

Revision of Paschen's Law Relating to the ESD of Aerospace Vehicle Surfaces

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Agenda

- Introduction
- Theoretical Development
 - Paschen's Law
 - Mach Number Formulation
 - Mach Number and Compressible Dynamic Pressure
 - A Hypothesized Effective Discharge Distance
- Wind Tunnel Experiments
 - Description of Wind Tunnel Experiments
 - Experimental Data
- Future work 2019 CIF project
- Summary



Introduction

- The purpose of this work is to develop a form of Paschen's law that takes into account the flow of gas past electrode surfaces.
- This work was performed under a NASA Science Innovation Fund (SIF) project at the Kennedy Space Center in collaboration with the University of Central Florida.
- In 2010 the Electrostatics and Surface Physics Laboratory (ESPL) at the Kennedy Space Center performed an electrostatic safety analysis on the flight termination system (FTS) antenna for the Ares I rocket.*
- Paschen's law, derived by Friedrich Paschen in 1889 to relate sparking voltage to gas pressure and electrode separation, does not take into account the effect of flowing gas between the electrodes.
- The safety of the FTS housing to triboelectric charging was shown only after extensive laboratory testing.

^{*}M. Hogue, C. Calle, ESPL Report, "Electrostatic Evaluation of the ARES I FTS Antenna Materials", ESPL-TR10-002, August 27, 2010. NASA, Kennedy Space Center.



Introduction

- Potential benefits of a form of Paschen's law that considers gas velocity.
 - Applicable to current and planned rockets and aerospace vehicles.
 - Possible relaxation of electrostatic launch criteria. Launch aborts can cost up to about a million US dollars depending on the vehicle.







Theoretical Development

- This effort is a first approximation at deriving a generalized form of Paschen's law to include gas velocity.
- We have theoretically derived a candidate revision of Paschen's law.
 - Uses the Mach number as a mitigating factor on the number of electron – ion pairs between the electrodes.
 - Compressible dynamic pressure terms were incorporated.
 - Hypothesized an apparent discharge path along the velocity profile.



Paschen's Law

Paschen's law

$$V_{s} = \frac{\frac{V_{i}}{LP_{a}}Pd}{ln(Pd) - ln\left[LP_{a}ln\left(1 + \frac{1}{\gamma}\right)\right]}$$

- Nomenclature: V_s Sparking discharge potential (Volts)
 - $V_{\rm i}$ Ionization potential of the ambient gas (Volts)
 - P Gas pressure (torr)
 - d Electrode separation (cm)
 - $P_{\rm a}$ Atmospheric pressure at sea level (760 torr)
 - L Mean free path at sea level $(6.8 \times 10^{-6} \text{ cm})$
 - γ Secondary electron emission coefficient of the electrode metal



Mach Number Formulation

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- Hypothesis: The loss of electron ion pairs due to gas velocity can be expressed by a dimensionless aerodynamic term such as the Mach number.
- The model equation must revert to Paschen's law when the mean gas velocity, $v_{xm} = 0$.
- The Mach number is the ratio of the mean gas velocity to the speed of sound, $M_N = v_{xm}/c$. Here c = 319 m/s at sea level.
- Using the Mach number to mitigate the concentration of electron

 ion pairs in the derivation of Paschen's Law we have

$$V_{S} = \frac{\frac{V_{i}}{LP_{a}}(Pd)}{ln(Pd) - ln\left[LP_{a}ln\left(1 + \frac{1}{\gamma}\right)\right] - M_{N}}$$

• This equation reverts to Paschen's law when $v_{xm} = 0$.

Mach Number and Compressible Dynamic Pressure

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 - For moving vehicles, pressure has two components
 - Static pressure: $P_{\rm s}$
 - Compressible dynamic pressure: P_{DC}
 - Above Mach 0.3 the compressible form of the dynamic pressure must be used.

$$P_{DC} = P_S \left[\left(1 + \frac{\gamma_a - 1}{2} M_N^2 \right)^{\frac{\gamma_a}{\gamma_a - 1}} - 1 \right] \quad \gamma_a = \text{Ratio of Specific Heats} = C_P / C_V$$

Total pressure

$$P = P_{S} + P_{DC} = P_{S} + P_{S} \left[\left(1 + \frac{\gamma_{a} - 1}{2} M_{N}^{2} \right)^{\frac{\gamma_{a}}{\gamma_{a} - 1}} - 1 \right]$$

$$P = P_s \left(1 + \frac{\gamma_a - 1}{2} M_N^2 \right)^{\frac{\gamma_a}{\gamma_a - 1}}$$

Mach Number and Compressible Dynamic Pressure Kennedy Space Center

• Substituting the total pressure in the model equation gives for the sparking voltage

$$V_{S} = \frac{\frac{V_{i}}{LP_{a}}\left(1 + \frac{\gamma_{a} - 1}{2}M_{N}^{2}\right)^{\frac{\gamma_{a}}{\gamma_{a} - 1}}P_{S}d}{ln\left[\left(1 + \frac{\gamma_{a} - 1}{2}M_{N}^{2}\right)^{\frac{\gamma_{a}}{\gamma_{a} - 1}}P_{S}d\right] - ln\left[LP_{a}ln\left(\frac{1}{\gamma} + 1\right)\right] - M_{N}}$$

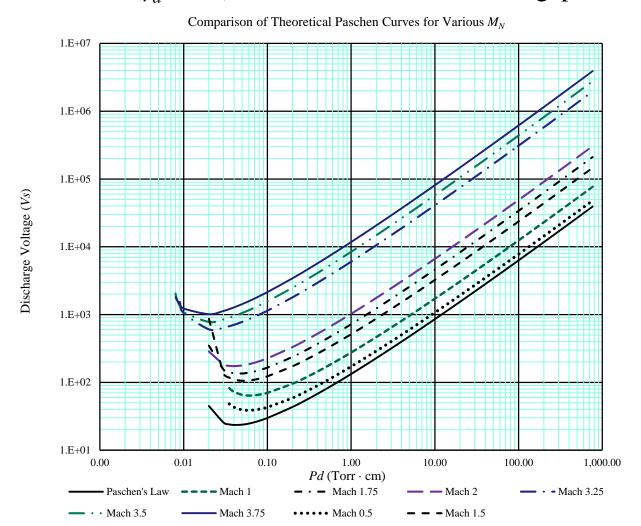
- This equation also meets the requirement that Paschen's law is returned when the mean gas velocity is zero.
- In this equation, the sparking voltage is a function of three variables: static pressure, electrode separation, and Mach number

$$V_S = f(P_S, d, M_N)$$



Theoretical Comparison

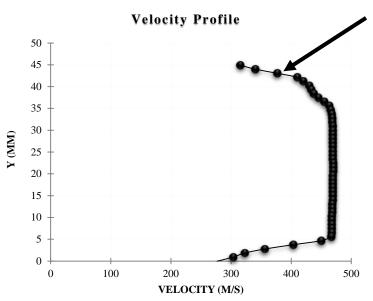
The model equation is graphed for stainless steel electrodes ($\gamma = 0.02$) at various Mach numbers for air ($\gamma_a = 1.4$) between 0.5 and 3.75 and a gap of 1.3 cm.





A Hypothesized Effective Discharge Path

Gap: 4.4 cm, Gas: air, Gas velocity: Mach 1.47



Wind tunnel velocity profile data provided by UCF.

Length of velocity profile measured to be ~ 11.7 cm from full scale print.

From inspection of the model equation, we can hypothesize an effective electrode separation

$$d' = \left(1 + \frac{\gamma_a - 1}{2} M_N^2\right)^{\frac{\gamma_a}{\gamma_a - 1}} d$$

- For air: $\gamma_a = 1.4$. At Mach 1.47 and d =4.4 cm this gives a value of d' of 15.48 cm only about 25% larger than measured value.
- Additional experiments will be needed to better evaluate this hypothesis. 11

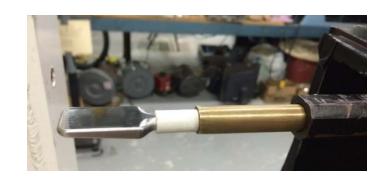


• Wind tunnel experiments were performed at the Florida Center for Advanced Aero-Propulsion (FCAAP) of the University of Central Florida (UCF)

• An existing wind tunnel was modified to incorporate a stainless steel electrode plate attached to a movable sting

mount in the test section.



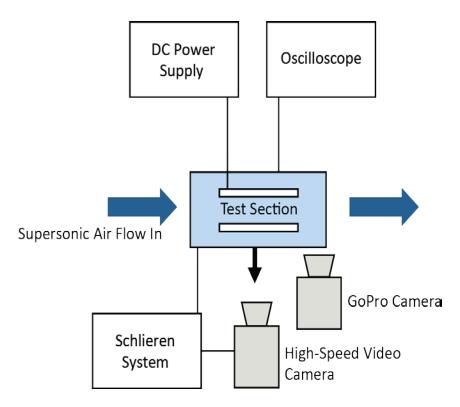


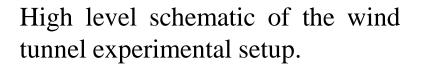


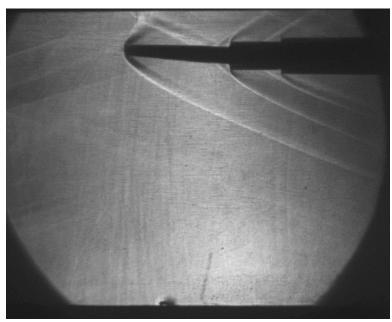
- The upper portion of the test section was also made from stainless steel and acted as the ground plate.
- 1.3 cm was the closest the electrode could be physically placed to the stainless steel upper surface.
- The test section was instrumented to input DC voltage to the electrode, measure static pressure, P_s , mean velocity, v_{xm} , and to provide video of the experiment.
- A high speed camera was used with a Schlieren system to capture images of the supersonic shocks around the electrode.











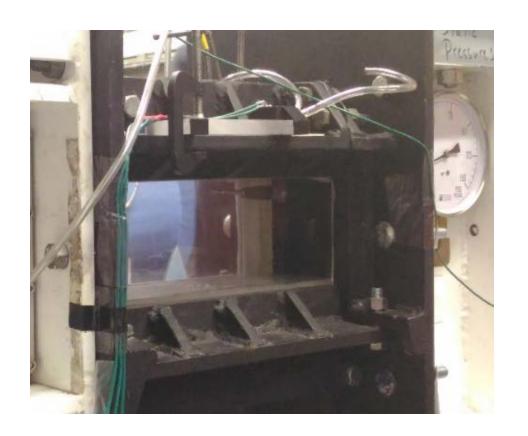
Typical shocks around the electrode. Mach 3.5



- Two types of experiments were performed.
 - Under steady supersonic flow, the electrode voltage was ramped up to observe and record any sparking.
 - Preload the electrode to achieve sparking during no-flow conditions, then turning on the wind tunnel to observe the effects of the supersonic flow.
- The voltage ramping experiments were difficult
 - short duration of steady supersonic flow (< 30 seconds)
 - shock reflections between the electrode and the wall of the test section affected pressure measurements.
 - High voltage supply was limited to about 35 kV due to the rating on the high voltage cabling that could fit through the sting mount.



- A new instrumented test section was attached to the wind tunnel.
 - Pressure sensing port located to more accurately measure static pressure between the electrodes.
 - Located further down the tunnel to mitigate air turbulence.
- Experiments were run at Mach 1.65 for this test section.





Experimental Data

• Video data shows sparking quenched by the onset of supersonic flow consistent with the theoretical model.



Sparking



Start of supersonic flow



Sparking quenched



Sparking resumes after supersonic flow ends



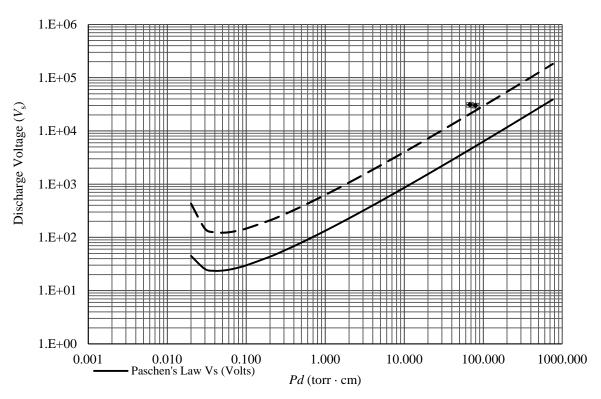
• Noted that the shape of the deformation of the spark prior to quenching is convex in appearance.



Experimental Data

Model Equation Comparison to Paschen's Law and Experimental Data (Mach 1.65, d = 1.3 cm)

- Two of the eleven Mach 1.65 experiments yielded measurable sparks during supersonic flow.
- These two data points compare well to the theoretical model with both the Mach number and compressible dynamic pressure terms.



- Model Equation with Mach Number & Comp. Dynamic Pressure Vs (Volts)
 - ◆ Exp. Data Vs (Volts)



Future Work

- Recent award of a FY 2019 Center Innovation Fund (CIF) project is continuing this work (project start 3/1/19).
- Theoretical work underway to put the model equation into a form that includes ambient temperature.
- New wind tunnel experiments under design
 - Develop LabViewTM control program
 - Design and fabricate new wind tunnel test sections to lessen shock reflections. The upper and lower panels will be the HV electrode and ground respectively.
 - Both voltage ramp and spark quenching experiments planned.
 - Gather more velocity profile data to better evaluate the hypothesized effective discharge distance.



Summary

- A first approximation theoretical model equation based on Paschen's law was developed to account for the effect of gas flow on the sparking voltage.
- An effective discharge distance due to gas velocity was hypothesized based the theoretical model and limited wind tunnel test data.
- Wind tunnel experiments were conducted that gave results consistent with the prediction of the model equation.
- Further theoretical revision of the model equation and wind tunnel experimentation via a KSC CIF project are underway.



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