

Material Response Analysis of a Titan Entry Heatshield

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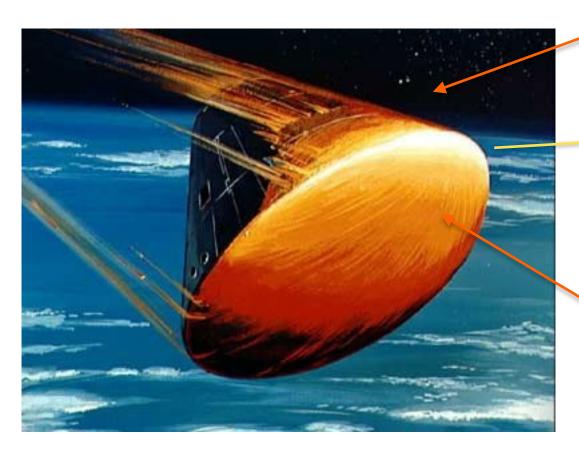
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10th Ablation Workshop, Burlington, VT, Sept 17-18, 2018

Abstract: Accurate calculation of thermal protection material response is critical to the vehicle design for missions to the Saturn moon Titan. In this study, Icarus, a three-dimensional, unstructured, finite-volume material response solver under active development at NASA Ames Research Center, is used to compute the in-depth material response of the Huygens spacecraft along its November 11 entry trajectory. The heatshield analyzed in this study consists of a five-layer stack-up of Phenolic Impregnated Carbon Ablator (PICA), aluminum honeycomb, adhesive, and face sheet materials. During planetary entry, the PICA outer layer is expected to undergo pyrolysis. A surface energy balance boundary condition that captures both time- and spatial-variance of surface properties during entry is used in the simulation.

Motivations....

• Design and sizing of the thermal protection system (TPS) of an entry vehicle requires high-fidelity material response codes coupled to computational fluid dynamics (CFD) and full radiation transport.



Mass flow due to material decomposition and surface ablation

Shock layer radiation out to the surroundings

> Strong convective and radiative heat flux to the surface

Planetary Entry Environment

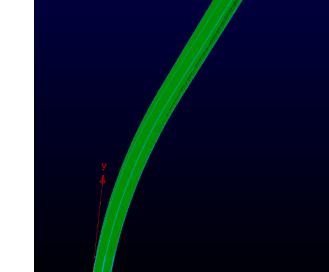
The goal of the current work is to apply the lcarus material response code to compute the in-depth material response of a *multi-layer TPS material stack-up along a representative Titan entry* trajectory.

Icarus

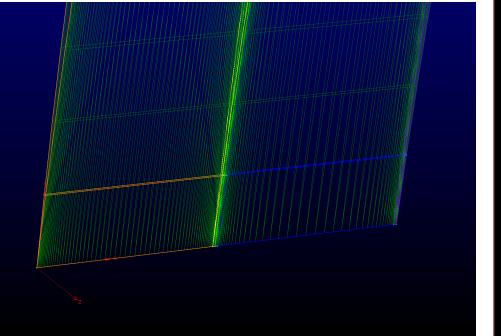
- Icarus is a 3-D, finite-volume, unstructured material response code.
- Can model ablating, pyrolyzing, melting, or vaporizing materials subject to a wide range of surface boundary conditions.

Icarus grid of Huygens entry vehicle is a 3-D wedge with a mixture of hexahedral and prismatic grid elements.

> Close-up of stagnation line showing 5-layer stack-up



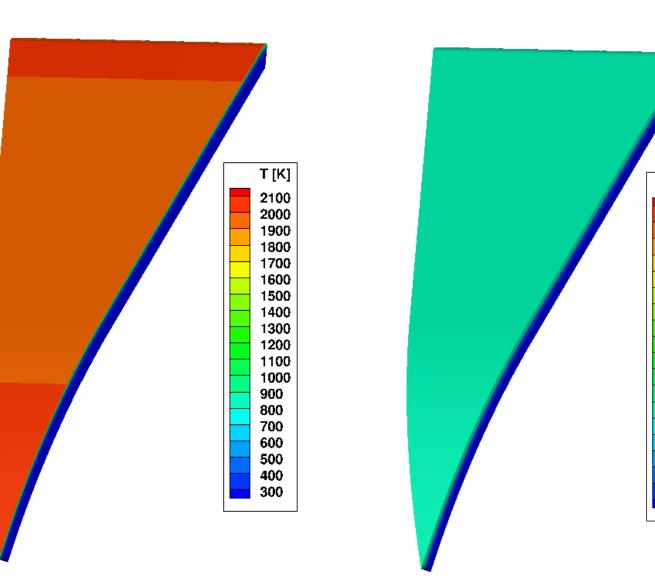
3-D wedge grid of Huygens heatshield



Surface Environments and **Boundary Conditions**

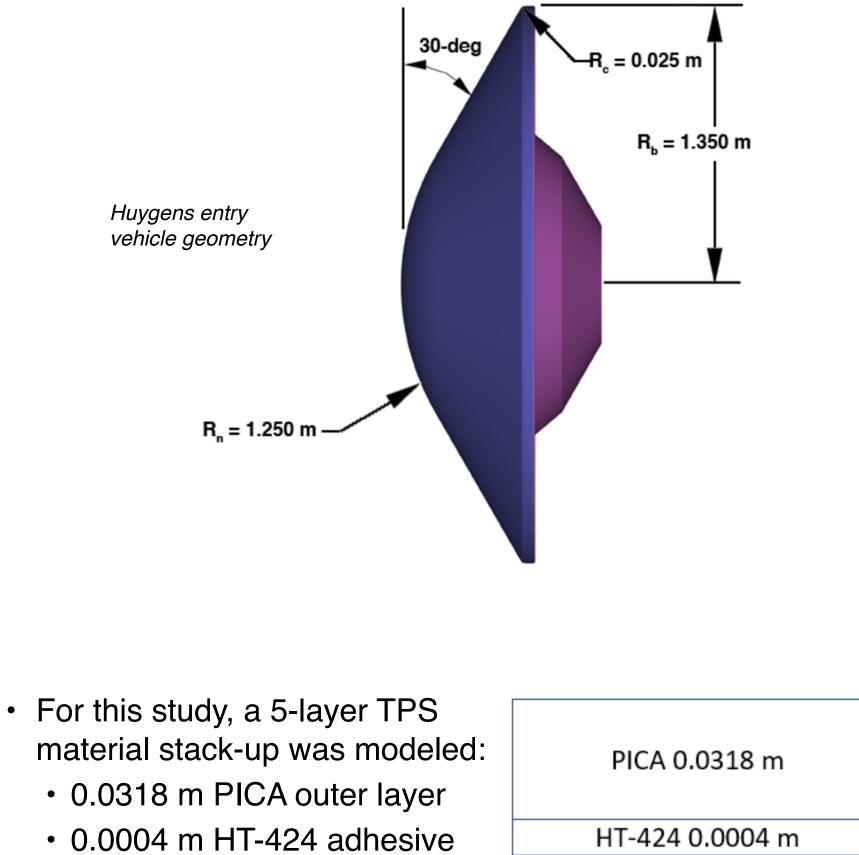
Results

- Icarus computation run for 100 seconds of simulation time starting at the 151 sec trajectory point conditions. Zero-heating cool-down conditions were applied after 225 sec.
- Surface boundary conditions were both time- and spatiallyvarying during the simulation.
- Surface temperatures reach a peak value of 2068 K at t = 189 sec. Surface then starts to cool as external heating rates decrease. Peak temperature at t = 225 sec is 1003 K.
- Because radiative heating increases along flank towards the shoulder, surface temperatures on the upper flank region are similar to stagnation point values.



Huygens Vehicle Geometry and TPS Material Stack-up

• The Huygens probe was a 60-deg half-angle spherecone with a 2.7 m base diameter and a 1.25 m nose radius.

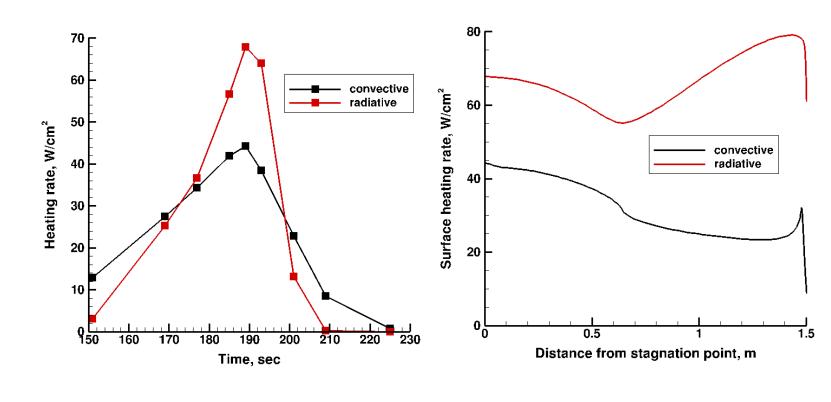


• 0.0005 m M55-J face sheet

PICA 0.0318 m
HT-424 0.0004 m
M55-J 0.0005 m

Al-honeycomb 0.0318 m

- The DPLR CFD code and NEQAIR line-by-line radiation codes were used to compute surface heating rates and pressure.
- 13-species gas chemistry model: CH4, CH3, CH2, N2, C2, H2, CH, NH, CN, N, C, H, Ar.
- N2: 0.970, CH4: 0.023, Ar: 0.007 by mole fraction
- Surface heating dominated by radiative component.
- Radiative heating increases along flank towards shoulder due to CN levels in shock layer.



- Convective and radiative heat pulse at the stagnation point.
 - Surface heating rates, t = 189 second trajectory point.
- DPLR/NEQAIR solutions at 9 points along Huygens November 11 trajectory (time = 151 - 225 sec) used to create time- and spatially-varying boundary conditions.
- An aeroheating surface energy balance (SEB) boundary condition is used in Icarus.

 $\dot{q}_{cond} = C_H (h_{rec} - [1 + B'_c + B'_g]h_w) + \dot{m}_c h_c + \dot{m}_g h_g +$

Surface temperatures, t=189 sec

t=225 sec

T [K]

2100 2000 1900

1800

1700

1600

1500

1400

1300 1200

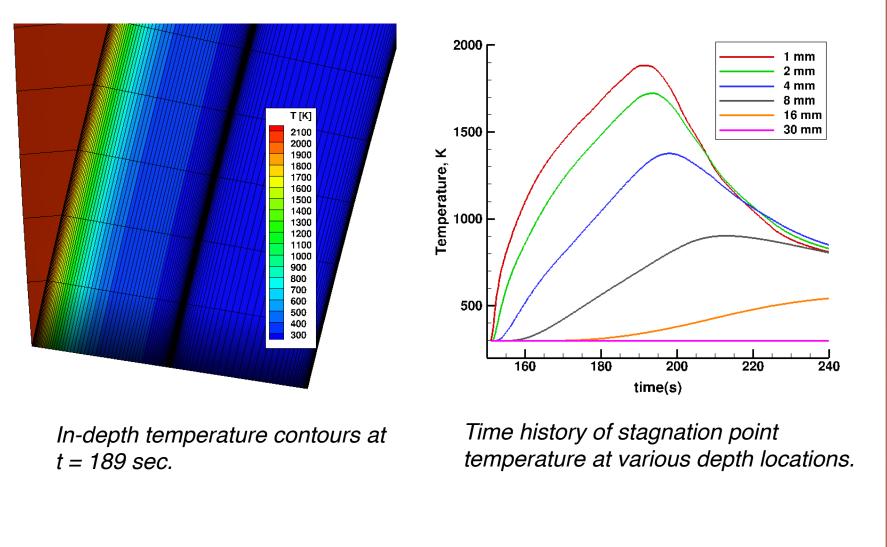
1100

1000

900 800 700

600 500 400

• In-depth temperature profiles indicate heat soak does not reach the PICA backface at the 100 second simulation time cut-off.



Summary/Conclusions

- Icarus material response solver demonstrated ability to compute in-depth material response of Huygens probe heatshield during an entry into Titan. The 100 second simulation time captured the entire entry heat pulse.
- Five-layer material stack-up was modeled.

- 0.0318 m layer of aluminum honeycomb
- 0.0005 m M55-J face sheet

TPS material stack-up for Titan entry vehicle

M55-J 0.0005 m

 $\alpha \dot{q}_{rad} - \sigma (\epsilon T_w^4 - \alpha T_\infty^4)$

- Normalized char mass flux computed using a 45-species PICA-Titan GSI gas mixture.
- Pyrolysis gas mass flux computed using a 39-species PICA pyrolysis gas mixture.

DPLR/NEQAIR simulations used to create 4-D, time- and spatially-varying surface boundary conditions

Future Work

• Implement Stanford/DLR dust particle model into Icarus for Mars entry simulations.

• Apply Icarus to other planetary entry scenarios.



Acknowledgments:

NASA work is a part of the Asteroid Threat Assessment Project (ATAP) funded by the NASA Planetary Defense Coordination Office (PDCO), managed by Lindley Johnson.'

References:

[1] Schulz, J., et al, "Development of an Unstructured, Three-Dimensional Material Response Code," AIAA Paper 2017-0384, Jan. 2017. [2] Hollis, B., Striepe, S., Wright, M., Bose, D., Sutton, K., and Takashima, N., "Prediction of the Aerothermal Environment of the Huygens Probe," AIAA-2005-4816, June, 2005. [3] Tran, H., Johnson, C., Rasch, D., Hui, F., Chen, Y.-K., and Hau, M.-T., "Phenolic Impregnated Carbon Ablators (PICA) for Discovery Class Missions," AIAA-1996-1911, Jan. 1996. [4] Wright, M., White, T., and Mangini, N., "Data Parallel Line Relaxation (DPLR) Code User Manual Acadia - Version 4.01.1, 2009