

The Impacts of Cabin Atmosphere Quality Standards and Control Loads on Atmosphere Revitalization Process Design

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Introduction

Atmosphere revitalization functions include:

- Carbon dioxide removal
- Trace contaminant control
- Particulate and debris removal

Standards defined by:

- NASA-STD-3001 Vol. 2

Supplemented by:

- NASA/SP-2010-3407 Rev. 1 (2014)
- Relevant literature



The Material Balance

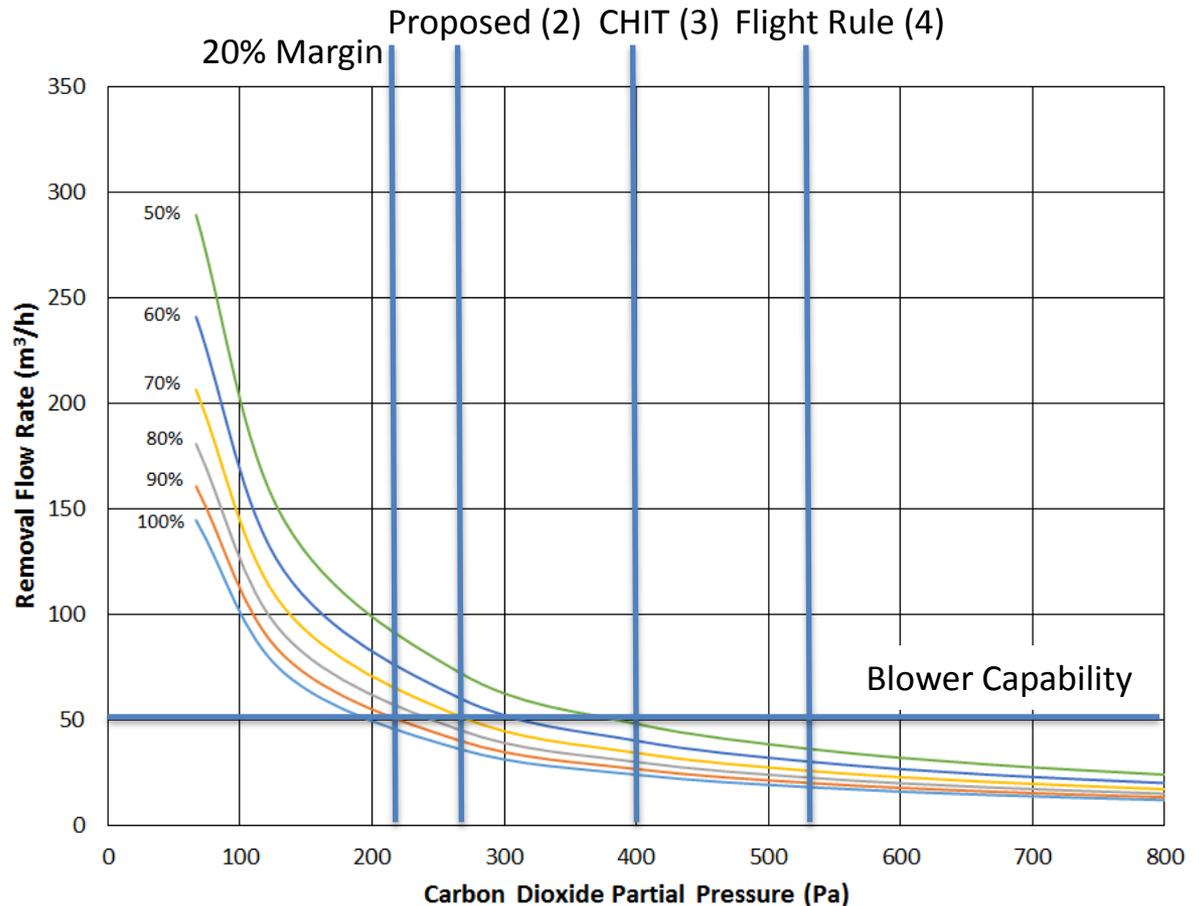
<i>Basis</i>	<i>Equation</i>	<i>Steady State</i>
<i>Mass:</i>	$\frac{dm}{dt} = r_i - \left(\frac{\eta \dot{v}}{V}\right) m$	$m = r_i V / \eta \dot{v}$
<i>Concentration:</i>	$\frac{dC}{dt} = r_i / V - \left(\frac{\eta \dot{v}}{V}\right) C$	$C = r_i / \eta \dot{v}$
<i>Pressure:</i>	$\frac{dp}{dt} = \left(\frac{RT}{MV}\right) r_i - \left(\frac{\eta \dot{v}}{V}\right) p$	$p = \left(\frac{RT}{M}\right) \left(r_i / \eta \dot{v}\right)$

Effective flow = Load/Control standard



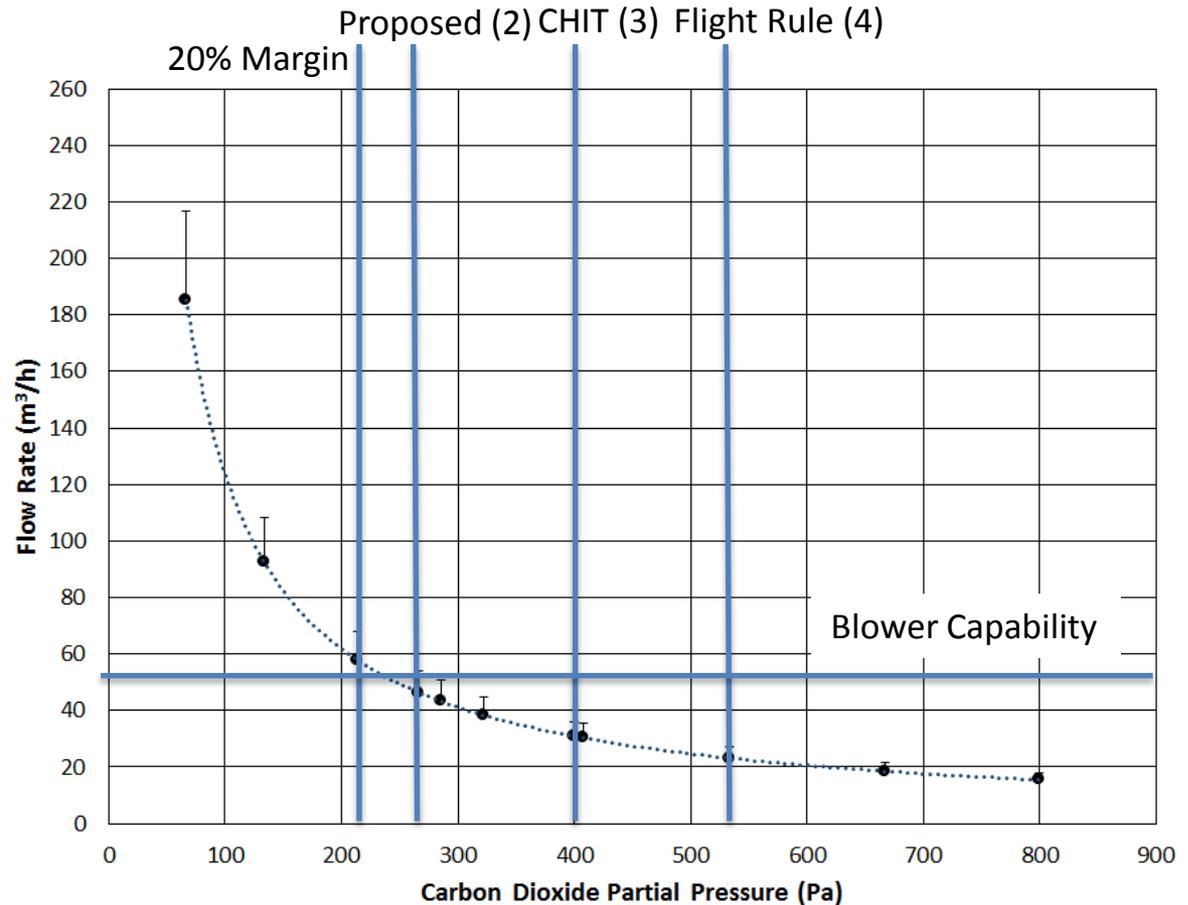
Carbon Dioxide – Part 1

- More challenging control standard for exploration.
- Effective flow increases rapidly for control standards <300 Pa.
- Flow for proposed standard with 20% margin is 150% higher than the ISS flight rule level and 88% higher than the CHIT level.



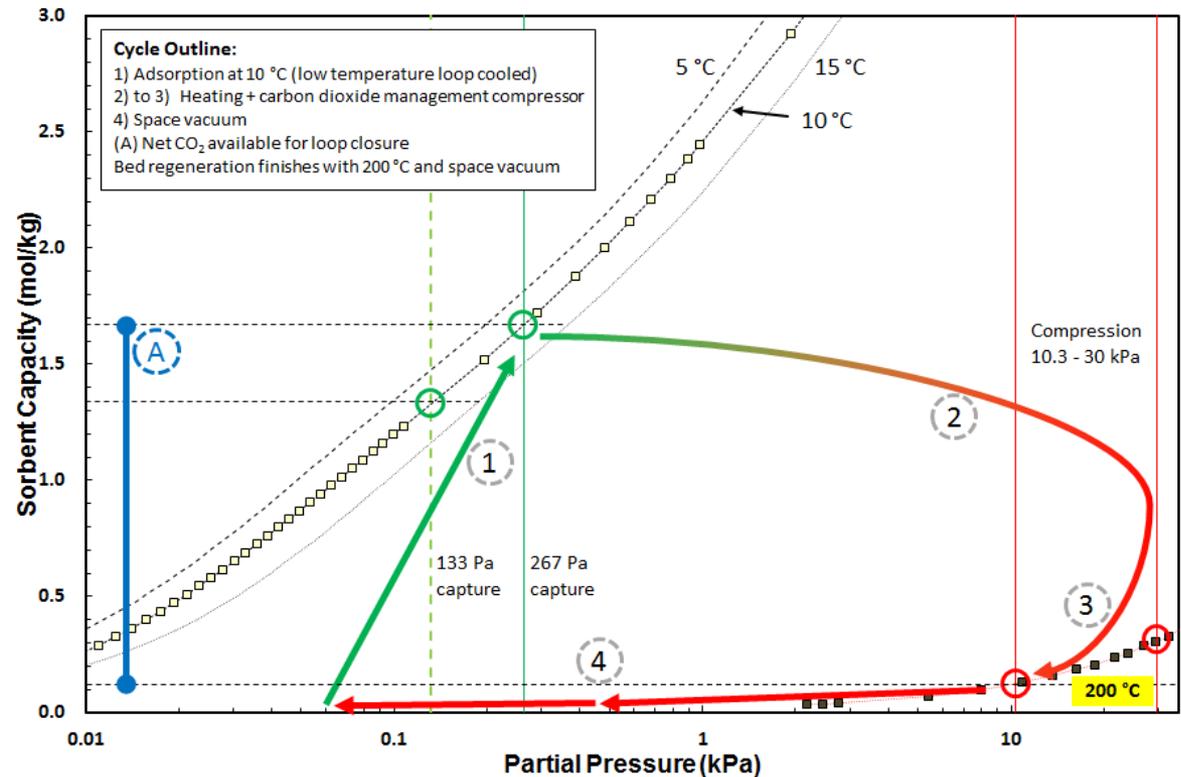
Carbon Dioxide – Part 2

- Flow margin is added to accommodate load variability.
- Exercise protocols and crew physical size.
- Up to 17% flow margin on top of the control standard impacts.
- Power growth at 213 Pa control standard is 62% higher than for 400 Pa control standard.



Carbon Dioxide – Part 3

- Lower carbon dioxide partial pressure reduces working capacity.
- With no other compensation or system growth, 33% loss in available carbon dioxide for reduction processes may result.



Courtesy Greg Cmarik.



Trace Contaminant Control

- Load source impacts lead to flow rate and size growth.
 - Urine distillation vent gases: 0.1 mg/h non-methane VOCs (<1%)
 - Heat melt trash compaction: 118 mg/h non-methane VOCS (4X flow)
 - Water recovery from urine distillation brine: 38 mg/h non-methane VOCs (2X flow)
- Impacts from maximum allowable concentration updates.
 - Design flow rate driver decreased from 7 mg/m³ to 2 mg/m³ (71% decrease)
 - Load decrease of 85% offset the maximum allowable concentration change.
- Maximum allowable concentration implementation.
 - Incorporating toxic hazard index increases flow by up to a factor of 2.4.

$$\eta \dot{v} = \left(1/T_H\right) \sum r_i / C_{max}$$



Particulate Matter Control

- Control standard in NASA-STD-3001 Vol. 2 is 80 times less challenging than that used by the ISS Program.
 - ISS Program based the design requirement on Class 100K cleanroom.
 - $<0.05 \text{ mg/m}^3$ for the size range $0.5 \text{ }\mu\text{m}$ to $100 \text{ }\mu\text{m}$.
 - NASA-STD-3001 Vol. 2 is based on human health effects.
 - $<1 \text{ mg/m}^3$ for the size range $0.5 \text{ }\mu\text{m}$ to $10 \text{ }\mu\text{m}$; $<3 \text{ mg/m}^3$ for the size range $10 \text{ }\mu\text{m}$ to $100 \text{ }\mu\text{m}$
- Particle generation load considerations.
 - Literature review indicates particulate generation to be ~ 4 times higher than used for design by the ISS Program: $1.33 \text{ mg/minute-person}$ vs. $0.31 \text{ mg/minute-person}$.
 - Flow required to comply with the NASA-STD-3001 Vol. 2 standard is 93% lower than to meet the ISS requirement for the increased load.
- Bioburden generation load considerations.
 - Load defined as 204 bacteria-related particles/minute-person and 53 fungal-related particles/minute-person.
 - Requires 22% higher flow than controlling the basic particle generation load.
- Surface dust intrusion considerations.
 - Lunar dust $<0.3 \text{ mg/m}^3$ for the size range $<10 \text{ }\mu\text{m}$.
 - Dust intrusion barriers and methods must be $>99.6\%$ effective to avoid substantial filtration flow rate increases.



Conclusion

- Changes to carbon dioxide control standards and loads:
 - Controlling to <267 Pa requires 88% higher flow than for <400 Pa.
 - Compensating for lower removal efficiency requires an additional 5% flow increase.
 - Higher load requires an additional 17% flow rate margin.
 - Up to 71 m³/h flow may be needed compared to 31 m³/h (129% increase).
 - Power required may increase by 62% over state-of-the-art equipment.
 - Up to 33% loss in working capacity may make oxygen recovery from carbon dioxide more challenging.
- Changes to trace contaminant control standards and loads:
 - Changes to trace contaminant control standards and design-driving load have offsetting impacts.
 - Adding new processes with contaminant loads may require trace contaminant control flow increases up to a factor of 4.
 - Incorporating toxic hazard index can increase the required flow by a factor of 2.4.
- Changes to particle filtration standards and load:
 - Changes to the design standard and loads have offsetting impacts.
 - The bioburden is the primary design driver for particle filtration (with no surface dust intrusion) and provides 22% functional margin for controlling the general particle generation load.
 - Surface dust intrusion is the greatest technical challenge and must employ barriers and operational controls that are >99% effective to minimize impacts to cabin filtration system design.



Acknowledgments

- Greg Cmarik for the analysis and carbon dioxide loop closure illustration.
- Jim Knox for foundational work on carbon dioxide removal power impacts.

