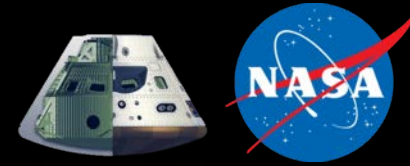


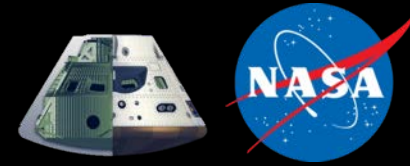
# CHARACTERIZATION OF THERMAL PROTECTION SYSTEMS



An Analysis of Optical & Thermal Properties

Brian Cole, Clemson University (AMA)  
Jay Feldman, NASA ARC (MEDLI2)  
Matthew Gasch, NASA ARC (PICA-D & HEEET)

NASA ARC Annual Research Symposium  
Moffett Field, CA August 8<sup>th</sup>, 2019



## **Background**

- Background & Objectives

## **Materials Introduction**

- Various Ablative Thermal Protection Systems (TPS)

## **Optical Properties**

- Infrared, Ultra-Violet, & Visible Radiation Spectra
- Emissivity & Absorptivity Calculations

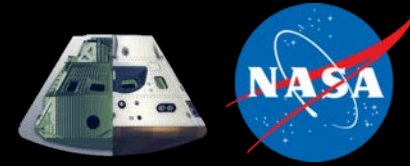
## **Thermal Properties**

- Specific Heat & Thermal Conductivity

## **Summary**

- Research Accomplishments & Contribution Towards Mars 2020

# Background & Objectives



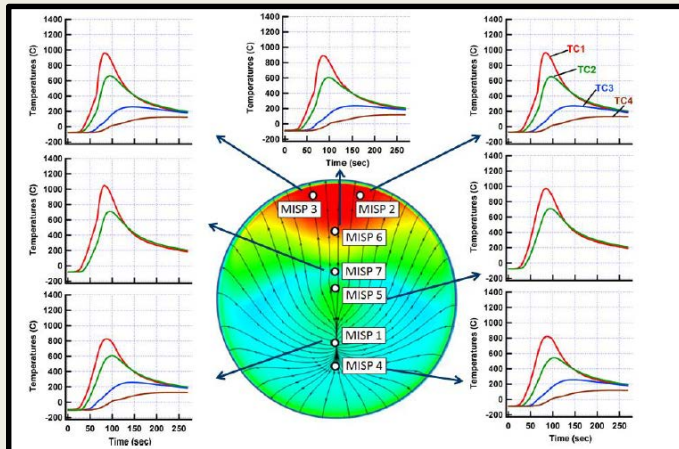
## We Aim To Measure Physical Properties:

### MEDLI Example

Improve Thermal Response Models



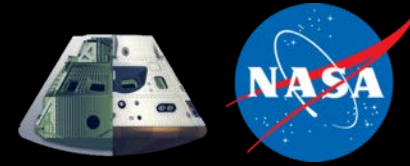
Reconstruct Flight Environments



Design TPS For Future Missions

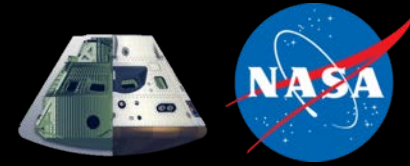


# Background & Objectives



- **Objective:** Characterize Properties of TPS Materials
  - Optical properties
  - Thermal properties
- This allows us to develop Thermal Response Models for TPS
- The models enable design of TPS for Flight Missions and analysis of flight data to understand Aerothermal Environments experienced on the mission
- Comparing pre-flight predictions with actual flight data can allow us to reduce TPS margins and improve designs
  - **MEDLI** and **MEDLI2** are examples of this to be discussed

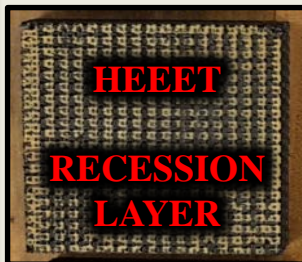
# Materials Studied



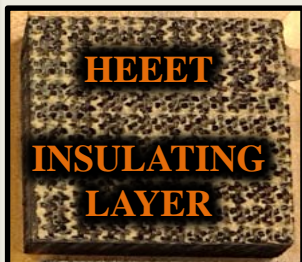
## TPS Materials



Low Density Ablative  
Sustainable Material  
Made in USA



High Density  
3D Woven Material  
Opens Doors For  
Venus & Saturn



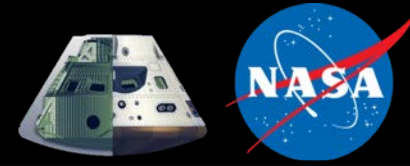
Lower Density  
3D Woven Material  
Lower Thermal Conductivity



## Thermal Control Coatings

AZ 93	\$440.00 per pint Standard White Inorganic Coating
AZ 2100	\$1800.00 per pint Electrically Conductive
AZ W	\$7200.00 per pint Very Low Solar Absorbance

# Optical Properties Overview



1

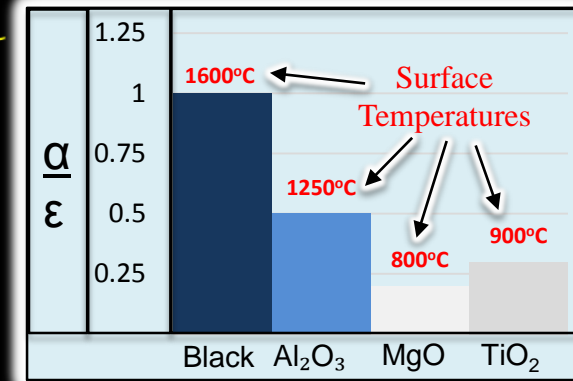


On Entry, Radiative Emission Is a Primary Cooling Method for TPS

2



On Orbit, Re-Emitting Solar Rays Reduces The Equilibrium Surface Temperature



FTIR (Fourier Transform Infrared Spectroscopy)

UV-Vis (Ultra-Violet & Visible Light Spectroscopy)



Calculate

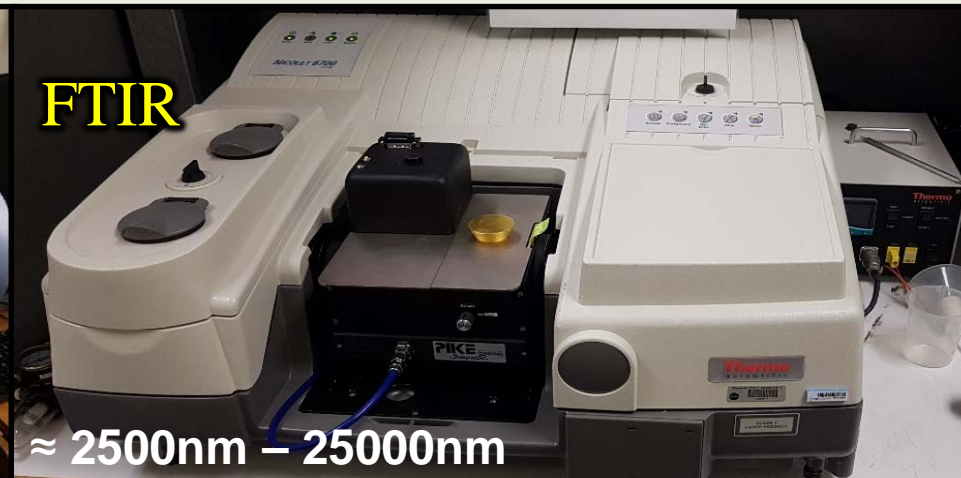
**Emissivity & Absorptivity**

**UV-VIS**



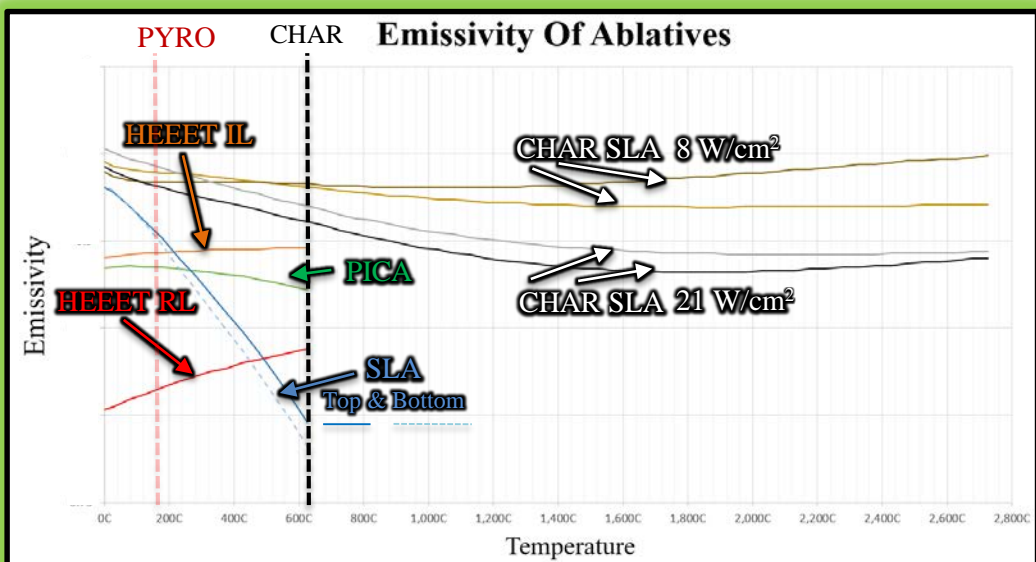
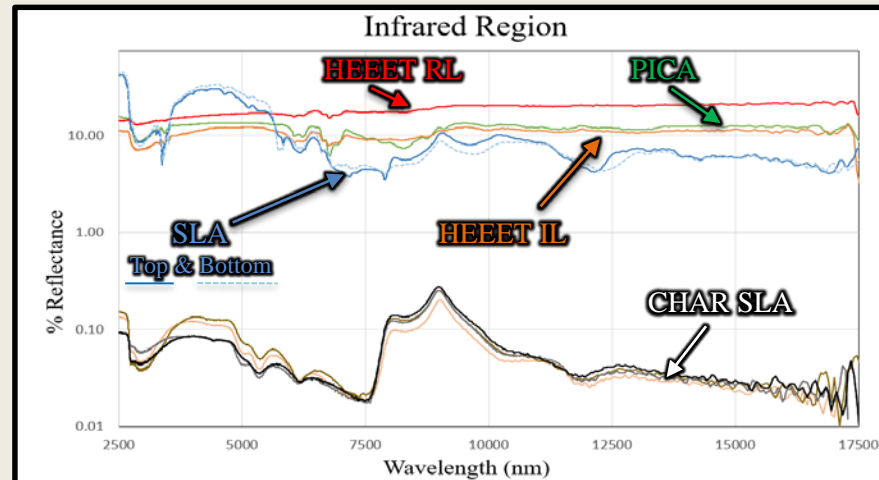
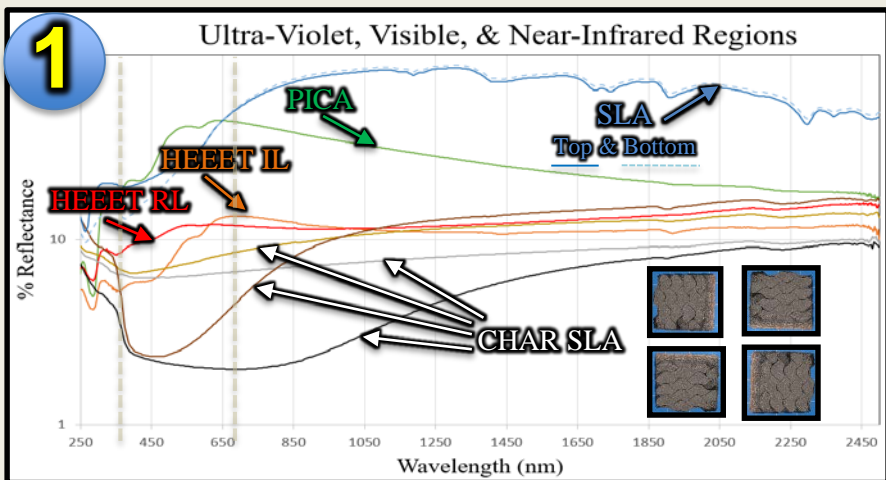
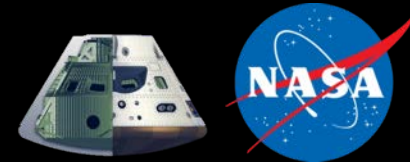
≈ 250nm – 2500nm

**FTIR**



≈ 2500nm – 25000nm

# SLA Optical Properties



## UV & VISIBLE REGIONS

- Char Consistent With Expectations (Absorbs Visible Light)

## INFRARED REGION

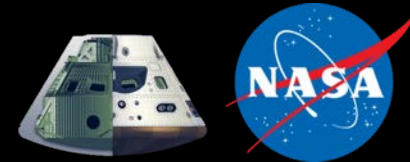
- Evidence of OH & CO Chemistry

## EMISSIVITY (0°C -> 2700°C)

NOTE: SLA Fully Chars at 600°C

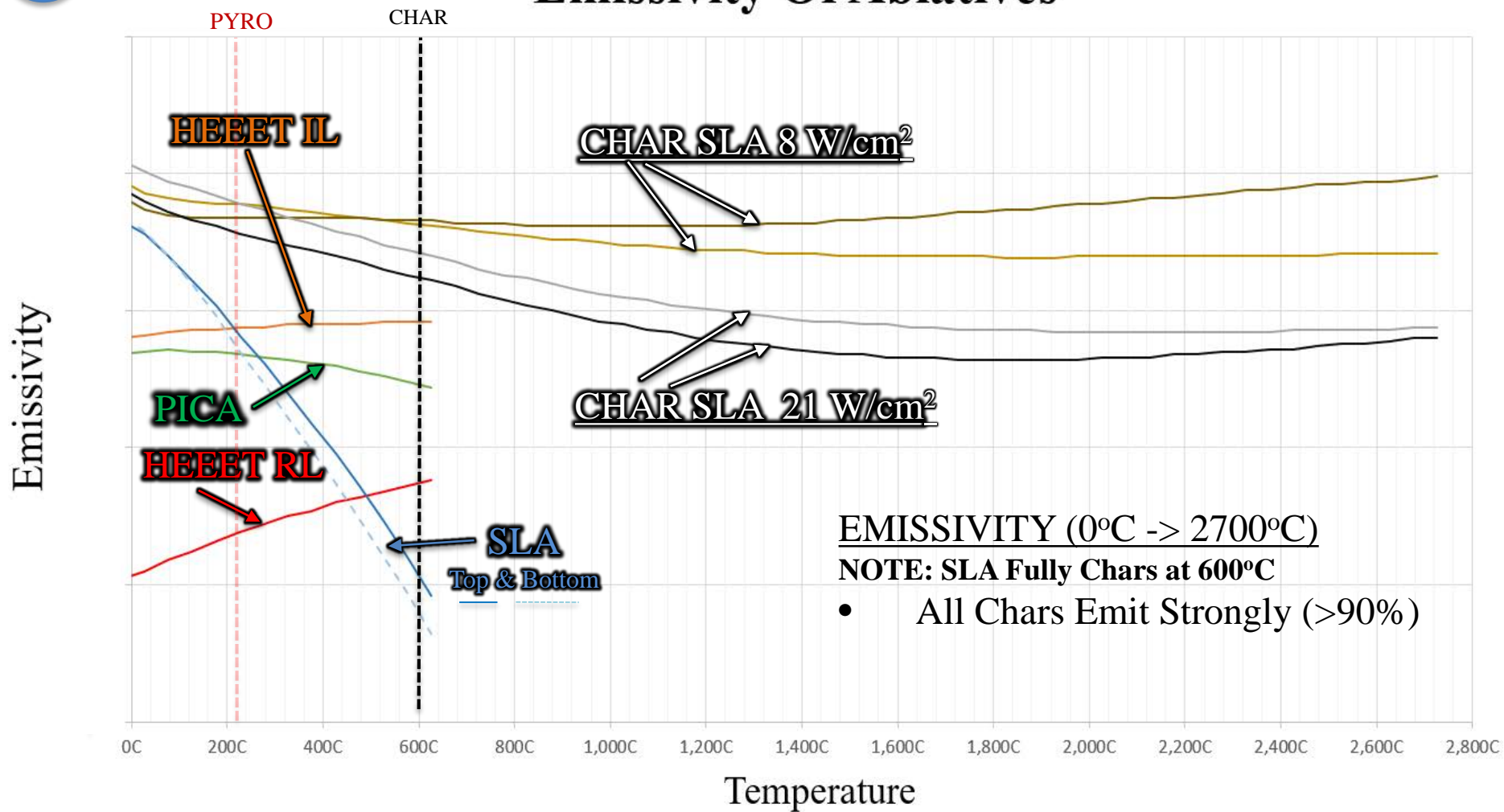
- All Chars Emit Strongly (>90%)

# SLA Emissivity



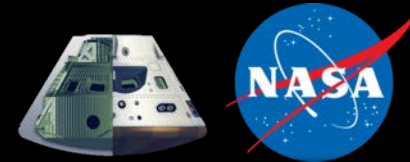
1

## Emissivity Of Ablatives



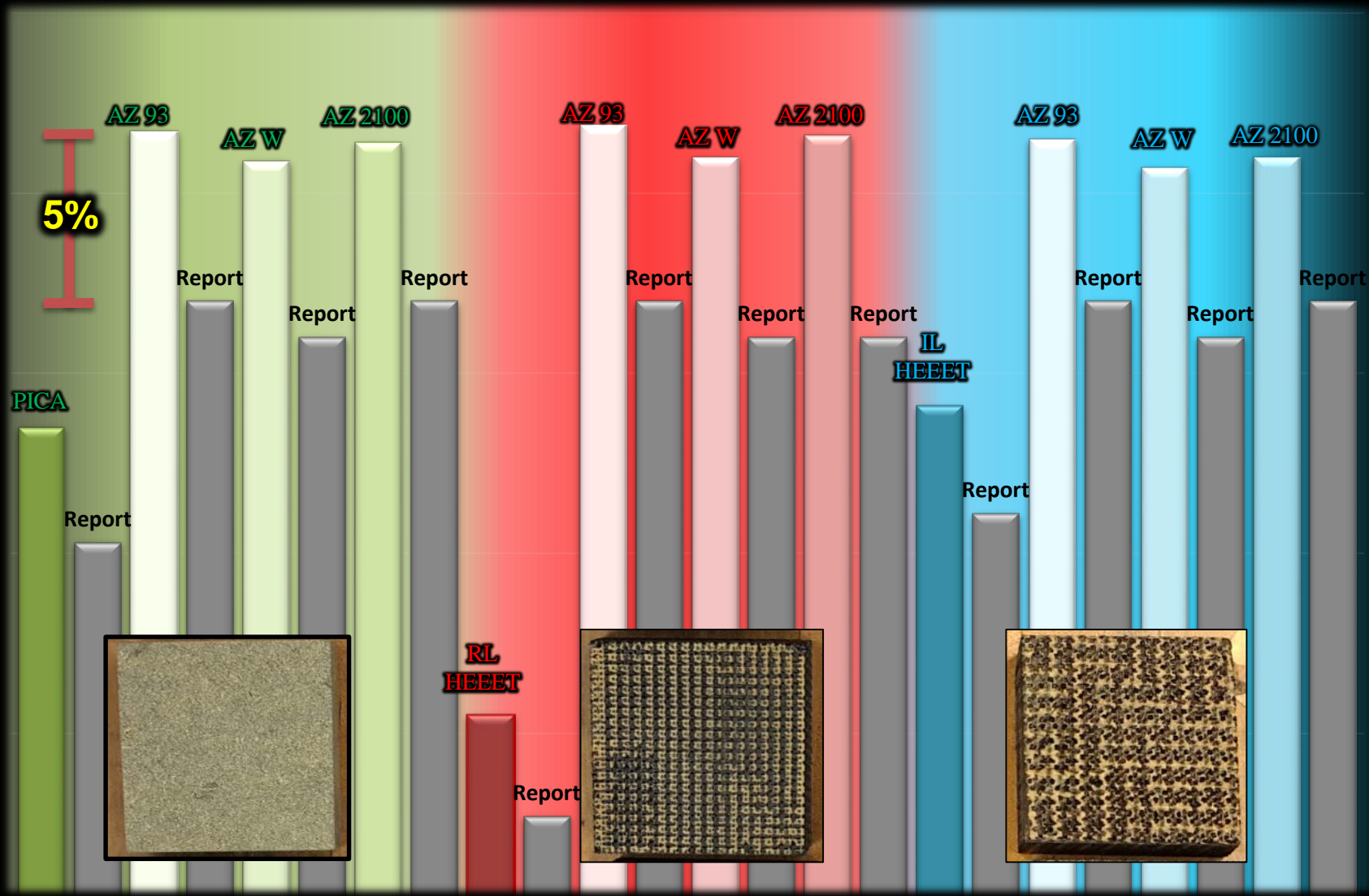


# Thermal Control Coating Emissivity

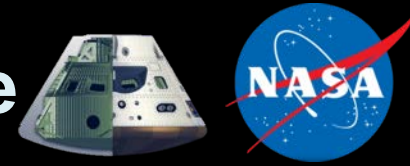


2

Emissivity at Room Temperature

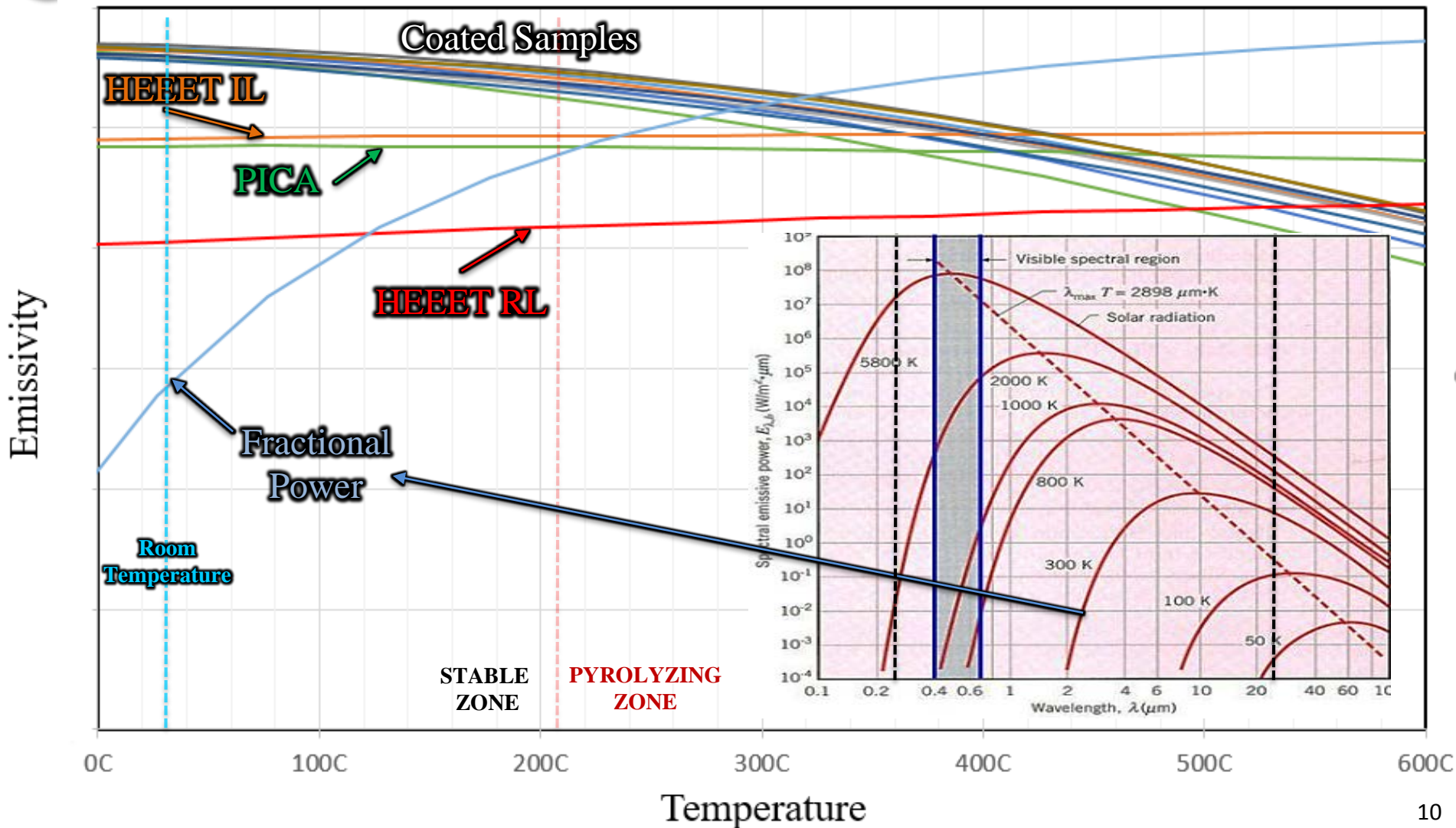


# Emissivity as a Function of Temperature

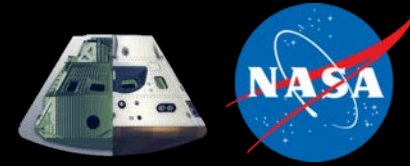


2

## The Effect of Various White Coatings On The Emissivity

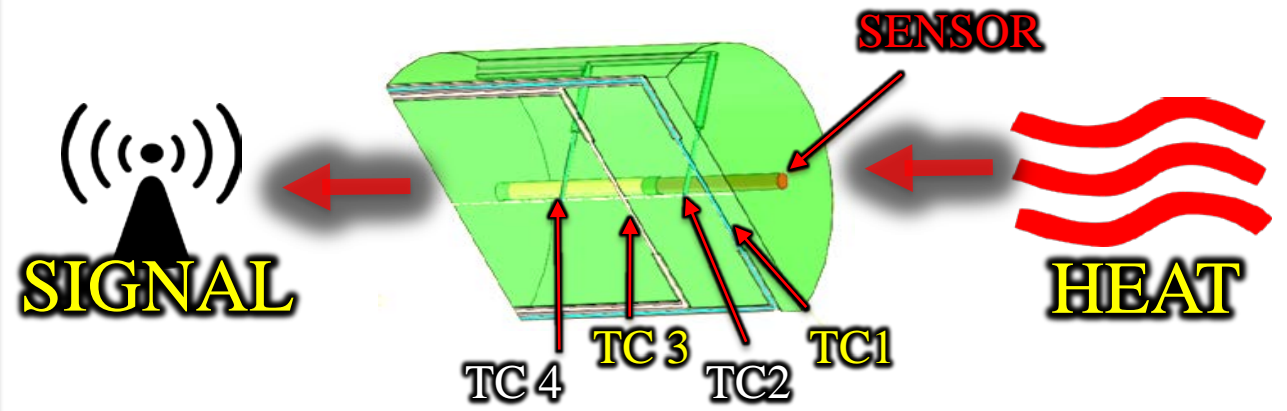


# Thermal Properties Overview



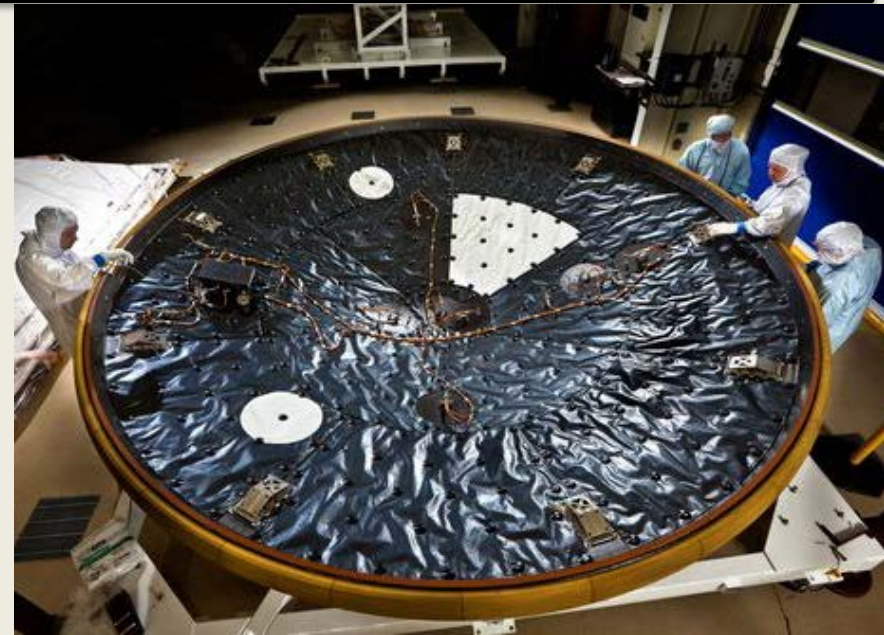
- Mars Science Laboratory (MSL) launched in Nov **2011** & landed Curiosity Aug **2012**

$c_p$  (Heat Capacity)  
&  
 $\lambda$  (Thermal Conductivity)  
-----  
Allows Us To Infer  
The In-Depth  
Thermal Response

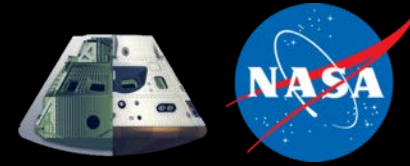


## Example: Original MEDLI

- Improved Engineered Models for Future Missions
- Predicted T & P Response of TPS
- Improved Margins Allowing an Increased Payload



# Solid State Heat Flow Meter Fox 50



## Instrument Specifications

- Sample Size [2"-2.5" Diameter]
- Range [ -10°C – 185°C ]
- Accuracy [ ± 4% ]
- Reproducibility [ ± 2% ]

## Methodology

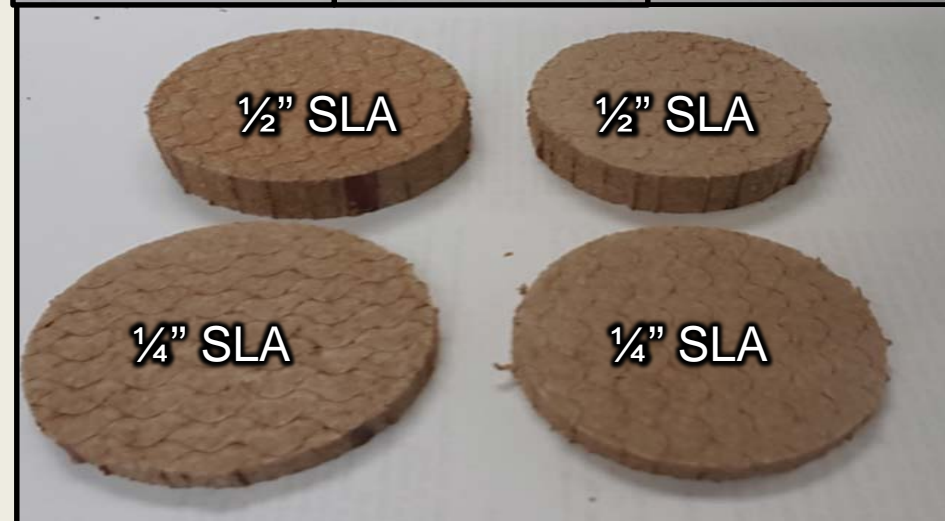
1. Obtain Contact Resistance of Rubber Matt  
– Via two dx exp. with Perspex Standard
2. Measure  $\lambda$  of Standards & Samples
3. Correct  $\lambda$  by Rubber Matt Subtraction

## Rubber Matt Subtraction Formula

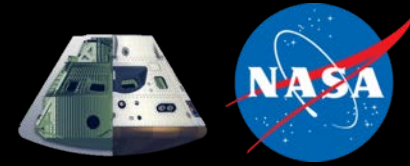
### Assumptions

- 1) [ $\lambda_T - \lambda_R$  is Negligible]
- 2) [ $\lambda_R \cong \lambda_S$ ]  $\rightarrow$  [ $\frac{\lambda_S}{\lambda_R} \cong 1$ ]
- 3) [ $T_t \cong S_t - R_t$ ]

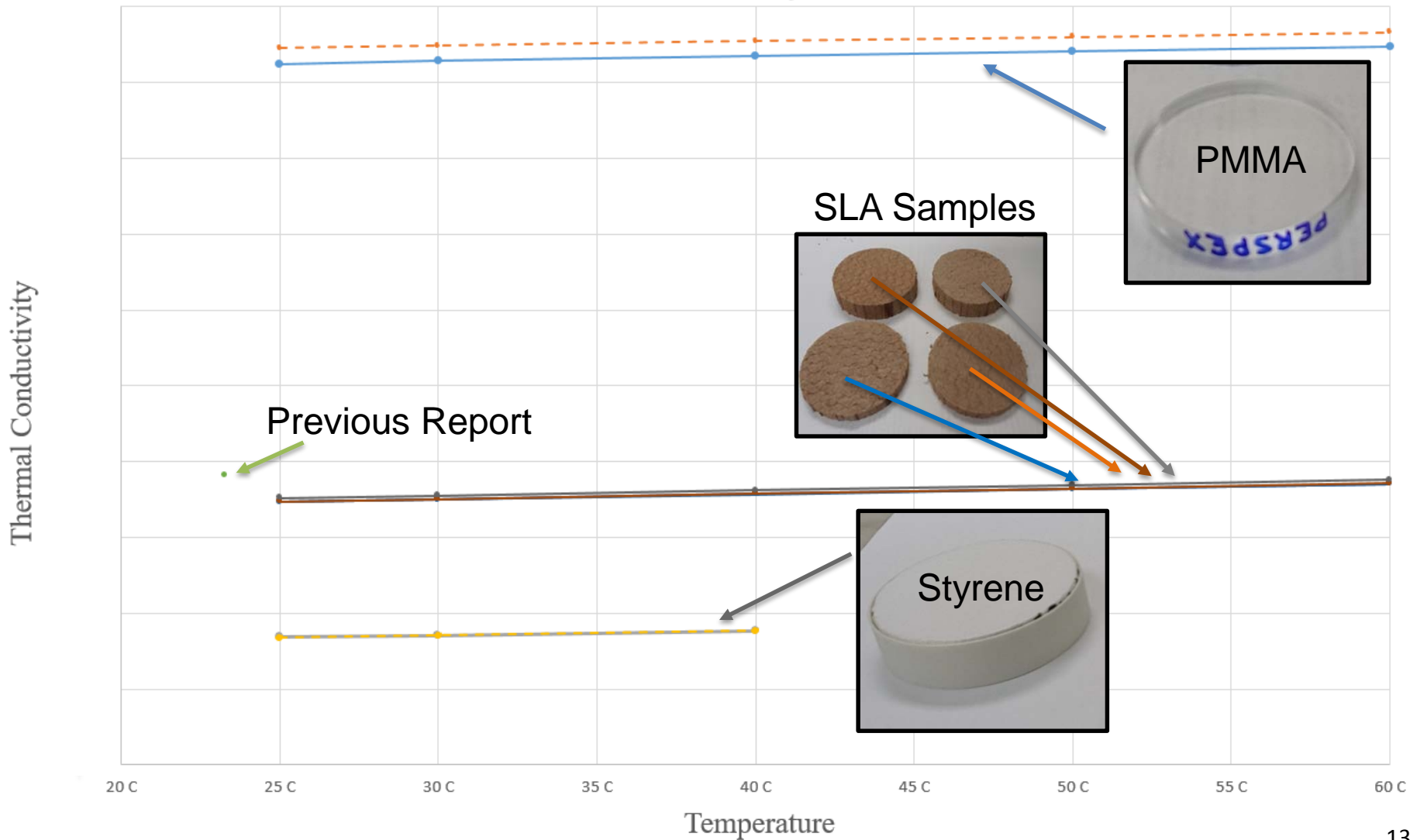
$$\frac{(T)_t - R_t}{\frac{(T)_t}{\lambda_T} - \frac{R_t}{\lambda_R}} = \lambda_S$$



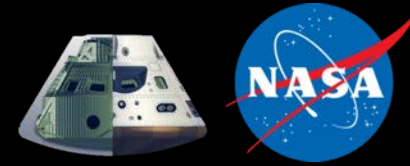
# Thermal Conductivity of SLA



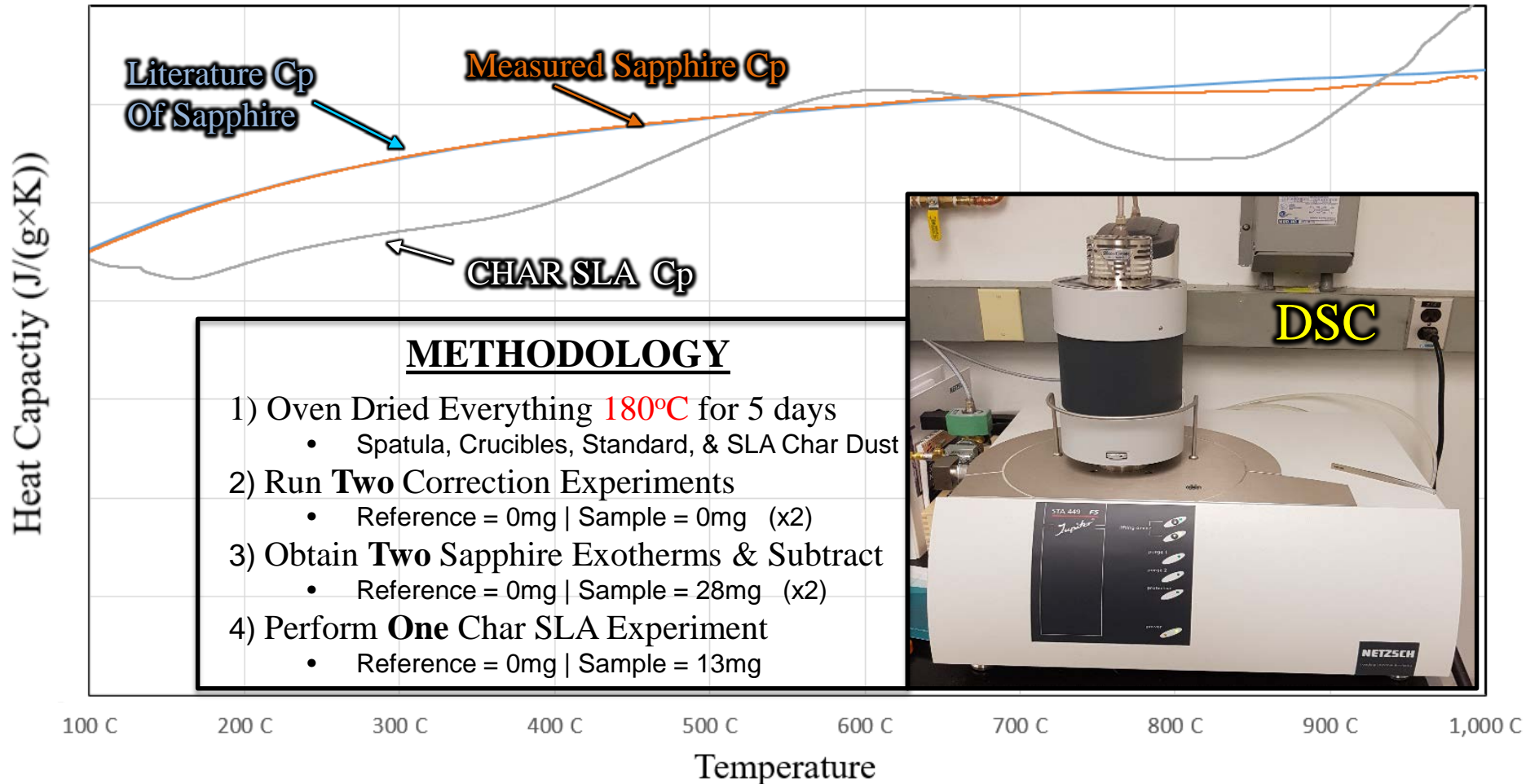
## Thermal Conductivity of SLA



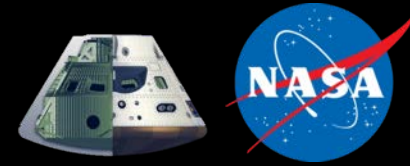
# Heat Capacity by DSC



## Specific Heat of SLA CHAR vs. Sapphire Standard

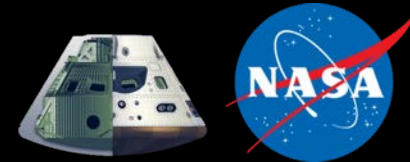


# Summary



- Reviewed Various Ablative Materials
  - Purpose & Utility In NASA Missions
- Contributed Values For MEDLI2 Thermal Response Models and PICA-D and HEEET thermal response models
  - Optical Properties (Emissivity & Absorptivity)
  - Thermal Properties (Heat Capacity & Thermal Conductivity)
- Some of This Work is Not Complete and Highlights Questions To Investigate in The Future

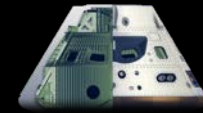
# Acknowledgments



## Special Thanks To:

- Jay Feldman
- Matthew Gasch
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- Tane Boghozian
- Greg Gonzales
- Susan White
- NASA AMES RESEARCH CENTER

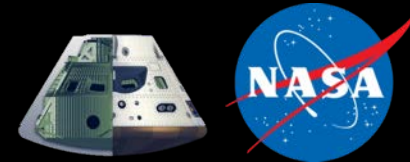




# Questions?



# Solid State Heat Flow Meter Fox 50



## Instrument Specifications

- Sample Size [2"-2.5" Diameter]
- Range [ 0°C – 190°C ]
- Accuracy [ ± 4% ]
- Reproducibility [ ± 2% ]



$$\frac{\left( \frac{(T)_t - R_t}{\lambda_T} - \frac{R_t}{\lambda_R} \right)}{\left( \frac{(T)_t - R_t}{\lambda_S} - \frac{R_t}{\lambda_S} \right)} = \frac{\left( \frac{S_t - R_t}{\lambda_S} - \frac{R_t}{\lambda_S} \right)}{\left( \frac{S_t + R_t}{\lambda_S} - \frac{R_t}{\lambda_S} \right)} = \frac{\left( \frac{S_t}{\lambda_S} \right)}{\left( \frac{S_t}{\lambda_S} \right)} = \frac{1}{1} = \lambda_S$$

1. Obtain
2. Measure
3. Correct

## Rubber Matt Subtraction Formula

- 1)  $[\lambda_T - \lambda_R \text{ is Negligible}]$
- 2)  $[\lambda_R \cong \lambda_S] \rightarrow \left[ \frac{\lambda_S}{\lambda_R} \cong 1 \right]$
- 3)  $[T_t \cong S_t - R_t]$

$$\frac{(T)_t - R_t}{\lambda_T} - \frac{R_t}{\lambda_R} = \lambda_S$$

