



SIMULATIONS OF THE NASA LANGLEY 14- BY 22-FOOT SUBSONIC TUNNEL FOR THE JUNCTURE FLOW EXPERIMENT

April 16, 2018

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Juncture Flow Experiment

Sponsored by NASA's Transformative Aeronautics Concepts Program's Transformational Tools and Technologies (T³) project

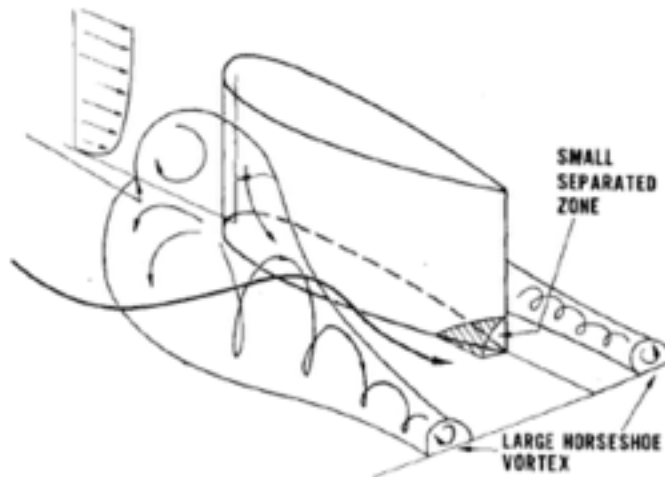
- Substantial effort to investigate the origin of separation bubbles found in wing-body juncture zones
- Primary goal is to gather validation level data, for future CFD code & turbulence model development
- Multi-year effort including several large-scale wind tunnel tests
 - First set of entries just finished: Nov 2017-April 2018
 - Planned Entries in 2019, 2020



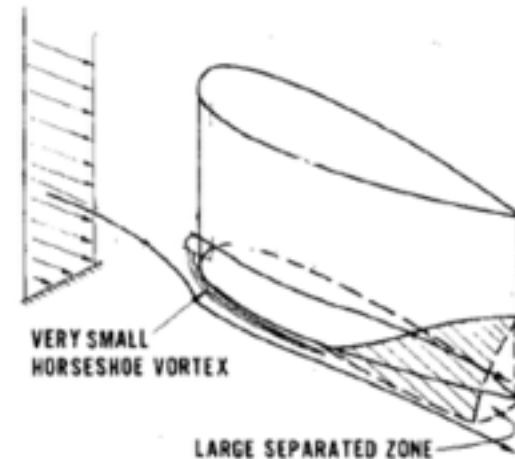
Juncture Flow Physics



- Flow physics of juncture flows is complex
 - Several vortical structures coexist: e.g., Horseshoe Vortex (HSV), corner vortex, stress-induced vortex
 - Many factors: incoming boundary layer momentum thickness, wing bluntness, and wing sweep, etc



(a) thick boundary layer

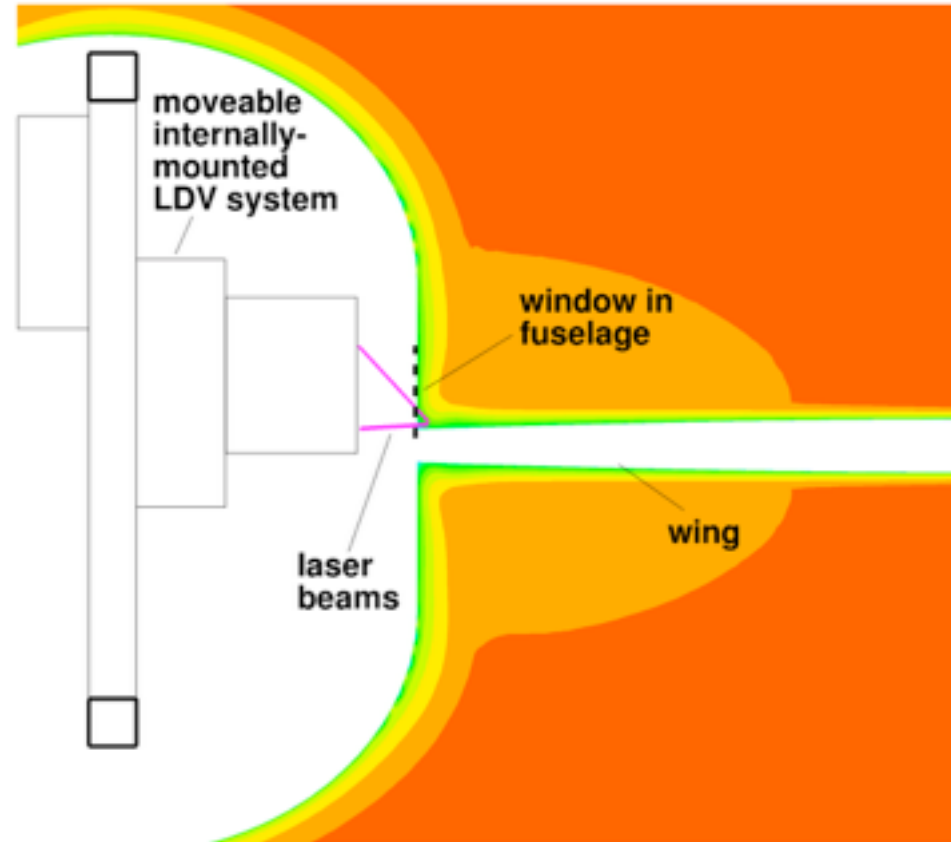


(b) thin boundary layer

Model proposed
by Barber et al.

Juncture Flow LDV

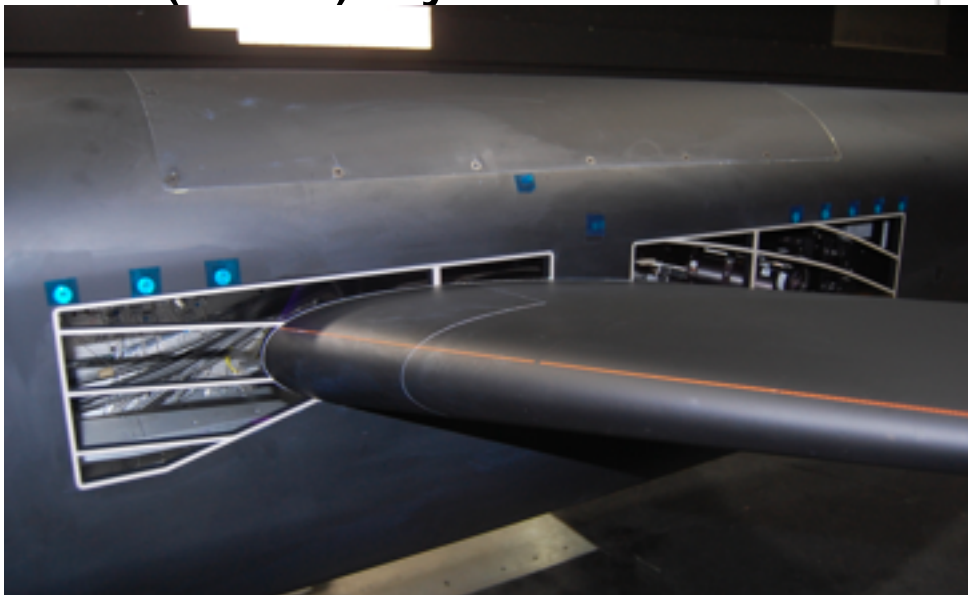
- Use internal Laser Doppler Velocimetry (LDV) system
 - Mounted inside of the fuselage
 - Movable three-axis traverse system
 - Measure the flow field through window on fuselage
 - Closest possible location to wing-body juncture



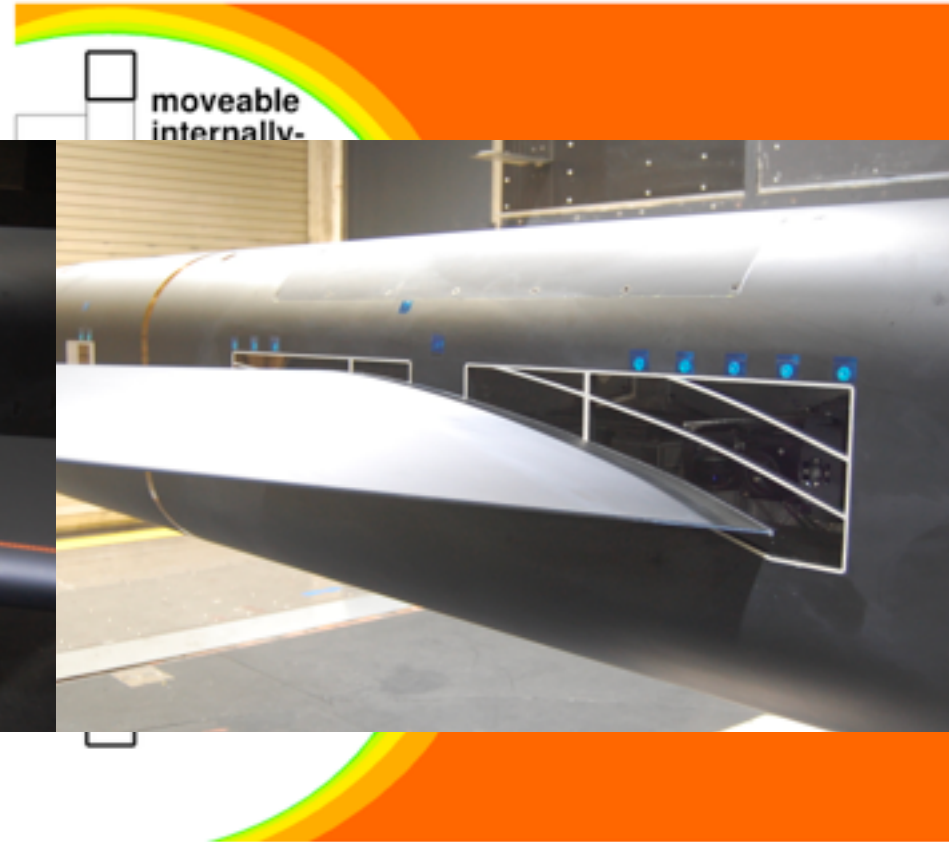
Juncture Flow LDV



- Use internal Laser Doppler Velocimetry (LDV) system



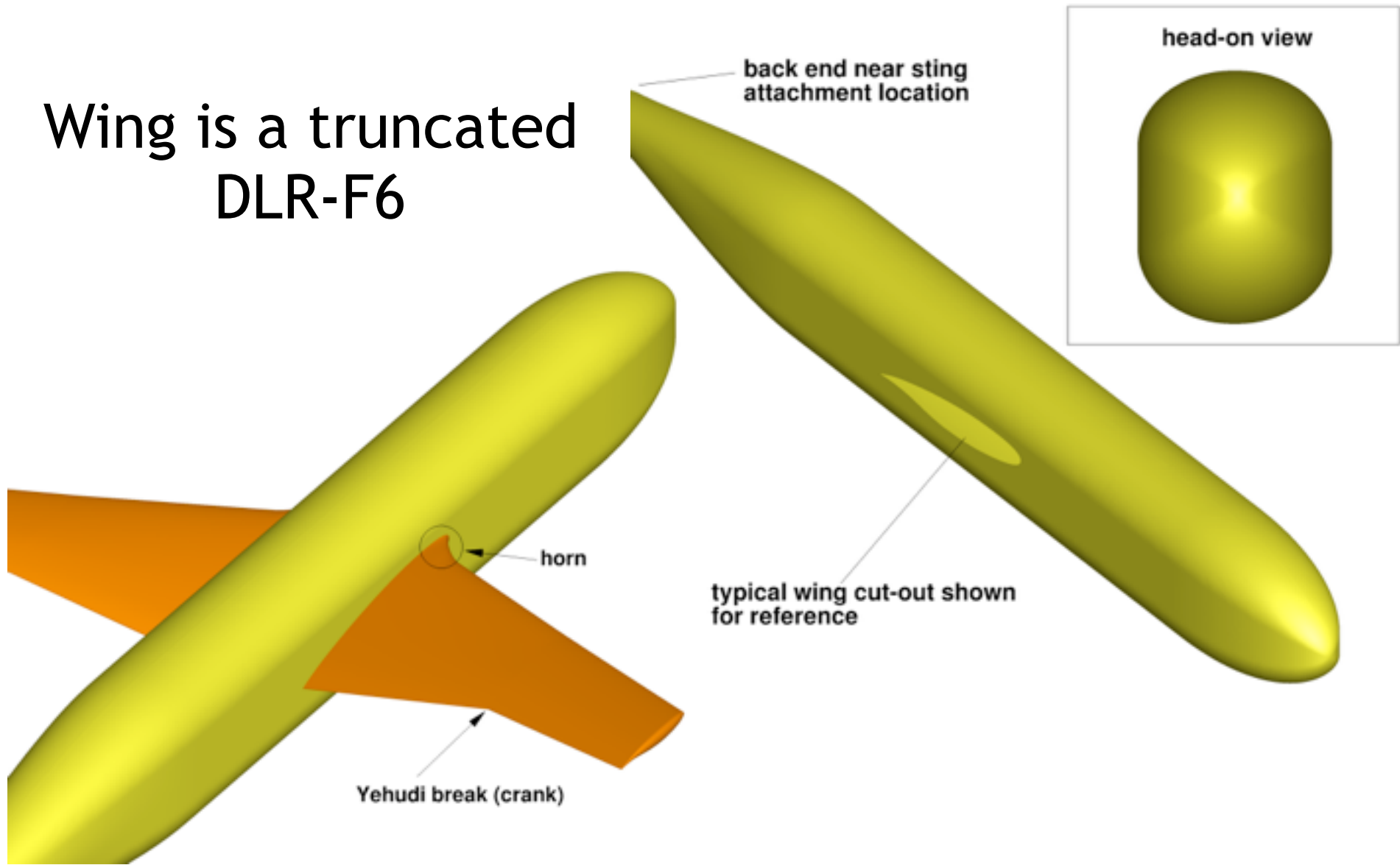
location to wing-body juncture



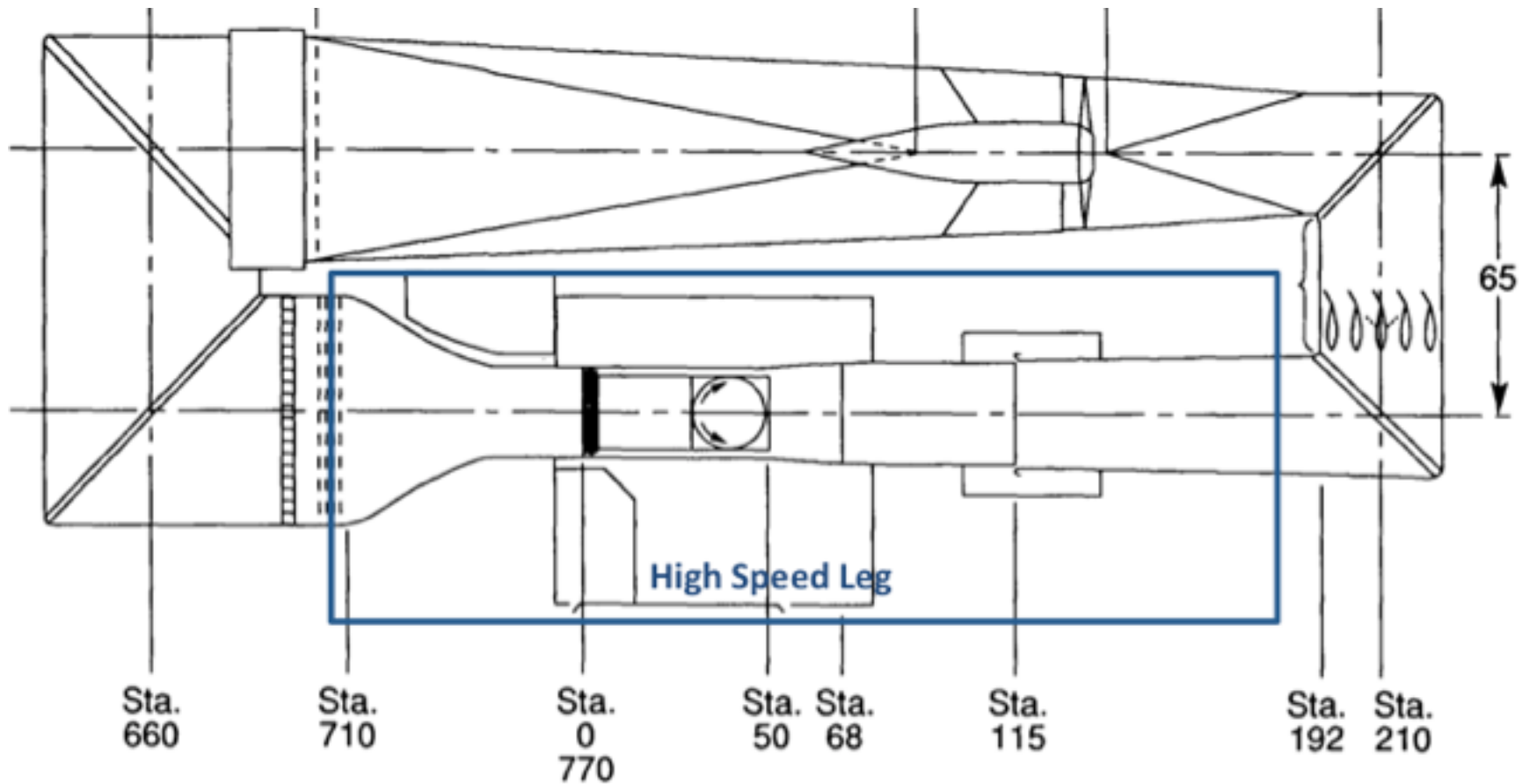


Juncture Flow Model Details

Wing is a truncated
DLR-F6



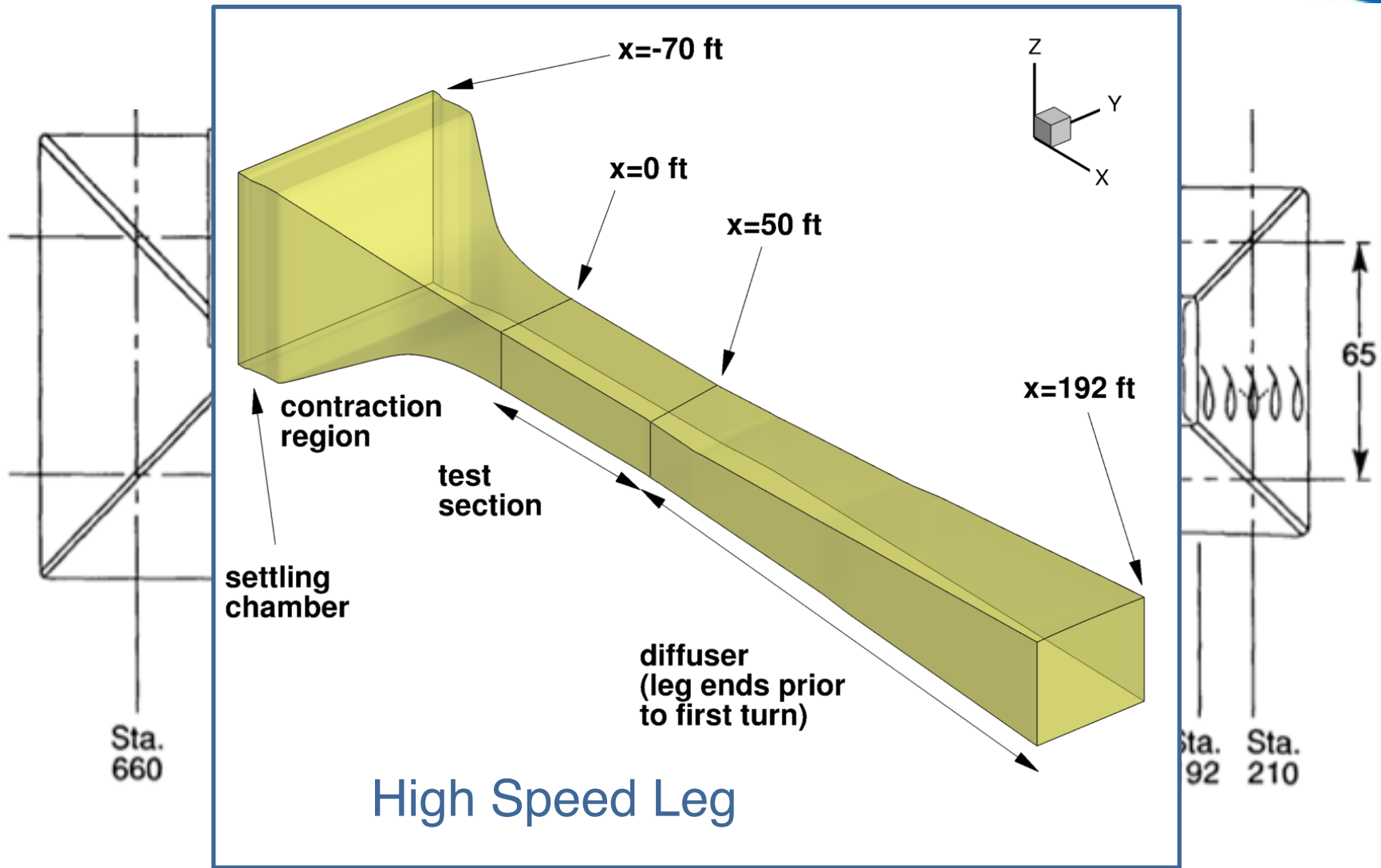
14x22 Wind Tunnel



Mach 0.2

Reynolds Number 2.4M

14x22 Wind Tunnel



Mach 0.2

Reynolds Number 2.4M

Introduction



- Juncture Flow (JF) Experiment
 - Heavy collaboration between CFD and WT design team
 - CFD used extensively in the experiment design
 - Companion CFD runs for all risk assessment experiments
 - Publications so far:
 - AIAA 2016-1557, AIAA 2017-4127, AIAA 2016-4126, NASA TM-2016-219348, etc
- Tasked to perform various parametric studies using CFD:
 - Effect of support hardware
 - Effect of wind tunnel walls on measurements

Introduction cont.



- CFD parametric studies approach:
 - Run 14x22 empty tunnel
 - Grid resolution study
 - Tunnel speed calculations
 - Solution acceleration approaches
 - Run 14x22 with JFM installed
 - Run with various support hardware included
 - Determine effect of wind tunnel walls

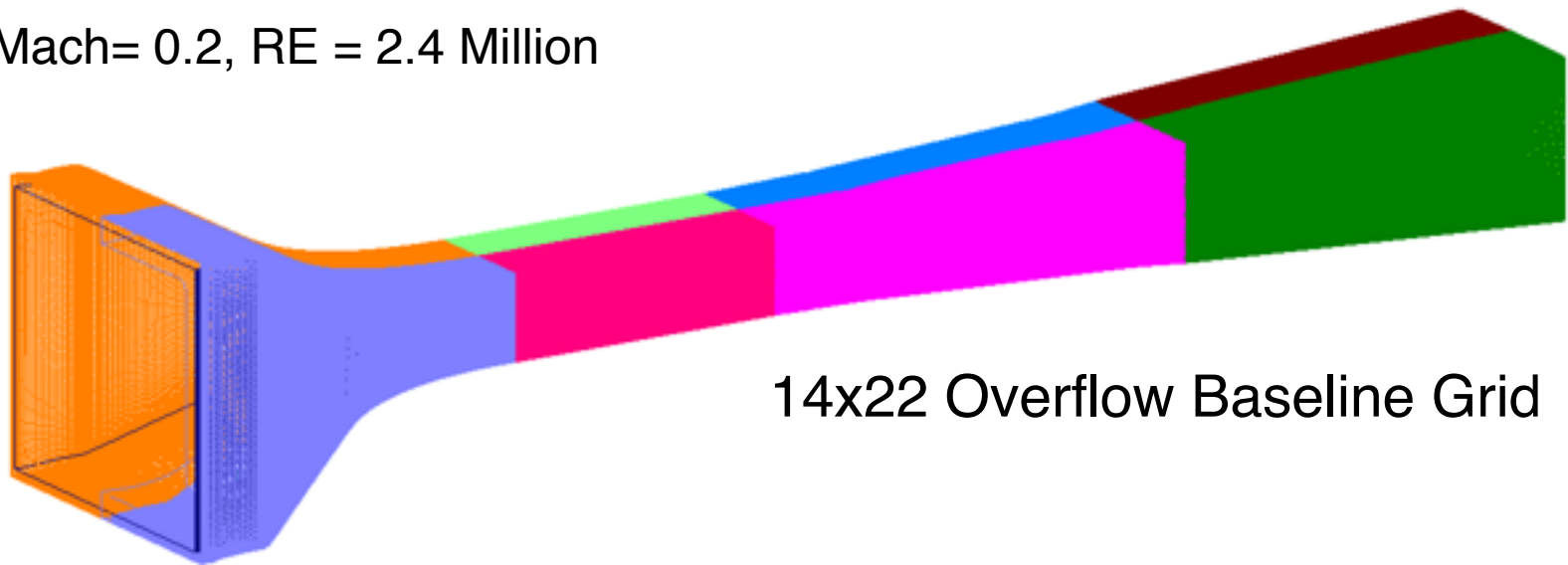
Introduction: Difficulties discovered

- CFD simulations of 14x22 empty tunnel
 - CFD tunnel is very sensitive to changes in back pressure
 - Long process:
 - Manual changes to back pressure
 - Slow to propagate downstream
 - Corner Separation
- CFD simulations with JFM installed
 - Determining tunnel speed - calibration point covered by model
 - Corner separation present in most cases
 - Tunnel speed is very sensitive
 - Inflow/Outflow BC issues

14x22 Empty Tunnel Studies



- Overset structured grids, built with Chimera Grid Tools
 - Coarse (9.3M), Medium (41.6M), Fine (118.7M)
- Overflow 2.2N
- 3rd-Order Roe upwind RHS, ARC3D Beam-Warming scalar pentadiagonal LHS
- Low-Mach preconditioning
- Spalart-Allmaras turbulence model + rotational correction + QCR
- Fully Turbulent, Steady State
- Inflow BC: Total Pressure/Temperature (P_0 , T_0)
- Outflow BC: Back Pressure ($P_{ratio} = P_0/P_{exit}$)
- Mach= 0.2, RE = 2.4 Million

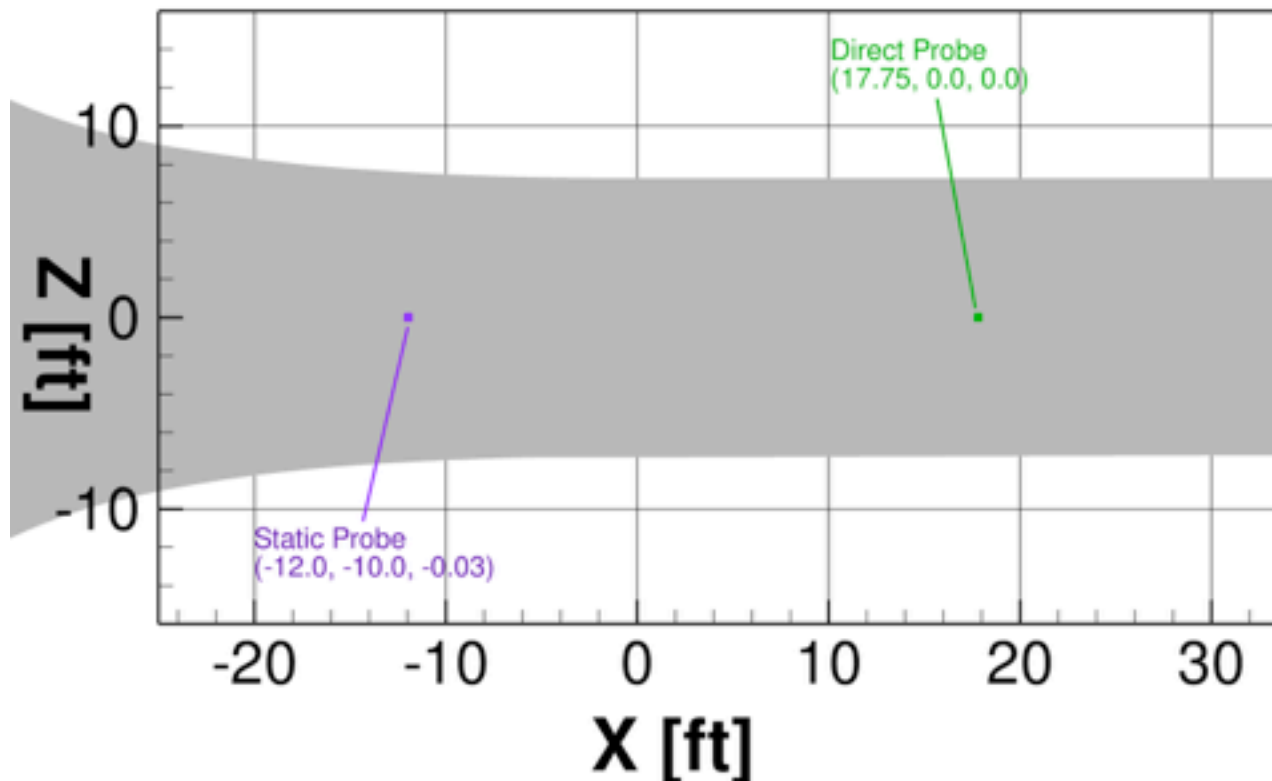


14x22 Overflow Baseline Grid

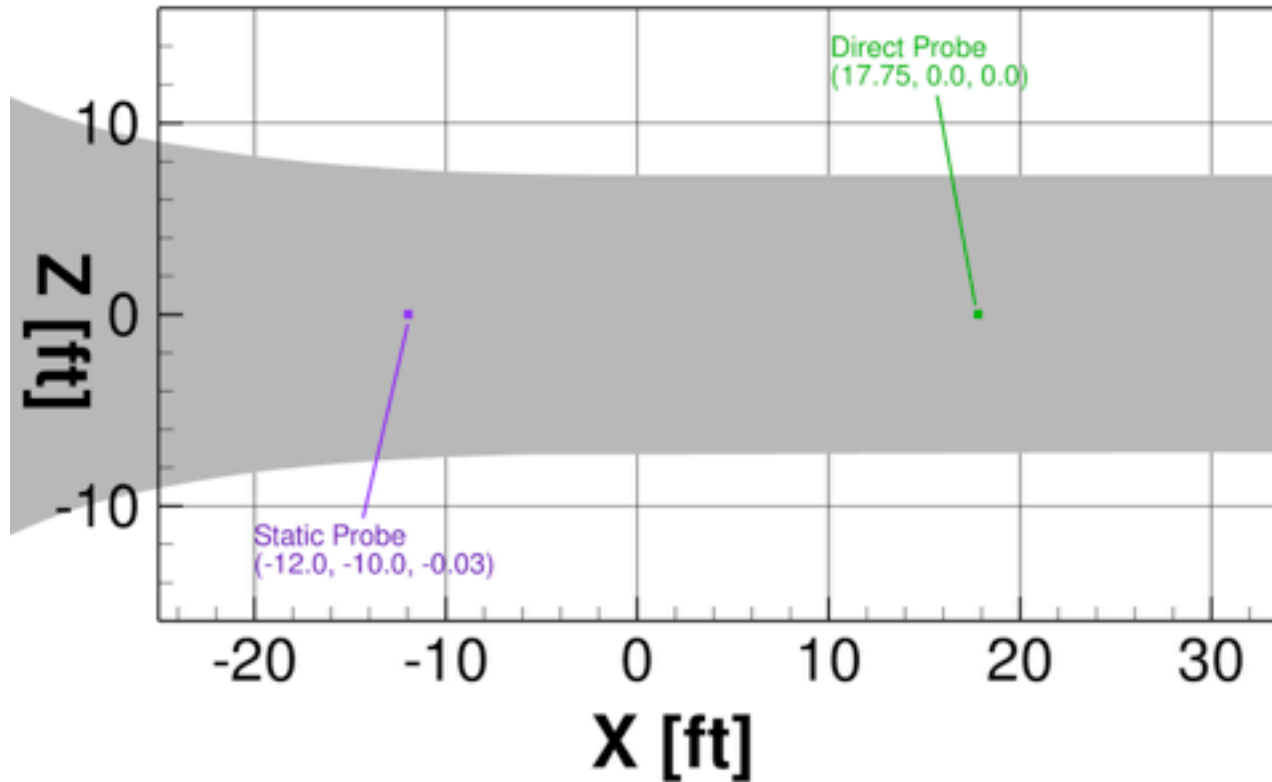
14x22 Tunnel Speed Calculation



- Tunnel Speed Calculation
 - Direct probe at (17.75,0.0,0.0)
 - Calibration point
 - Model is often located here
 - Calculated using wind tunnel method:
 - Uses total pressure & static pressure “probe” values from their locations
 - Calibrated equations -> tunnel speed



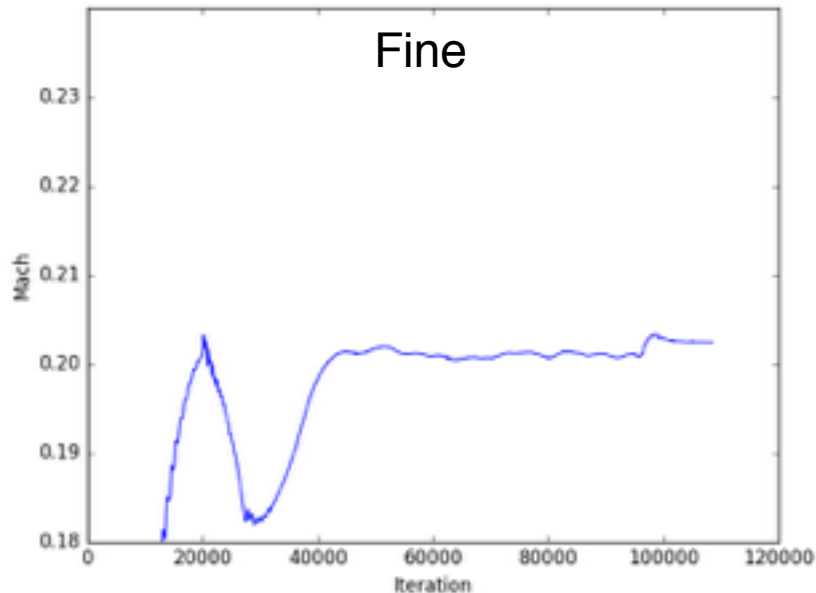
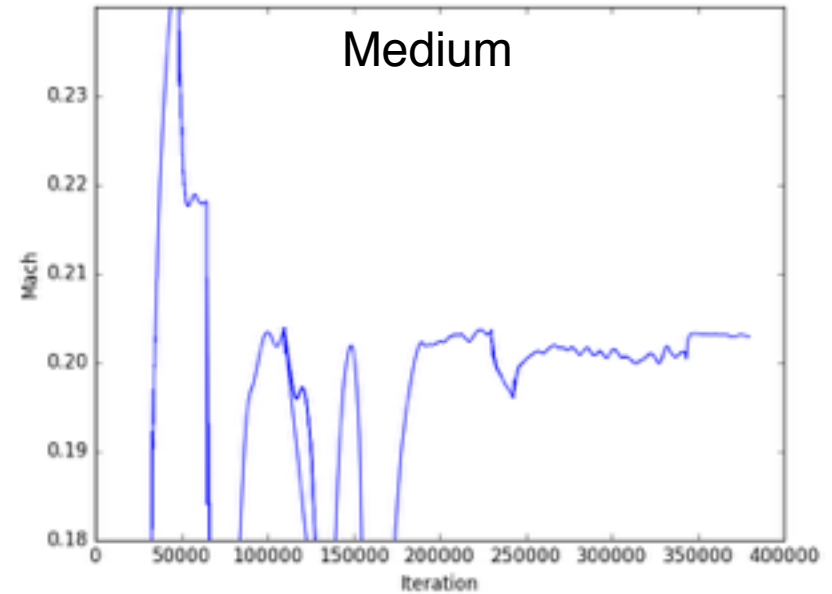
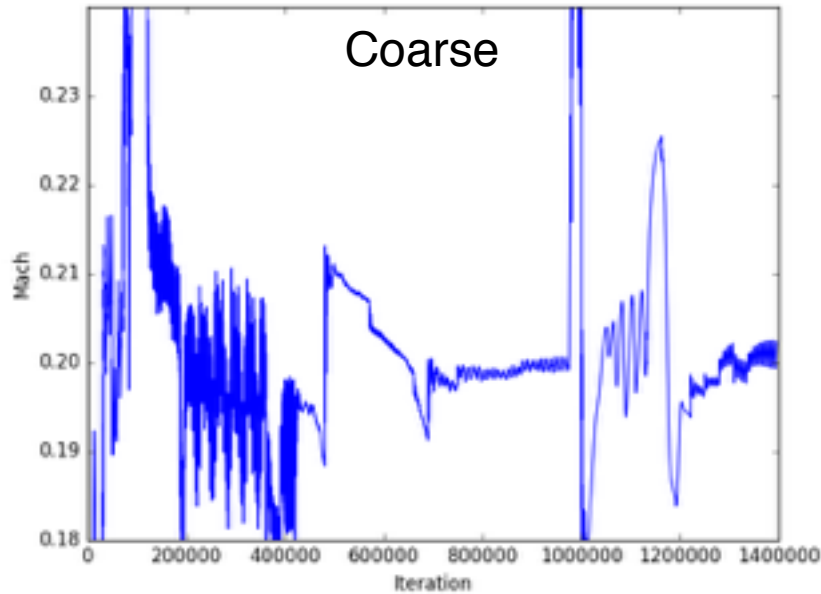
14x22 Tunnel Speed Calculation



Grid	Calculated Mach	Direct Mach Probe
Coarse	0.2023	0.1995
Medium	0.2029	0.2004
Fine	0.2025	0.2000

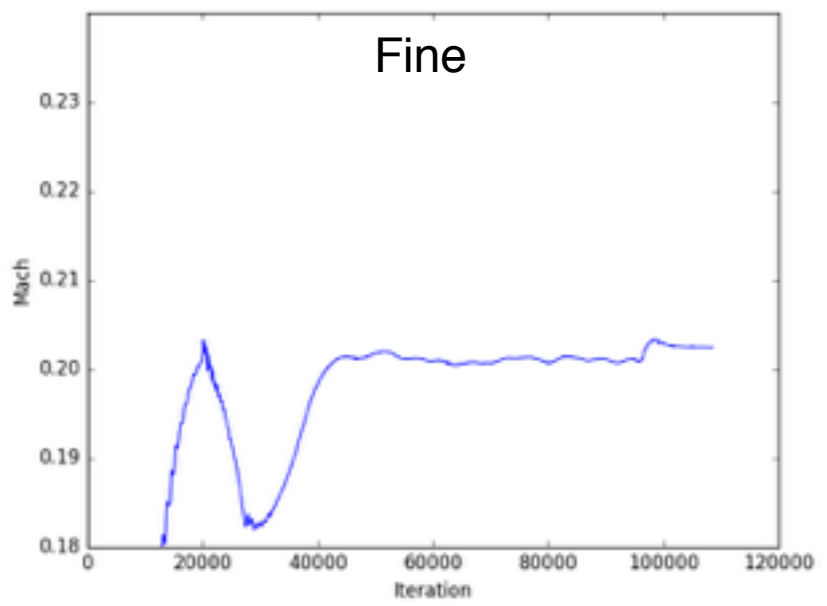
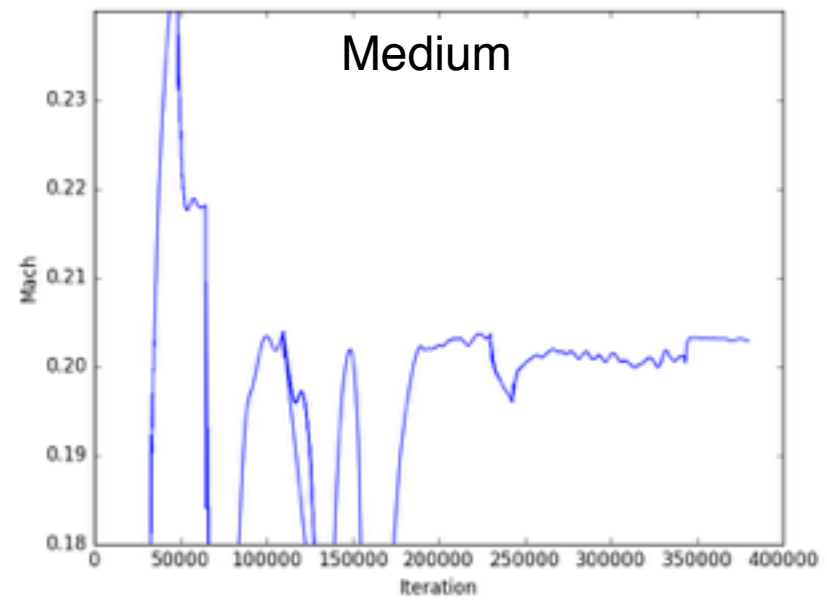
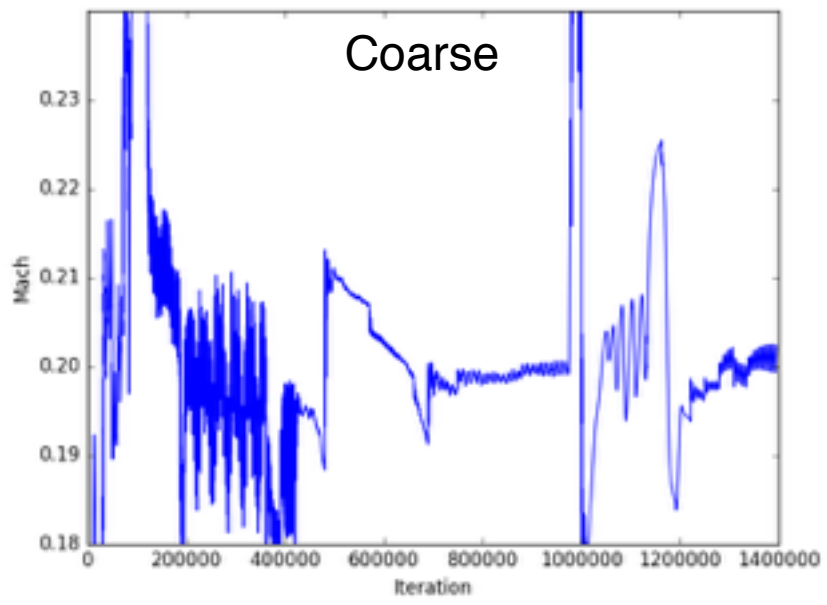
Mach values are nearly identical: can calculate wind tunnel speeds using same method

14x22 Grid Refinement (Overflow)



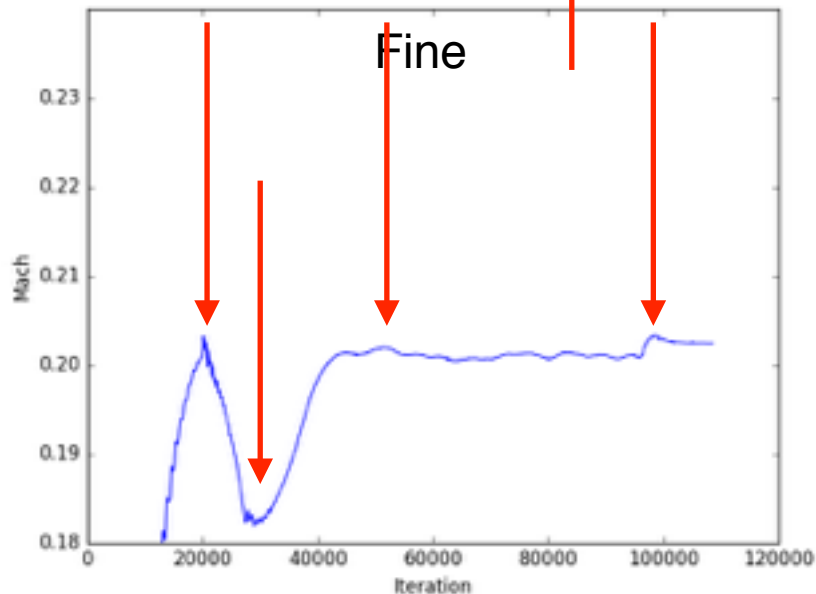
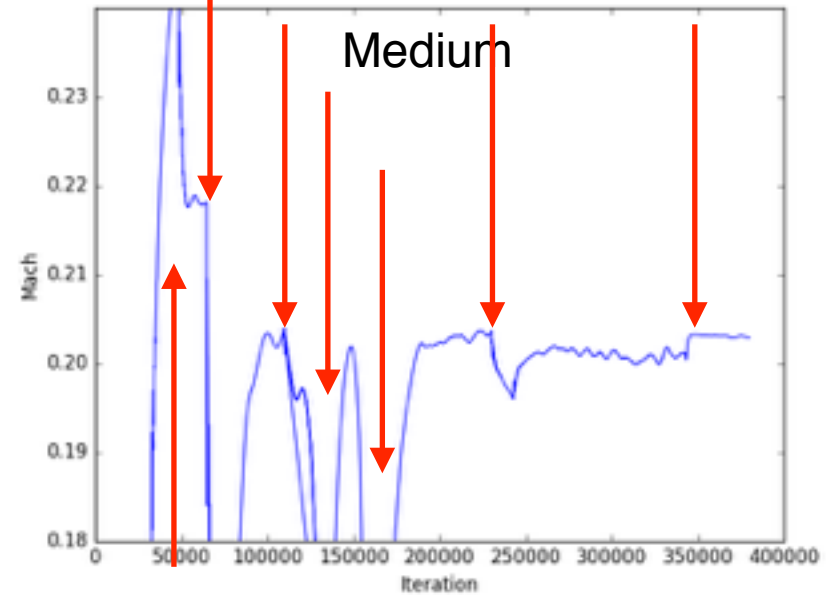
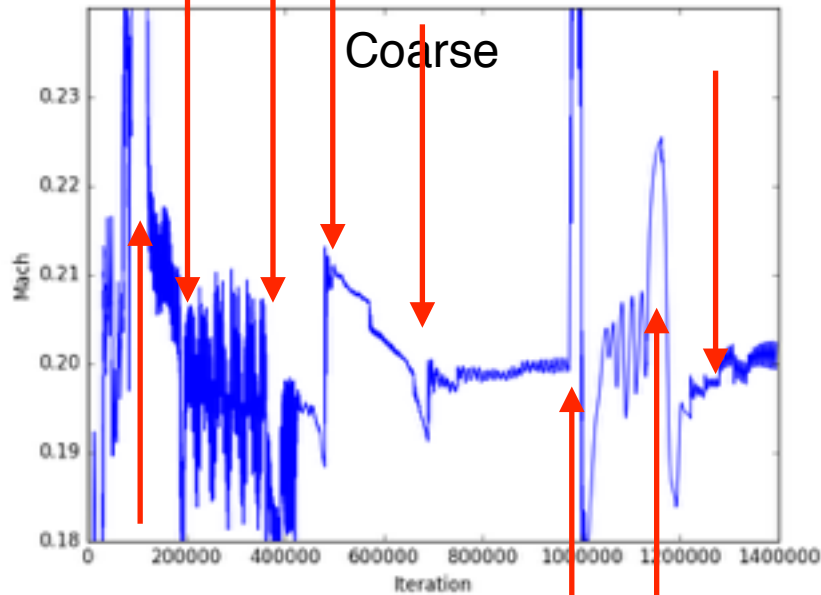
- Mach number of tunnel vs iteration
- Tunnel speed is calculated using pressure probes

14x22 Grid Refinement (Overflow)



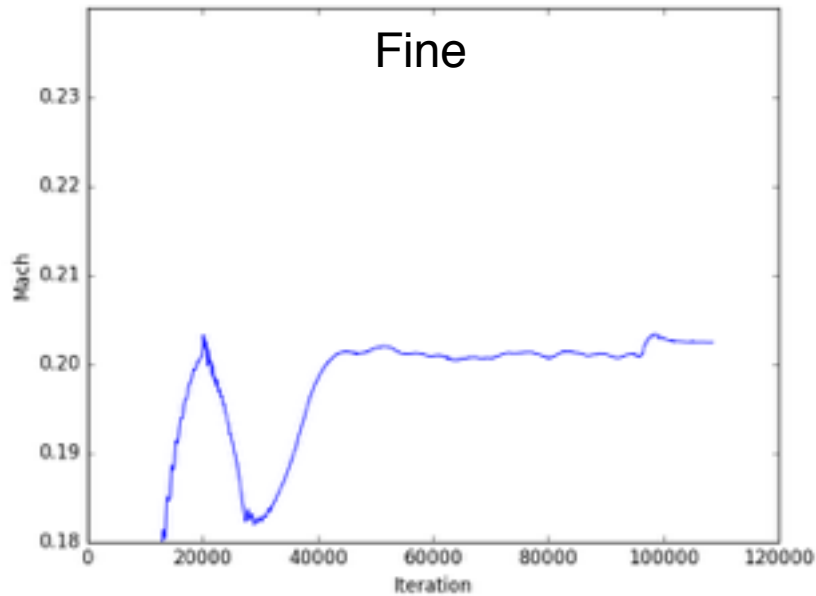
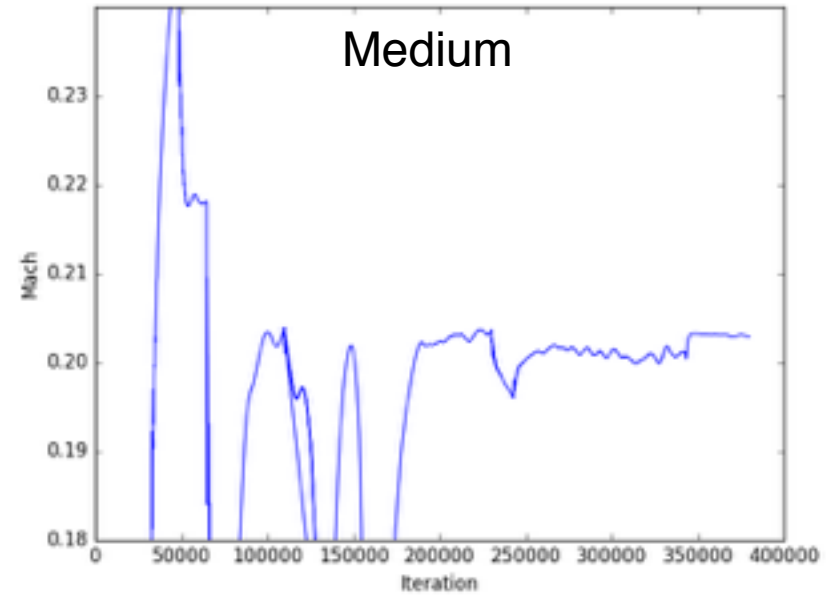
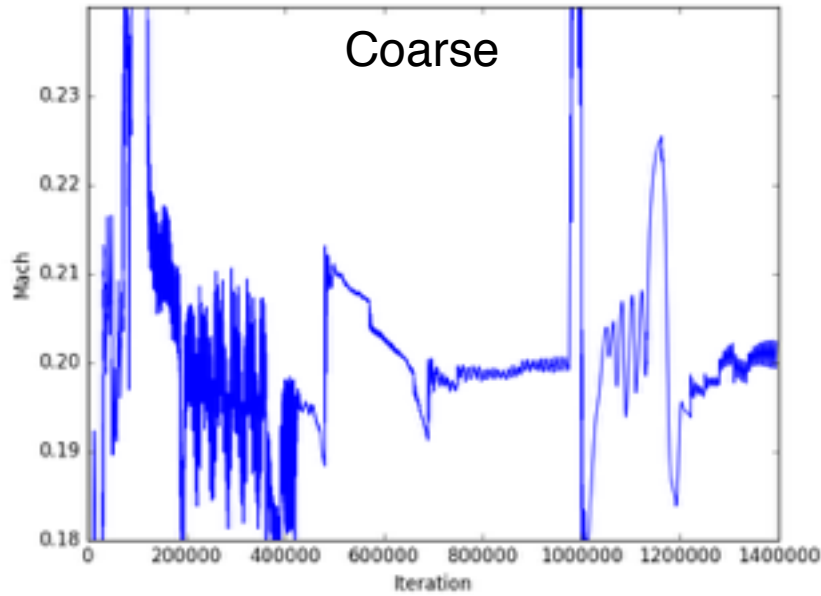


14x22 Grid Refinement (Overflow)



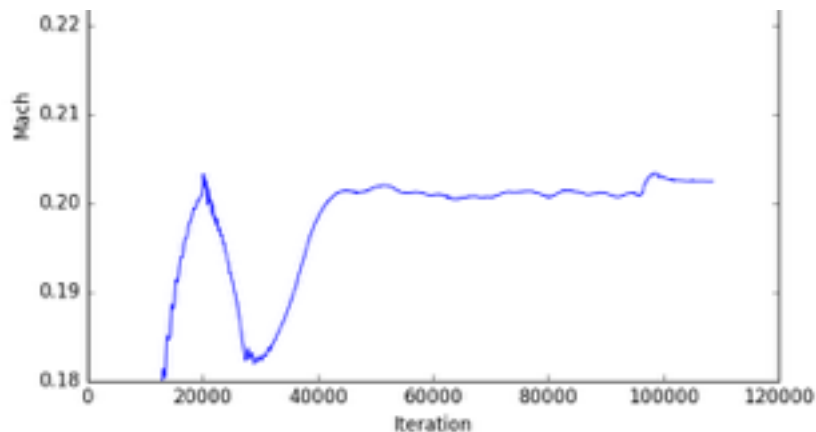
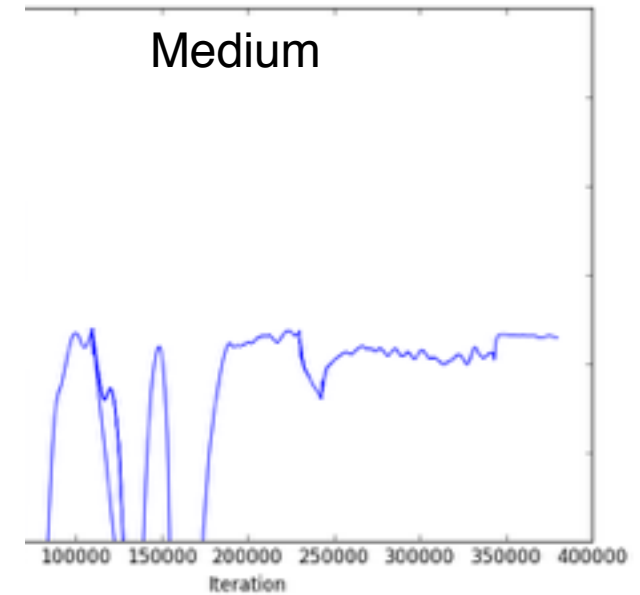
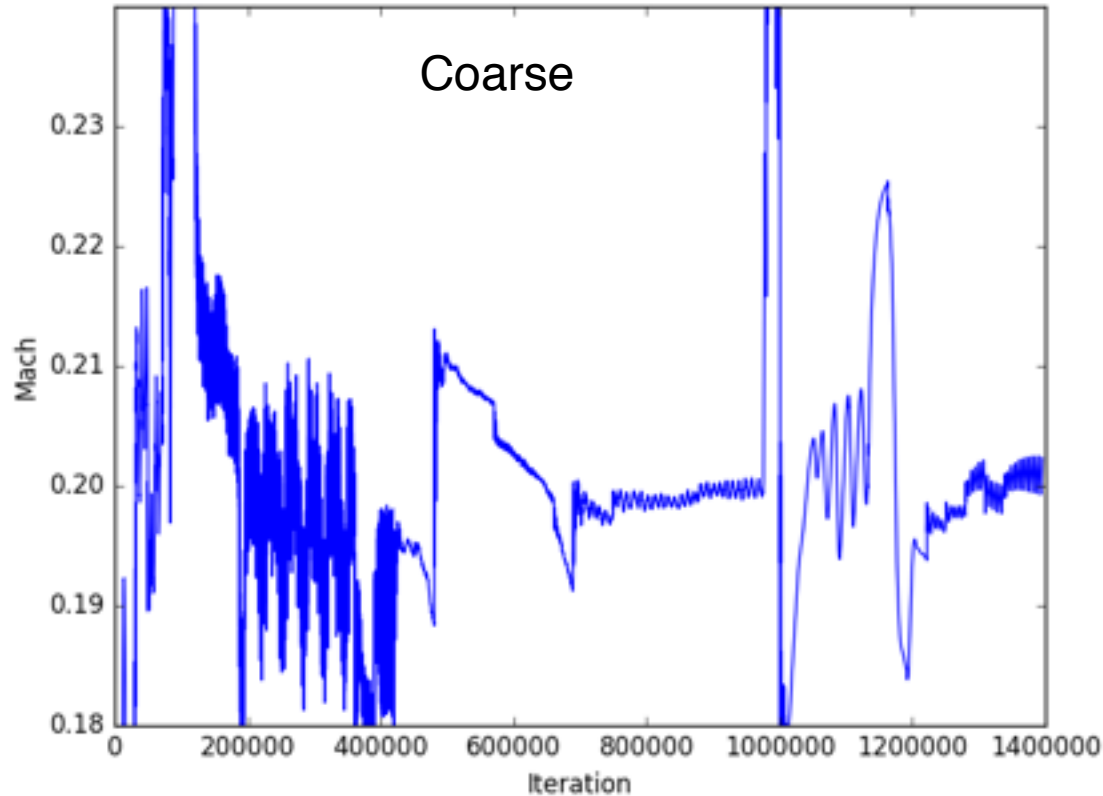
- Spikes/drops caused by manual changes in back pressure
- Each change required 10,000 steps to “settle”
- Solutions require 100,000 to 1,000,000+ steps!

14x22 Grid Refinement (Overflow)



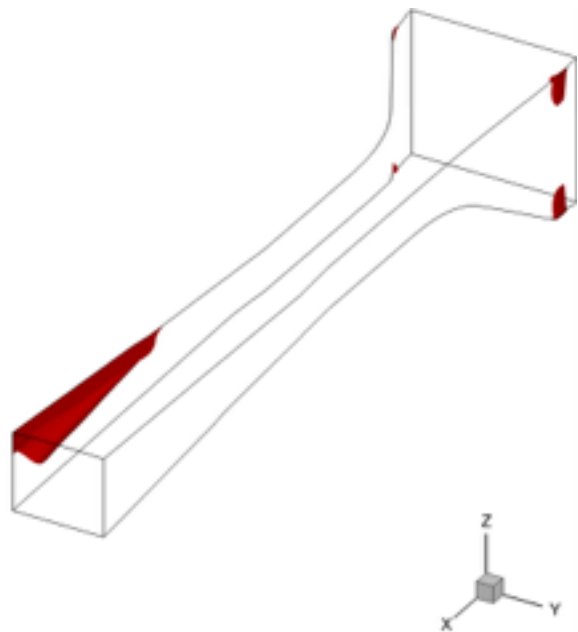


14x22 Grid Refinement (Overflow)

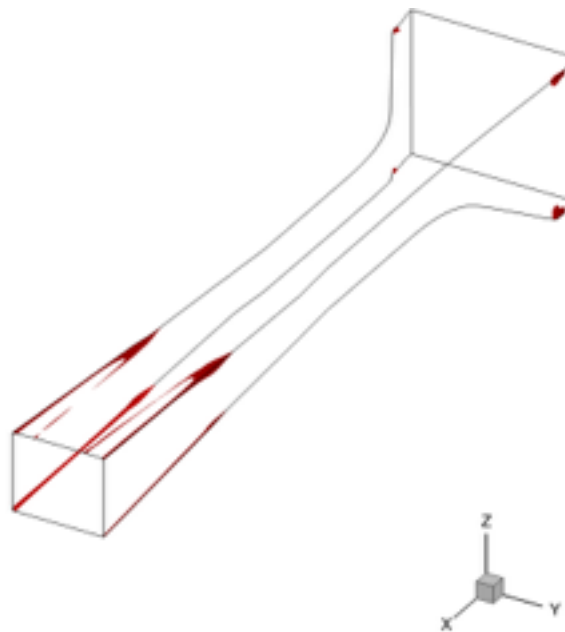


- Coarse grid tunnel speed was extremely noisy

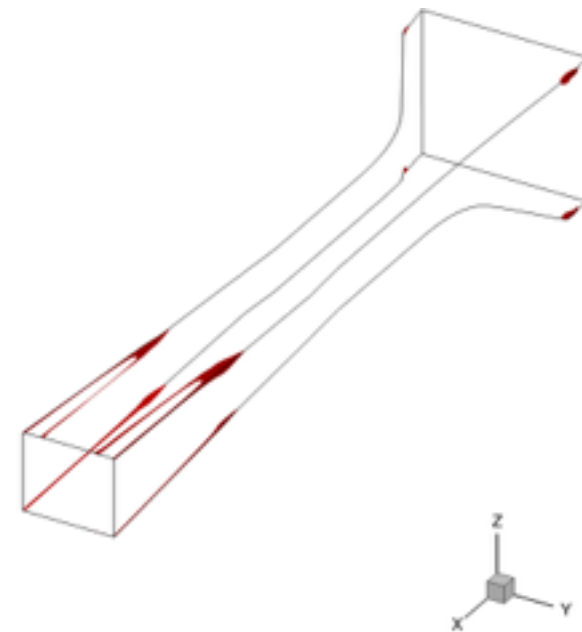
14x22 Grid Refinement



Coarse



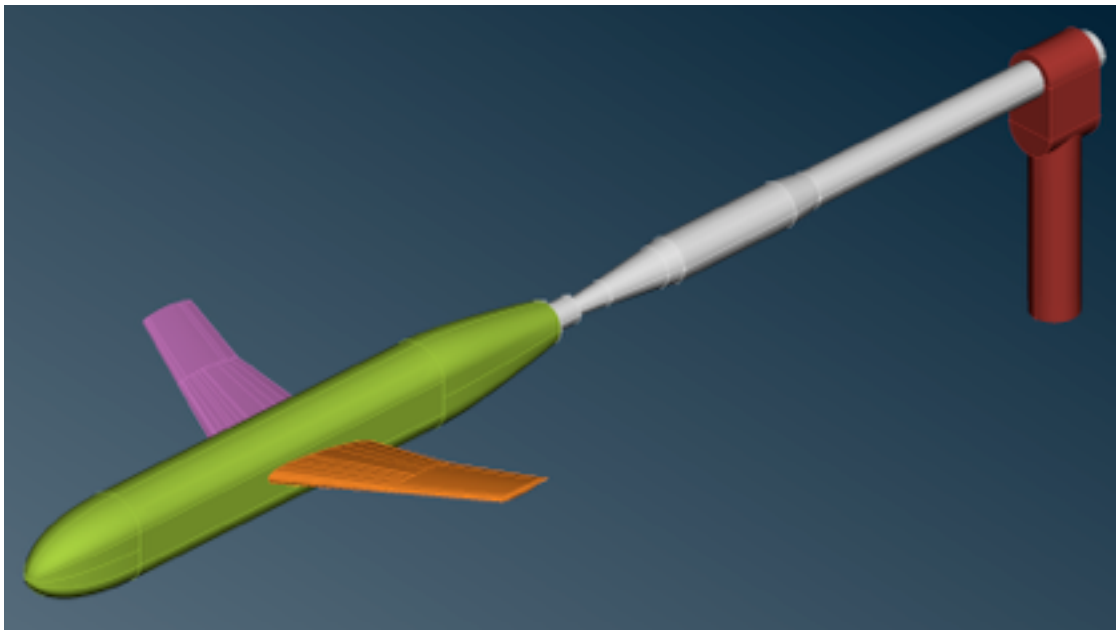
Medium



Fine

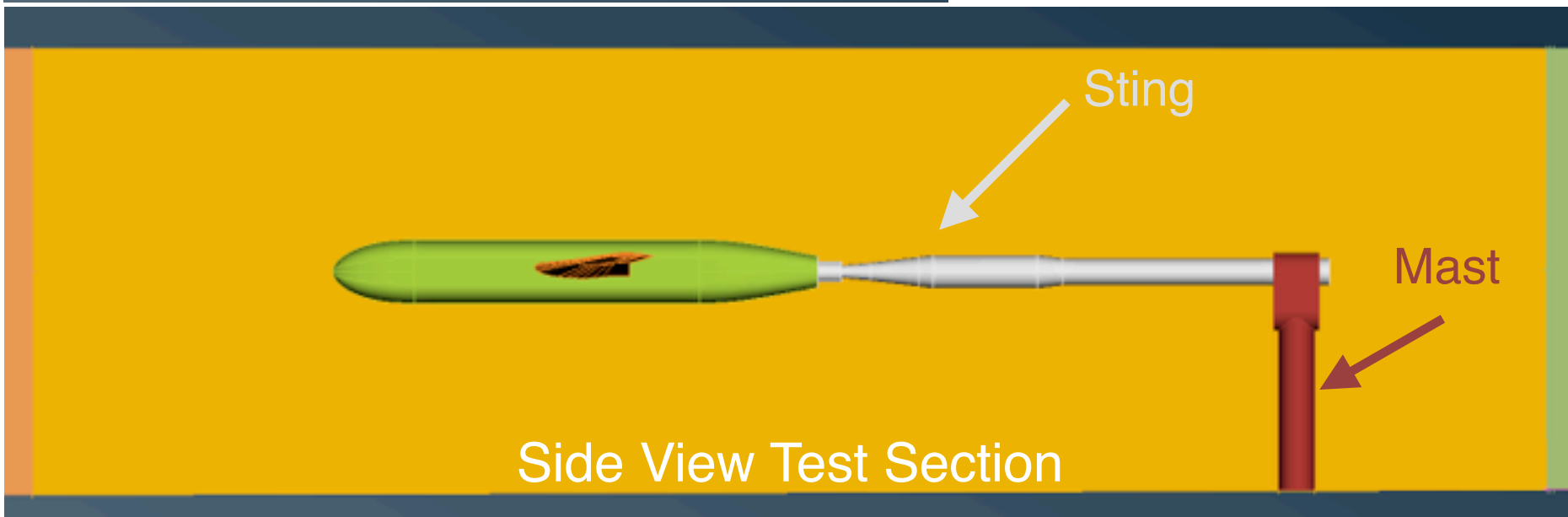
- Red isosurfaces - reverse flow
- Large diffuser separation in Coarse grid
- Tunnel Mach number was “noisy” due to corner separation

Juncture Flow Model with WT walls



JFM 8% model with
roll sting and mast

Using medium WT grid

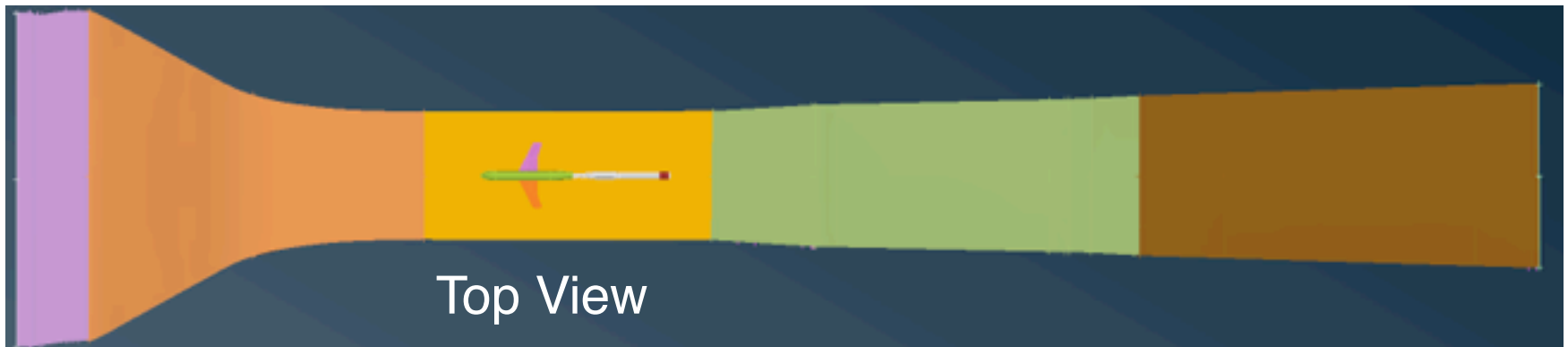


Side View Test Section

JFM 8% Conditions

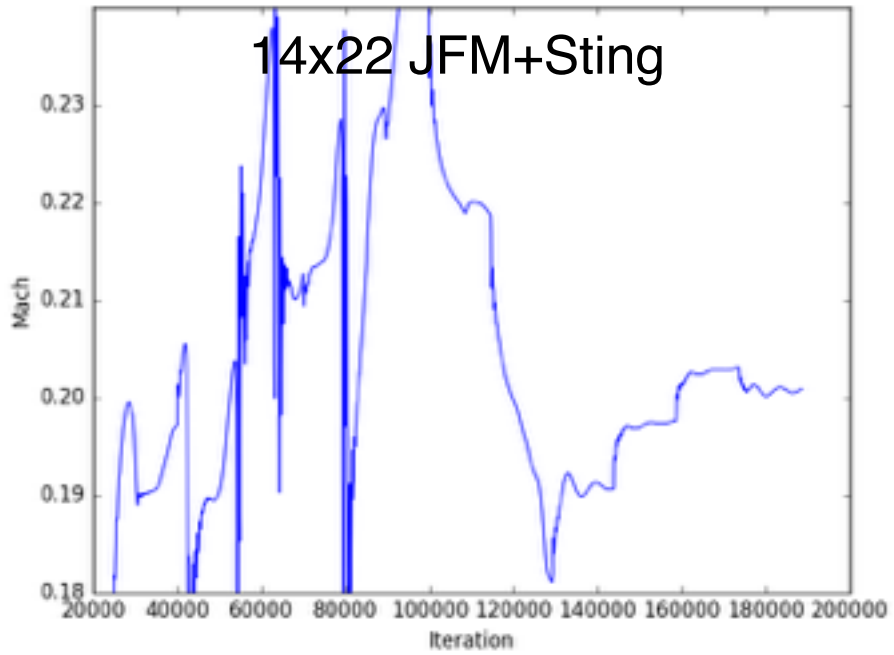
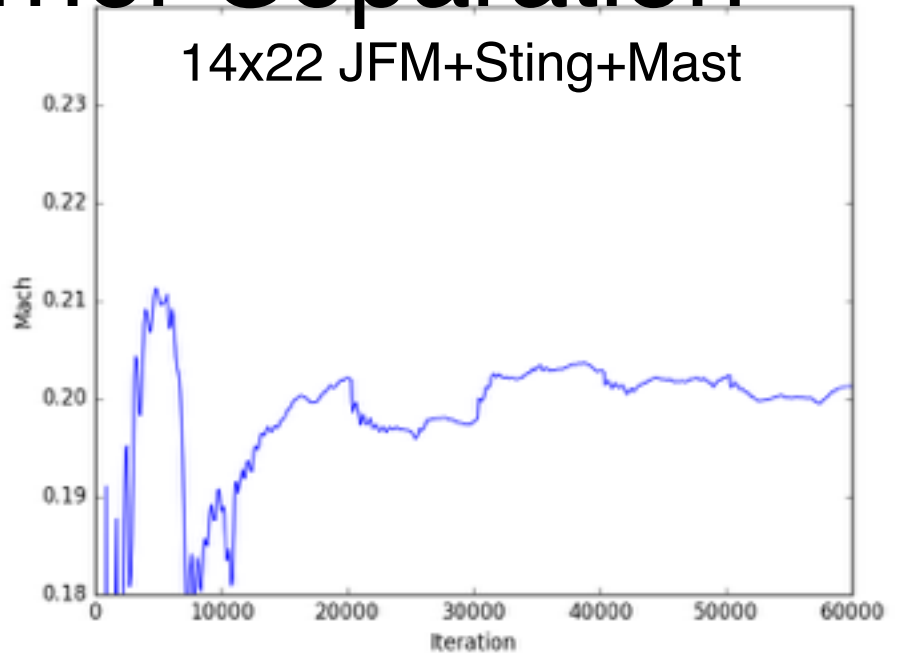
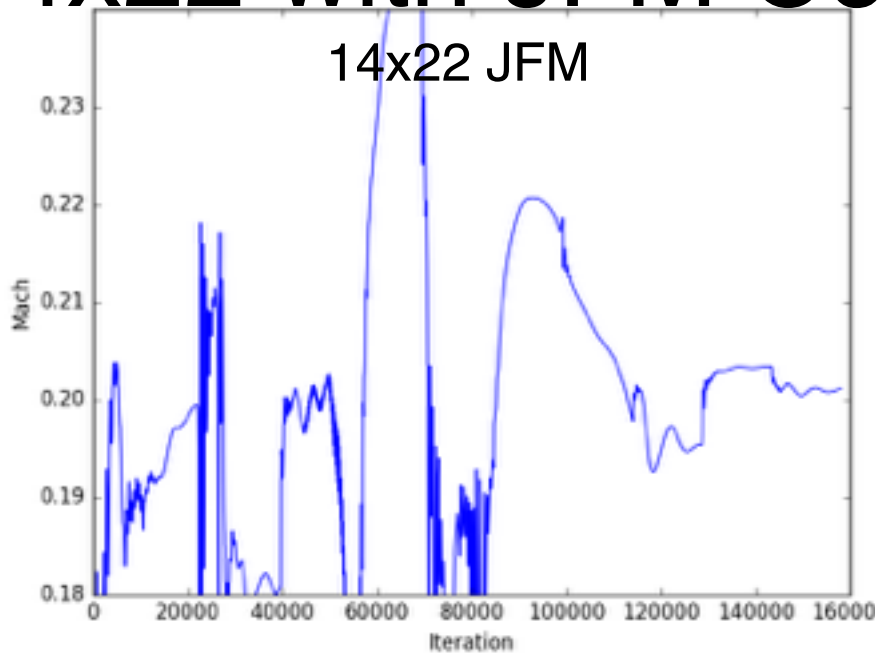


- RE = 2.4M based on yehudi break chord 21.97 inches
- T = 560 Rankine (hot day in the tunnel, Q~55)
- Mach = 0.2
- Process:
 - Speed calculation with WT walls computed with Static/Stagnation pressure probe calculations
 - Inflow BC: Stagnation T & P, Outflow BC: Pback ratio (iterated)





14x22 with JFM Corner Separation

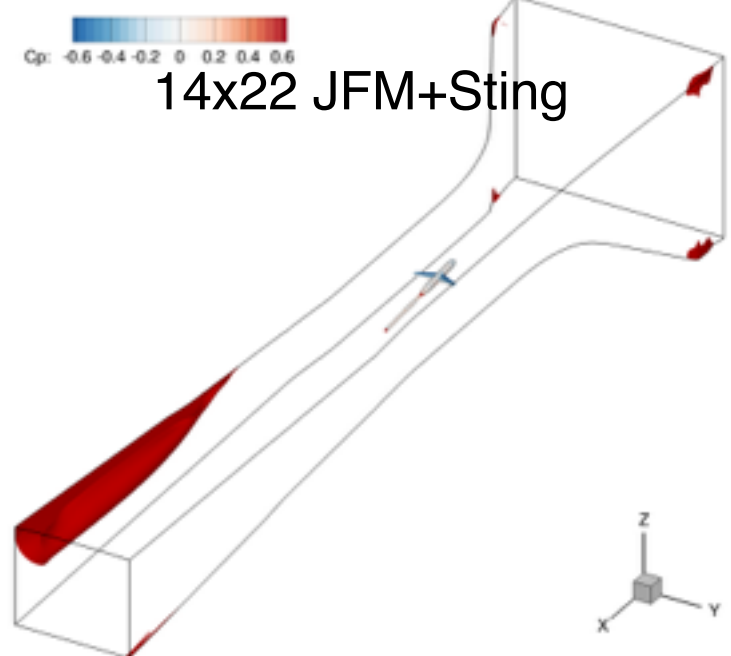
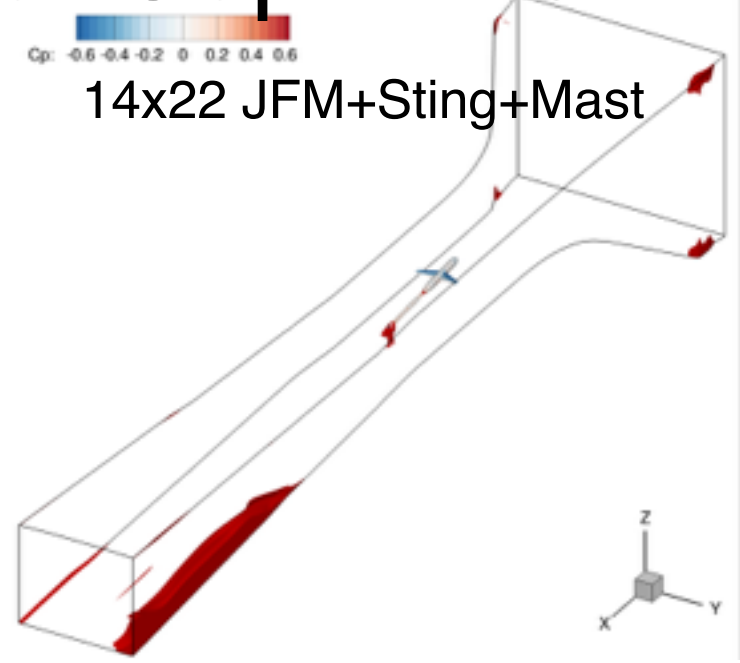
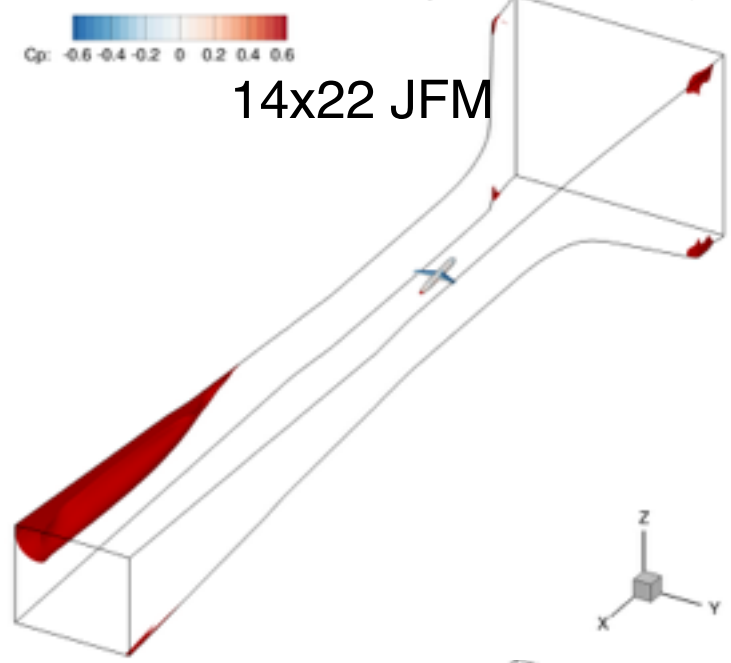


- Cases were very hard to converge
- Mach response to ratio changes were erratic

AOA 5 degrees



14x22 with JFM Corner Separation



- Most configurations at some +AOA had corner separation

AOA 5 degrees

14x22 Inflow/Outflow BC's



- Inflow/Exit BC's are based on inviscid assumptions:
 - Running regions near BC inviscid may help speed up convergence
 - May reduce corner separation
- Blue sections are run as Inviscid
- Same exit pressure ratio (1.02188) used for both

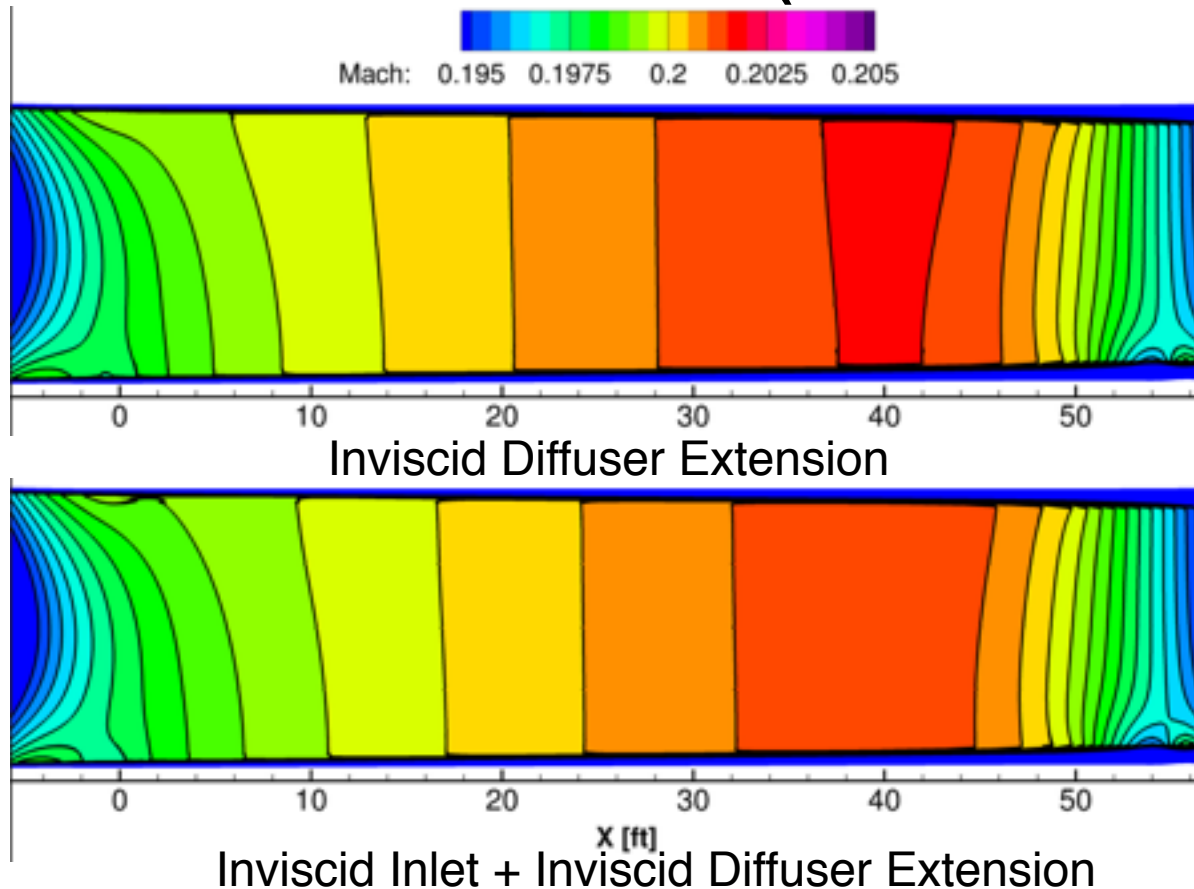


Inviscid Diffuser Extension



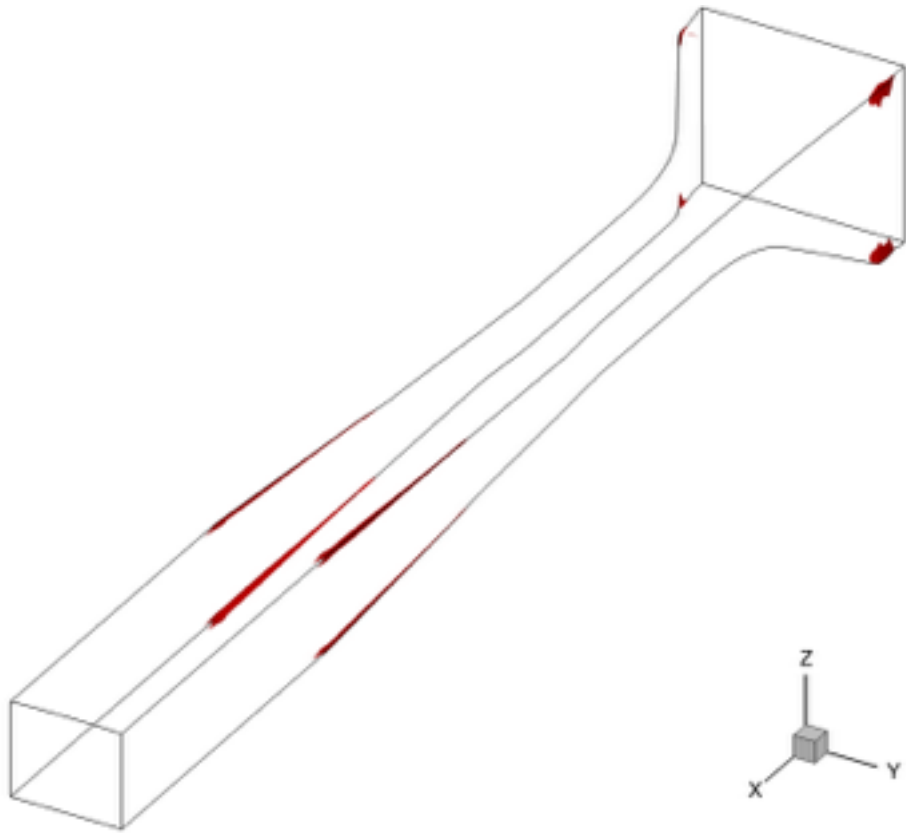
Inviscid Inlet + Inviscid Diffuser Extension

14x22 Inviscid BC's (Overflow)

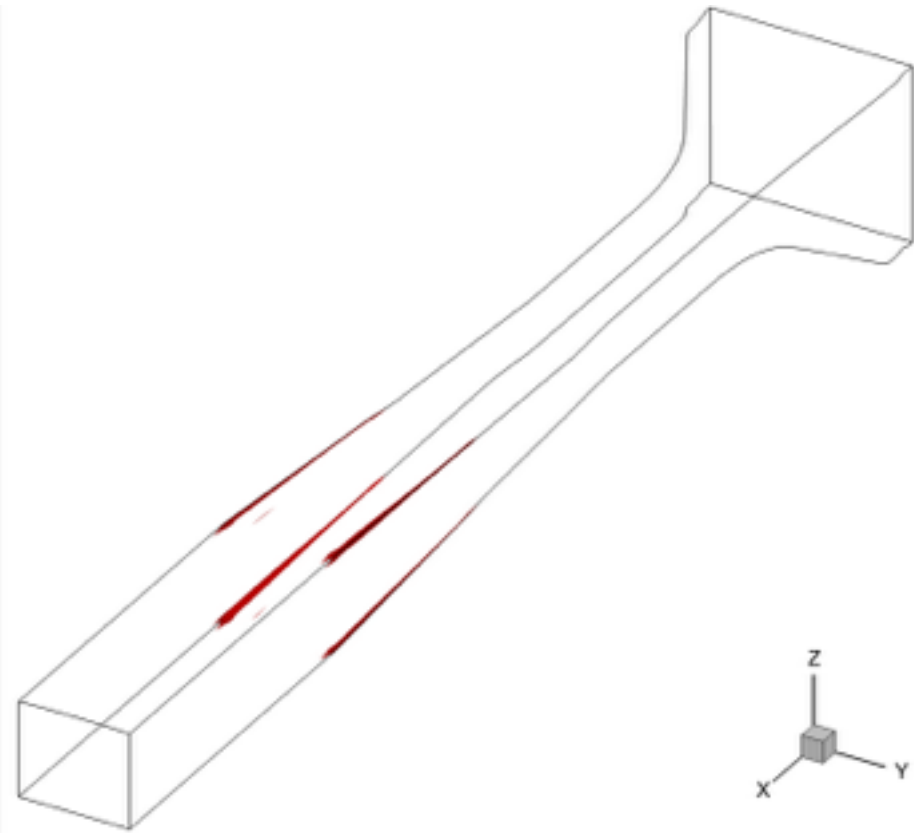


- Slice down middle of test section, mach contours
- Inviscid Inlet has a slightly lower speed in test section
- Very similar results

14x22 Inviscid BC's (Overflow)



Inviscid Diffuser Extension



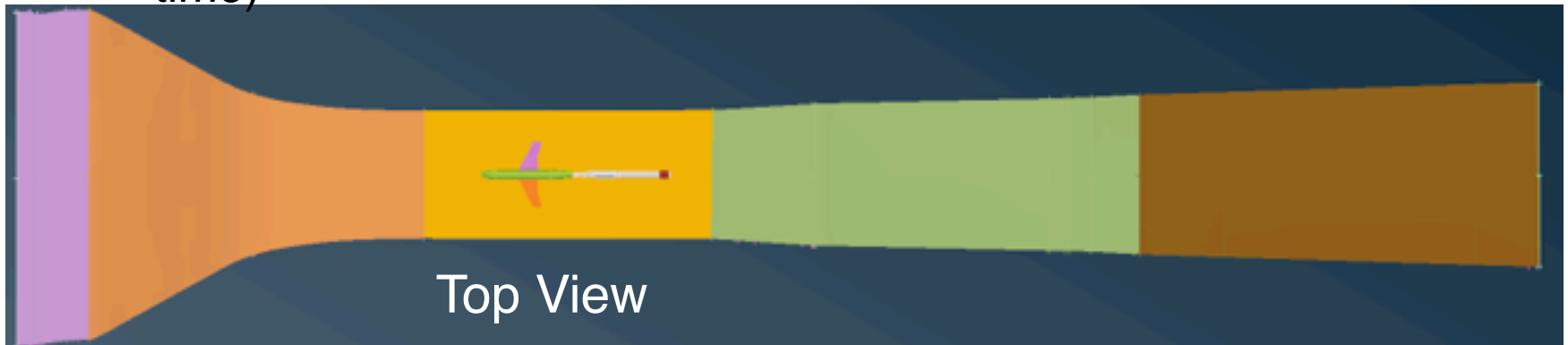
Inviscid Inlet + Inviscid Diffuser Extension

- Inviscid Inlet suppresses the separation present in the corners of the inlet
- Both suppress diffuser corner separation

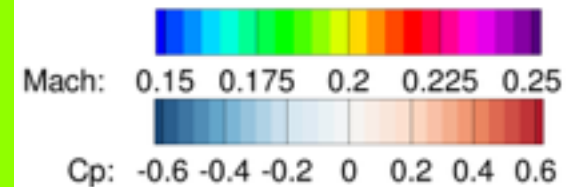
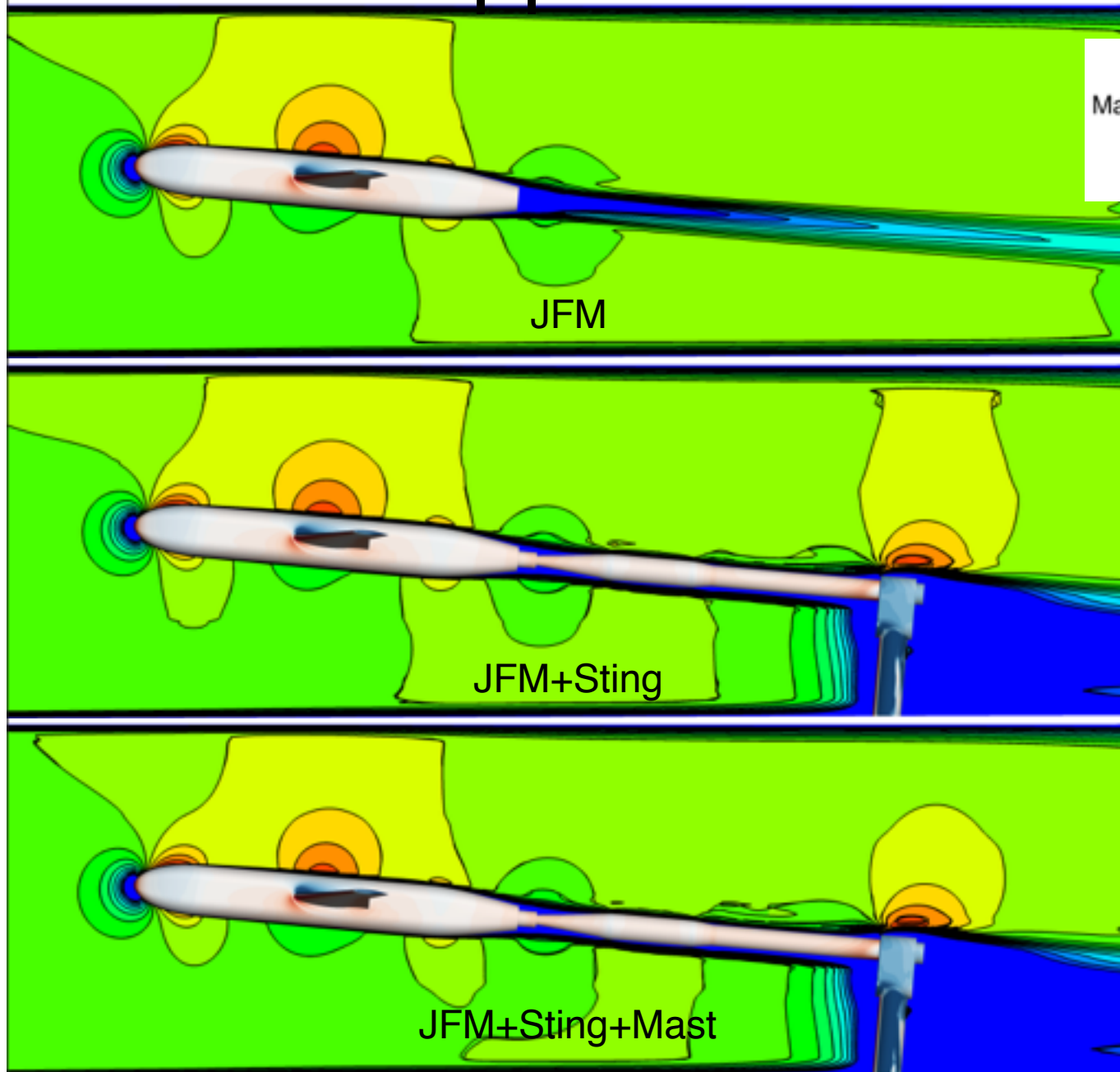
JFM 8% Installed in 14x22



- Increment Analysis: Support Hardware, WT Extension
 - 14x22 WT: JFM, JFM+Sting, JFM+Sting+Mast (42-46M Grid points)
 - 14x22 WT Extended: JFM+Sting+Mast (84M-88M Grid Points) (Inviscid Diffuser)
 - 14x22 WT Extended with inviscid inlet & diffuser (didn't finish in time)



JFM 8% Support Hardware Effect

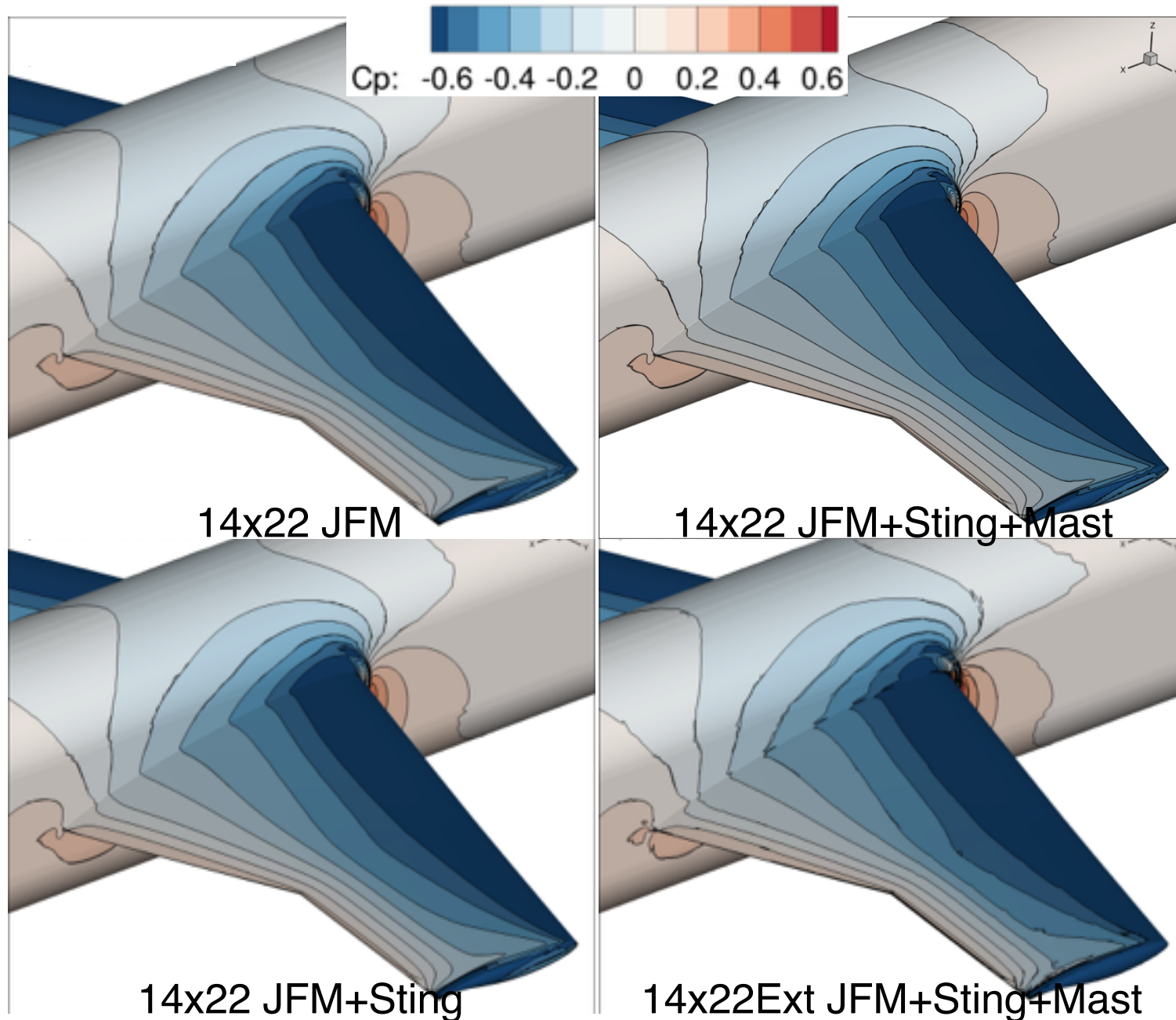


Effect of the support hardware on:

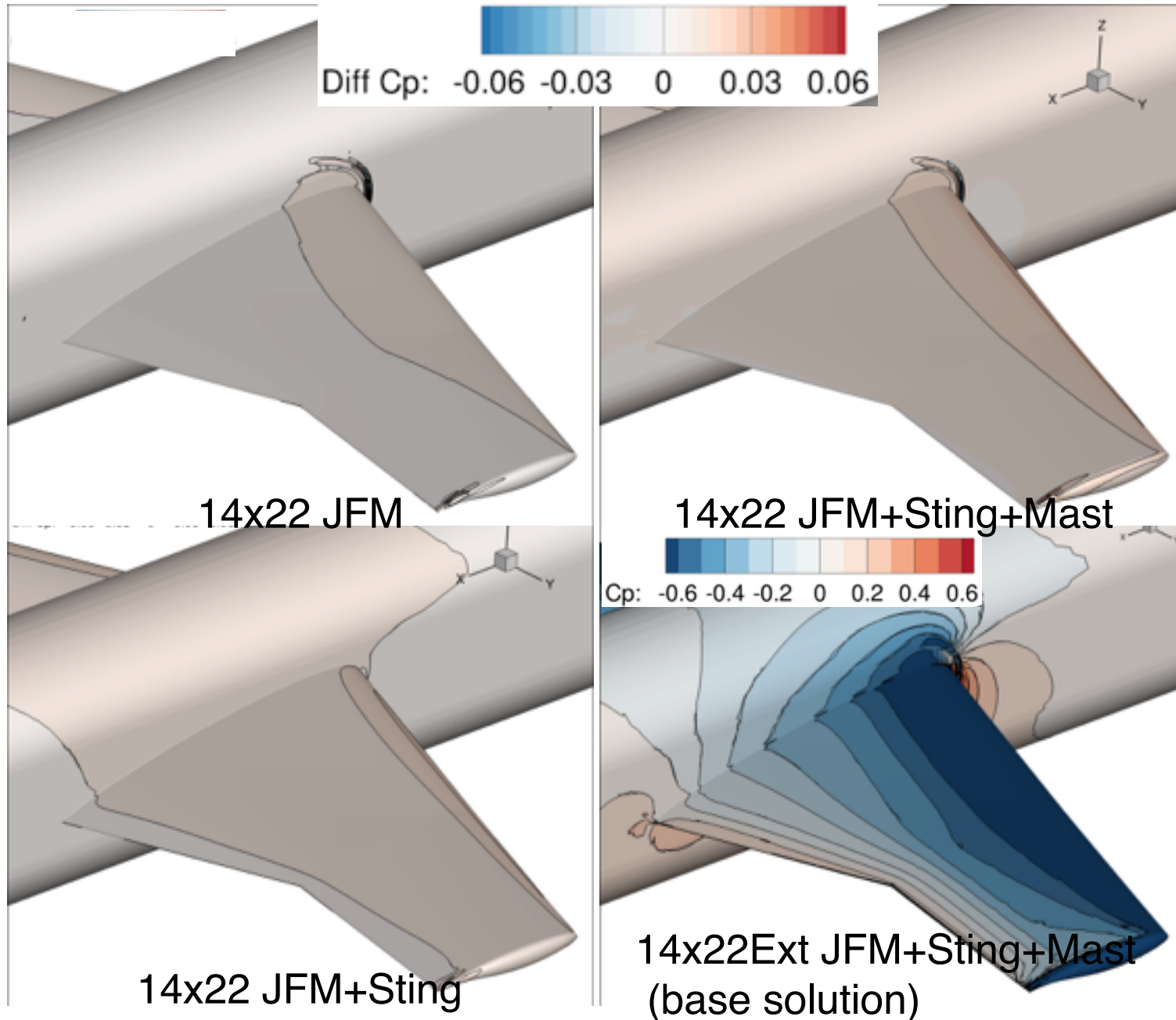
- Wing/Bubble
- Solution

All results at AOA 5 degrees

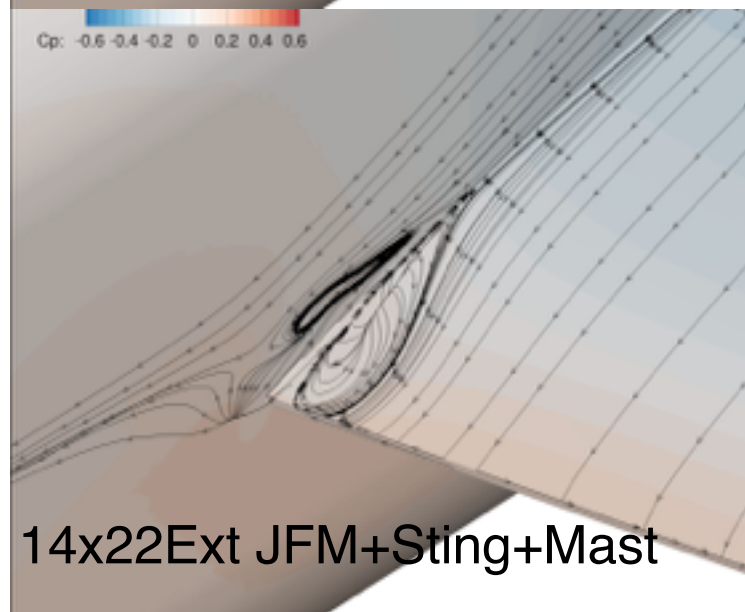
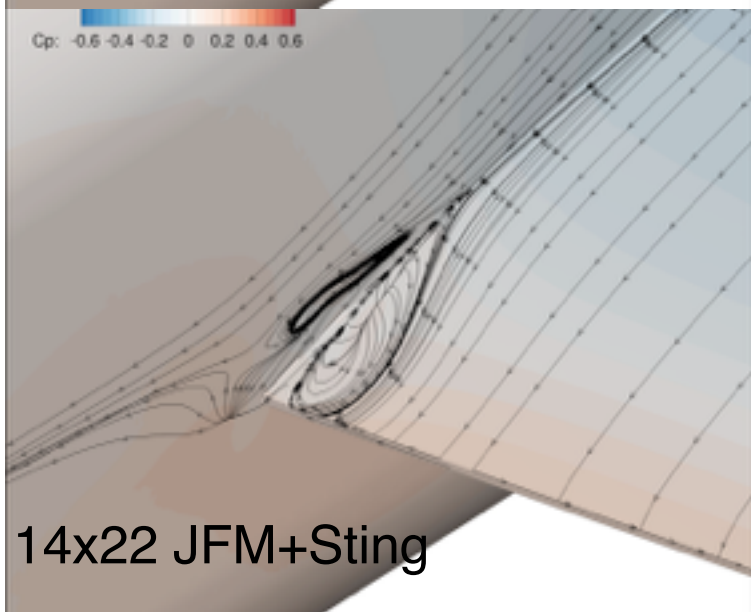
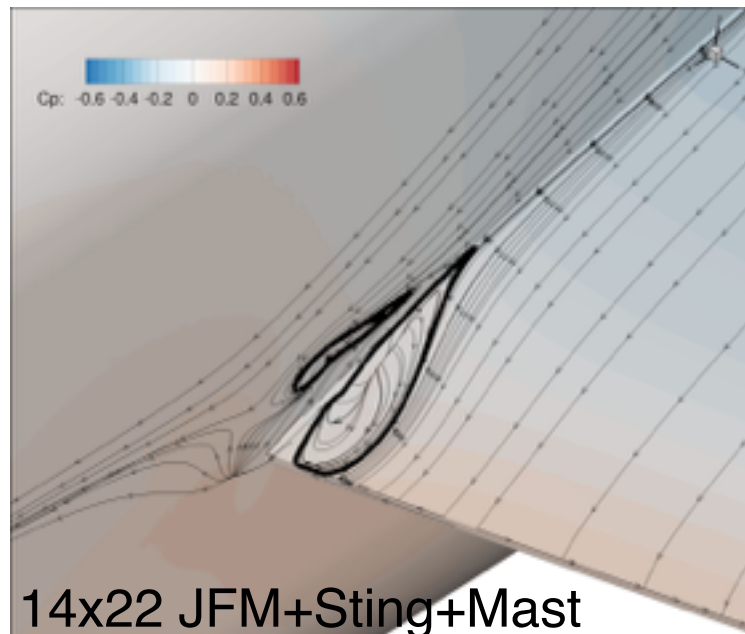
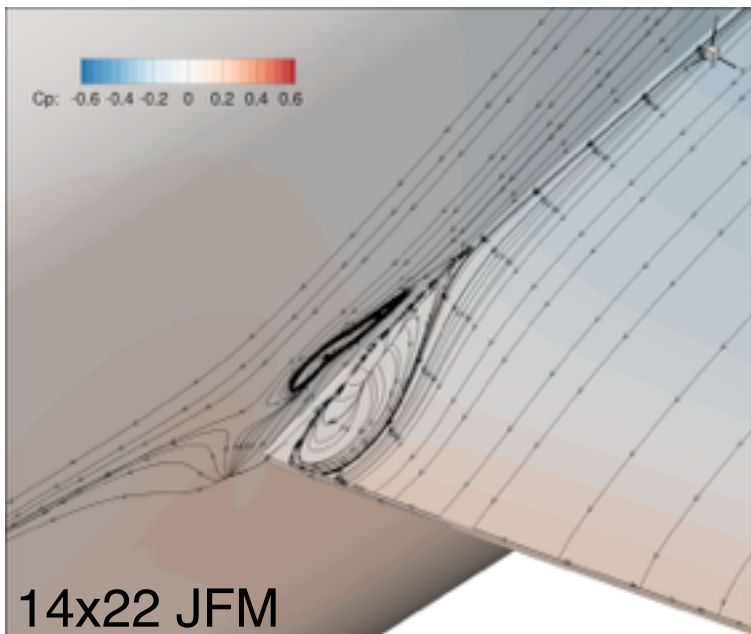
14x22 JFM Support Hardware Comparison $\alpha=5.0^\circ$



14x22 JFM ΔC_p Comparison $\alpha=5.0^\circ$



14x22 JFM Bubble Comparison $\alpha=5.0^\circ$

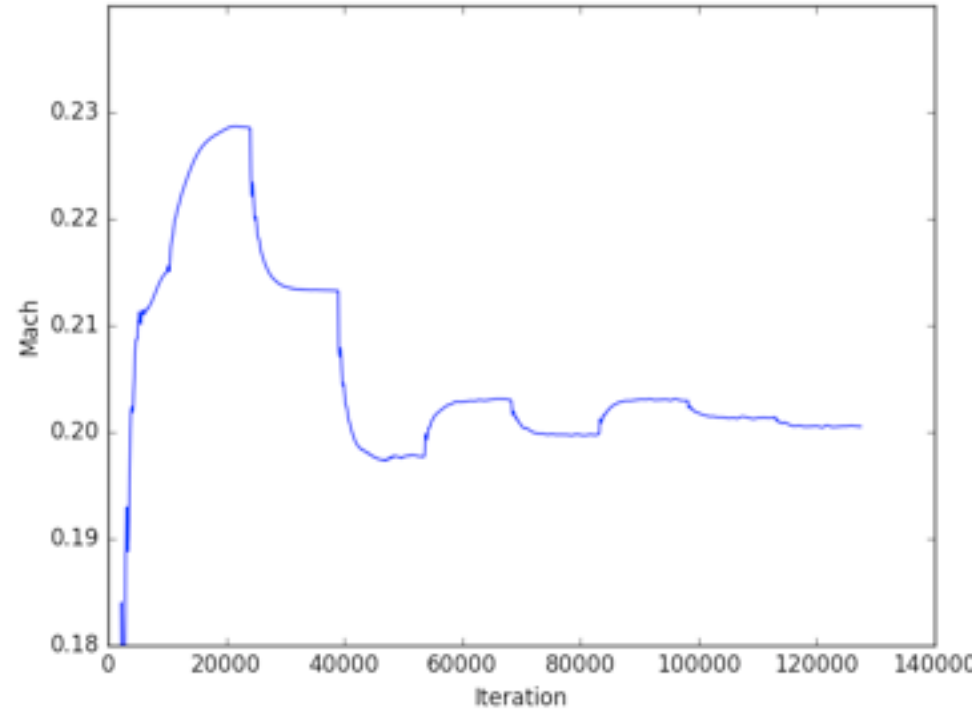
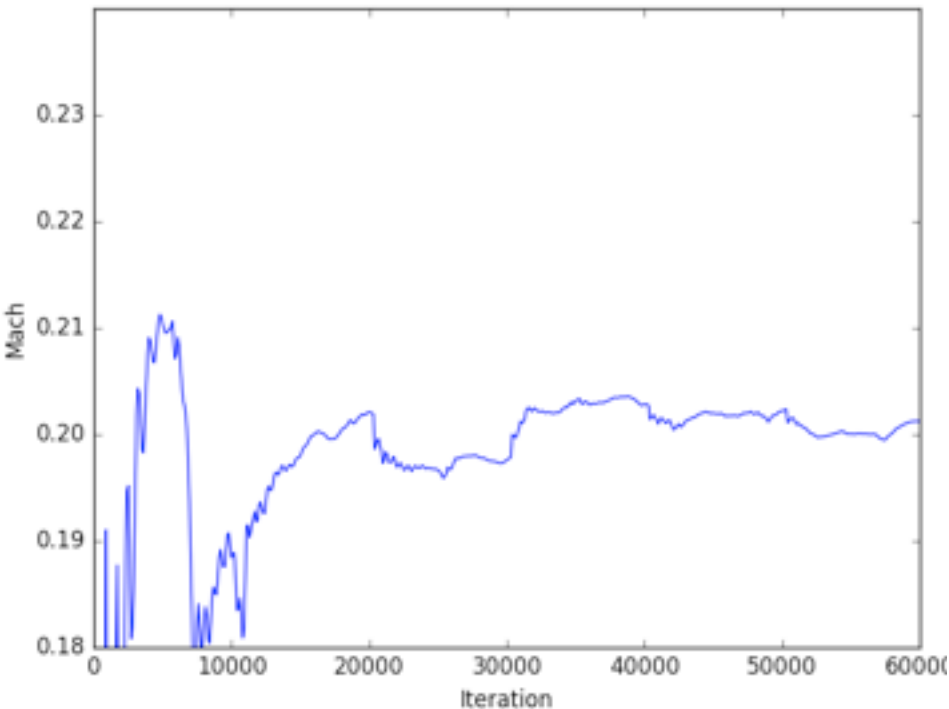


14x22 Tunnel Extension Effect



14x22 wo/Extension
JFM+Sting+Mast

14x22 w/Extension
JFM+Sting+Mast



AOA 5 degrees

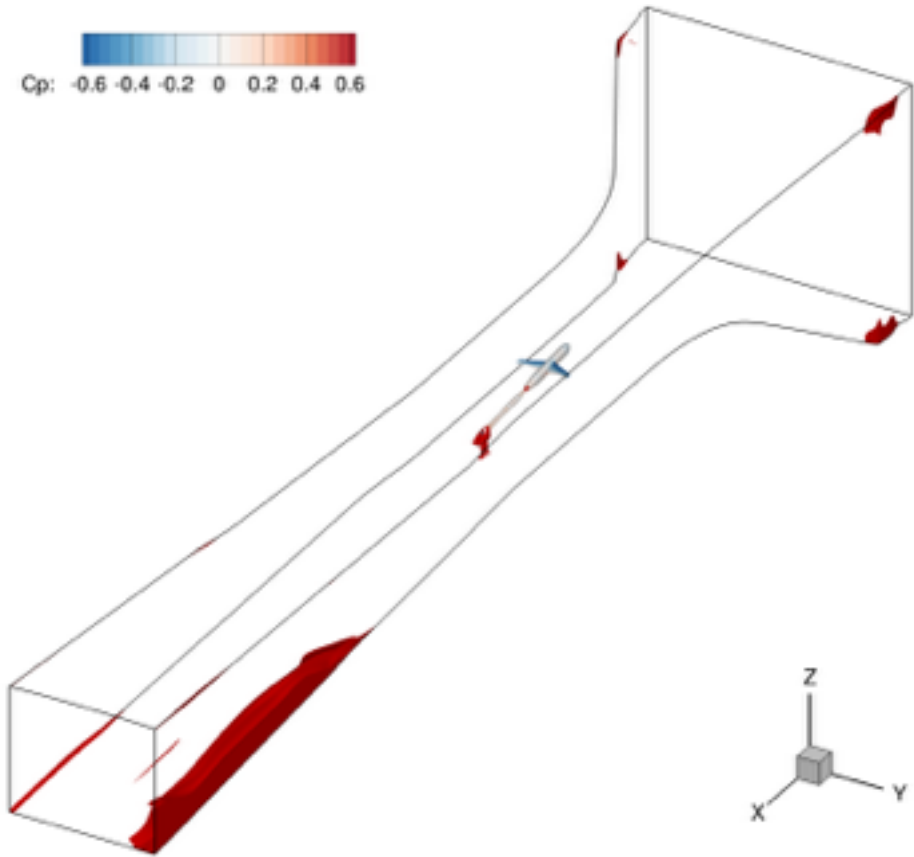
14x22 Tunnel Extension Effect



14x22 JFM+Sting+Mast
w/Extension

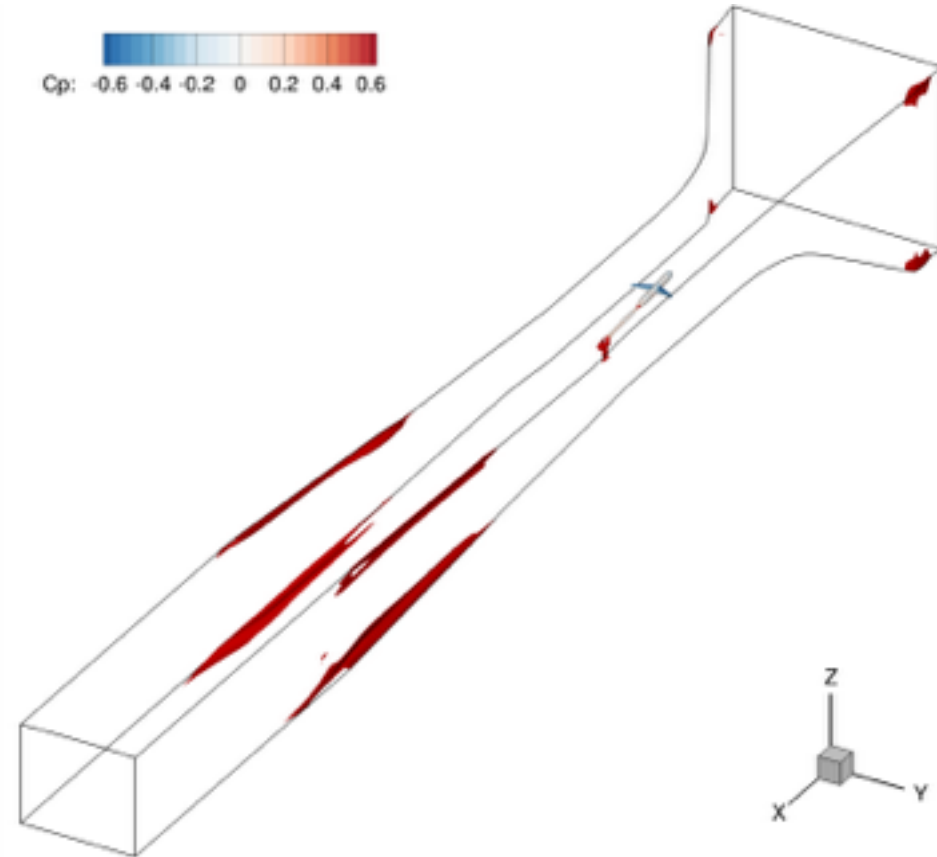
14x22 JFM+Sting+Mast

Cp: -0.6 -0.4 -0.2 0 0.2 0.4 0.6



Pexit ratio = 1.0196

Cp: -0.6 -0.4 -0.2 0 0.2 0.4 0.6



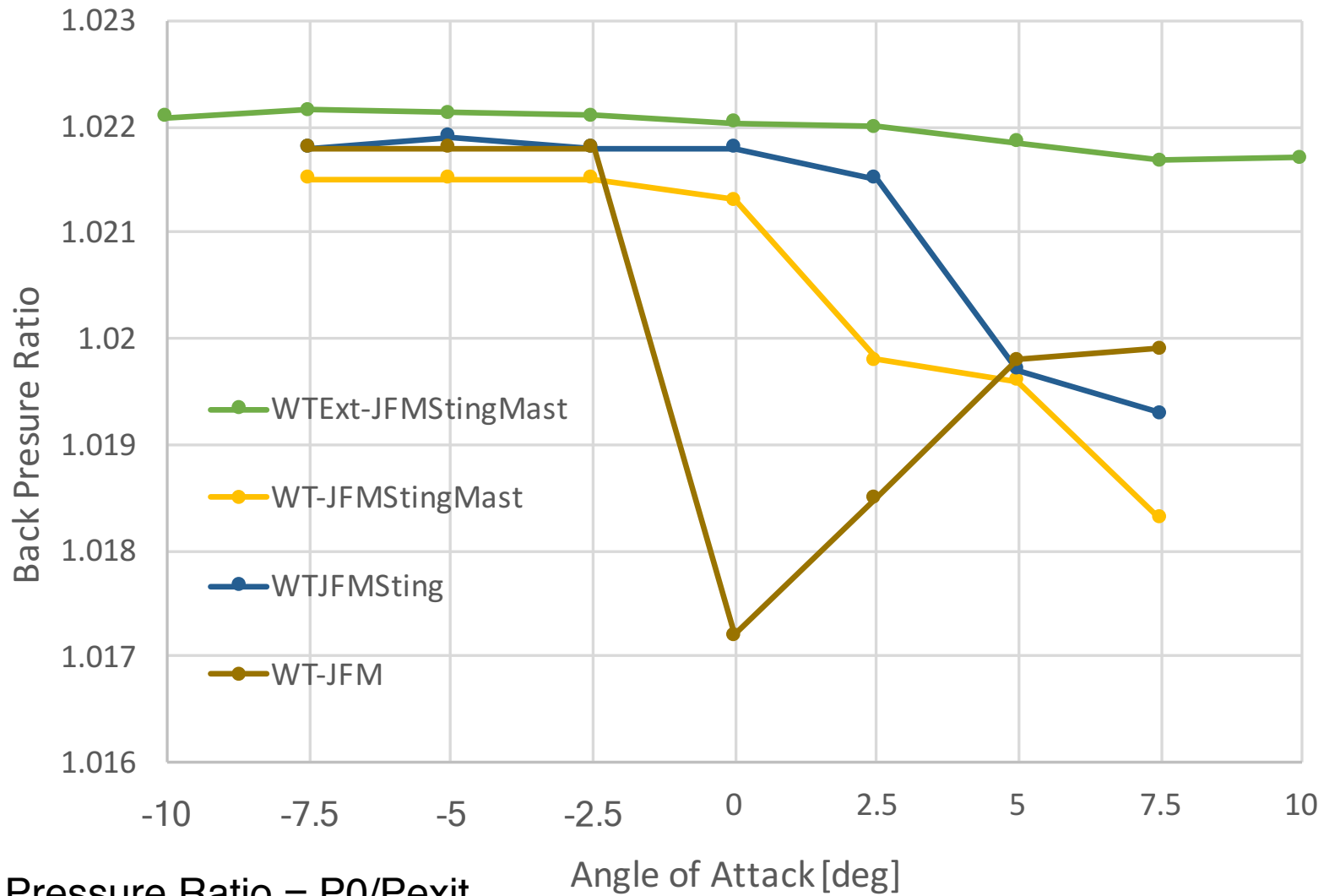
Pexit ratio = 1.02185

AOA 5 degrees

14x22 Back Pressure Ratio Mach 0.2



Back Pressure Ratio vs Angle of Attack

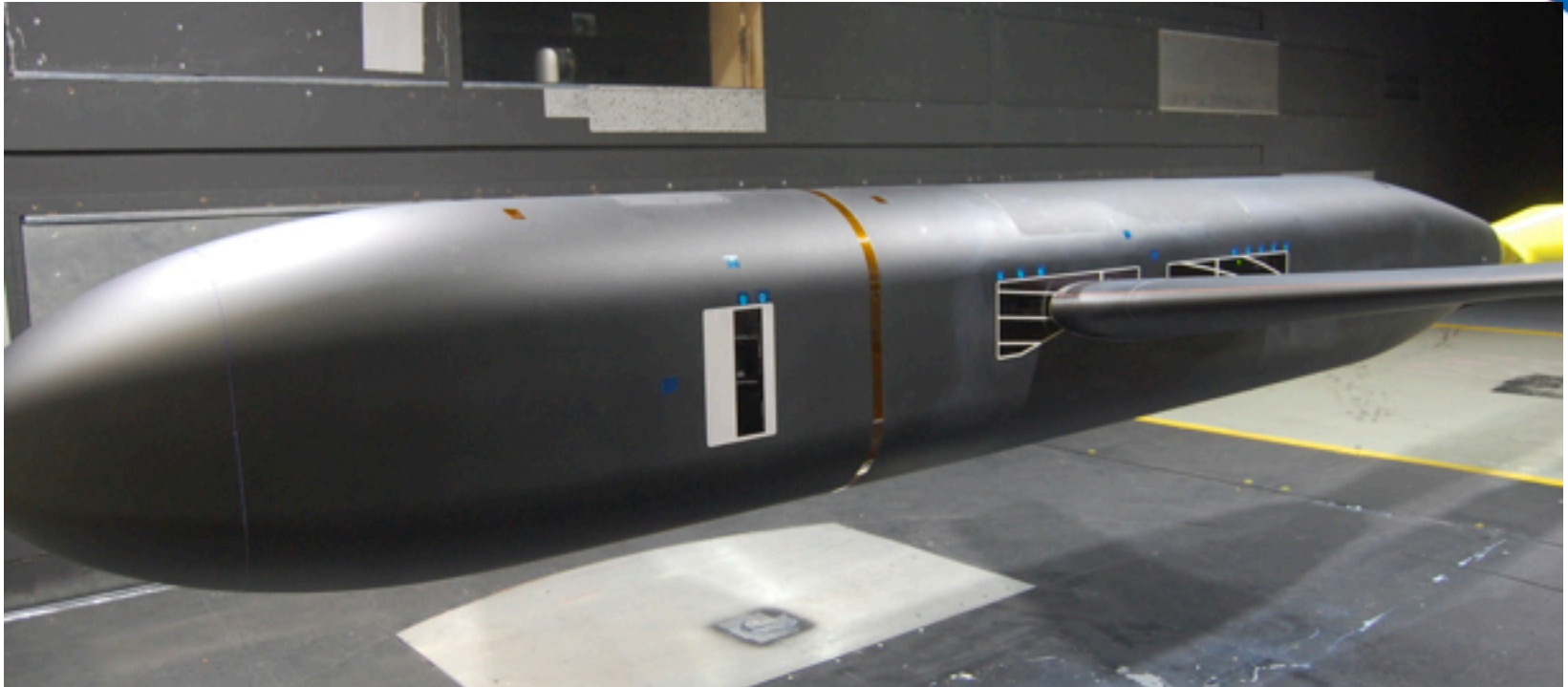


Back Pressure Ratio = P_0/P_{exit}

14x22 8% JFM Increment Summary

- Support Hardware
 - Pressures were very similar for all results
 - Bubble size was insensitive to support hardware, and tunnel extension (preliminary result)
- 14x22 WT vs 14x22 WT with Inviscid Extension
 - Suppresses the corner separation in the diffuser
 - Back pressure does not need to be as high
 - Extension Exit Pressure ratio is closer to empty tunnel value (1.022)
 - Tunnel speed settles out much faster
- Need to still look at effect of adding Inviscid Inlet on JFM

Future Work



- Compare CFD WT to CFD Free Air
- Compare with WT data once available
 - Cp profiles, oil flows
 - Velocity & Reynolds stress profiles
- Automate back pressure ratio (PID controller)

Acknowledgements



NASA's Transformational Tools and Technologies (T³) Project

Chris Rumsey and the Juncture Flow committee:

NASA Langley: P. Balakumar, Mark Cagle, Dick Campbell, Jan-Renee Carlson, Andy Davenport, Kevin Distill, Judy Hannon, Luther Jenkins, Bil Kleb, Mujeeb Malik, Cathy McGinley, Joe Morrison, Frank Quinto, Don Smith, Sandy Webb

NASA Ames: Henry Lee, Thomas Pulliam, James Bell, Nettie Roozeboom, Laura Simurda, Greg Zilliac

Boeing: Mike Beyer, Neal Harrison, Peter Hartwich, Philippe Spalart, Tony Sclafani, John Vassberg

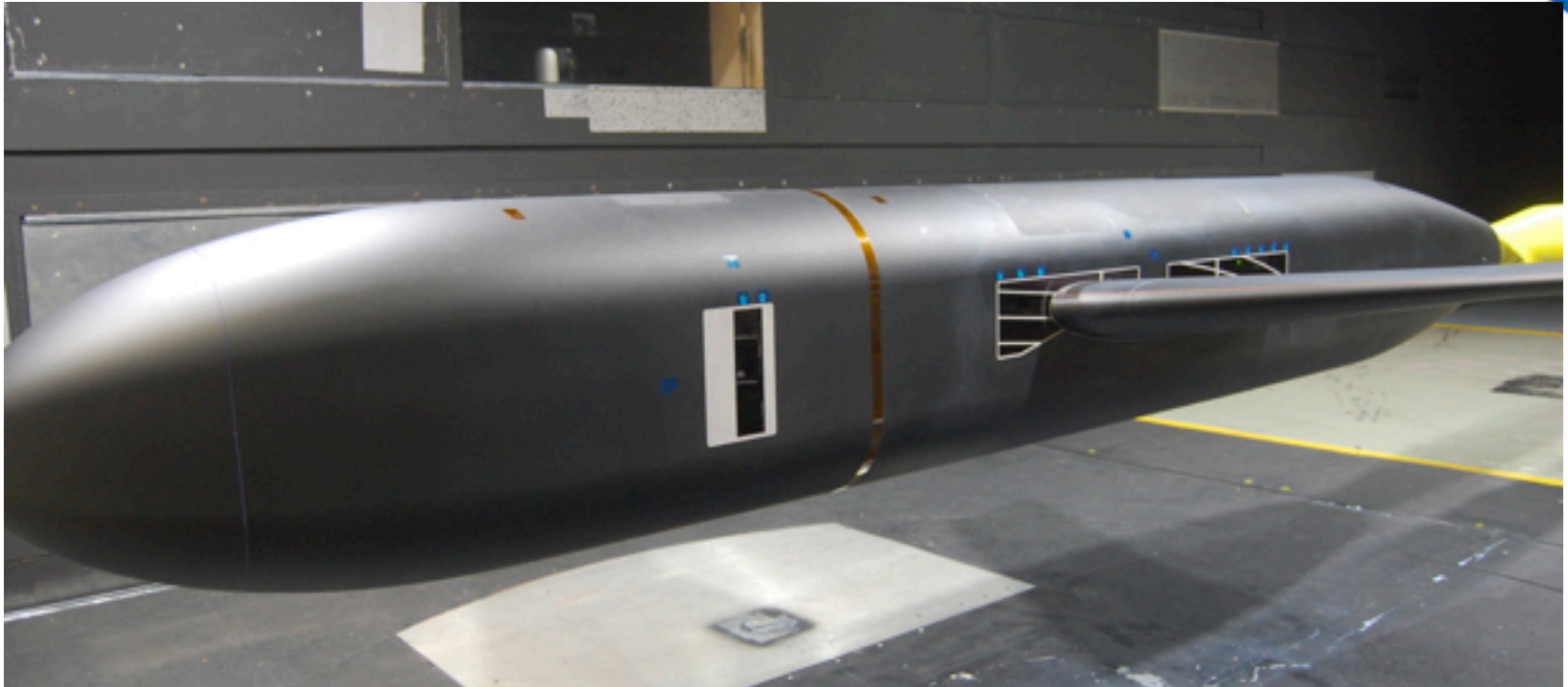
AUR: Gwibo Byun and Roger Simpson

Virginia Tech: Aurelien Borgoltz and Todd Lowe

University of Kentucky: Jim Coder

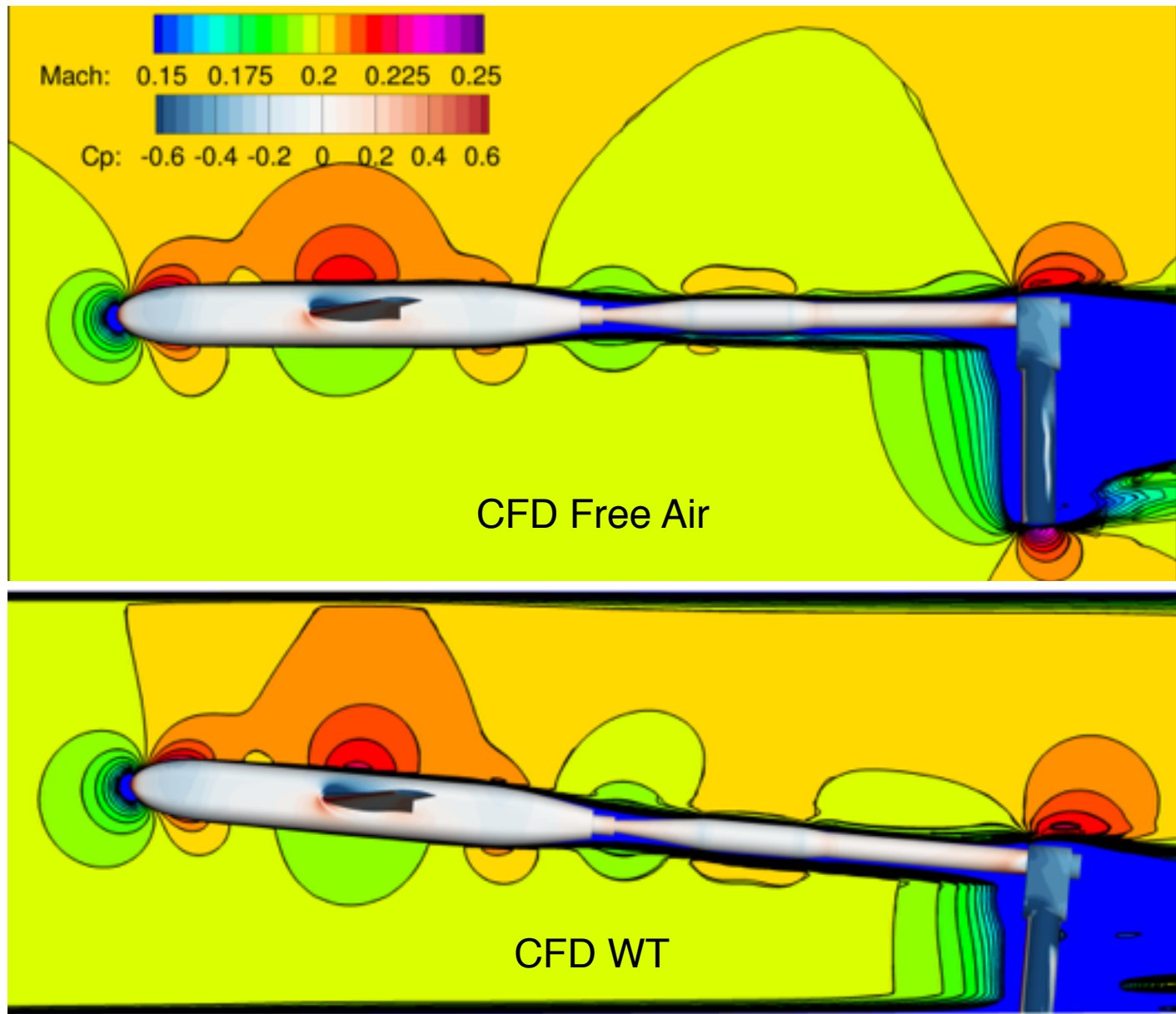
Bill Oberkampf

Discussion



- How else can we improve modeling with WT walls?
- What do we need to do to this dataset to best help CFD community improve their models?

Preliminary CFD Free Air vs CFD WT



AOA 5 degrees