



## Fluid Transient Analysis of Propellant Feedlines during a Priming Event

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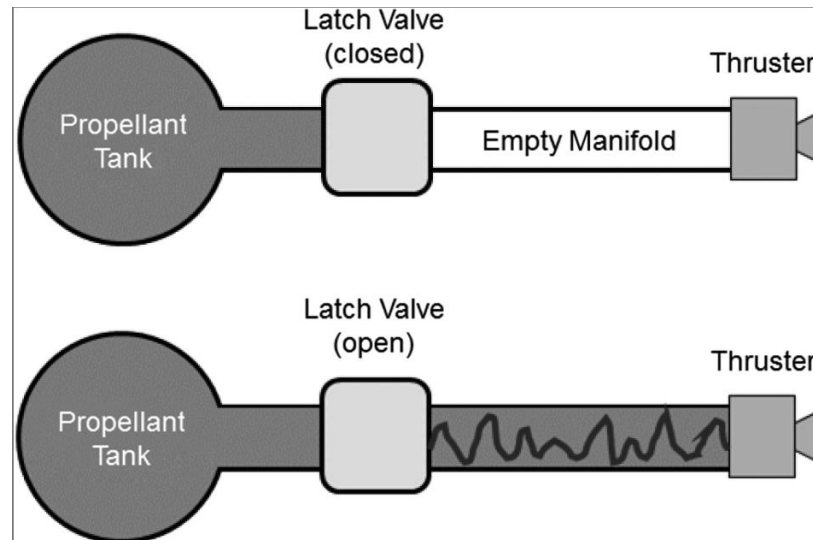


Presented By  
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**TFAWS**  
LaRC 2019

Thermal & Fluids Analysis Workshop  
TFAWS 2019  
August 26-30, 2019  
NASA Langley Research Center  
Hampton, VA

- Priming is the process of filling an evacuated pipe line.
  - For safety reasons, storable propellants such as hydrazine are separated from thrusters by one or more valves.
  - Once in orbit, the valve is opened, and the evacuated line is filled with propellant.



Picture Credit: Moore et al., JSR, 2018.

# Background

- The velocity change when the fluid hits the dead end can cause a brief pressure surge.

- The pressure rise can be as high as:

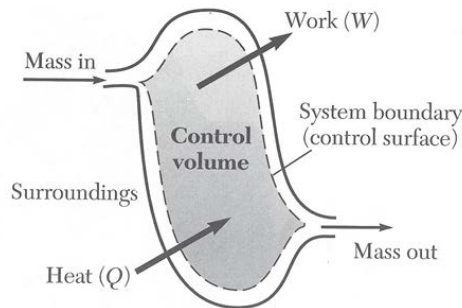
$$\Delta P = \rho c \Delta V$$

- For example, if liquid water is suddenly stopped from 10 m/s, the pressure rise could be:

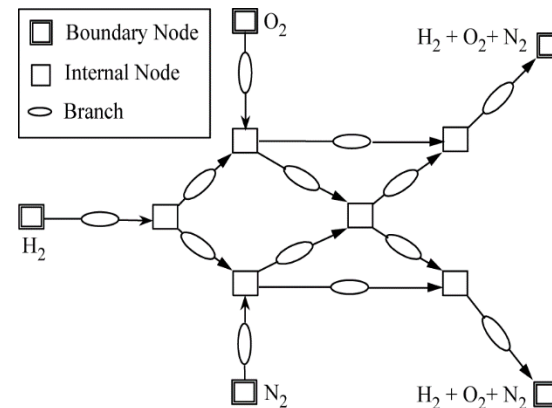
$$\Delta P = \left( 1000 \frac{kg}{m^3} \right) \left( 1500 \frac{m}{s} \right) \left( 10 \frac{m}{s} \right) = 15 MPa$$

- Accurate prediction of maximum pressure aids in the design of a propulsion system that is not too conservatively heavy.

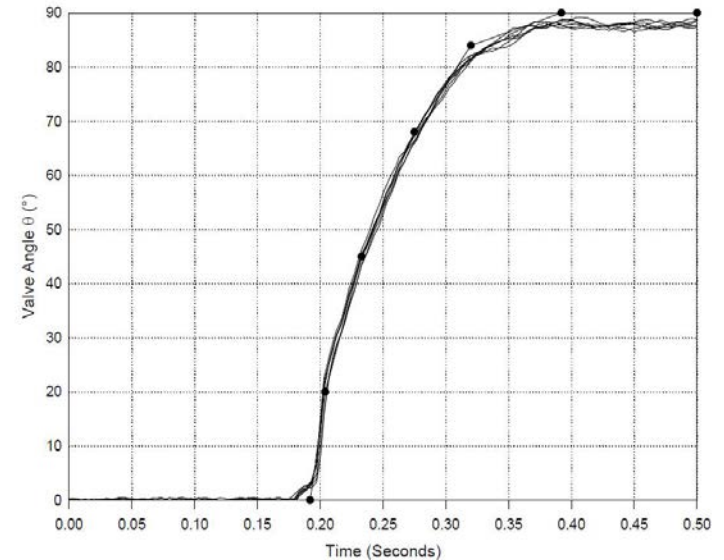
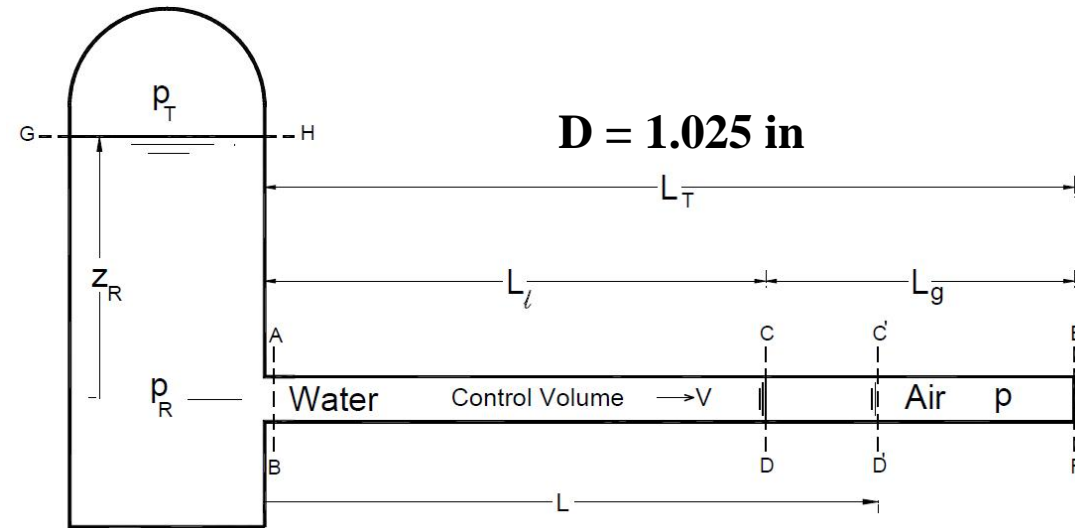
- The Generalized Fluid System Simulation Program (GFSSP) is a general-purpose computer program to calculate pressures, temperatures, and flow rates in a fluid network.
- Fluid networks are discretized into nodes and branches.
  - Mass and energy equations are solved in the nodes.
  - Momentum equation is solved in the branches.



**Control Volume Analysis**



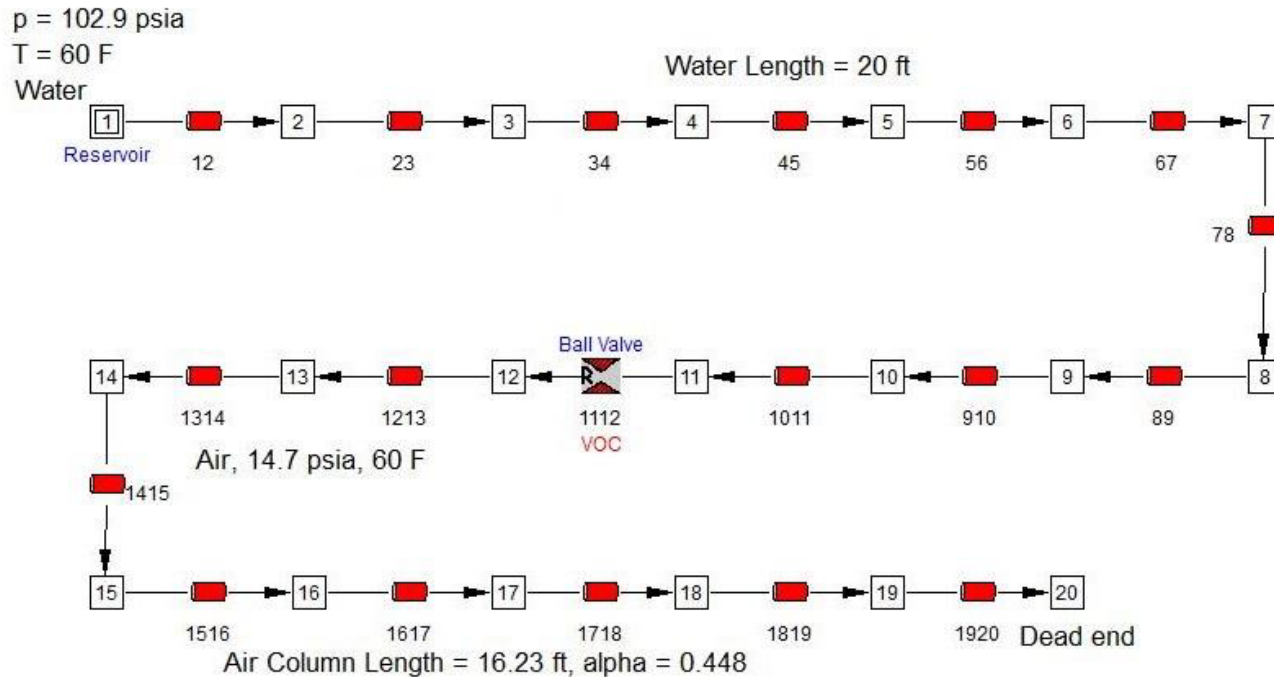
**Finite Volume Analysis**



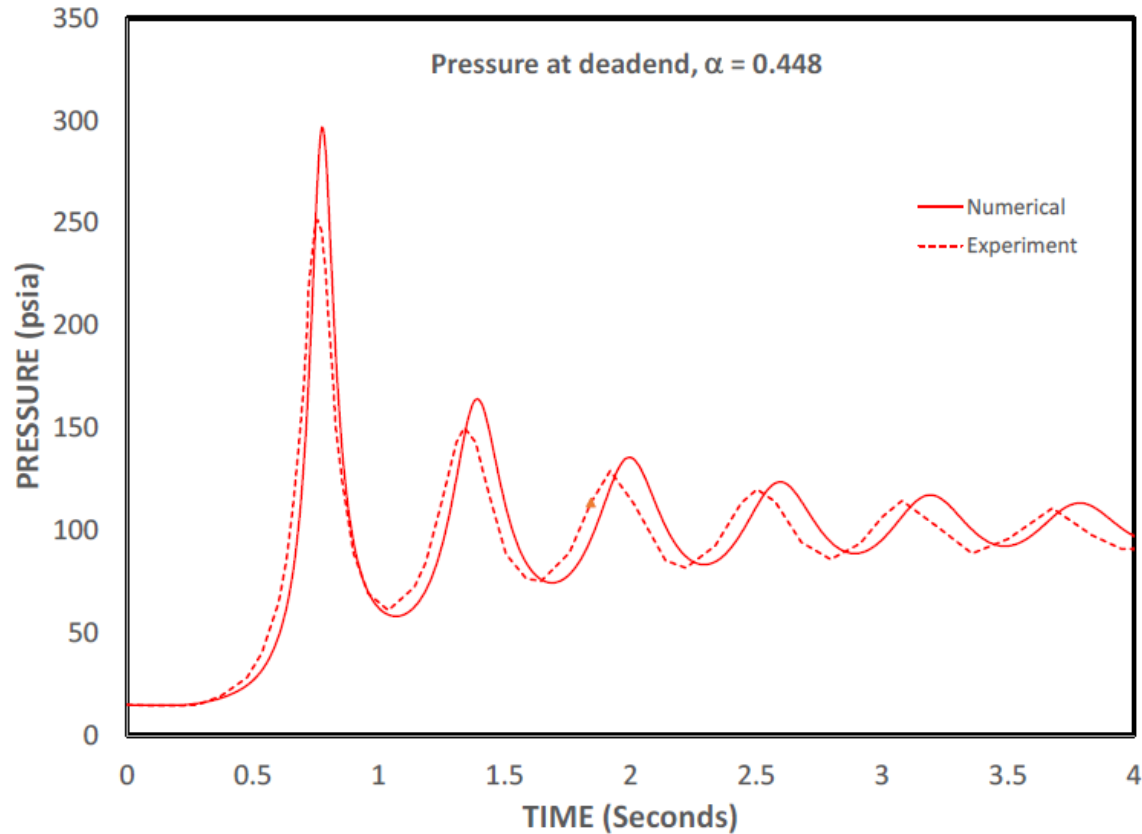
*Ph.D. dissertation by N. H. Lee, 2005*

Test series varied:

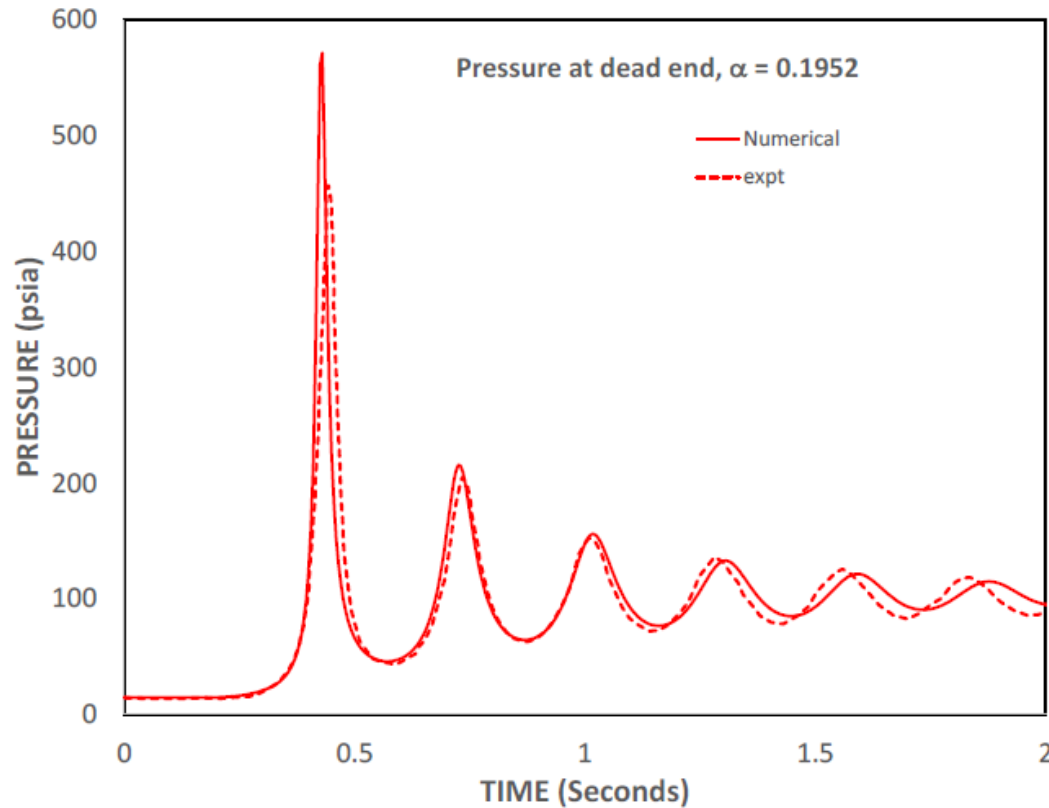
- Reservoir pressure: 2 to 7 atm
- Gas volume proportion:  $\alpha = L_g/L_T$



- Nodes 1-11 initially contain liquid water at 102.9 psia.
- Nodes 12-20 initially contain air (as an ideal gas) at 14.7 psia.
- A Fortran user subroutine fixes all temperatures in model at 60° F. Air temperature increase by compression is neglected.

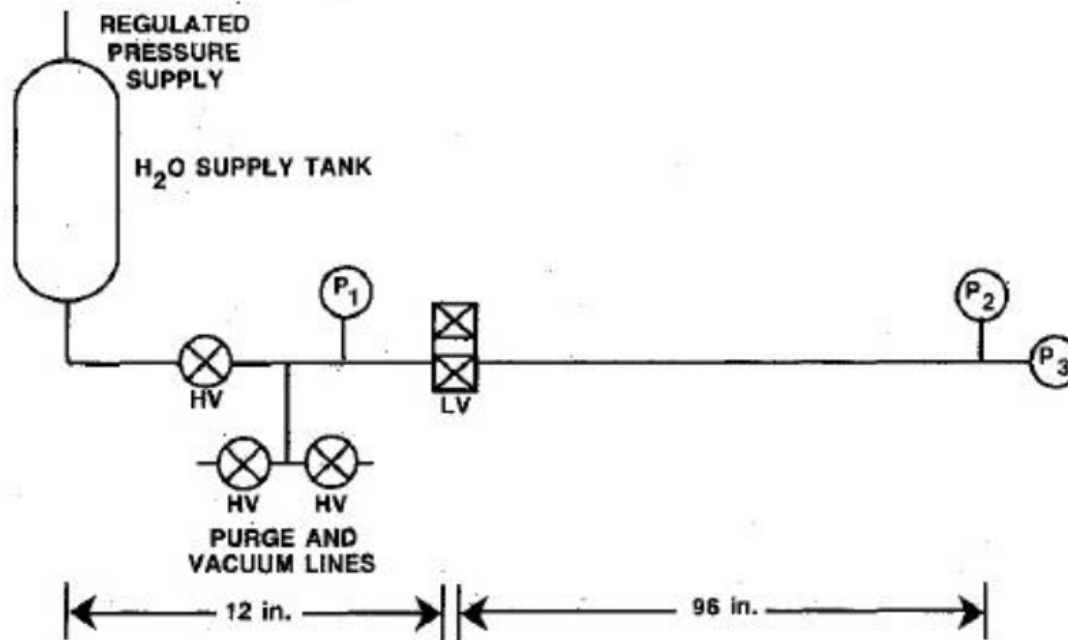


- Predicted peak pressure is 20% higher than experimental.



- Maximum pressure increases when trapped air length is decreased:
  - $\alpha = 0.448$ ,  $P_{\max} = 250$  psia
  - $\alpha = 0.195$ ,  $P_{\max} = 450$  psia

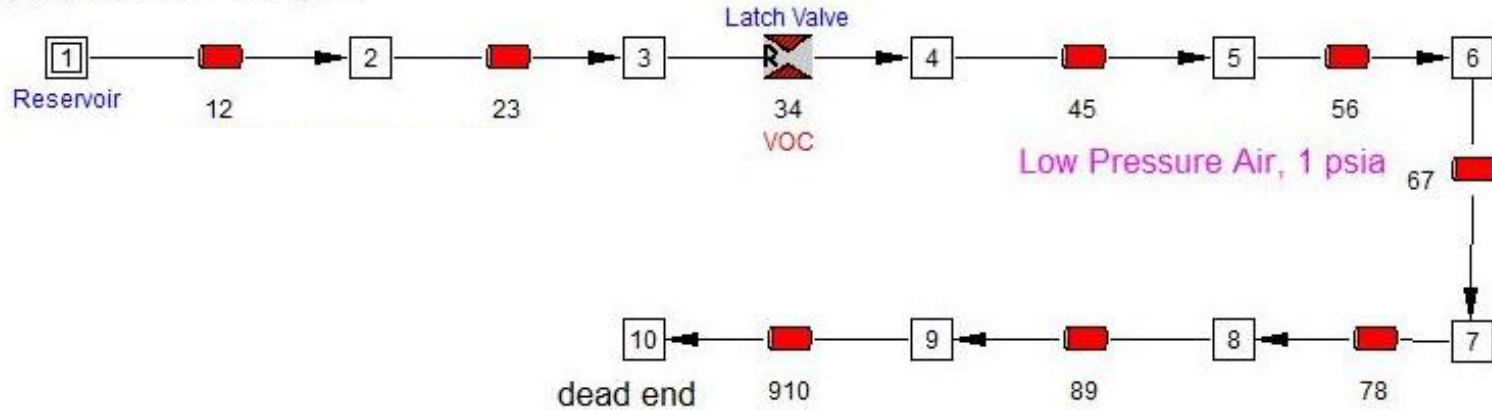




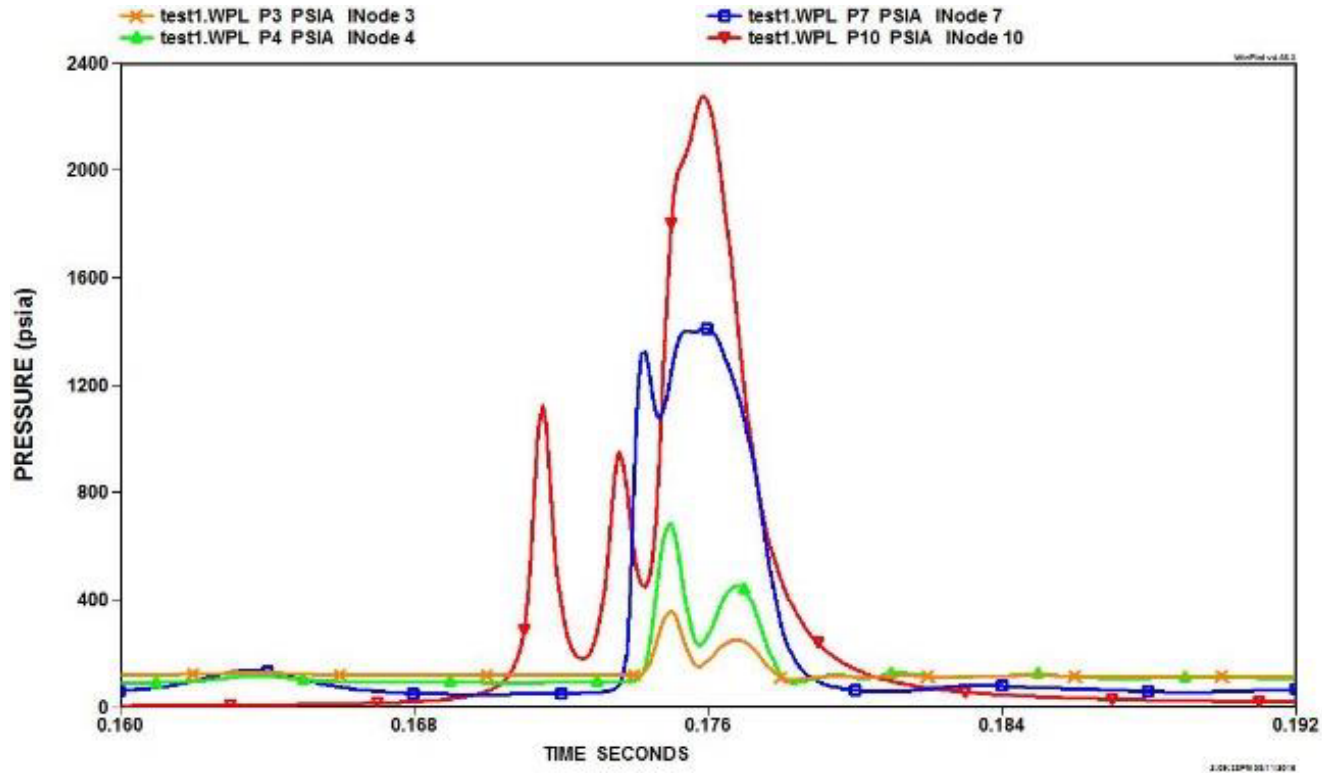
*Prickett et al., 1992*

- Test series varied reservoir pressure: 30 to 120 psia
- Pipe diameter: 0.25 in.
- Pipe downstream of latch valve (LV) is initially evacuated.

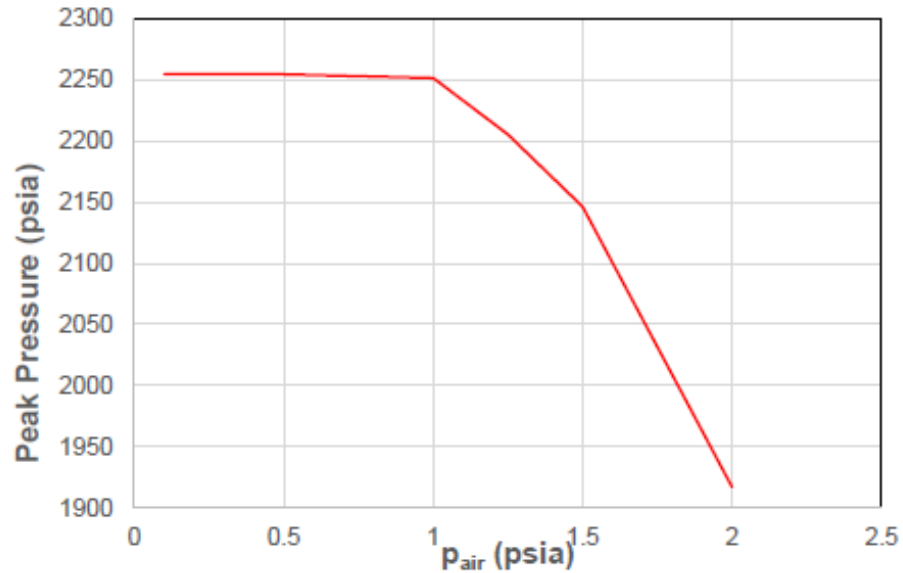
Supply pressure = 120 psia



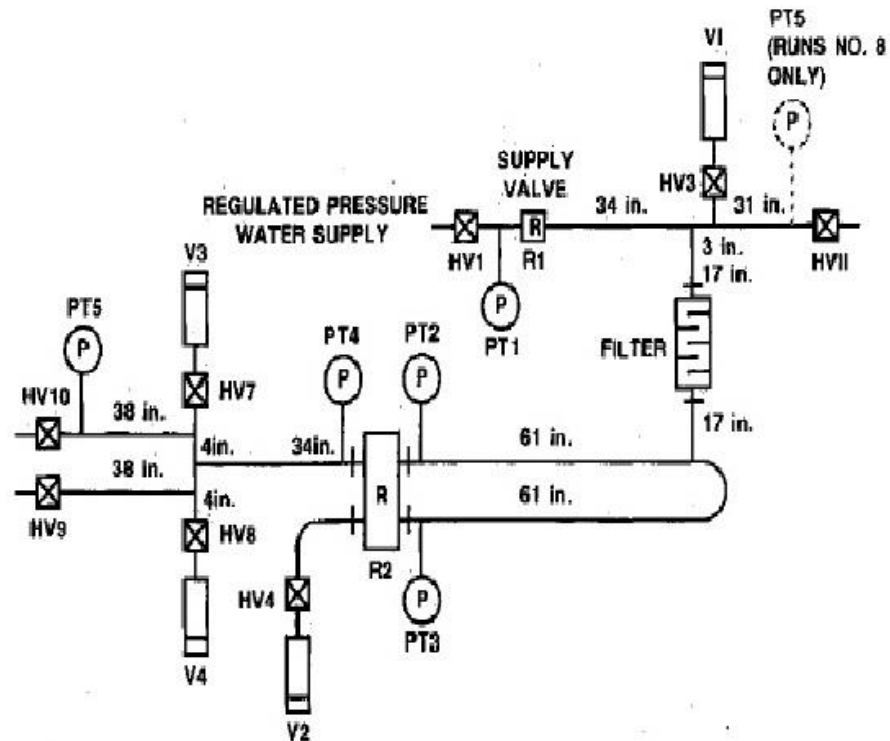
- GFSSP does not understand “empty”, so the evacuated line is initially filled with ideal gas air at low pressure.



- Reported maximum pressure is 2350 psia in the dead end at 0.17 sec.
- GFSSP predicts 2279 psia at 0.176 sec.

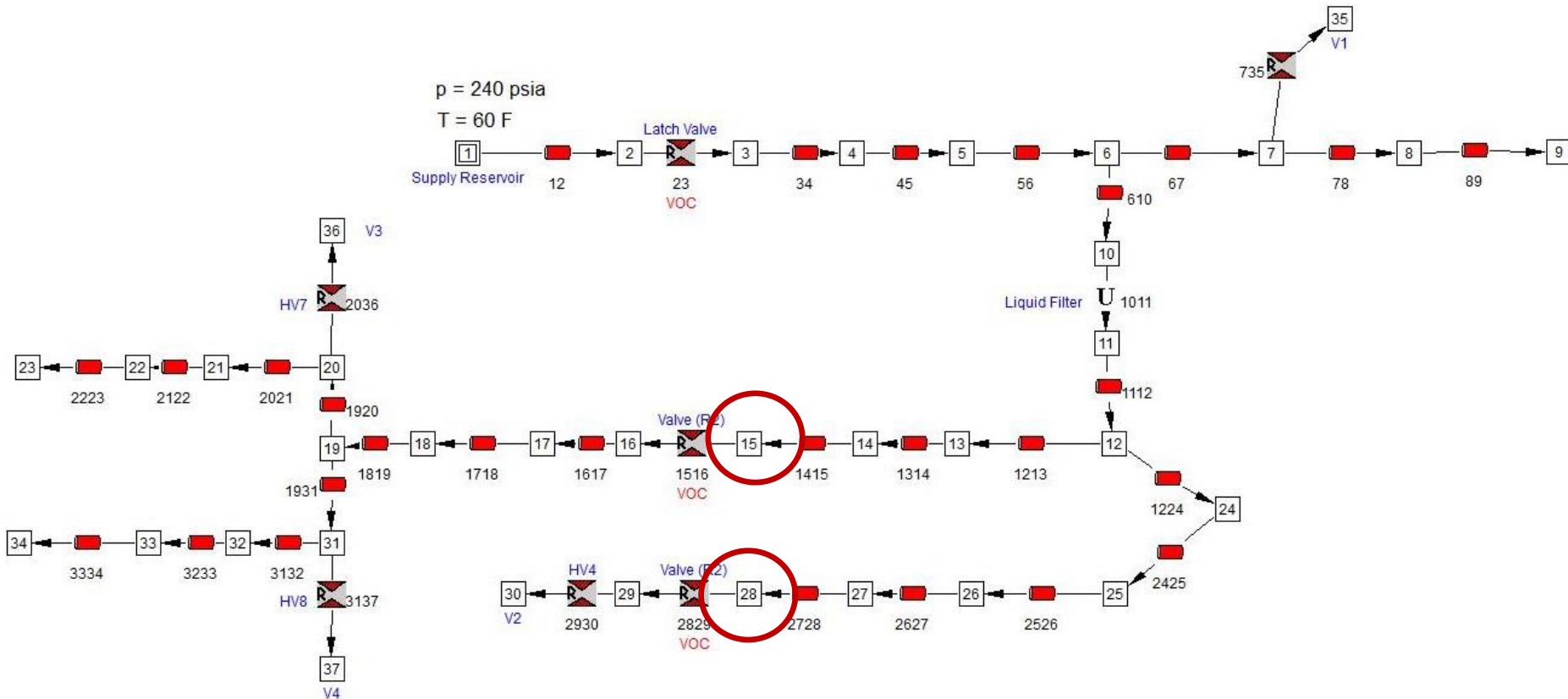


- Decreasing initial air pressure of evacuated lines increased the maximum pressure, although there was little change when  $P_{air} < 1$  psia.

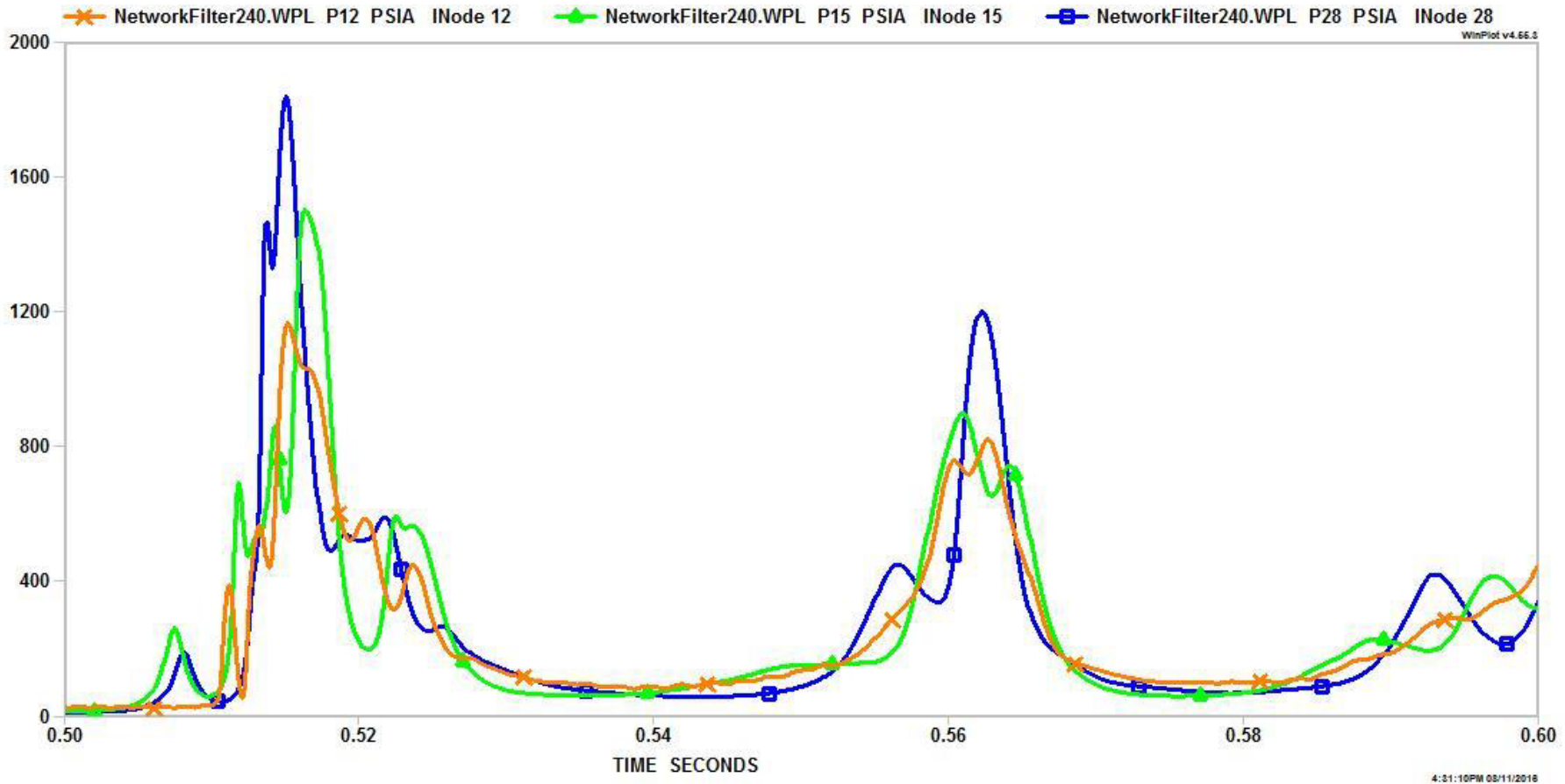


*Prickett et al., 1992*

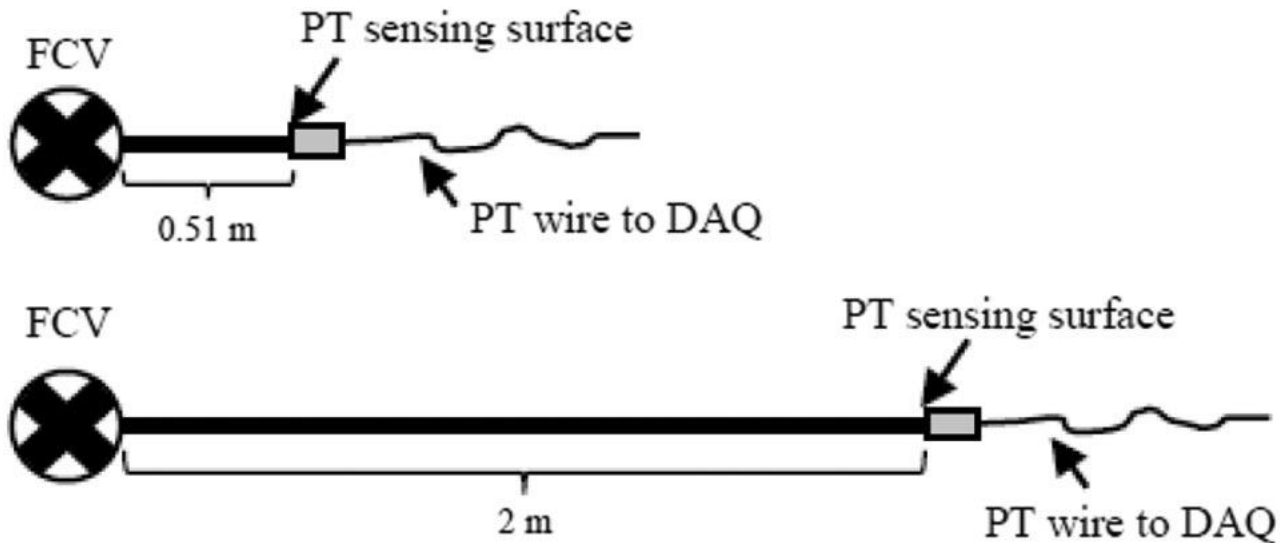
- Reservoir pressure: 240 psia
- Pipe diameter: 0.25 in.
- R1 is the suddenly opening valve.
- R2 is a pair of valves that close quickly during priming event.



- Evacuated nodes are modeled as ideal gas air initially at 1 psia.
- Pressure data available at nodes 15 and 28.



- Maximum pressure in lower branch is 1837 psia at node 28. Measured pressure at this location is 1800 psia.
- Maximum pressure in upper branch is 3500 psia at node 9. No test data were reported for this location.

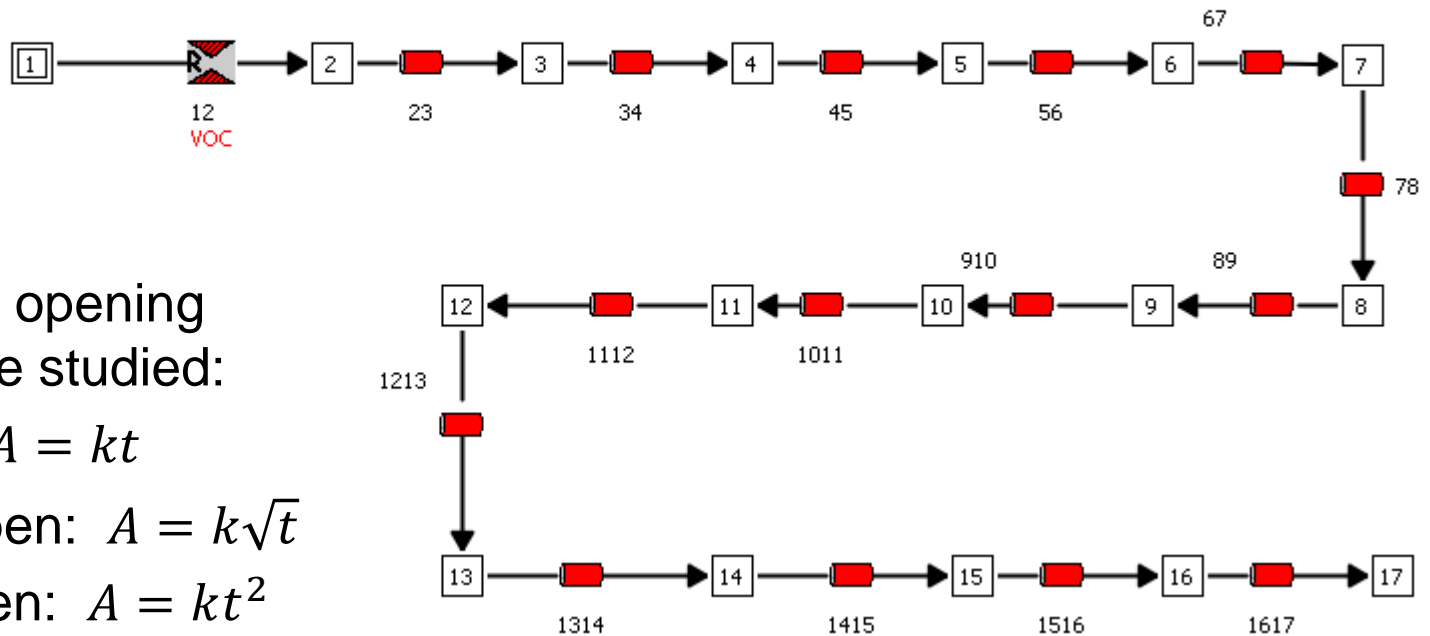


*Moore et al., JSR, 2019*

- Reservoir pressure: 1.5, 2.2, or 2.9 MPa
- Line lengths: 0.51 or 2.0 m
- Line diameters: 6.5, 9.5, or 12.7 mm
- Flow Control Valve  $C_v$ : 0.037, 1.5, or 4.0
- Initial air pressure in line: 4, 15, 101 kPa

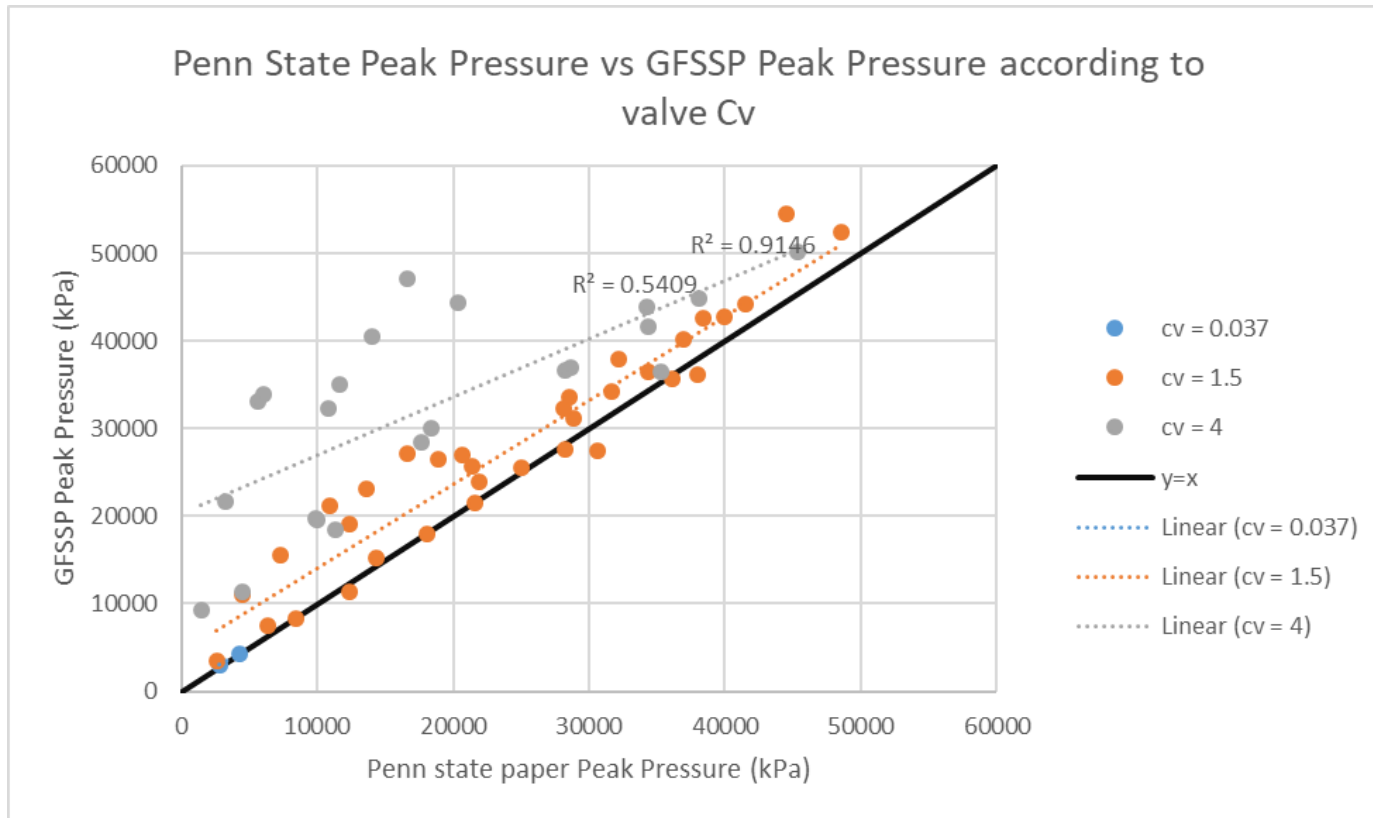


Main Model

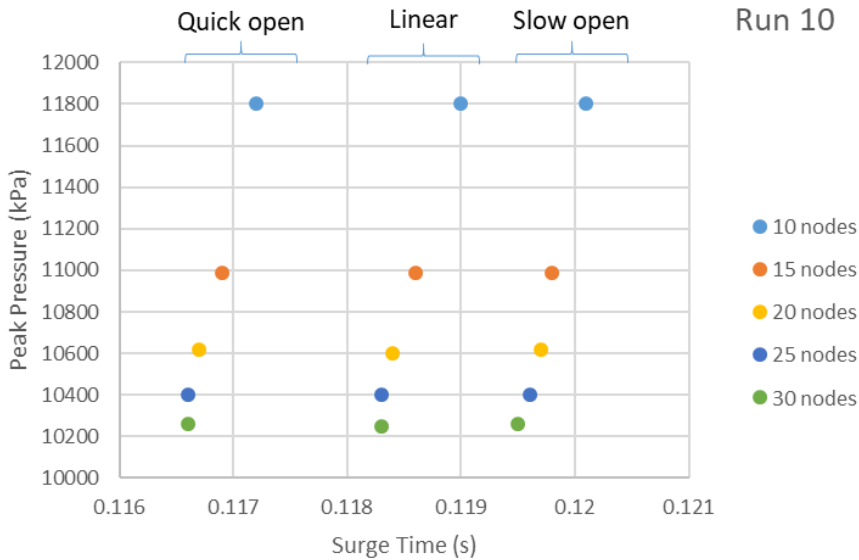


Three valve opening profiles were studied:

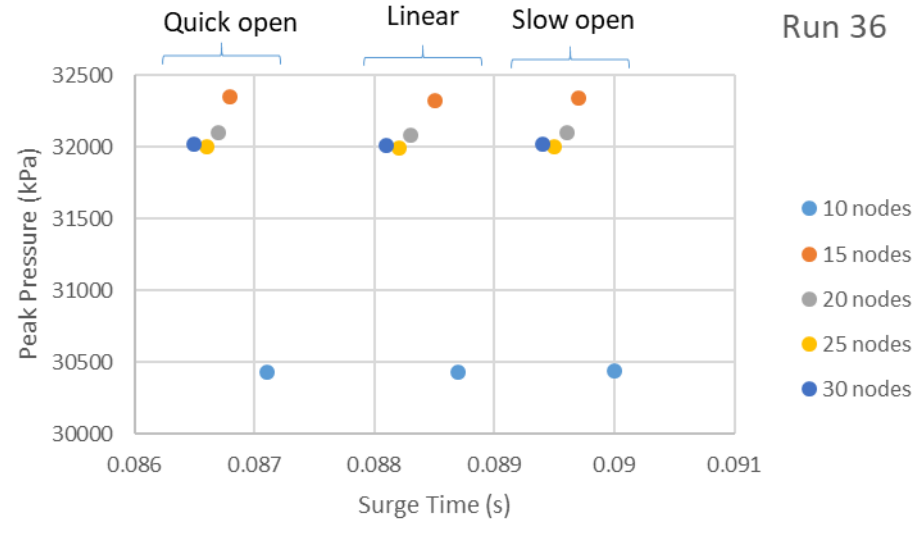
- Linear:  $A = kt$
- Quick open:  $A = k\sqrt{t}$
- Slow open:  $A = kt^2$



- Predictions are reasonable for cases with FCV  $C_v = 0.037$  and 1.5.
- For cases with  $C_v = 4.0$ , GFSSP consistently over-predicts peak pressure.
- No clear relationship seen between GFSSP prediction accuracy and tank pressure or initial line pressure.

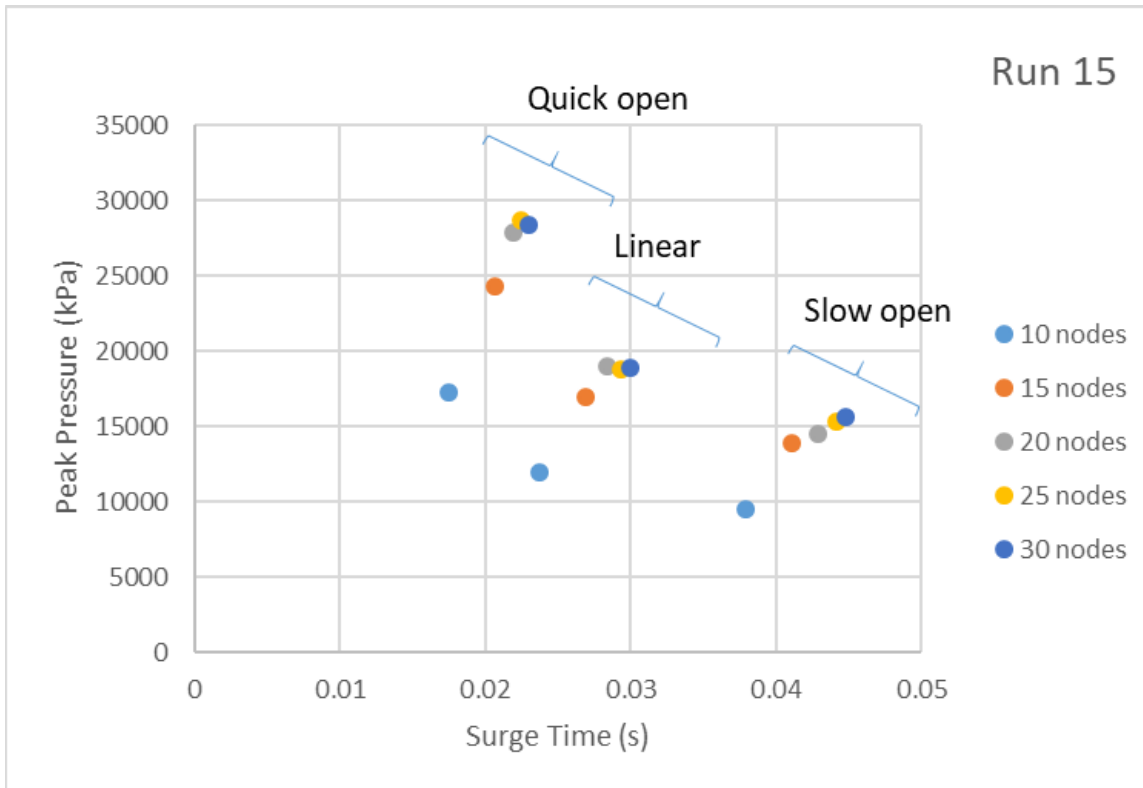


$C_v = 1.5$ ,  $D = 12.7$  mm,  $L = 2$  m  
 $P_{\text{tank}} = 2.9$  MPa,  $P_{\text{init}} = 101$  kPa  
 $P_{\text{meas}} = 4510$  kPa at 0.172 sec



$C_v = 1.5$ ,  $D = 9.53$  mm,  $L = 2$  m  
 $P_{\text{tank}} = 2.2$  MPa,  $P_{\text{init}} = 15$  kPa  
 $P_{\text{meas}} = 28,140$  kPa at 0.106 sec

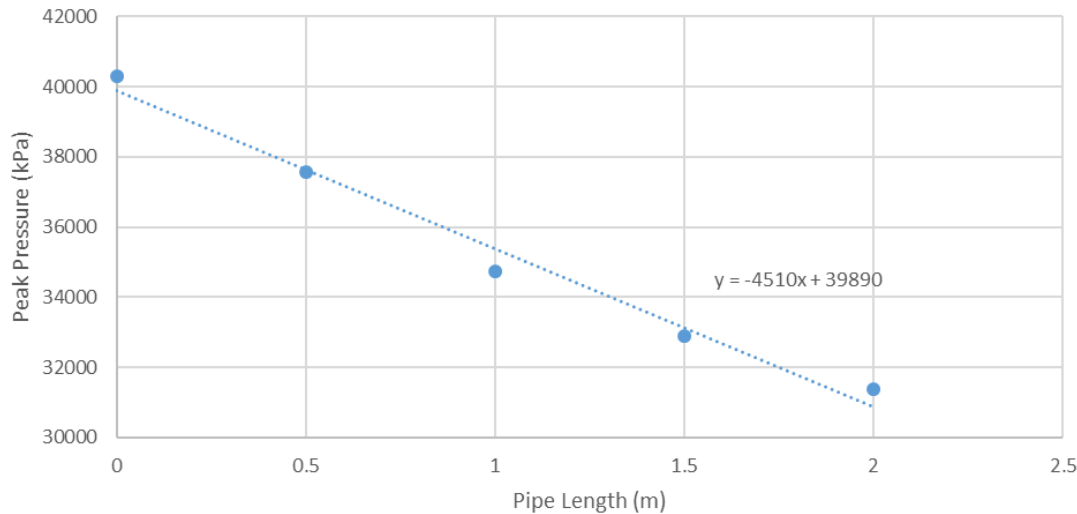
- Discretization study found that predicted peak pressure values slowly converged as more nodes were added to model.
- Valve history profile (linear or parabolic) usually had little effect on the peak pressure, and only a small effect on predicted time of peak pressure.



$C_v = 4$ ,  $D = 9.53$  mm,  $L = 0.51$  m  
 $P_{\text{tank}} = 2.2$  MPa,  $P_{\text{init}} = 101$  kPa  
 $P_{\text{meas}} = 11,290$  kPa at 0.055 sec

- However, choice of valve opening profile did have an effect on those runs where the valve was not completely open before the pressure surge time.
  - Shorter line with narrow-or-medium diameter.
  - Moderate-or-high tank pressure
  - High  $C_v$  valve with slow opening time (0.075 s)

Effect of a Pipe before the Valve (Run 45)

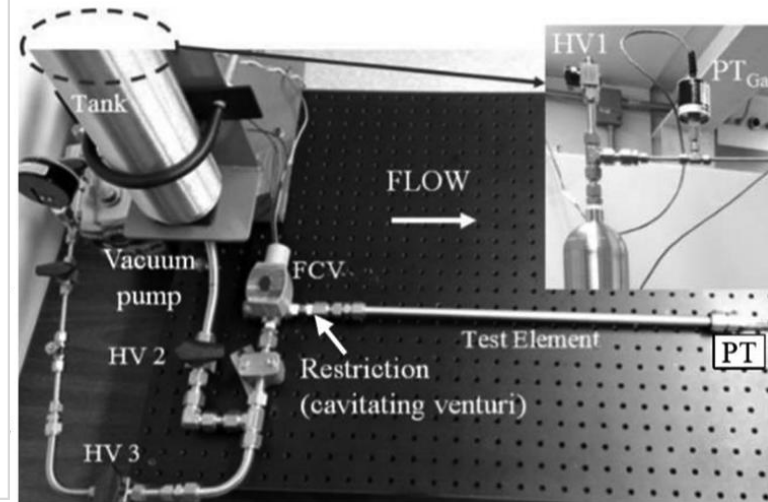


$C_v = 4$ ,  $D = 9.53$  mm,  $L = 2$  m

$P_{\text{tank}} = 2.2$  MPa,  $P_{\text{init}} = 15$  kPa

$P_{\text{meas}} = 14,080$  kPa

- Penn State paper did not provide line length and minor losses between tank and flow control valve.
- Adding an arbitrary line length between the boundary and the valve decreased peak pressure, but not enough to match data.



Moore et al., JSR, 2019



# Discussion



- GFSSP's predictions of peak pressure during a priming event are usually either accurate or too high.
- Models of the Penn State Experiments stress the importance of the valve opening time and profile shape to the peak pressure prediction when a slow-opening valve is matched with a small volume to be filled.
- Future work:
  - More complex fluid networks
  - Effect of a cavitating venturi in the line
  - Implicit vs. explicit solution of the conservations equations



# References



- Lee, N.H. “Effect of Pressurization and Expulsion of Entrapped Air in Pipelines.” Ph.D. Thesis. Georgia Institute of Technology. August 2005.
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- Prickett, R.P. et al. “Water Hammer in a Spacecraft Propellant Feed System.” Journal of Propulsion and Power. Volume 8, Number 3. May-June 1992.
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