



# Experimental and Computational Sonic Boom Assessment of Boeing N+2 Low Boom Models

*Fundamental Aeronautics Program  
High Speed Project*

Don Durston  
Alaa Elmiligui  
Susan Cliff  
Courtney Winski  
Melissa Carter  
Eric Walker

Ames Research Center  
Langley Research Center  
Ames Research Center  
Langley Research Center  
Langley Research Center  
Langley Research Center

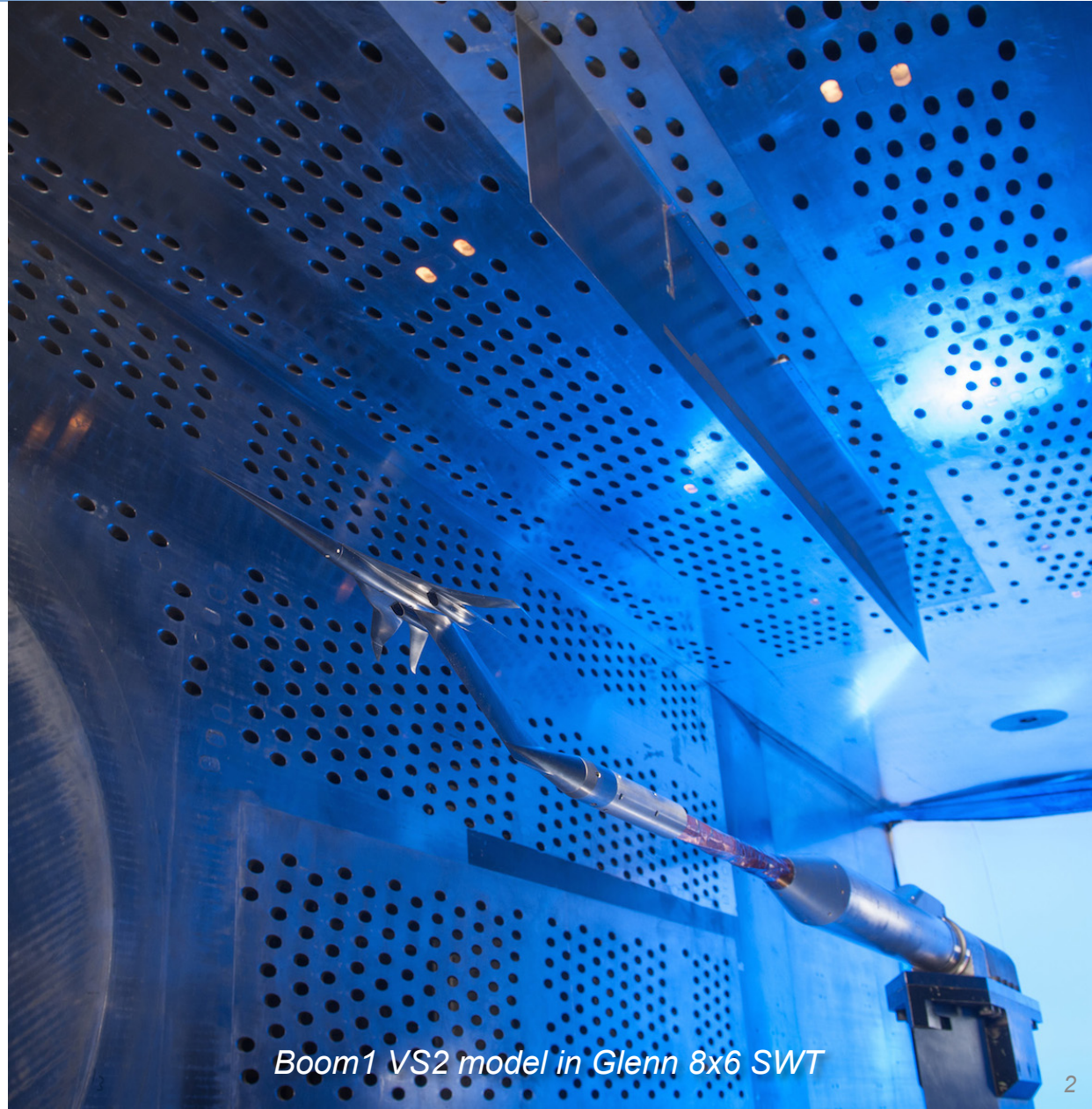
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*Image courtesy of The Boeing Company*



# Outline

- N+2 NRA Studies
  - Study Goals and Objectives
  - Boeing Full-Scale QEVC
- Wind Tunnel Tests
  - Facilities, Models
  - Test Techniques
  - Selected Results
- Computational Tools
- Experiment / CFD Comparisons
  - AS2
  - Boom Models
  - Performance Model
- Conclusions



*Boom1 VS2 model in Glenn 8x6 SWT*

# N+2 NRA Studies

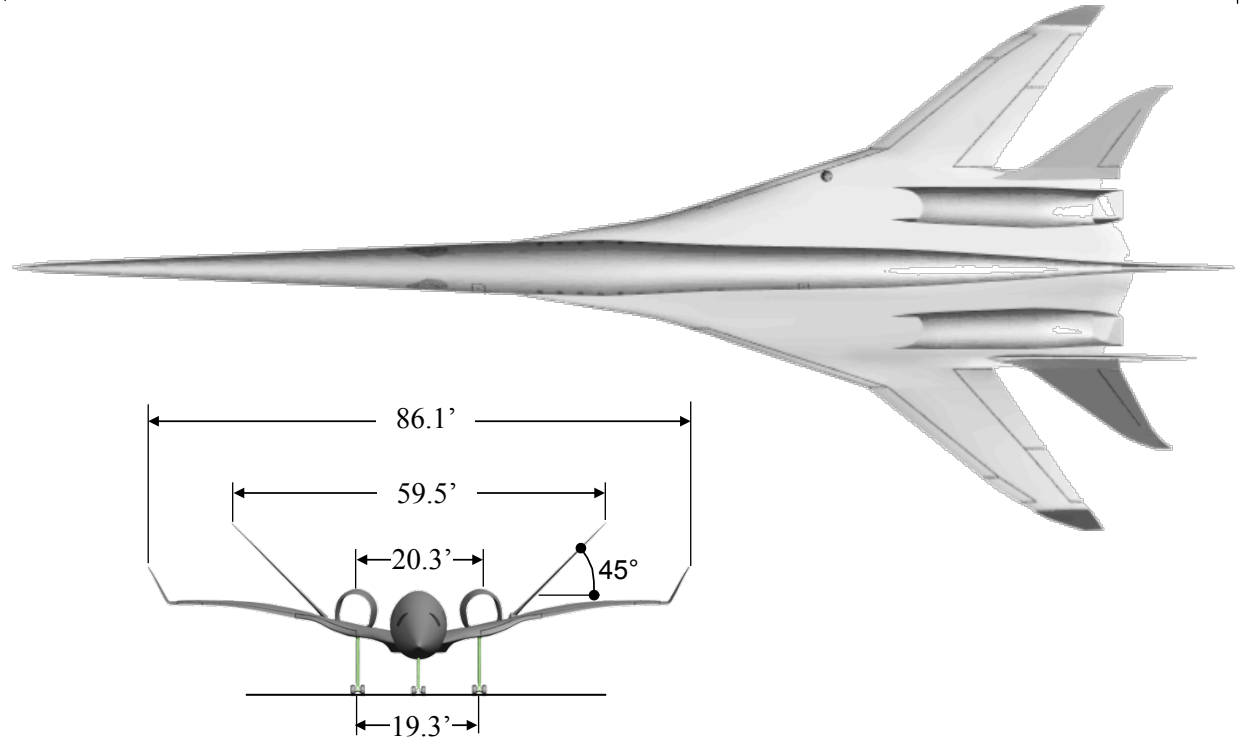
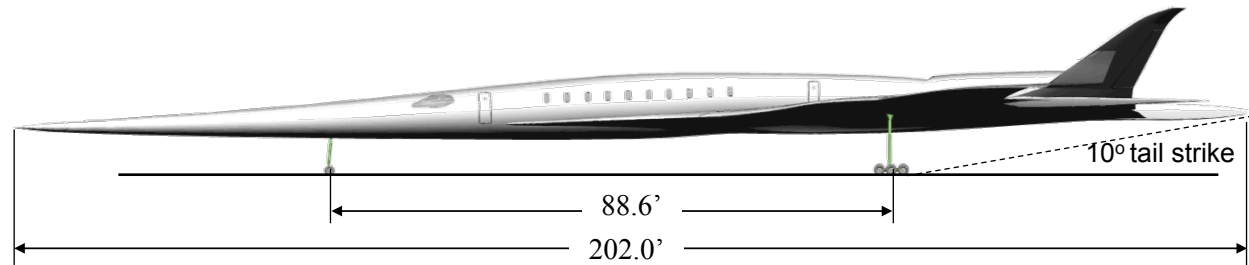
- 3-year, 2-phase study contracts with Boeing and Lockheed-Martin
- Design for N+2 (2<sup>nd</sup>-generation) supersonic transport to meet goals:

Environmental Goals	
Sonic Boom	85 PLdB
Airport Noise (cumulative below stage 3)	10–20 EPNdB
Cruise Emissions	< 10 EIN Ox
Performance Goals	
Cruise Speed	Mach 1.6–1.8 low boom flight
Range	4000 nm
Passengers	35–70
Fuel Efficiency (px-nm per lb of fuel)	3.0

- Phase I: Design for low boom and aerodynamic efficiency
- Phase II: Nacelle/airframe integration, inlet performance and effects on boom

# Boeing QEVC

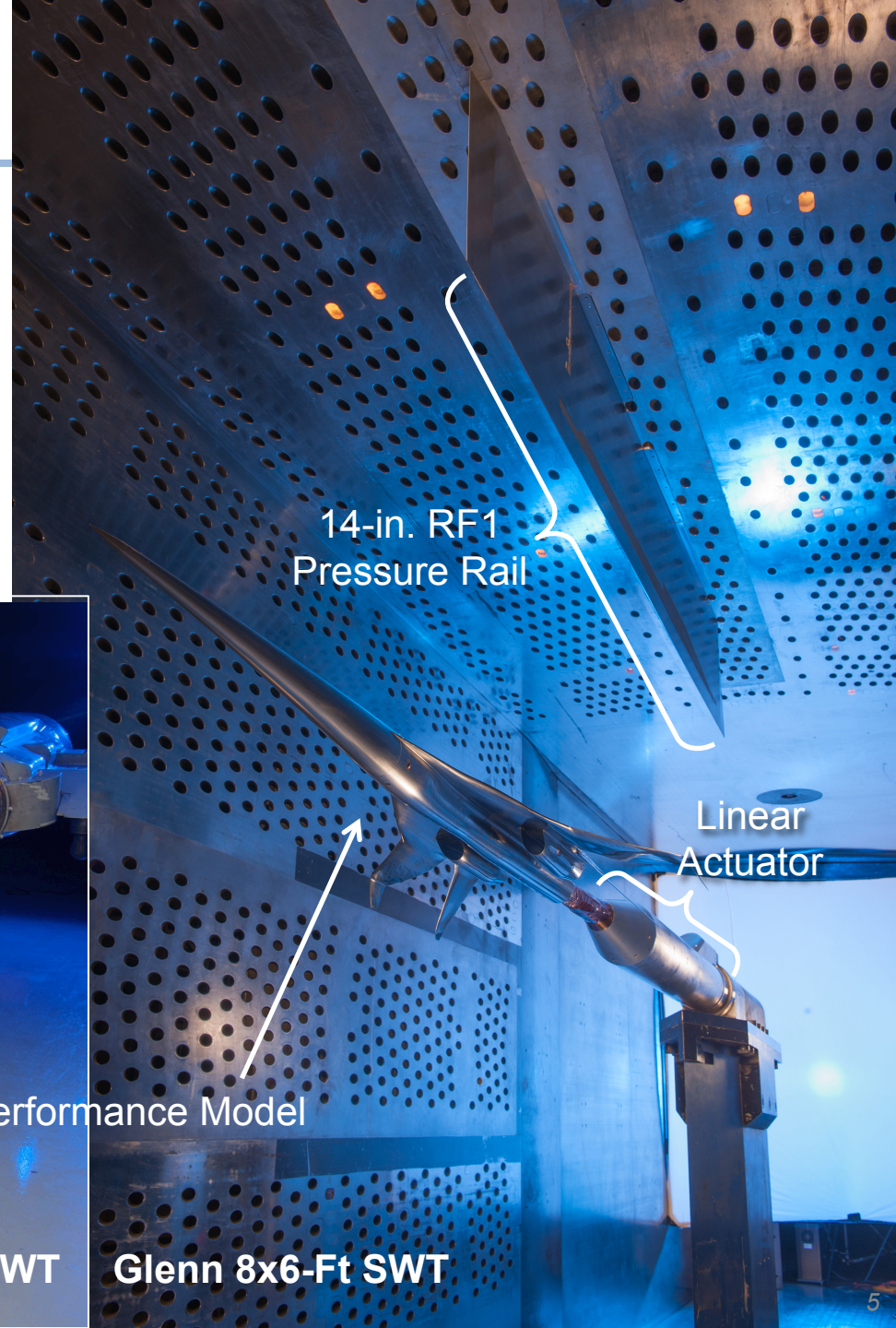
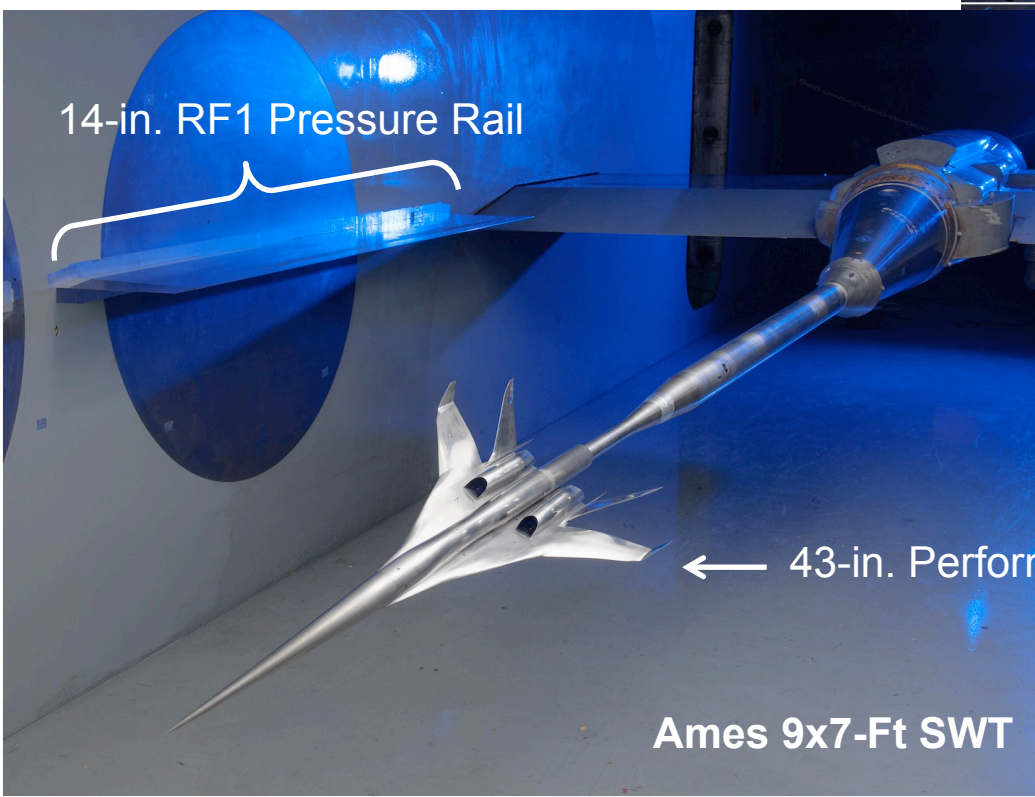
- Quiet Experimental Validation Concept designed in 2009
- Design flight conditions:
  - Mach 1.8
  - $C_L = 0.104$
  - $\alpha = 3.28^\circ$
- 35 to 70 passengers
- Range 4000 nm





# Wind Tunnel Tests

- Ames 9x7 and Glenn 8x6 Supersonic Wind Tunnels
- 14" RF1 pressure rail and 2" flat-top pressure rail
- Mostly Mach 1.6 and 1.8
- Performance model shown here, plus AS2 and Boom models (next page)

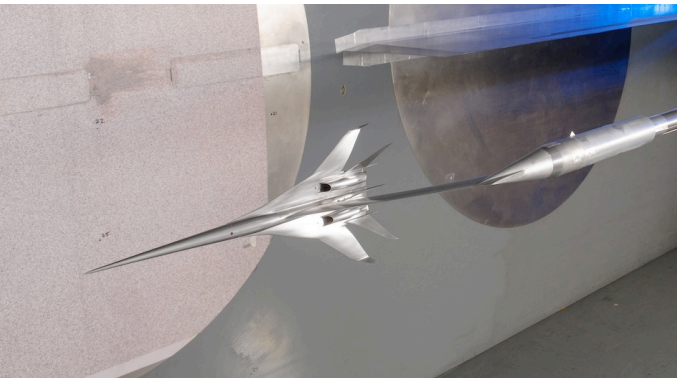


# AS2 and Boom Models and Struts

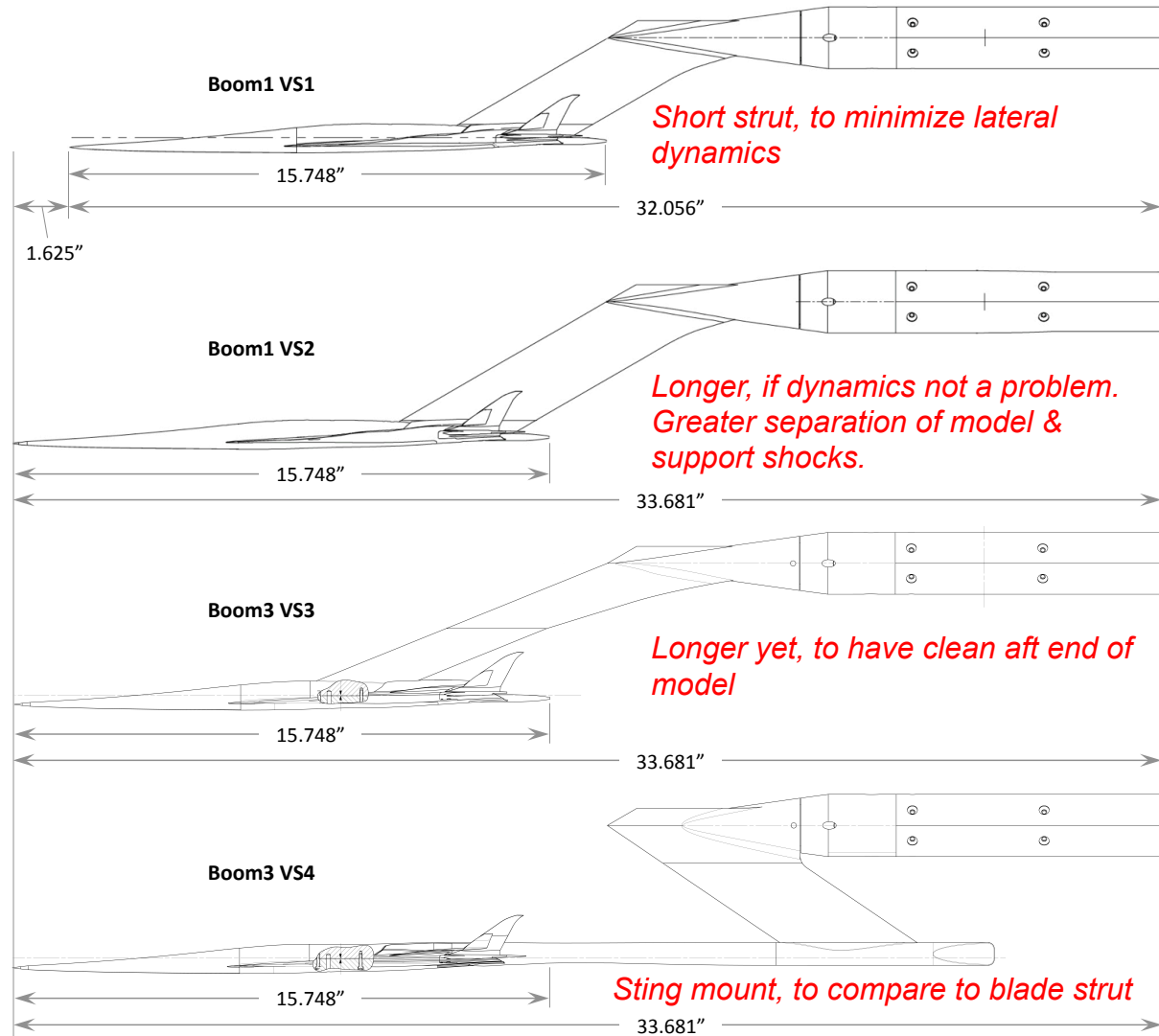
AS2 body of revolution



Boom1 model, VS2 strut



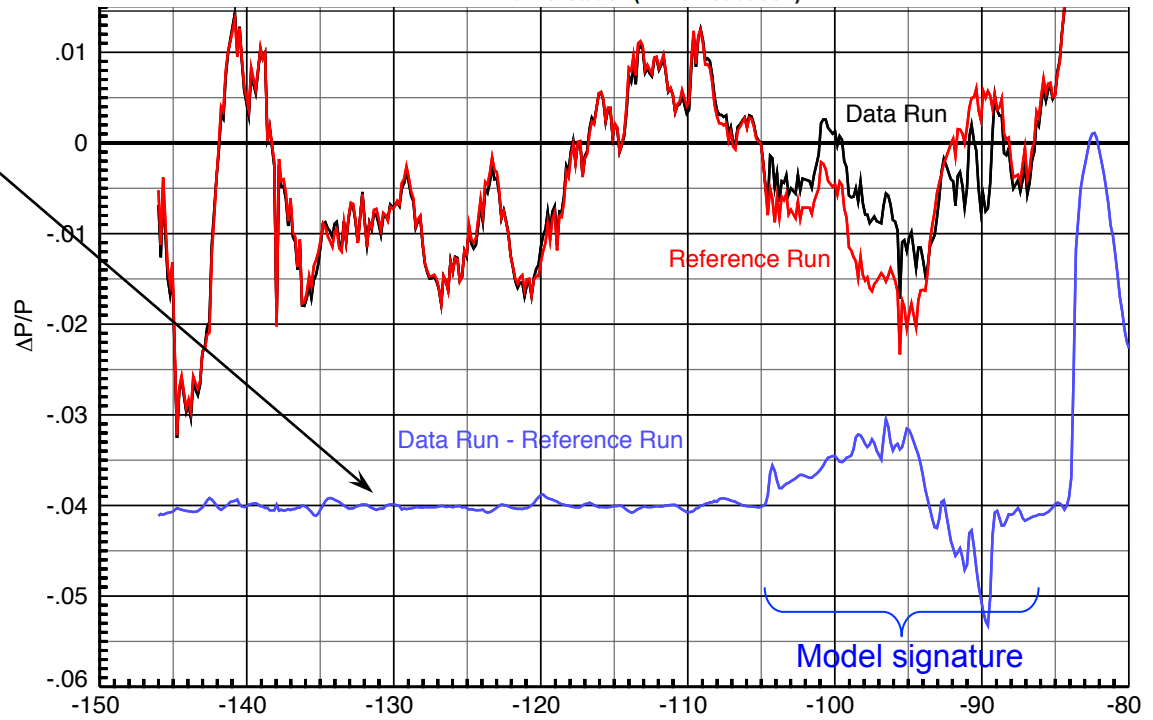
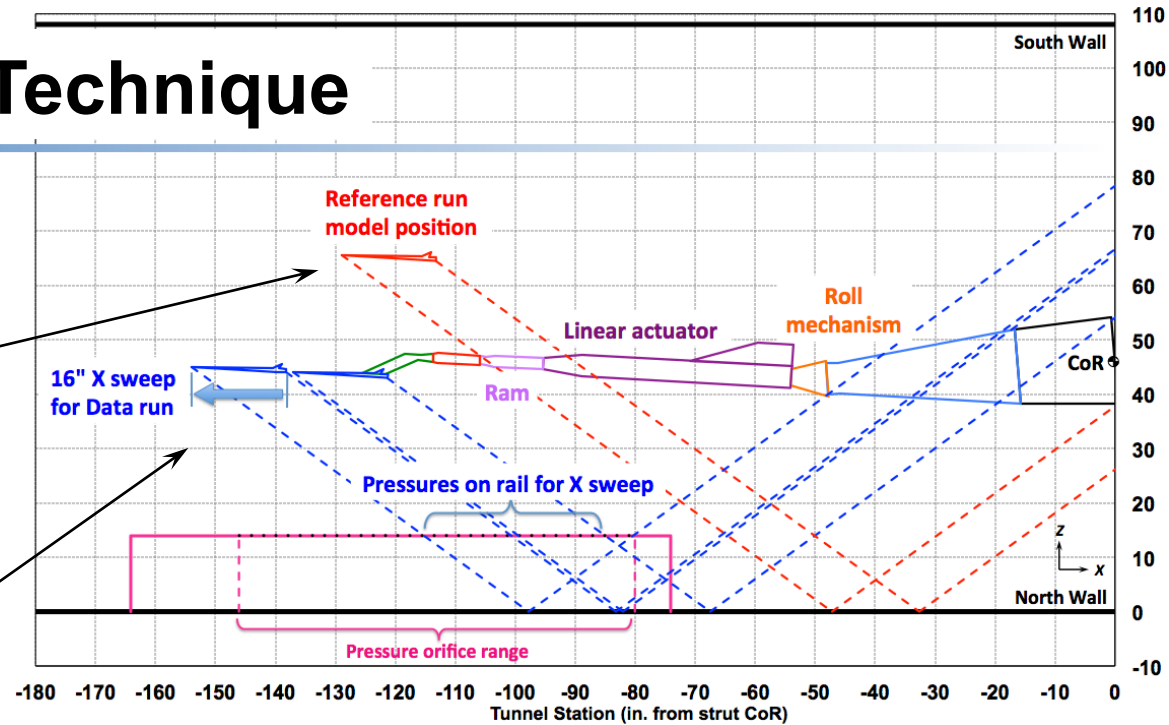
## 4 blade strut options for Boom models





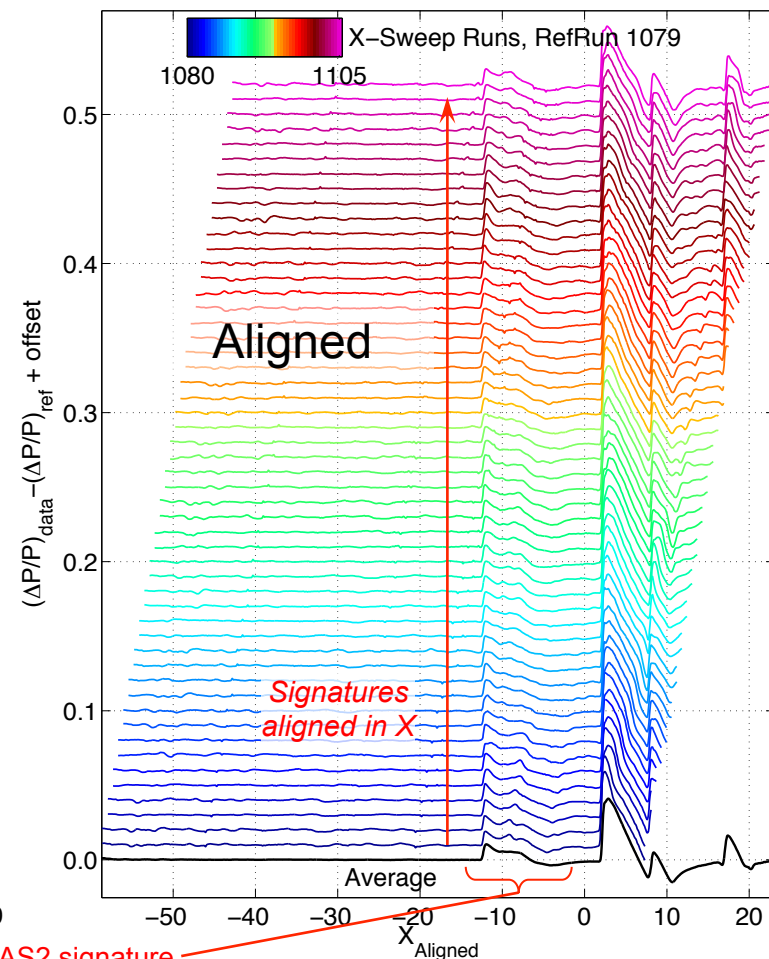
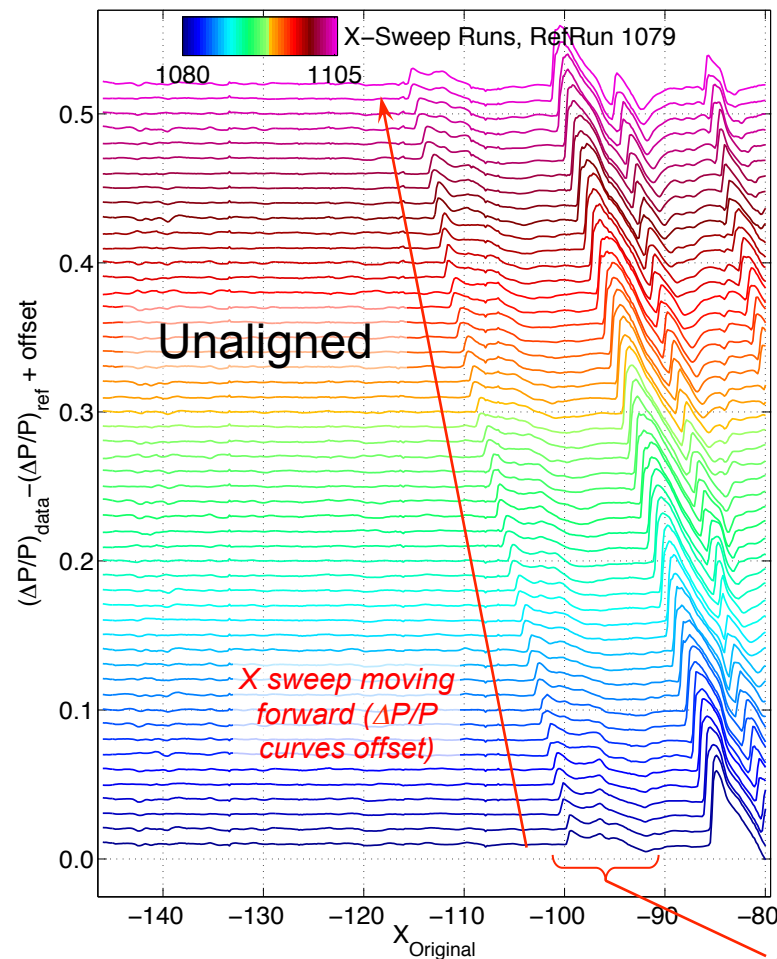
# Pressure Rail Test Technique

- Pressure rail on wall has 420 orifices to capture entire model signature at once
- Reference run taken with model shocks off rail (or at least downstream of where model shocks will be)
- Data run taken with model shocks on rail
- Model signature is *difference* between reference and data runs
- X or Z sweeps conducted to acquire signatures in different regions of tunnel flow
- Sweeps allow for averaging out tunnel spatial flow variations
- Temporal averaging also done with appropriate sampling durations



# Spatial Averaging of Model Signatures

- Example: 26 signatures acquired with ram extension from 8" to 24" (0.63" spacing)
- Distortions due to tunnel flow spatial variations and model vibrations are evident in individual signatures, but averaging reduces these effects



AS2 model  
X sweep in  
9x7 WT,  
Mach 1.6



# Shock Wave Imaging

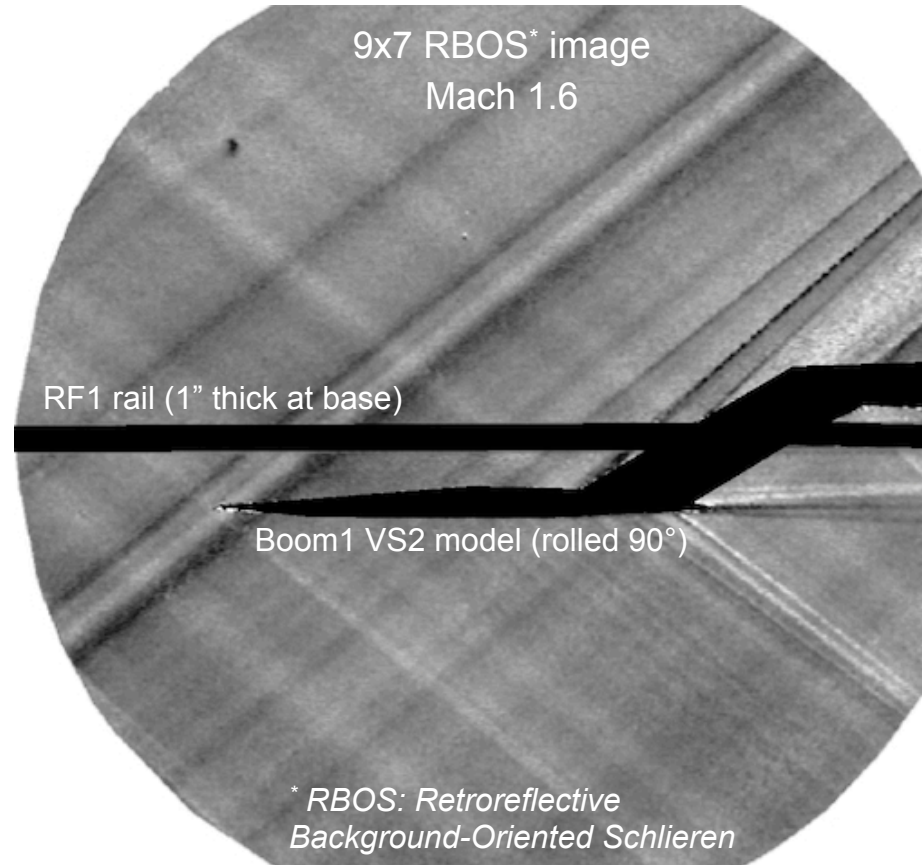
- Facility-generated shock waves often as strong or stronger than model shocks being measured
- Reference runs and spatial averaging minimize effects of facility shocks but cannot eliminate these effects

9x7 shadowgraph  
Empty tunnel  
Mach 1.6



Average Image  
run16 M=1.6 psf=1450  
contrast enhanced  
upstream fwd

9x7 RBOS\* image  
Mach 1.6



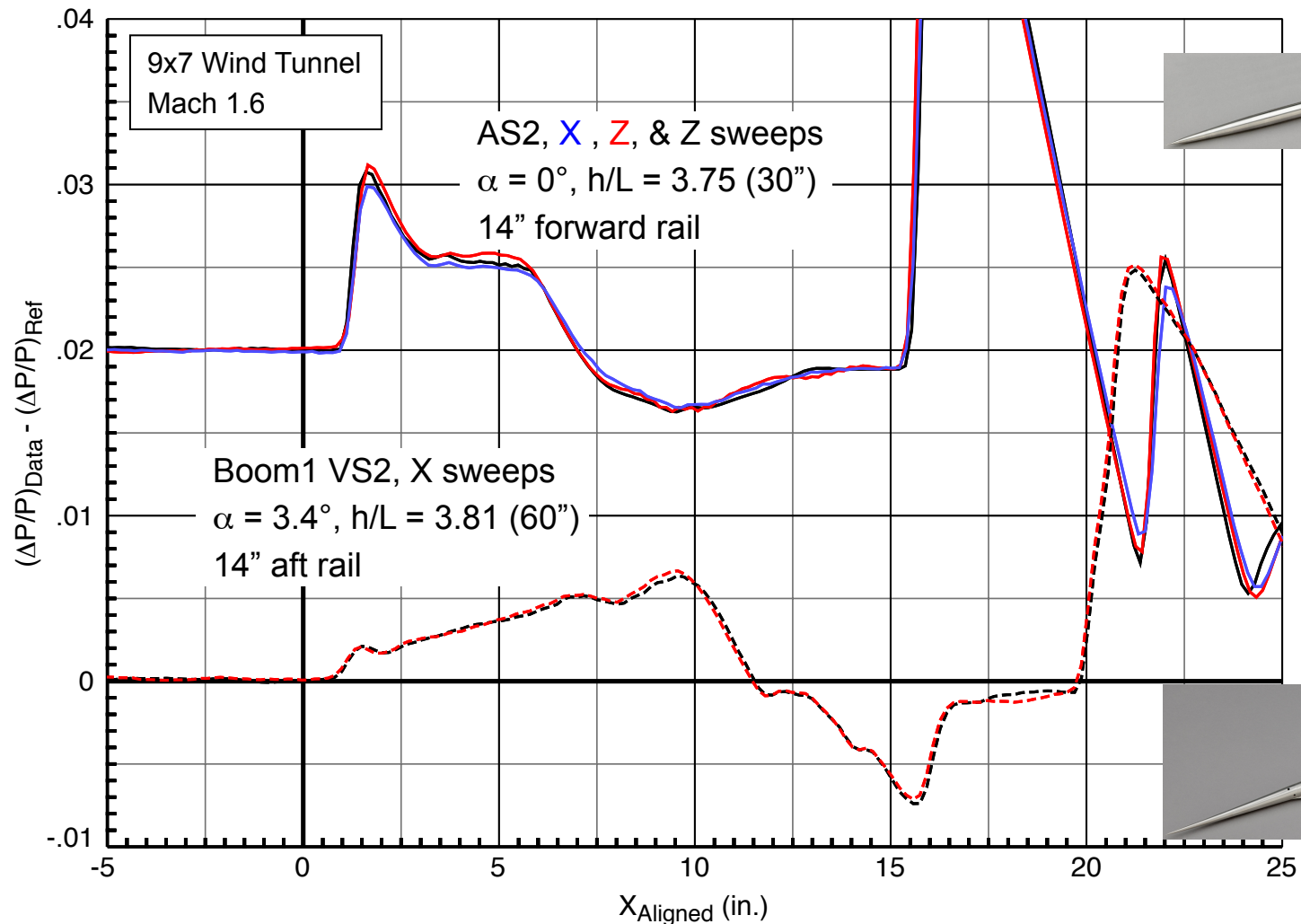
RF1 rail (1" thick at base)

Boom1 VS2 model (rolled 90°)

\* RBOS: Retroreflective  
Background-Oriented Schlieren

# Repeatability of Experimental Data

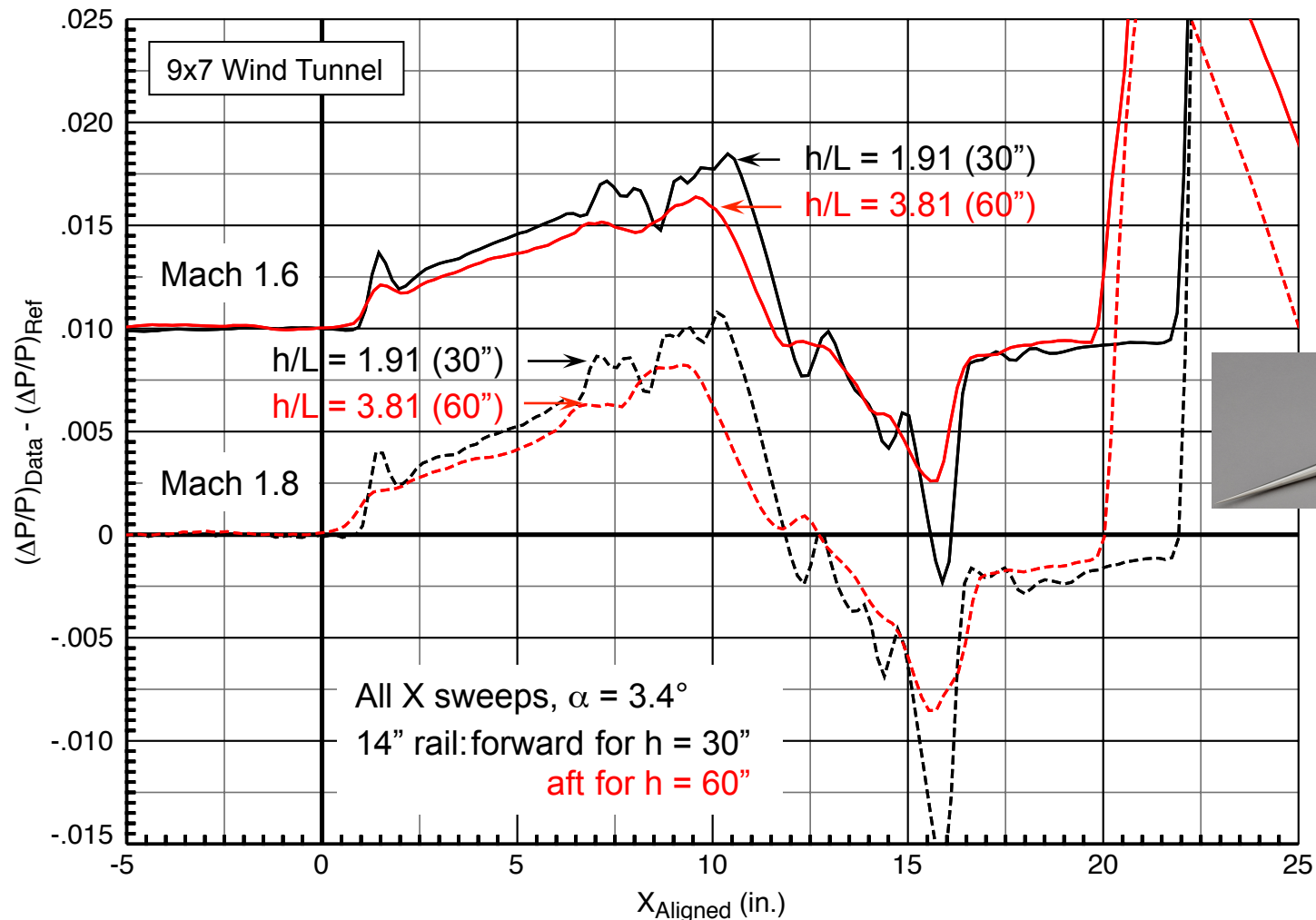
- AS2 and Boom1 VS2 repeat runs show excellent repeatability
- X and Z sweeps give similar results





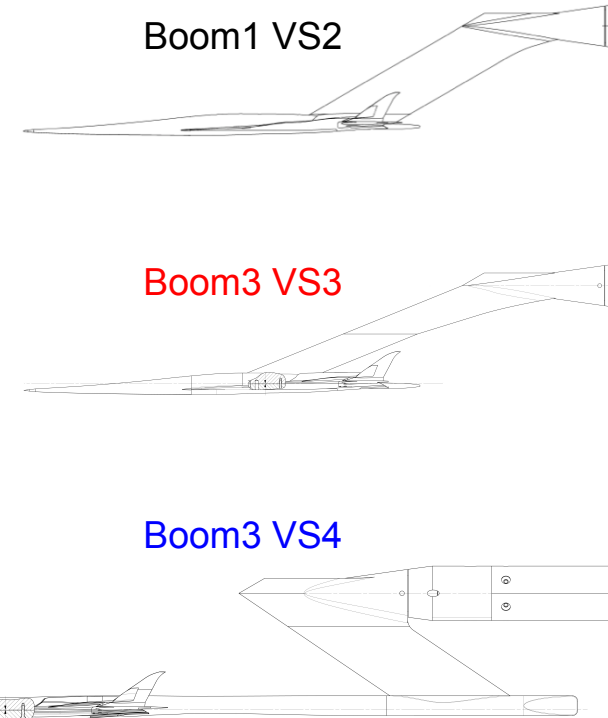
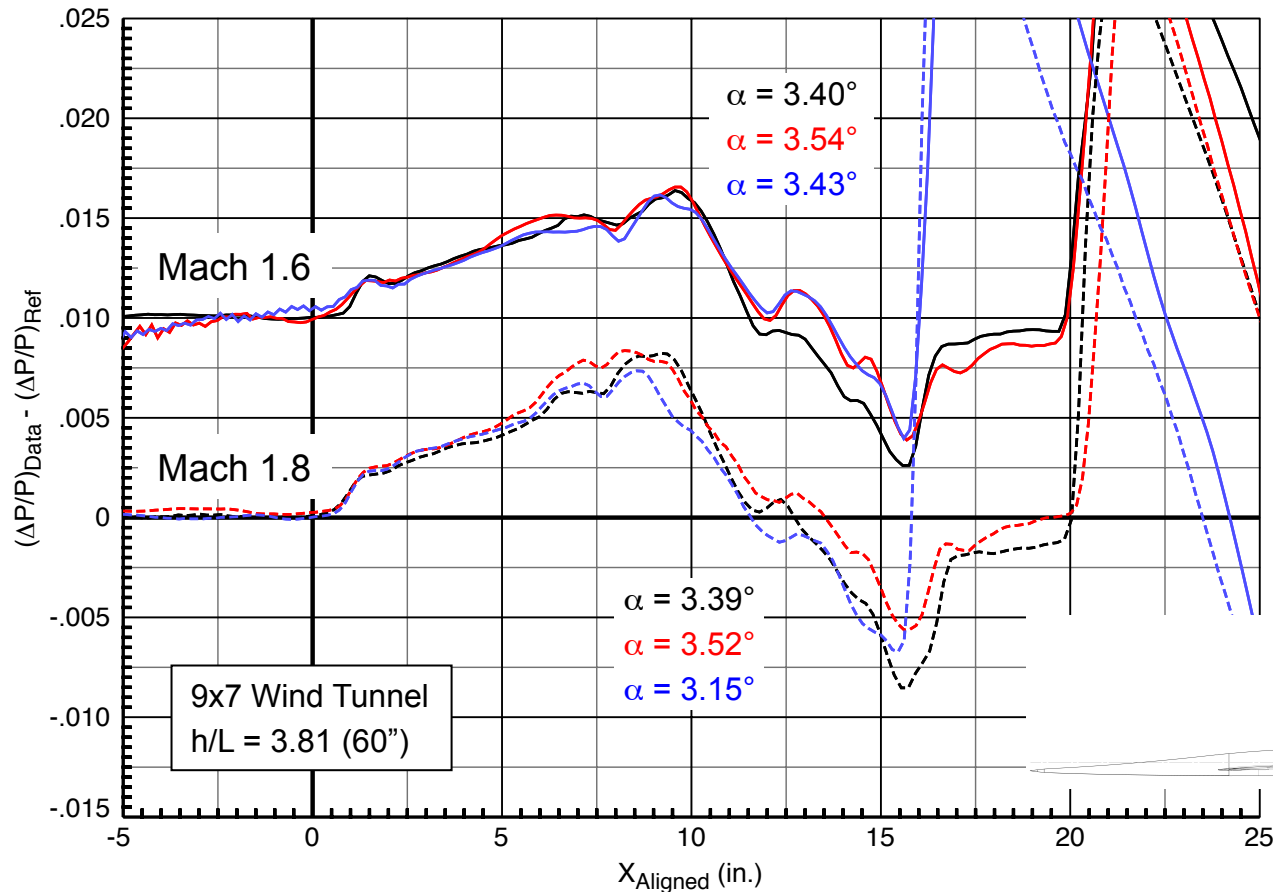
# Effect of Model Height, Boom1 VS2

- Increased height causes rounding of signatures due to aging
- Overall pressure levels decrease with height



# Mounting Strut Effects, Boom Models

- VS2,3,4 struts, Mach 1.6 & 1.8, 14" aft rail, height = 60"
- VS2 & VS3 more similar to each other than to VS4, but VS3 & 4 pressures more similar at Mach 1.6
- Greater differences between VS3 & 4 exist at Mach 1.8, though angle-of-attack differences could account for part of this
- VS4 blade shock overtakes aft end of model signature at both Mach numbers





# Computational Methods

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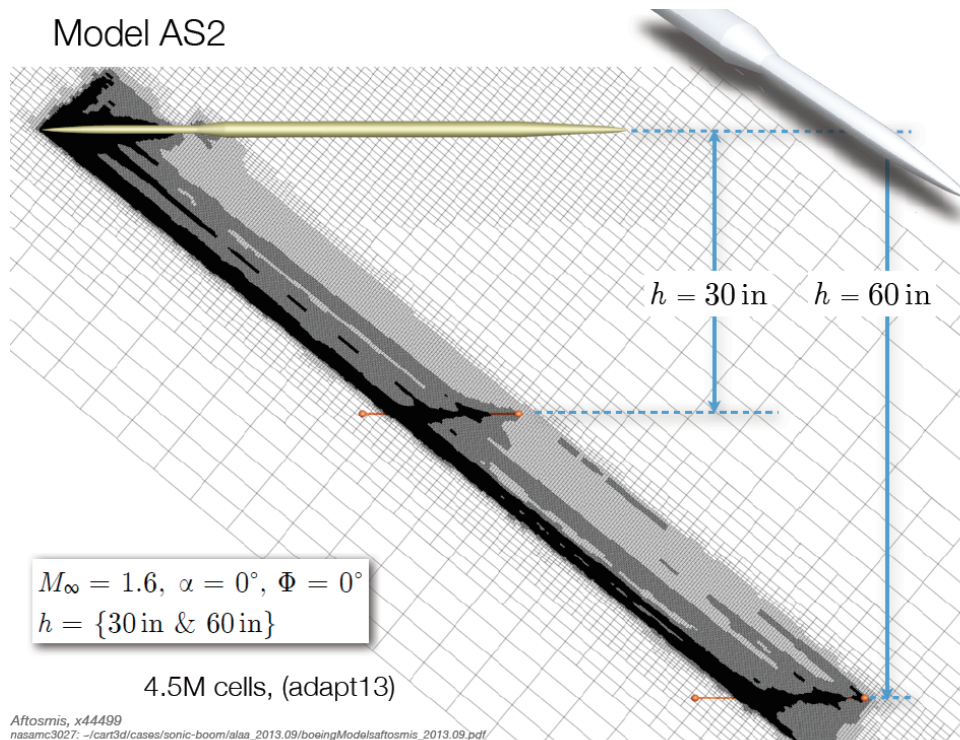
Results from 3 codes presented here:

- **Cart3D**
  - Fast, inviscid, unstructured-mesh analysis package for conceptual and preliminary aerodynamic design
  - Used with Adjoint Error Optimization (AERO) module
- **USM3D**
  - Tetrahedral cell-centered, finite volume Euler and Navier-Stokes (N-S) method
  - Run both inviscid and viscous (laminar, and turbulent with Spalart-Allmaras turbulence model) for this study
- **OVERFLOW**
  - OVERset structured grid FLOW solver used by Boeing for present results
  - Inviscid and turbulent with Spalart-Allmaras turbulence model

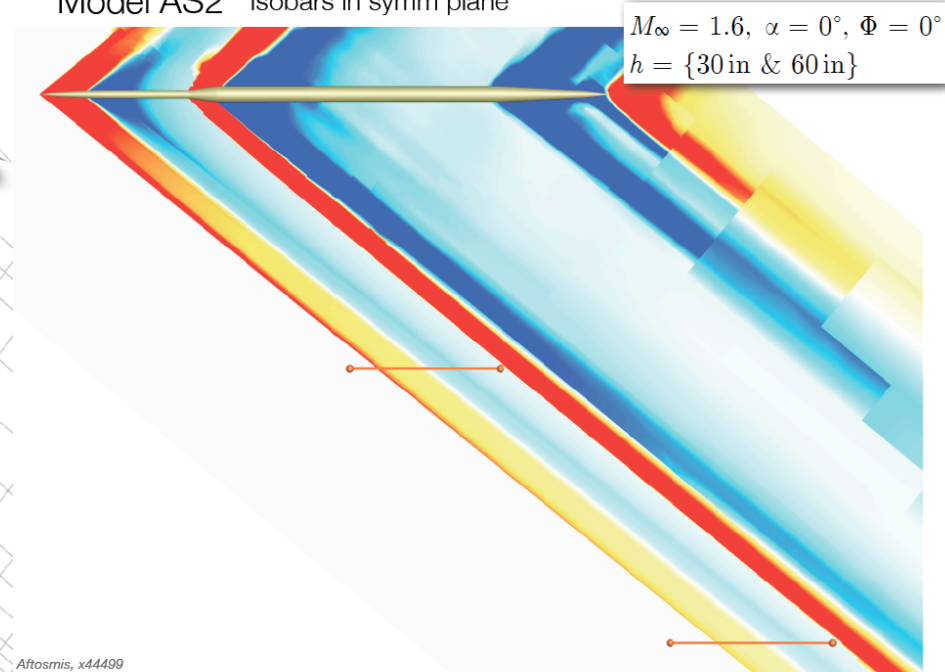
# AS2 Grid and Pressure Contours

- Cart3D adjoint-adapted grid and isobars in symmetry plane
- Sensor lines shown at heights of 30" and 60" for extracting pressure signatures
- Mach 1.6,  $\alpha = 0^\circ$

Model AS2



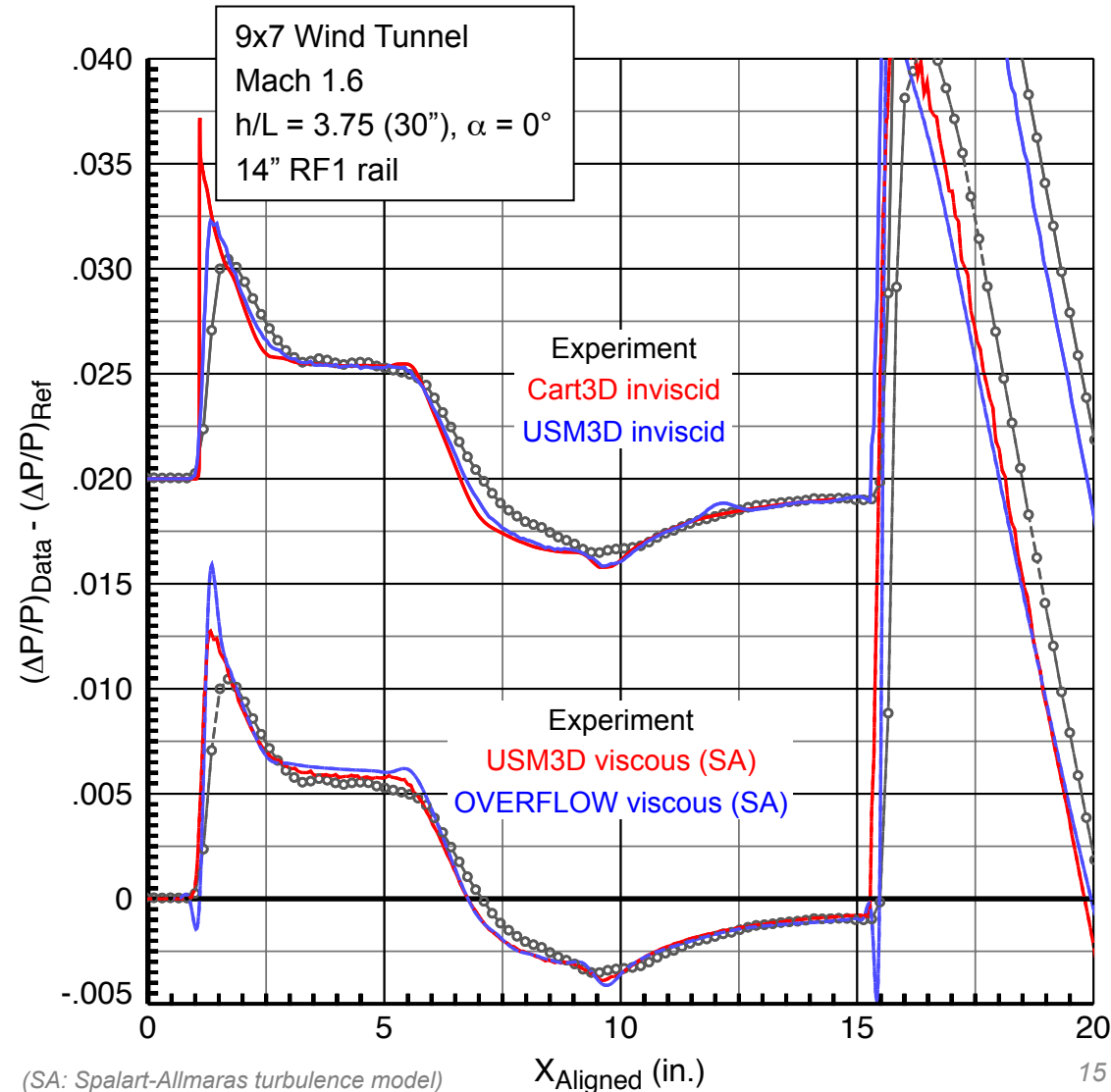
Model AS2 Isobars in symm plane



# AS2 Experiment / CFD Comparisons



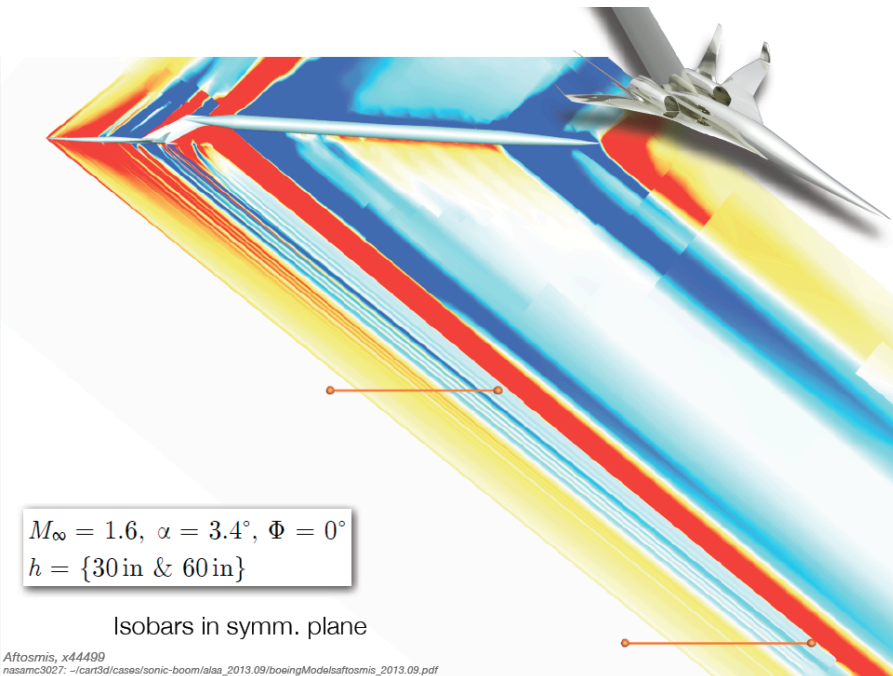
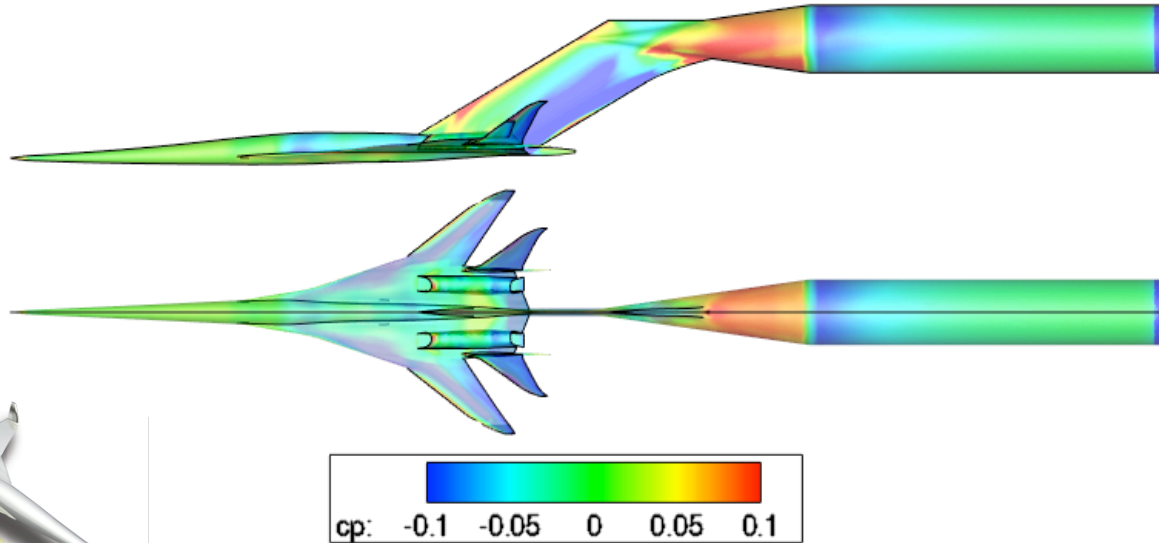
- Flat region aft of nose shock predicted well
- All CFD codes overpredict nose shock relative to experiment
  - Shock in WT data may be rounded due to flow irregularities
  - Viscous solutions not necessarily better than inviscid
- All CFD codes predict lower pressures in main expansion than experiment
  - Similar differences found for other bodies of revolution tested (not shown here)
  - Error was thought to be related to impingement of rail LE shock on aft part of model, but that was found to not be a factor





# Boom1 VS2 Pressure Contours

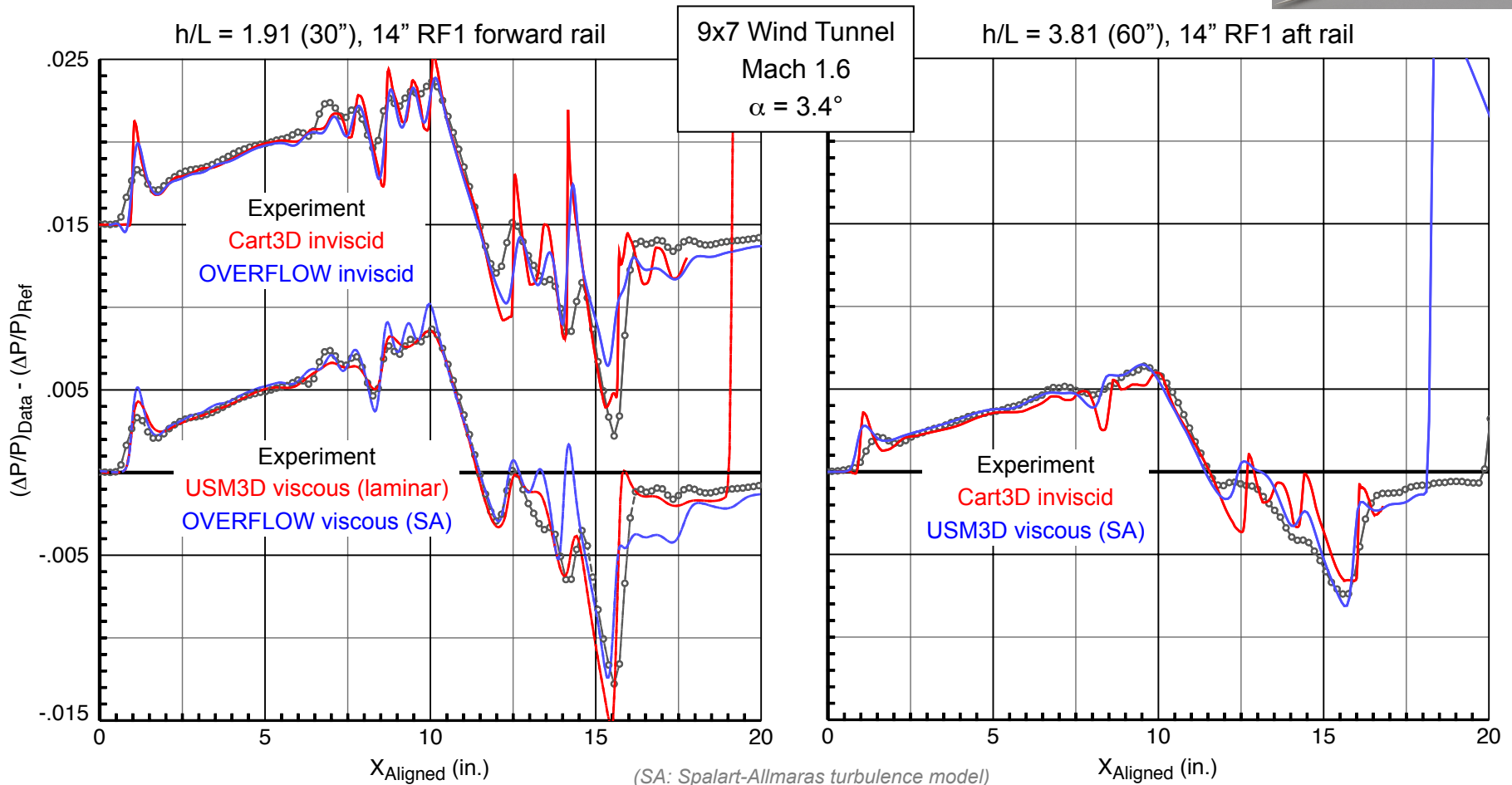
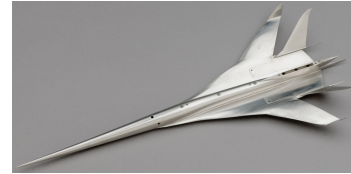
- Surface pressure contours computed by USM3D with laminar boundary layers
- Mach 1.6,  $\alpha = 3.4^\circ$



- Symmetry plane pressure contours computed by Cart3D
- Mach 1.6,  $\alpha = 3.4^\circ$

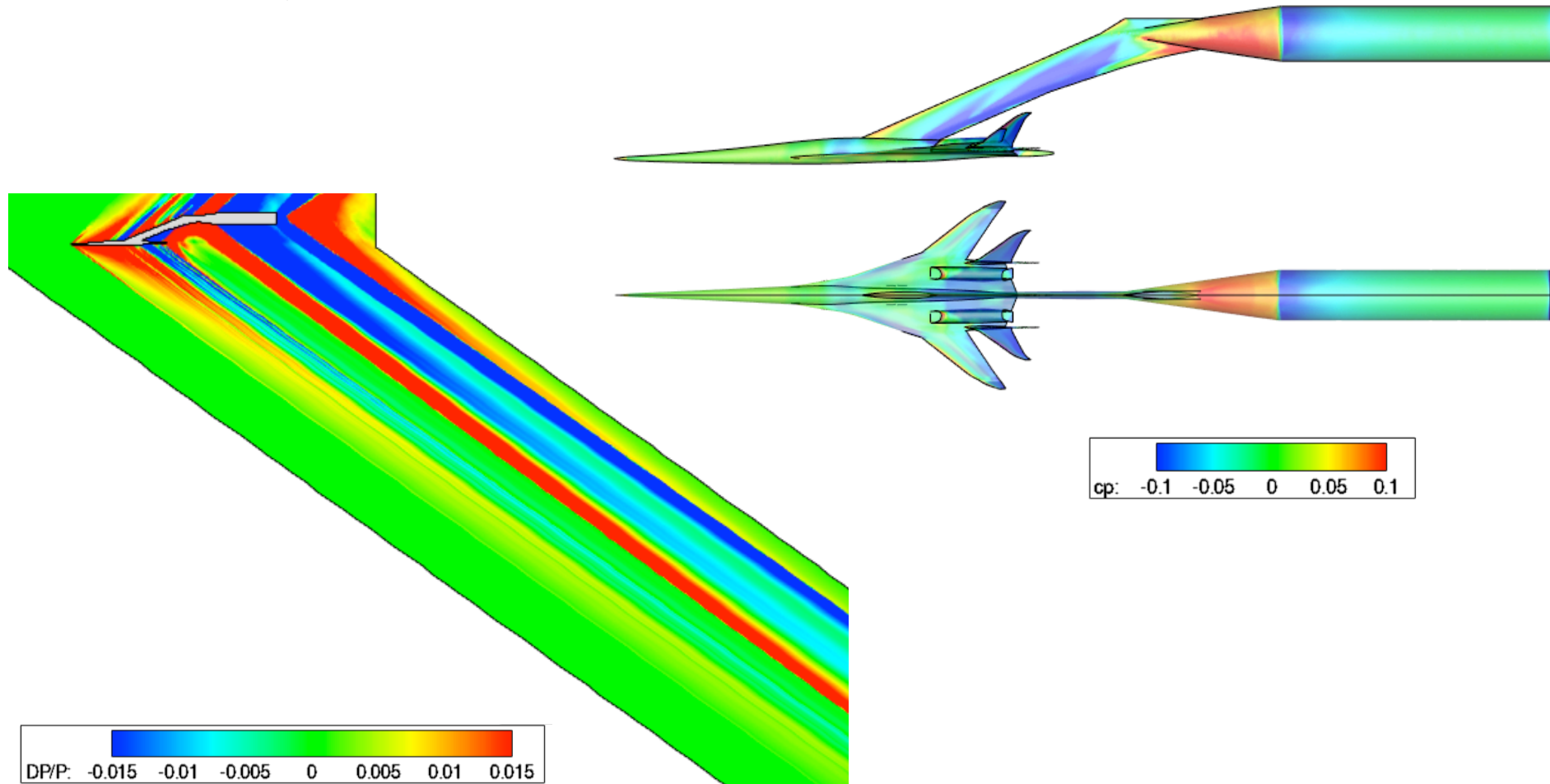
# Boom1 VS2 Experiment / CFD Comparisons

- Inviscid shock peaks are overpredicted relative to viscous
- USM3D laminar prediction matches exp. data better than turbulent prediction from OVERFLOW
- Effects of model height well-captured by predictions



# Boom3 VS3 Pressure Contours

- Surface pressures and symmetry plane flow field pressures computed by USM3D with laminar boundary layers
- Mach 1.6,  $\alpha = 3.1^\circ$

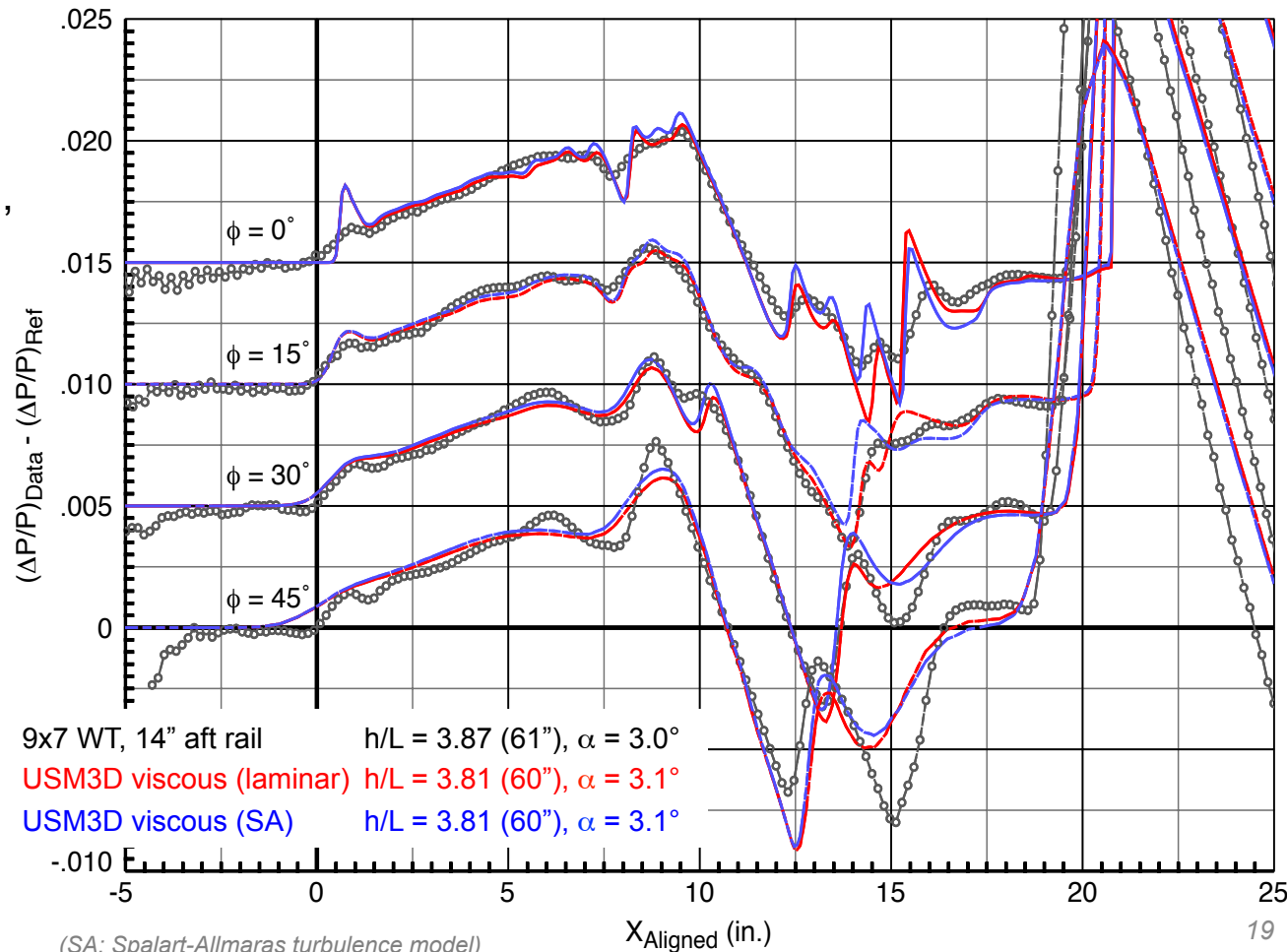




# Boom3 VS3 Experiment / CFD Comparisons at Various Off-Track Angles

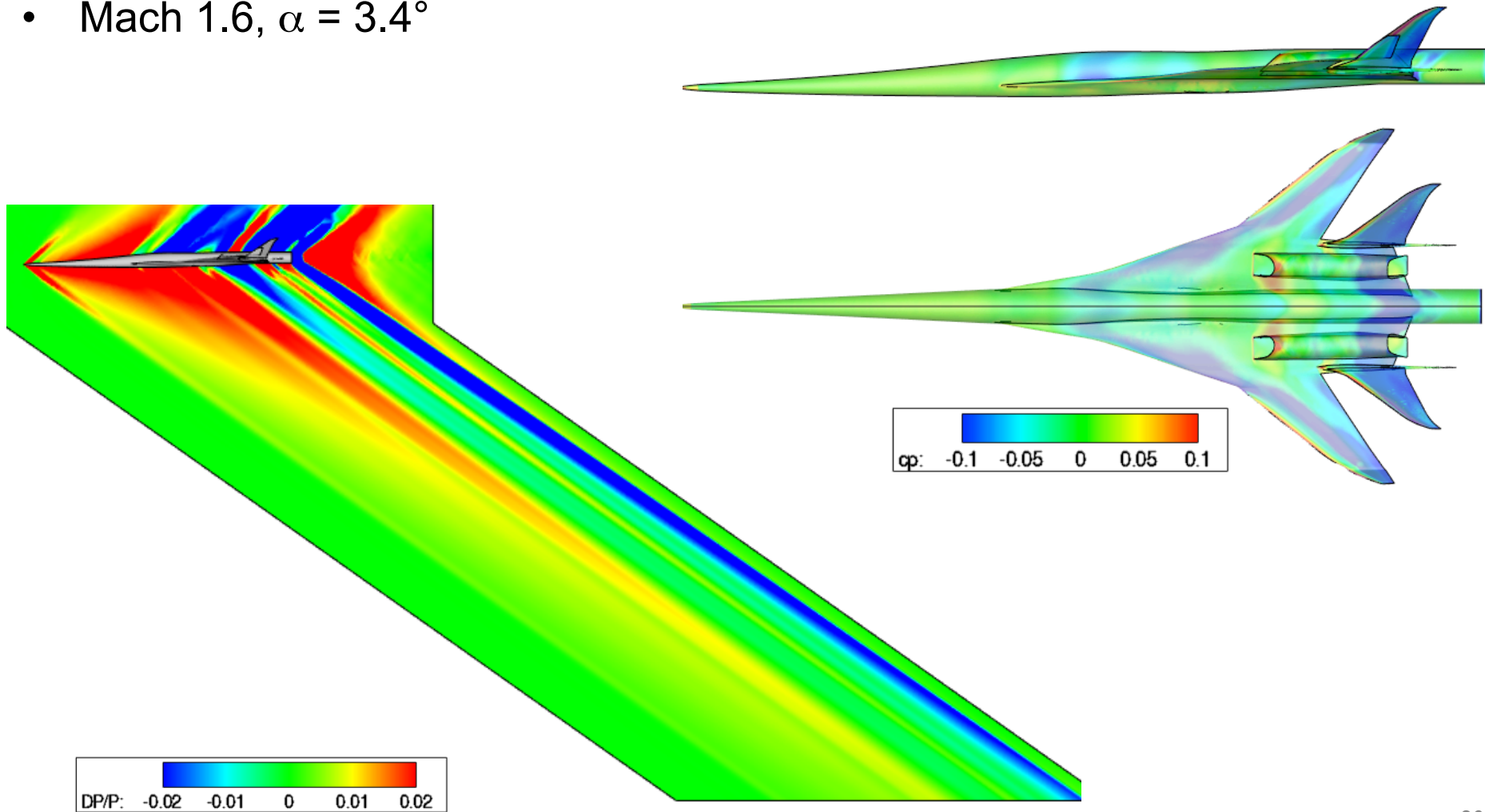


- Best exp./CFD agreement at 15° off-track angle, though all predictions capture front ramp and main expansion fairly well
- Nose shock strength overpredicted by USM3D at  $\phi = 0^\circ$ , but this diminishes to no shock by  $\phi = 45^\circ$ , even though experimental data still show it
- Experimental shocks somewhat washed out by spatial averaging, CFD tends to show more detail, especially at  $\phi = 0^\circ$
- *Issues with experimental & CFD data are still being investigated...*



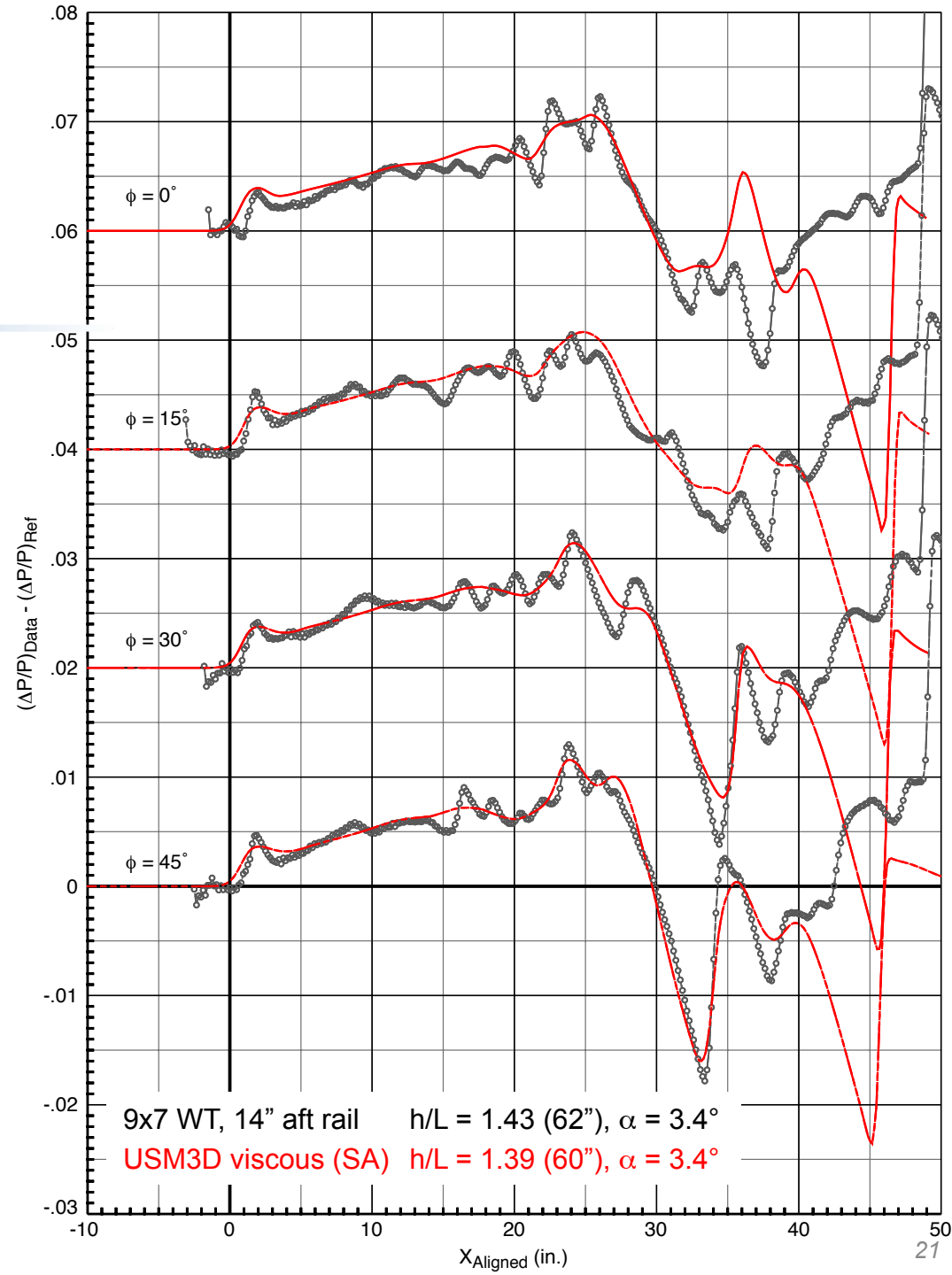
# Performance Model Surface Pressure Contours

- Surface pressures and symmetry plane flow field pressures computed by USM3D with SA turbulent model
- Mach 1.6,  $\alpha = 3.4^\circ$



# Performance Model Experiment / CFD Comparisons at Various Off-Track Angles

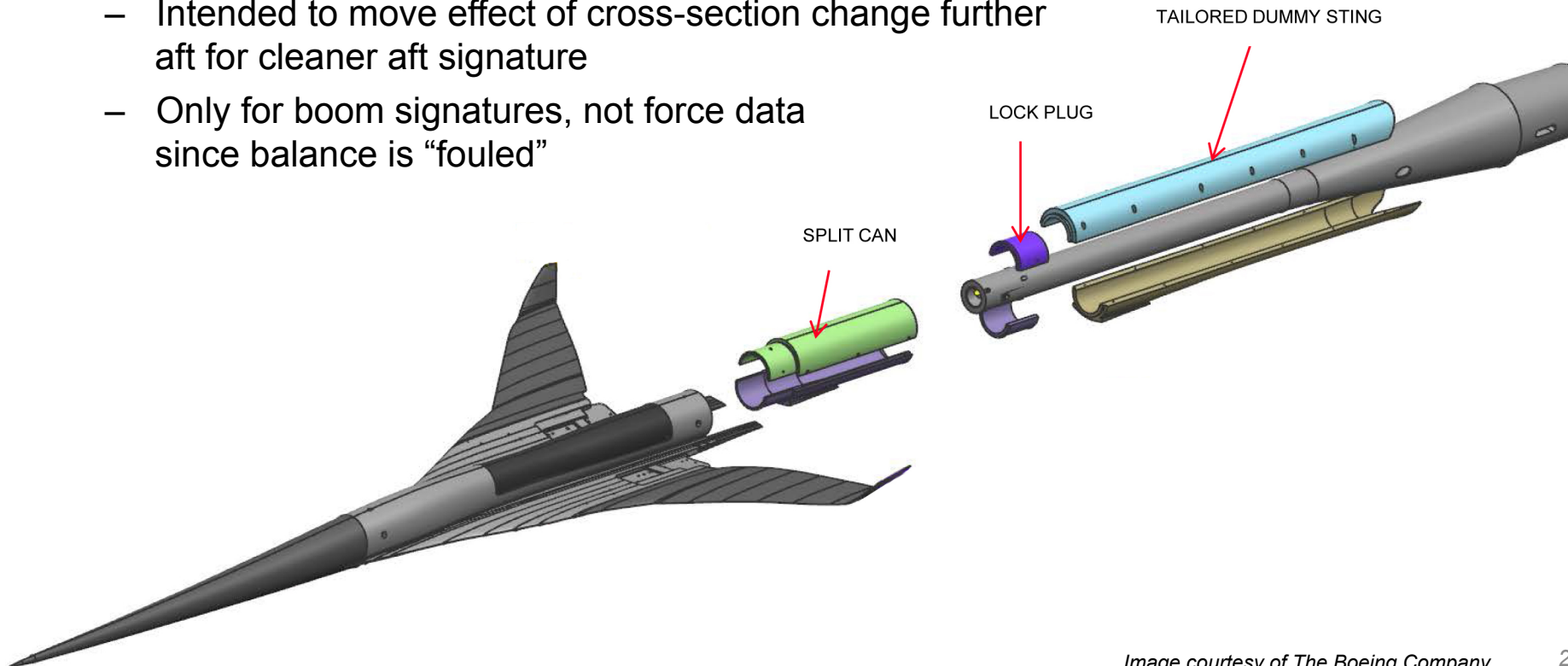
- Exp.: Performance model with tailored dummy sting  
CFD: Performance model with sting can
  - Shocks after main expansion not expected to match
- CFD captures general trends of front ramp and main expansion, but exp. data have many more small shocks
  - These small shocks not seen in Boom model data
  - Forebody contours on Performance model are smooth, not sure what is causing the shocks
- *Issues with experimental & CFD data are still being investigated...*





# Performance Model Sting Options

- Model originally run with sting can
  - Extends circular shape of aft body about 6"
  - Has cavity and aft-facing step down to sting diameter
- Tailored dummy sting (covers) made during Phase II
  - Used in place of sting can
  - Continues aft-body shape about 17" behind model
  - Intended to move effect of cross-section change further aft for cleaner aft signature
  - Only for boom signatures, not force data since balance is "fouled"



# Conclusions

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- Wind tunnel tests were conducted and CFD predictions were made in support of N+2 NRA studies
- Spatial-averaging test technique yielded good repeatability of model signatures—removed distortions due to different locations of models relative to rail
- 14-in. “RF1” rail data matched CFD fairly well, 2-in. rail data required correction for reflection factor
- Inviscid CFD flow solvers generally overpredicted shock strengths, inclusion of boundary layer effects in viscous solvers gave better results
- **Validation of CFD predictions with test data in these N+2 studies has significantly advanced the state of the art in low-boom aircraft design and test, and gives confidence in being able to design for low boom**

# Questions?

