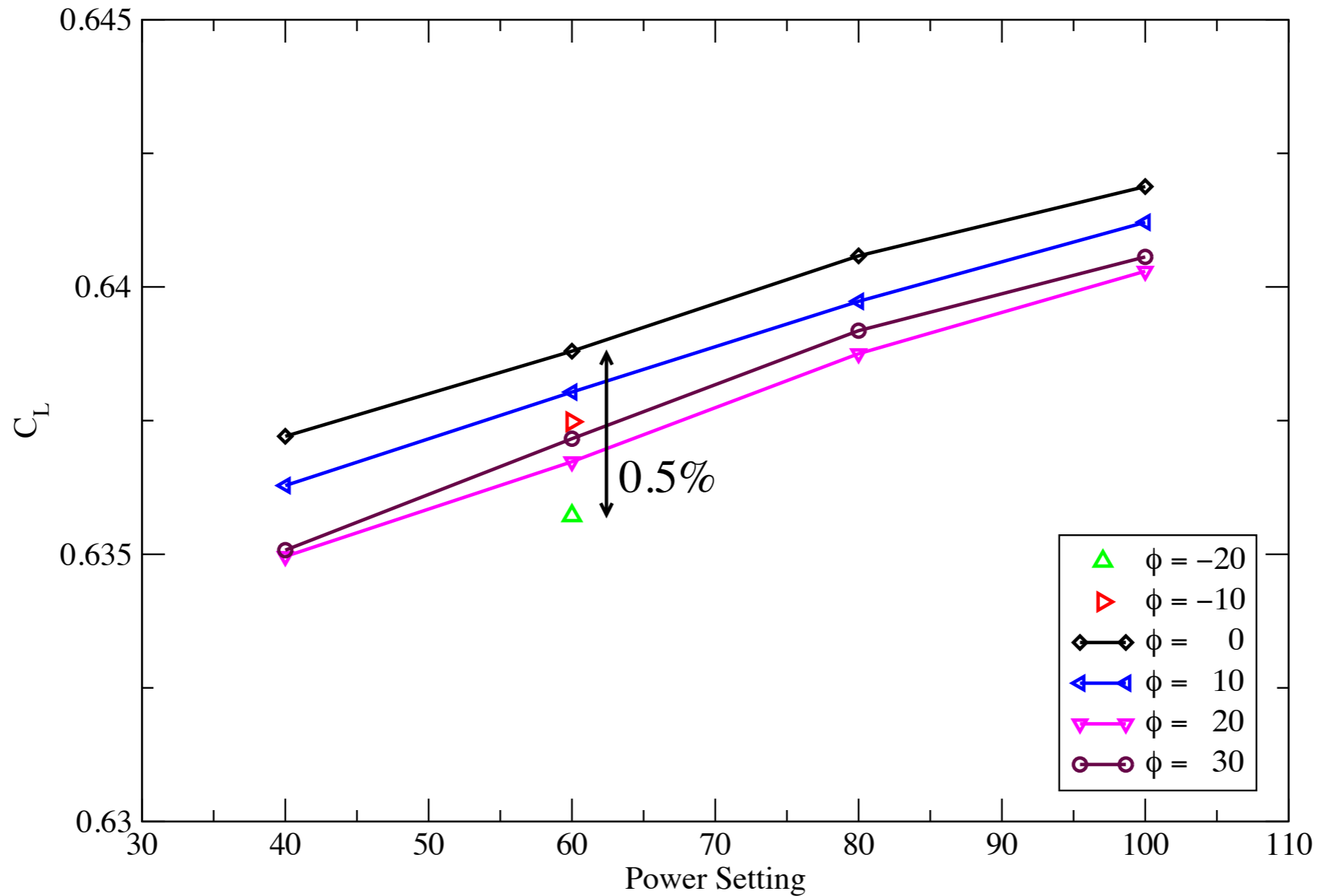


# Stagnation Pressure Loss ( $\phi=30^\circ$ ) prior to entering the nacelle



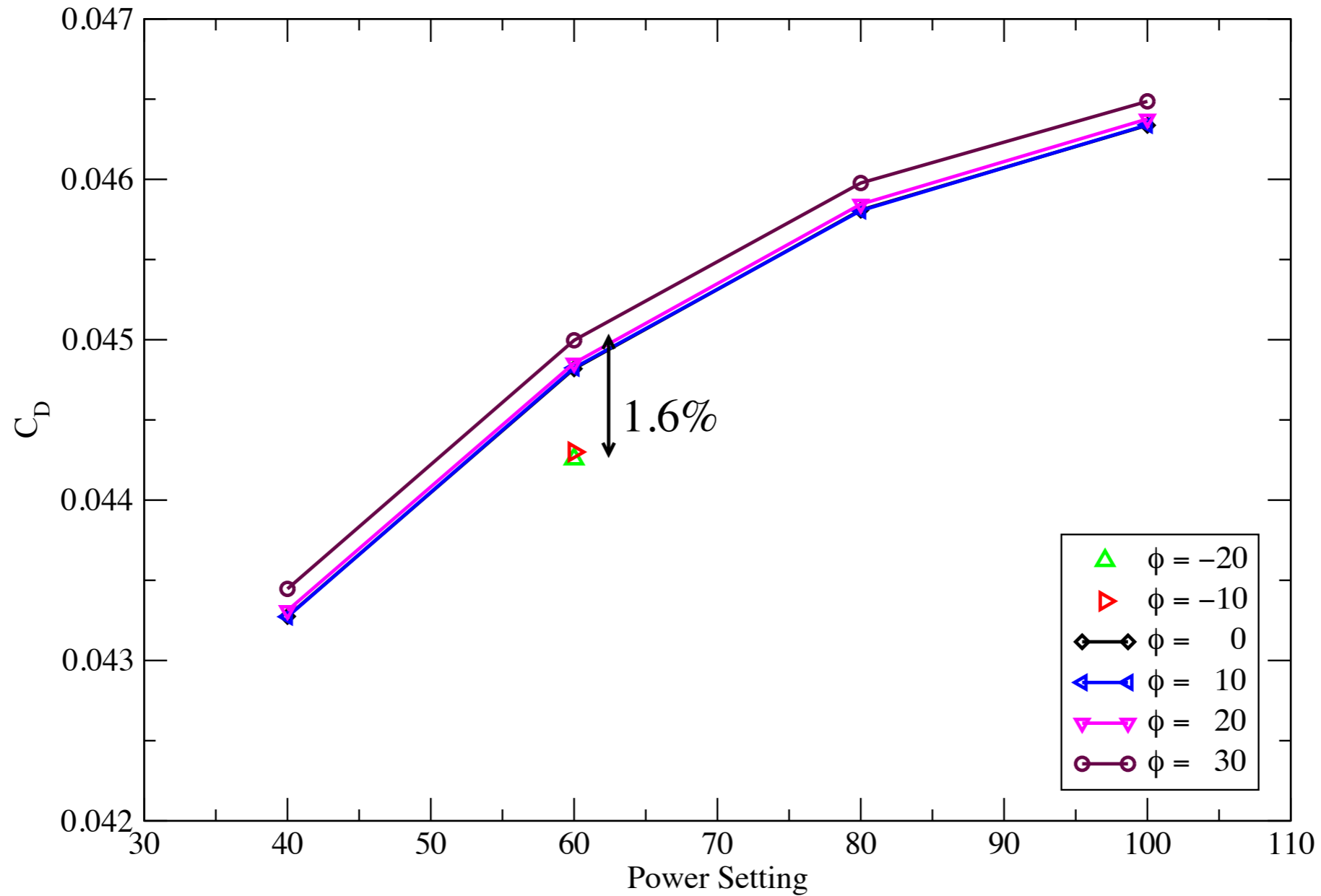
# Stagnation Pressure Loss ( $\phi = -20^\circ$ ) behind the nacelle





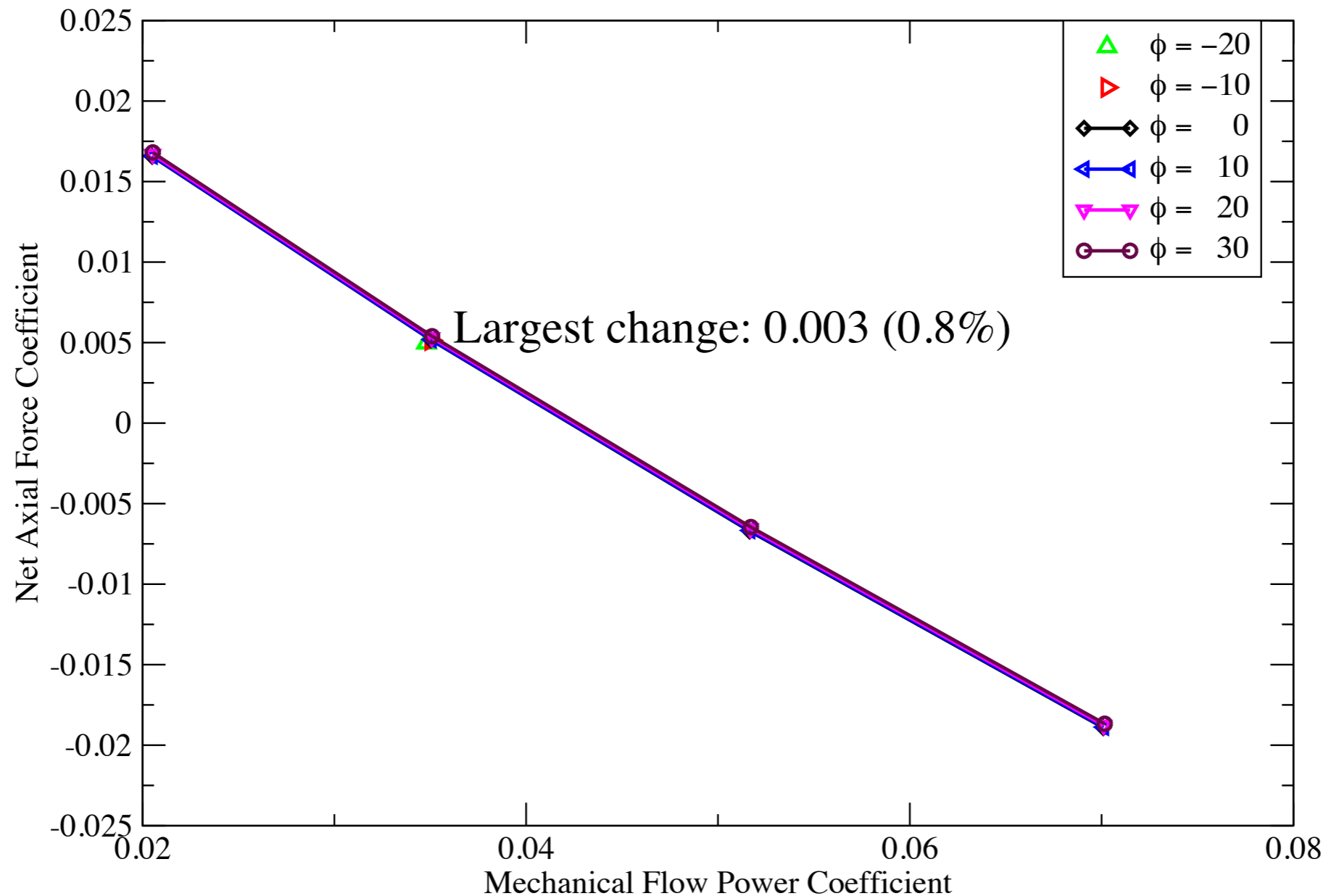
# Effect of Pylon Deflection

Lift



# Effect of Pylon Deflection

Drag



# Effect of Pylon Deflection

Axial Force vs. Mech. Flow Power with power settings of 40, 60, 80 and 100%



# Concluding Remarks

- BLI benefit is:
  - 9% less Mechanical flow power with BLI
- Wake ingestion benefit is:
  - 0.8% less Mechanical flow power with wake ingestion
- BLI has the potential to reduce fuel burn
- Wake Ingestion is not worth pursuing
- Future Work:
  - Full scale aircraft at cruise  $Ma$ , and  $Re$ .
  - Other operating conditions
  - Improve actuator disk model



# Acknowledgements

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- Co-investigators at Ames:

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