

# Slow crack growth of boron nitrides for electric propulsion components

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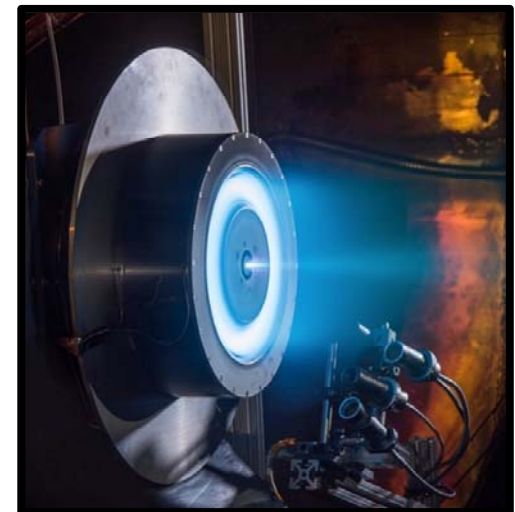
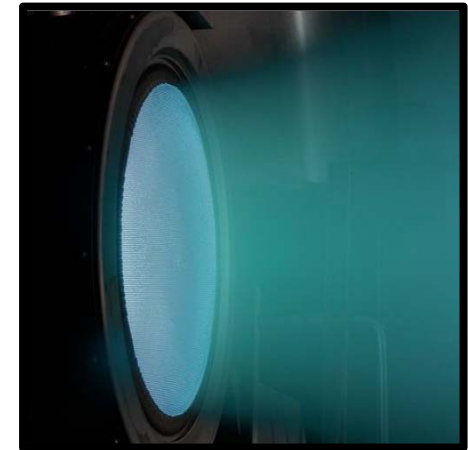
# Outline

- Background
- Materials and properties of interest
- Past work
  - Chemistry, microstructure, texture, moisture absorption
  - Strength, modulus, CTE, conductivity
- Slow crack growth
  - procedure
  - failure sources
- Fracture toughness
- Summary



# Background

- Electric propulsion systems subject components to harsh environments including:
  - High temperature plasma (600°C)
  - low temperature (-200°C), vacuum, and back-sputtered deposition.
- Both Hall and ion thrusters require ceramics:
  - electrical isolation
  - thermal management
  - structural performance.
- Ceramic components range in size from  $<1/4''$  to  $>10''$ .
- Historically, material selection has primarily been determined from cost, secondary electron emission yield, and sputtering yield.
  - Hot pressed hexagonal boron nitride





# Materials of Interest

- The grades commercial hexagonal boron nitride being considered were selected from historical usage and/or geometric considerations.
- Similar costs w/exception of Tokuyama
- Several grades contain significant silica:

Grade Name*	Vendor*	Description	Relative Cost**
HP	Saint-Gobain	BN CaF <sub>2</sub> Binder, Hot Pressed	1.0
M26	Saint-Gobain	BN/SiO <sub>2</sub> Composite, Hot Pressed	1.1
M	Saint-Gobain	BN/SiO <sub>2</sub> Composite, Hot Pressed	1.0
BN-XX	Kennametal	BN/SiO <sub>2</sub> /ZrO <sub>2</sub> Composite, Hot Pressed	1.0
Hi-M	Tokuyama	AlN/BN Composite, Hot Pressed	4.6

\* Trade names and vendors are used for identification purposes only.

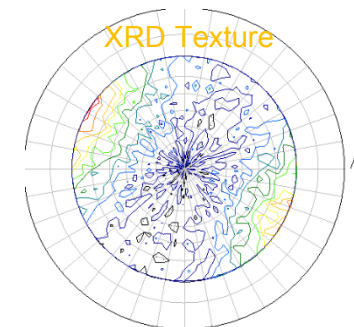
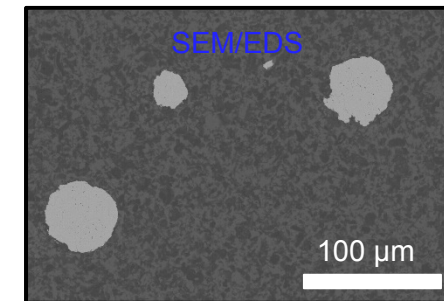
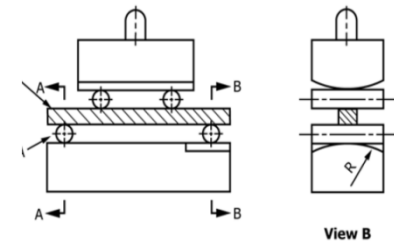
\*\* Cost based on recent quotes for similar size lots of material, normalized to the cost of HP.



# Factors of Interest

- **Primary** factors of interest:
  - dielectric properties
  - thermal properties and stability
  - mechanical properties
  - moisture sensitivity
  - secondary electron emission yield
  - erosion resistance in a plasma environment
- **Secondary** factors of interest:
  - Microstructure, crystal structure, details of processing, and mass spectroscopy.
- **Additional** factors to consider:
  - Hot press anisotropy, lot-to-lot and variability, billet uniformity/property variability, storage/handling concerns, and machining concerns.
- **Beyond** materials characterization work:
  - Component fabrication, component testing.

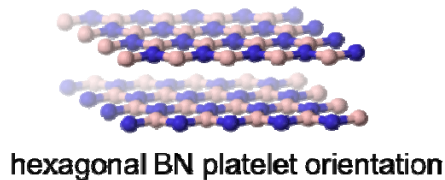
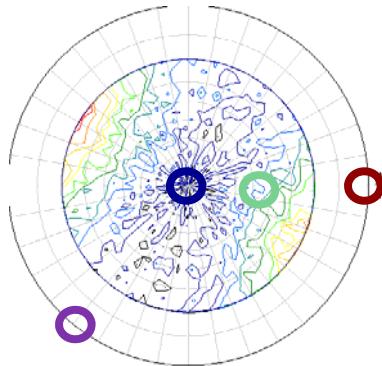
Property Testing





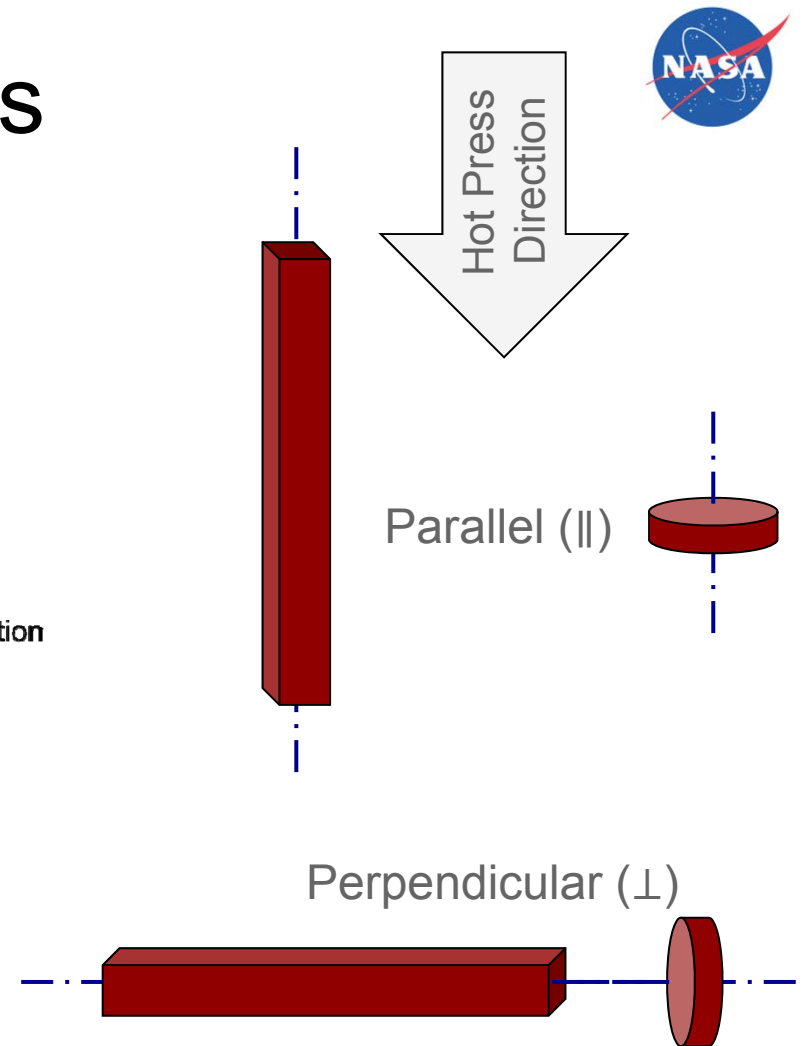
# Property Measurements

- Building dataset to compare grades:
  - Collecting data from 25 to 900°C .



- Collecting data on samples with orientation “Parallel  $\parallel$ ” or “Perpendicular  $\perp$ ” to the hot press direction.

NASA/TM—2018-219949  
“Evaluation of Boron Nitride Materials for Hall Thruster Discharge Channels”  
*Jonathan A. Mackey, Jonathan A. Salem, and Hani Kamhawi.....*



# Property Trends & SiO<sub>2</sub> Content in BN



Property	Method	HP	M26	BN-XX	M
		/ ⊥	/ ⊥	/ ⊥	/ ⊥
XRD BN Phase (wt%)	Rietveld-refinement	98	70	56	45
Porosity (%)	ASTM C830	<14	<4.7	<2.4	<3.0
CTE (μm/m-K)	Dilatometry	3.1 / 0.4	2.9 / 0.5	N/A	0.5 / 0.6
Dielectric Constant	Impedance Spectroscopy	4.7 / 4.6	4.6 / 4.7	4.1	4.0 / 4.2
Thermal Conductivity (W/m-K)	ASTM E1461	33 / 31	22 / 28	6	9 / 12
Elastic Modulus (GPa)	ASTM C1259	80 / 79	55 / 47	N/A	16 / 61

\* All data collected at NASA GRC or California Institute of Technology

- Properties are quite different! Function of orientation.
- HP exhibits the largest values in all categories!

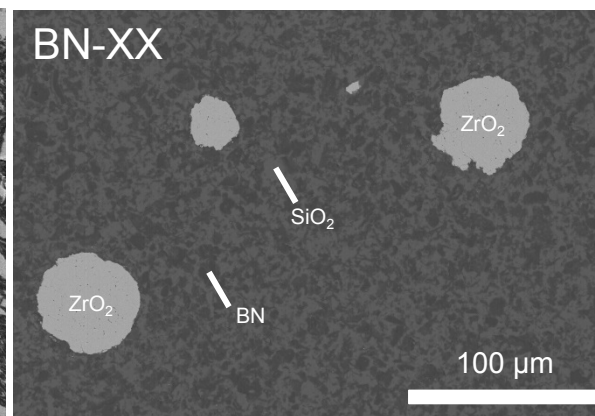
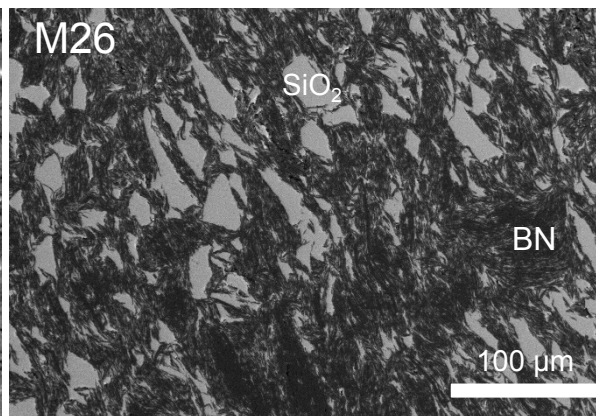
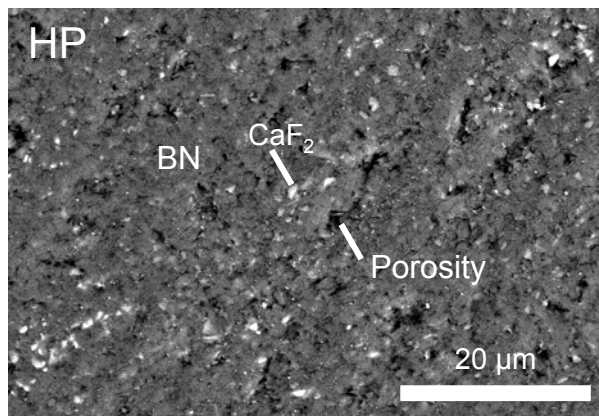
# Microstructure Overview

- Very different microstructure.
- Texture is not clearly apparent in SEM microstructure.
- Porosity is apparent in HP grade, less in other grades.
- Large silica content is a concern for crack growth.

Powder XRD Rietveld Refinement (wt%)

Grade	BN	CaF <sub>2</sub>	ZrO <sub>2</sub>	AlN	Amorp.
HP	98	2	0	0	0
M26	68	0	0	0	32
BN-XX	56	0	1	0	43
M	41	0	0	0	59
Hi-M	27	0	0	72	0

\*Amorphous content is likely SiO<sub>2</sub>, confirmed with EDS.





## Another Interesting Issue: Moisture Absorption

- Samples were subjected to one of three moisture levels for >20 days while mass change was tracked:
  - Drying Oven, 100C, <5% rel. humidity.
  - Environmental Chamber, 50C, 90% rel. humidity.
  - Submerged Water Bath, 25C, 100% rel. humidity.
  - Each hot press orientation was investigated on high aspect ratio samples.

Drying Oven  
100C, <5% rel. humidity, 50 days



Submerged in Water  
25C, 100% rel. humidity, 90 days





# Moisture Absorption (cont.)

- Mass change tracks with open pore porosity (**high**, **medium**, **low**).
- HP hot press orientation has influence on the transfer of moisture (**high**, **low**).
- HP samples produced a  $\text{CaB}_6\text{O}_9(\text{OH})_2(\text{H}_2\text{O})_3$  salt on the surface of the submerged samples.

Sample	Porosity (%)	Dry Oven, 100C Mass Loss (%)	90% Chamber, 50C Mass Gain (%)	Submerged, 25C Mass Gain (%)	
HP	<14	1.1 ± 0.5	0.97 ± 0.07	4.6 ± 0.3	
HP ⊥	<14	0.12 ± 0.01	0.33 ± 0.05	3.7 ± 0.5	% OP
M26	<4.7	0.025 ± 0.003	0.020 ± 0.005	2.7 ± 0.3	
M26 ⊥	<4.7	0.035 ± 0.004	0.019 ± 0.008	3.2 ± 0.8	BN wt%
M	<3.0	0.026 ± 0.005	0.018 ± 0.005	1.8 ± 0.1	
M ⊥	<3.0	0.036 ± 0.003	0.005 ± 0.003	1.7 ± 0.1	



# Moisture Sensitivity on Strength

- Samples from moisture absorption study were tested for flexural strength and elastic modulus after soak.
- HP  $\parallel$ , HP  $\perp$ , and M  $\parallel$ , all have significant changes in strength and elastic modulus properties with moisture exposure ( $P < 0.05$ ).

Sample	<5% Rel. Humidity Dry Oven Strength (MPa)	~60% Rel. Humidity As-machined Strength (MPa)	90% Rel. Humidity 90% Chamber Strength (MPa)	P-Value [Oven>Chamber]
HP $\parallel$	52.1	42.5	27.5	0.000005
HP $\perp$	80.1	76.1	69.7	0.005
M26 $\parallel$	59.9	61.8	57.9	0.3
M26 $\perp$	43.2	49.6	39.7	0.2
M $\parallel$	23.9	24.7	22.3	0.01
M $\perp$	60.1	62.4	59.2	0.3



# Slow Crack Growth (SCG)

- Ceramics and glass exhibit loss of strength over time under static loads. The phenomenon is known as slow crack growth or “static fatigue” and is a form of stress corrosion.
- No data is in the literature on BN.
- We need to know the SCG parameters for BN to see if stress corrosion should be a design consideration.
- Usual model: 
$$v = \frac{da}{dt} = AK_I^n = A * \left[ \frac{K_I}{K_{IC}} \right]^n$$

## Sensitivity Parameter n

- < 20 high sensitivity (glasses)
- < 40 intermediate (alumina's)
- > 50 low ( $\text{Si}_3\text{N}_4$ )
- > 100 ~ insensitive (Ge, Si,  $\alpha$  SiC)

- $v$  – crack velocity
- $\sigma$  is Stress
- $n$  &  $A$  are SCG parameters
- $K_{IC}$  is Fracture toughness



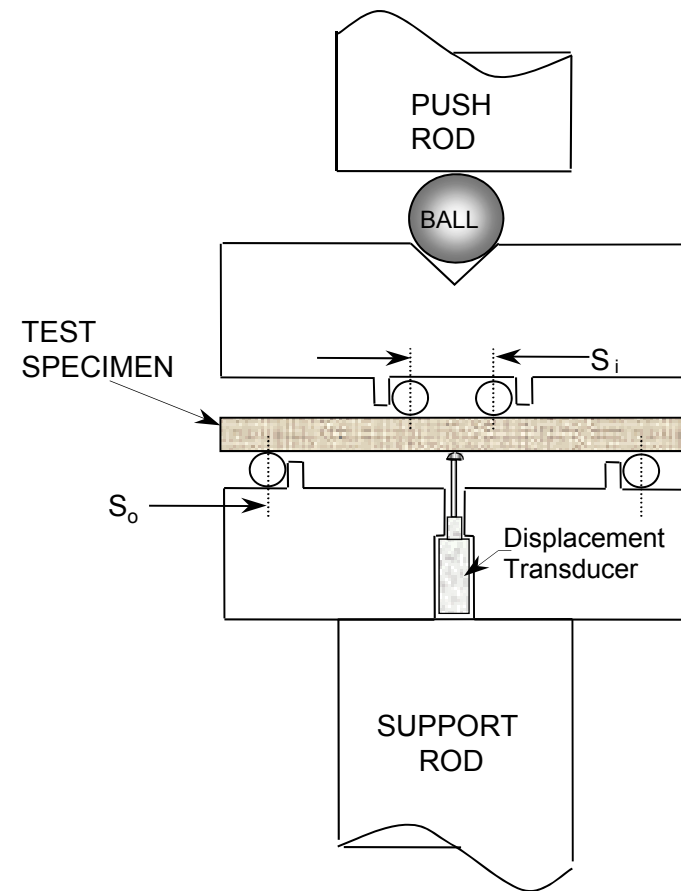
# Rapid Technique for SCG Parameters

- Constant Stress Rate Testing (Dynamic fatigue):
  - well defined time-to-failure
  - can be rapid
  - simple
- Strength based approach with advantages & disadvantages:
  - samples the inherent, small flaws (length scale)
  - statistical scatter (many specimens needed)
  - averaging of fatigue regions
  - shorter time scale than application

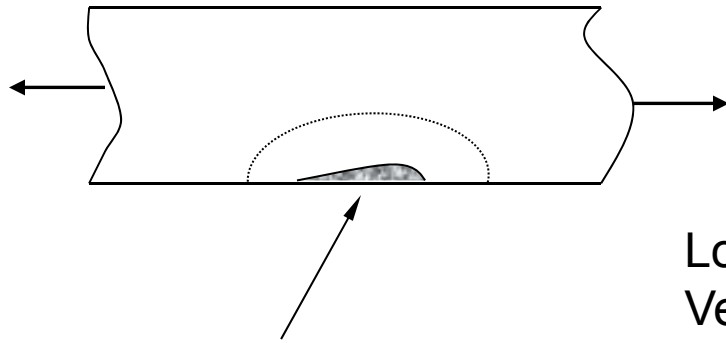


# Experimental Procedure

- Constant Stress Rate Tests  
(200 to 0.002 MPa/s)
- Uniaxial Flexure (4-point)
- Air : 60% RH
- As-machined surfaces
- 60 tests per condition

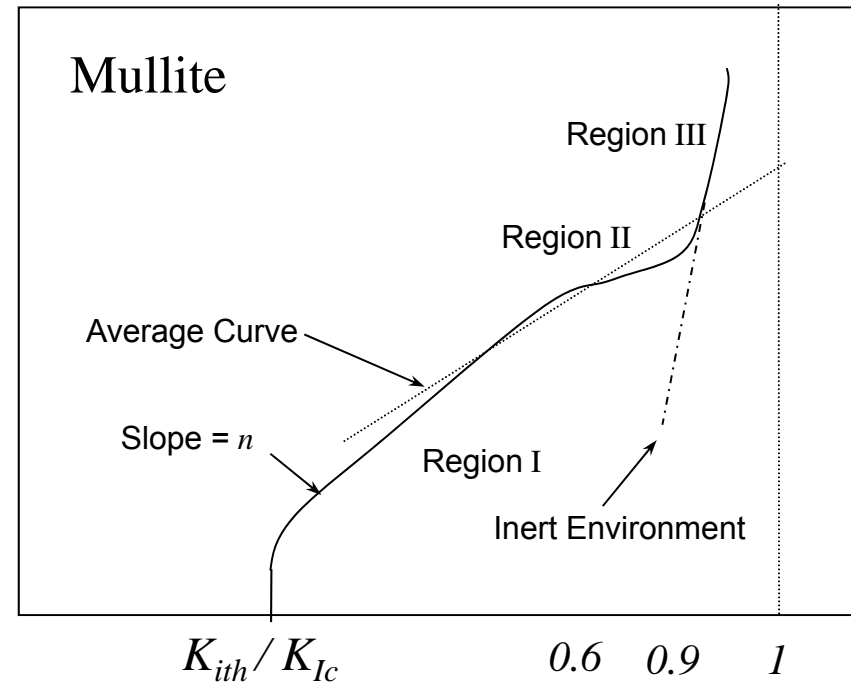


# SCG FORMULATIONS



Defect/Damage

Log Crack Velocity,  $v$



Log Stress Intensity Factor,  $K_I/K_{Ic}$

□ Crack growth Function: 
$$v = \frac{da}{dt} = AK_I^n = A * \left[ \frac{K_I}{K_{IC}} \right]^n$$



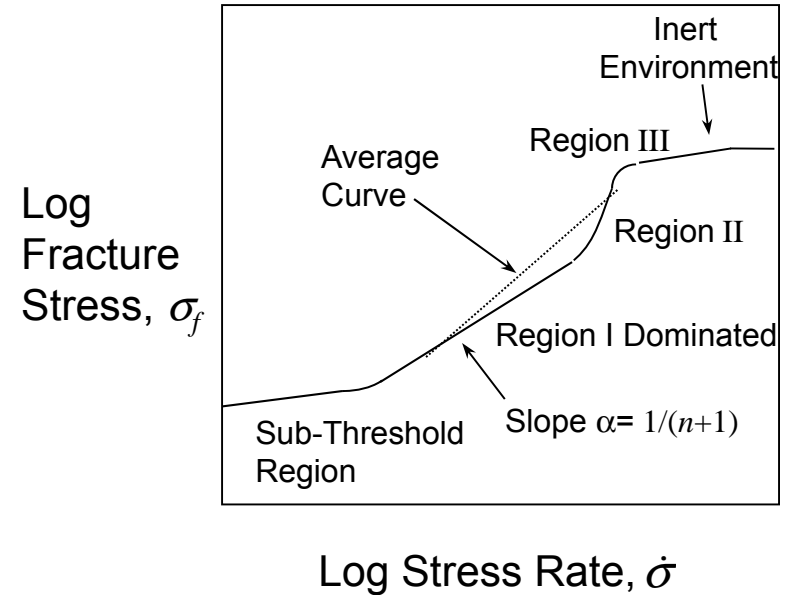
# SCG Analysis

## □ Crack growth Function:

$$v = \frac{da}{dt} = AK_I^n = A * \left[ \frac{K_I}{K_{IC}} \right]^n$$

## □ Constant Stress Rate Testing:

$$\sigma_f = \left[ B(n + 1) \sigma_i^{n-2} \dot{\sigma} \right]^{1/(n+1)}$$

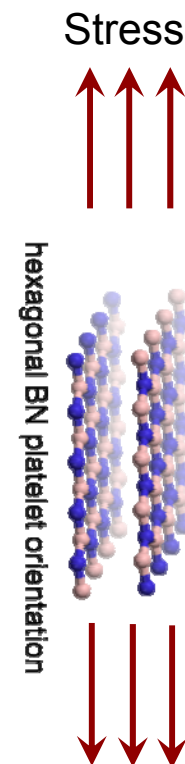
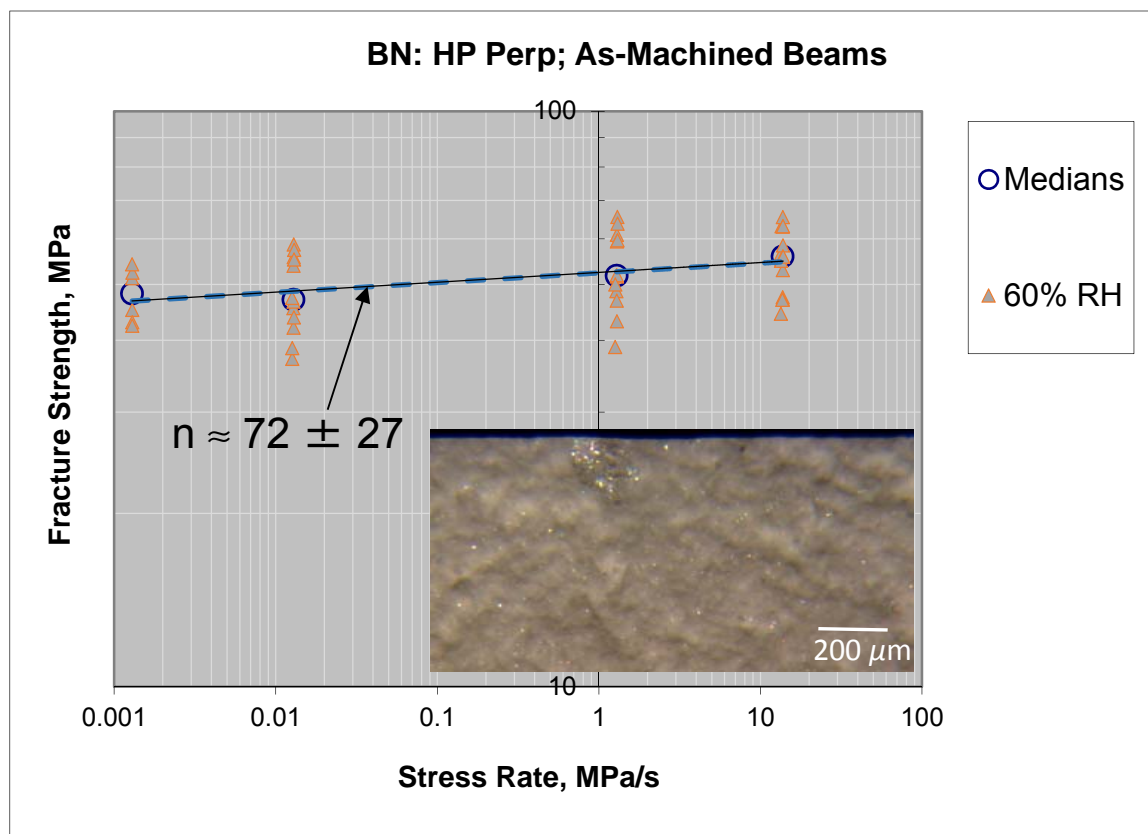


## □ Parameter extraction via regression:

$$\log_{10} \sigma_f = \frac{1}{n+1} \log_{10} \dot{\sigma} + \log_{10} D \quad \log_{10} D = \frac{1}{n+1} \log_{10} \left[ B(n+1) \sigma_i^{n-2} \right]$$

(Slope  $\alpha$ )                      (Intercept  $\beta$ )

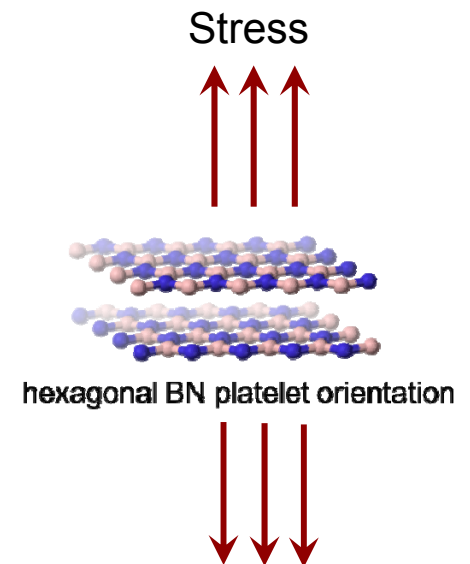
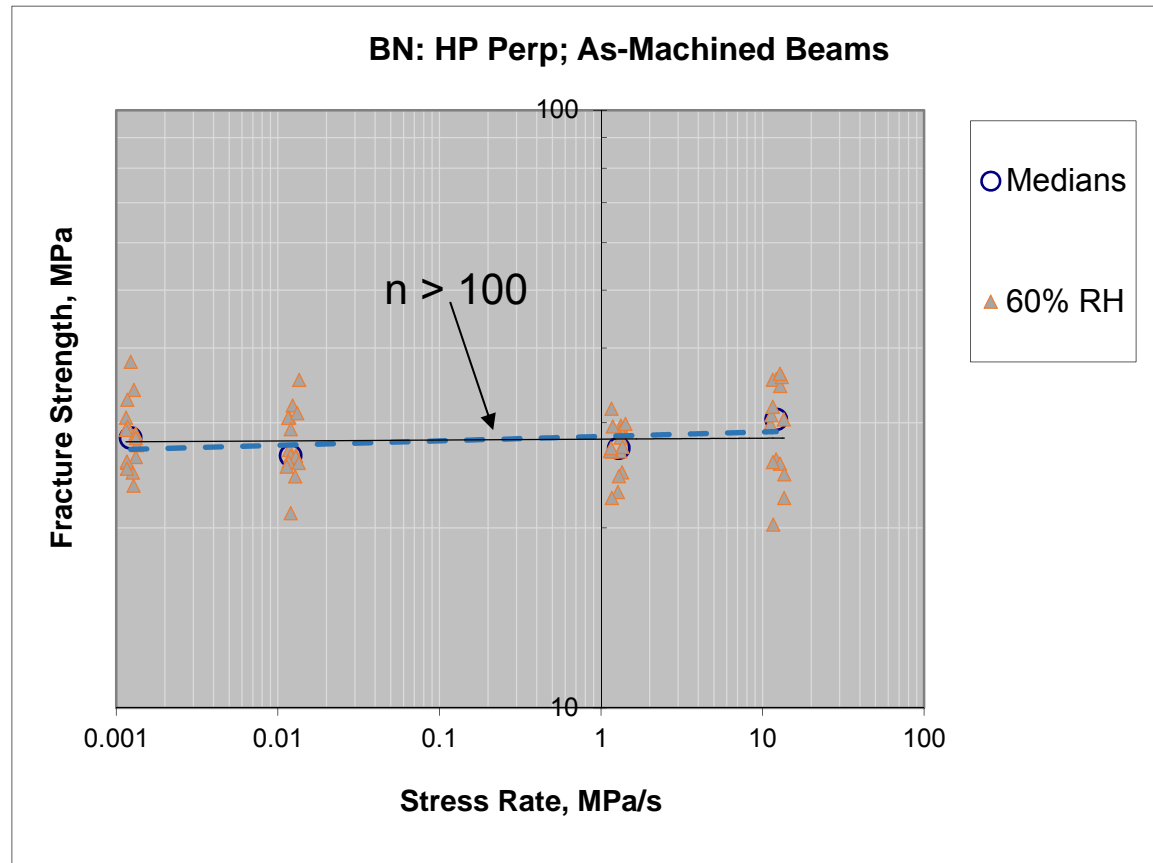
# Results for HP BN Perpendicular



- SCG parameter  $n = \sim 72 \pm 27$
- Resistant to SCG.



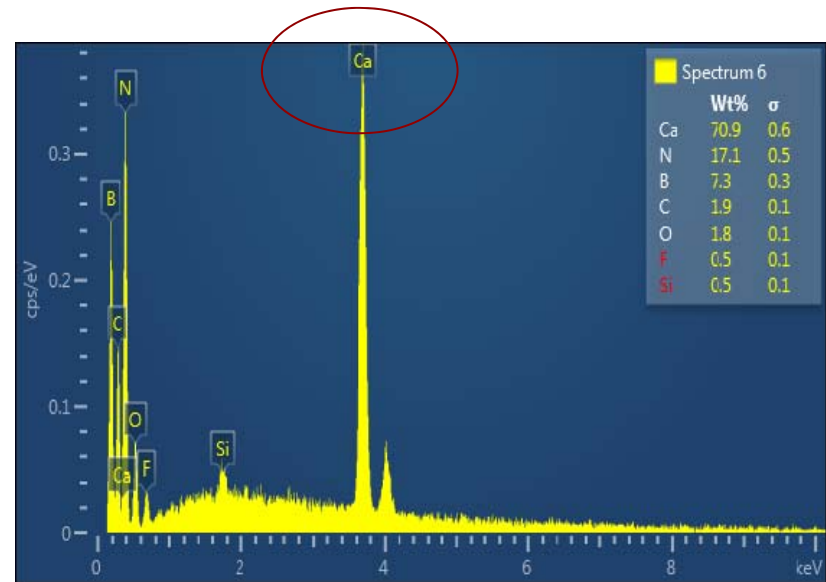
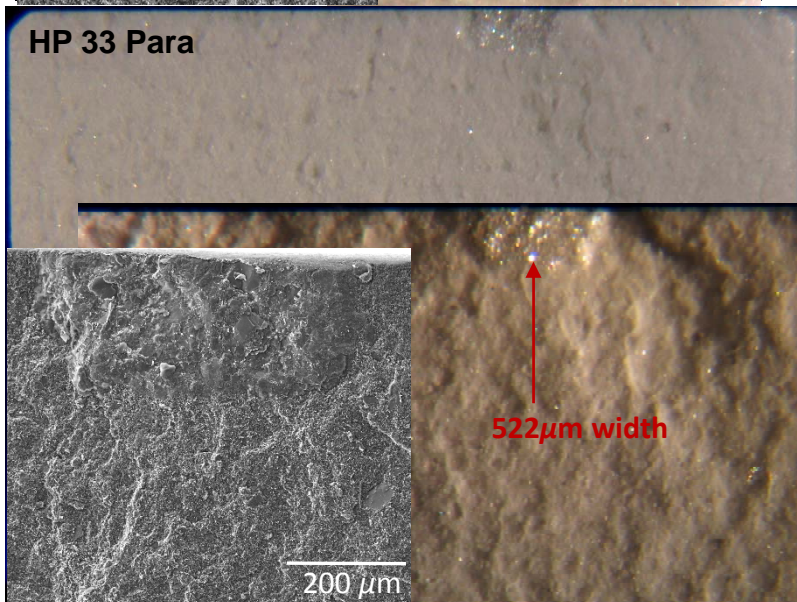
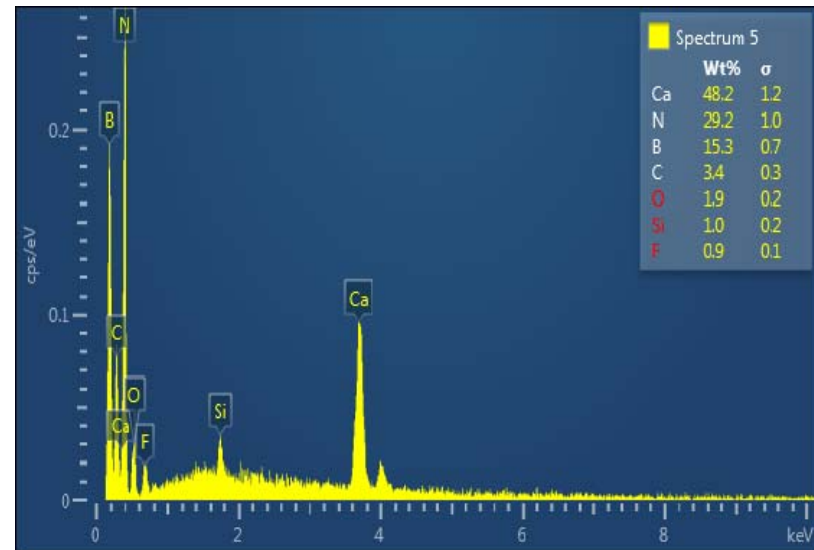
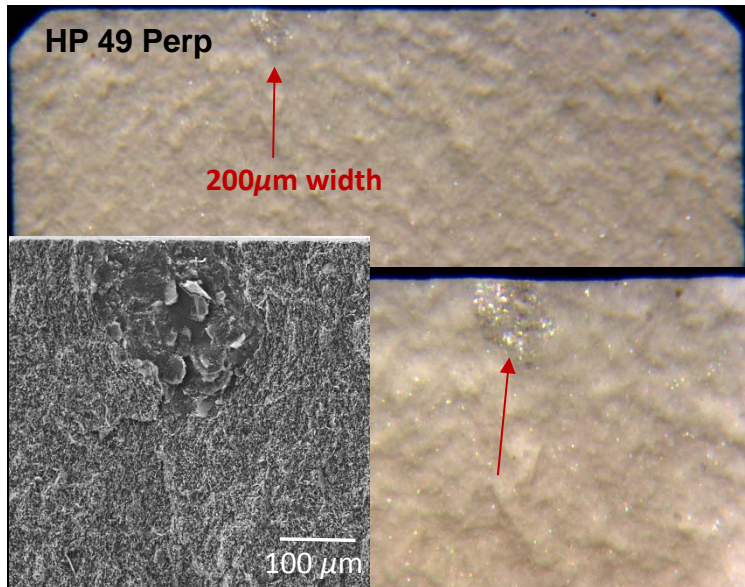
# Results for HP BN Parallel



- SCG parameter  $n > 100$  is very high.
- Very resistant to SCG. ....platelets corrossion.

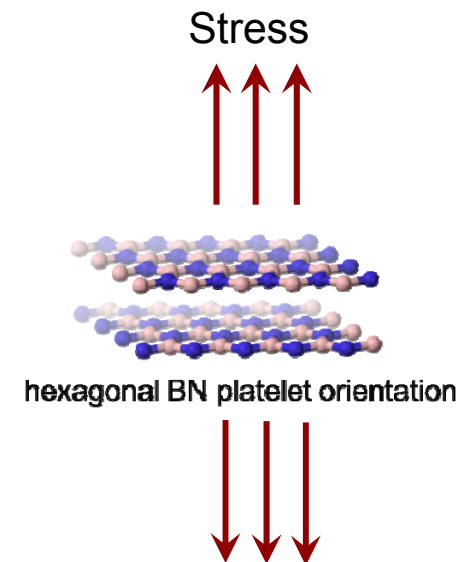
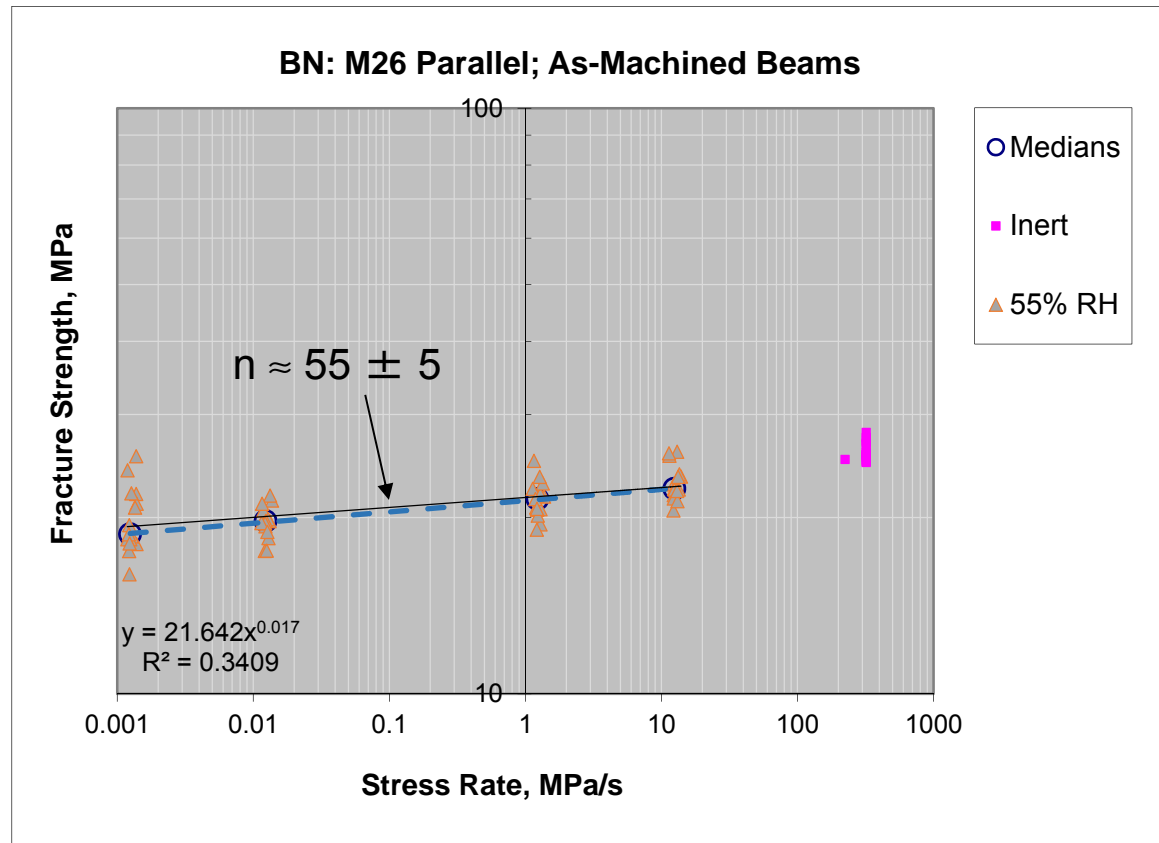


# HP Failure Source: Ca rich agglomerates





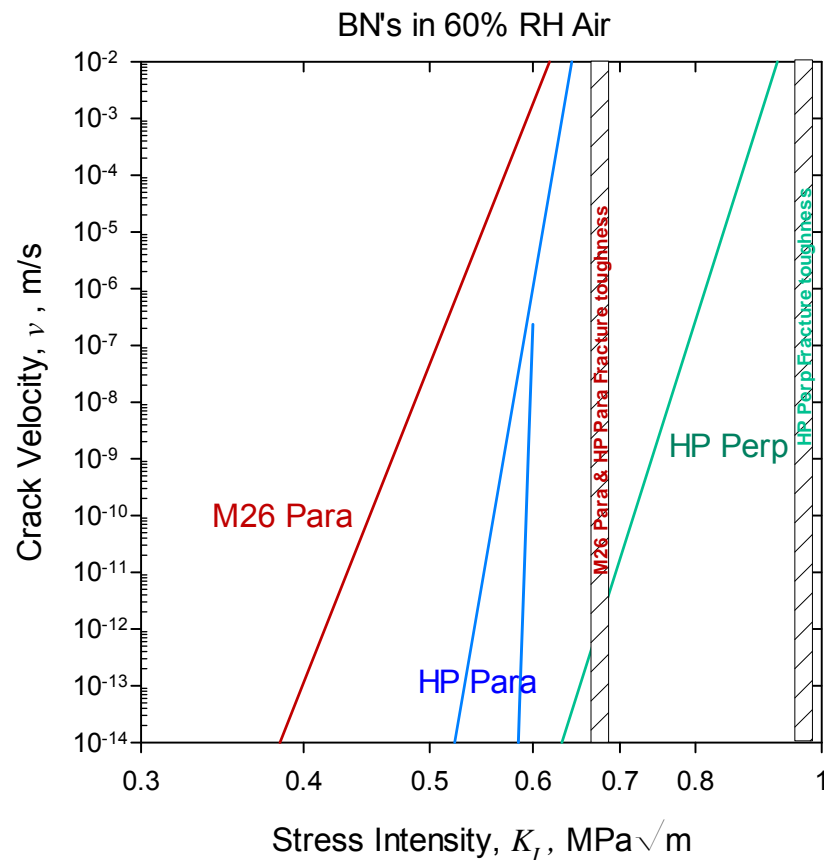
# Results for M26 BN Parallel



- SCG parameter  $n = 55 \pm 5$  is lower (more silica).
- Fairly resistant to SCG. ....

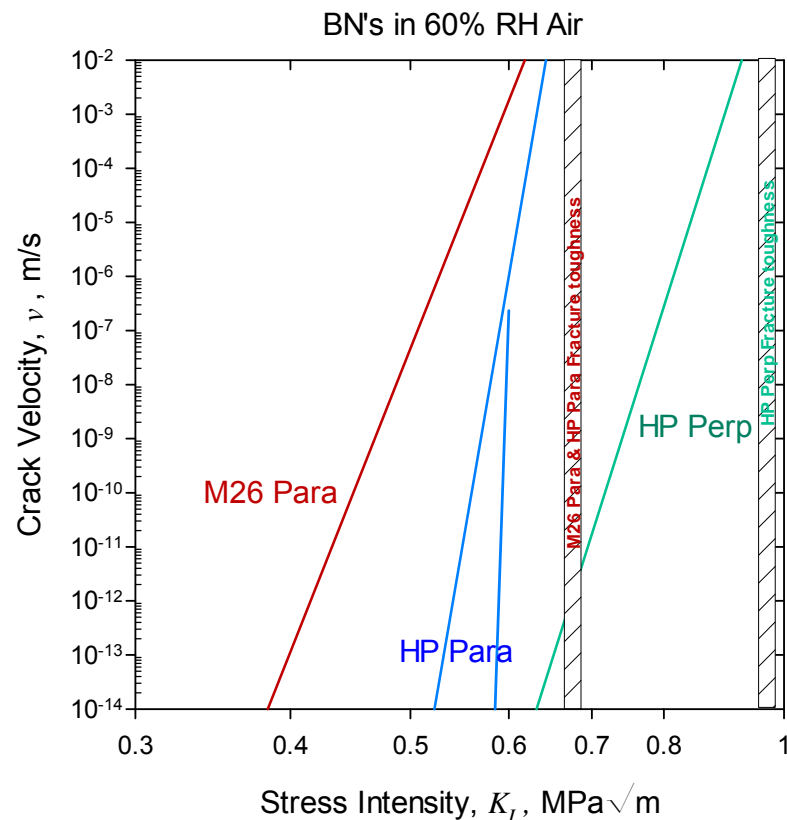


# Crack Velocity Curves

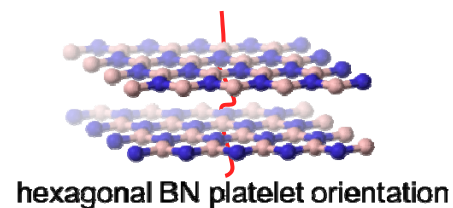


- M26 is the most sensitive to SCG: low  $n$  and low  $K_{Ic}$ .
- Crack growth in HP perp starts around the  $K_{Ic}$  of M26 and HP parallel.

# Crack Velocity Curve



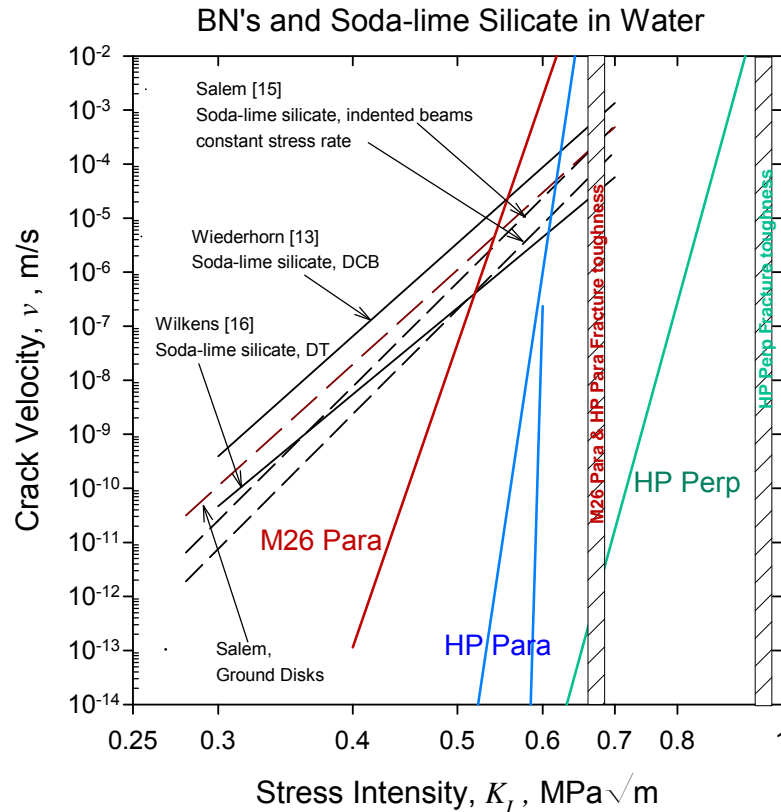
Material	n	Silica Content wt. %
HP Perp	$72 \pm 27$	0
HP Para	$>100$	0
M26 Perp	$58 \pm 11$	32
M26 Para	?	32



- SCG correlates with silica content.....
- Bonds in HP between platelets are insensitive to water.....
- SCG mechanism across platelets may be ionic dissociation of bonds within platelets.



# Crack Velocity Curve



Glasses readily exhibit SCG and thus are a good comparison.

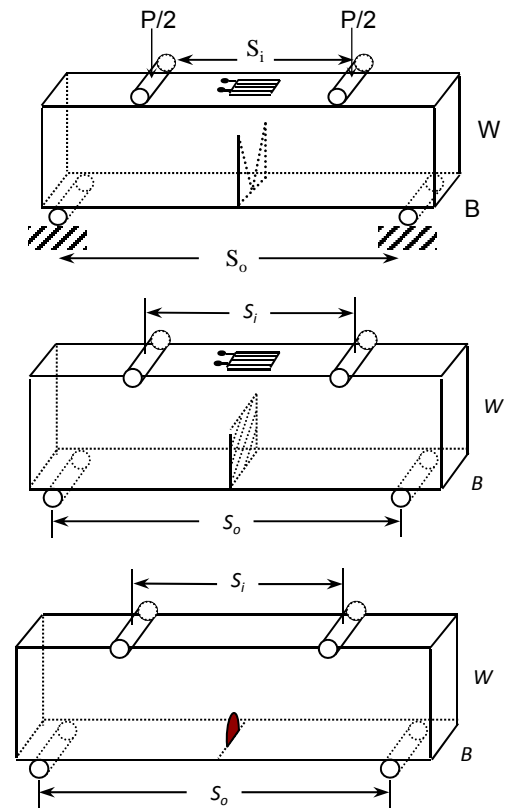
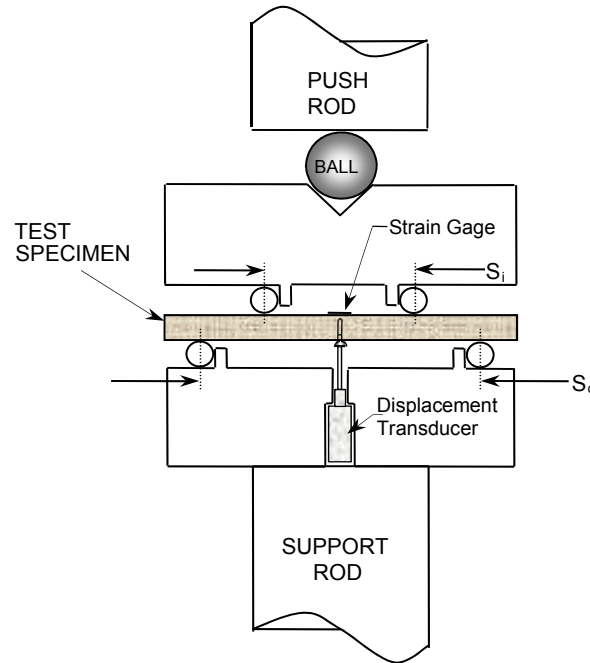
Material	n	Silica Content wt. %
HP Perp	$72 \pm 27$	0
HP Para	$>100$	0
M26 Perp	$58 \pm 11$	32
Glass	20	73
Fused $\text{SiO}_2$	40	100

- As compared to glass, M26 and HP parallel are less sensitive to changes in  $K_I$ , but lower  $K_{IC}$ .



# Fracture Toughness

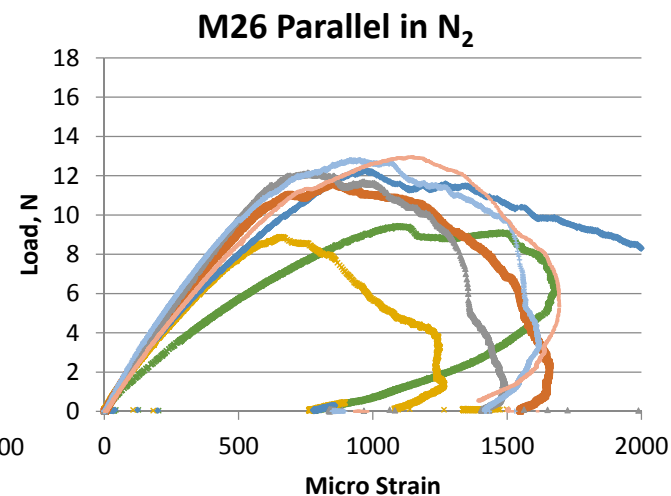
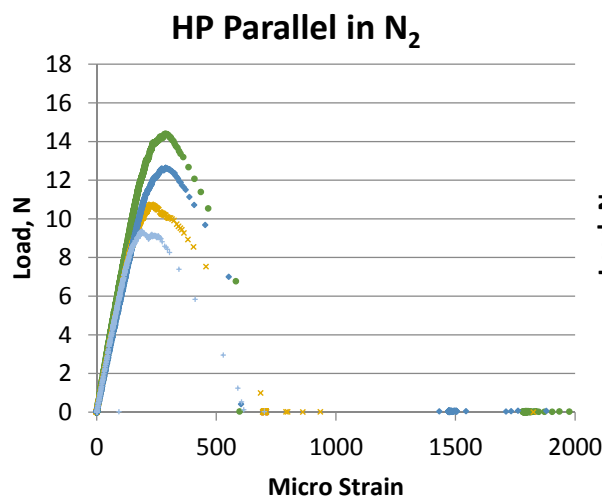
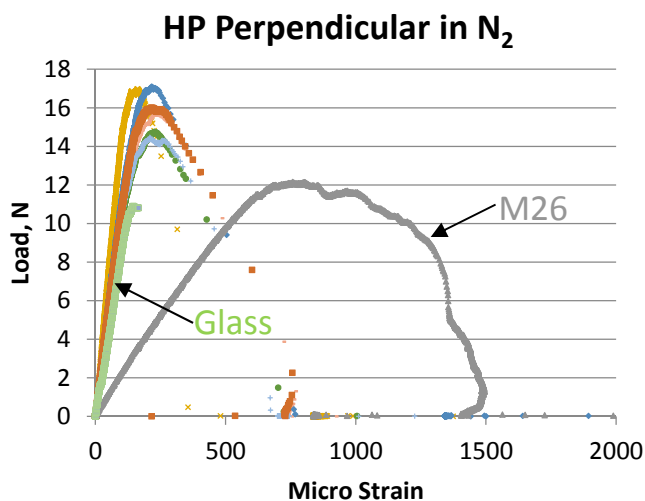
- ❑ Three standard methods are available.
- ❑ Indentation caused crushing w/o cracking.
- ❑ Used the chevron notch.



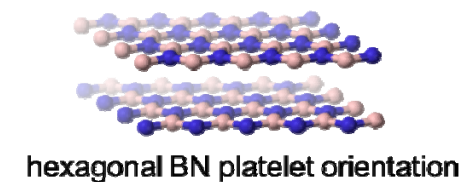
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- ❑ Relatively simple fixtures: test frame, load cell, recording device.

# Fracture Toughness



Material	K (60%)	$K_{Ivb}$ (N <sub>2</sub> ) MPavm	Other Material	$K_{Ivb}$
HP Perp		$0.97 \pm 0.07$	Glass	0.78
HP Para		$0.69 \pm 0.08$	Silca	0.75
M26 Perp		$0.67 \pm 0.05$	SiC	2.8
M26 Para		?	Alumina	4



- Similar to glass. Easier to separate than split the platelets.



# Summary

- BN's exhibits limited slow crack growth in humidity. Testing continues.
- SCG parameters correlate with silica content (?).
- Slow crack growth parameter are a function of test orientation due crystallographic texture & bond type.
- Bonds between platelet are not sensitive to water.
- Bonds within platelets are sensitive to water.
- Fracture toughness is low, around that of glass, and is a function of orientation.
- It is easier to drive a crack between hexagonal BN platelets than across platelets (weak bonds between platelets).



# Summary

- Continuing work:
  - Lot-to-lot variability, fracture toughness, slow crack growth, compression strength, and secondary electron yield.



# Acknowledgements

- Funding provided by NASA Space Technology Mission Directorate.
- Technical assistance provided by NASA Glenn Research Center.

