

# COMPLETION OF THE LONG DURATION WEAR TEST OF THE NASA HERMES HALL THRUSTER

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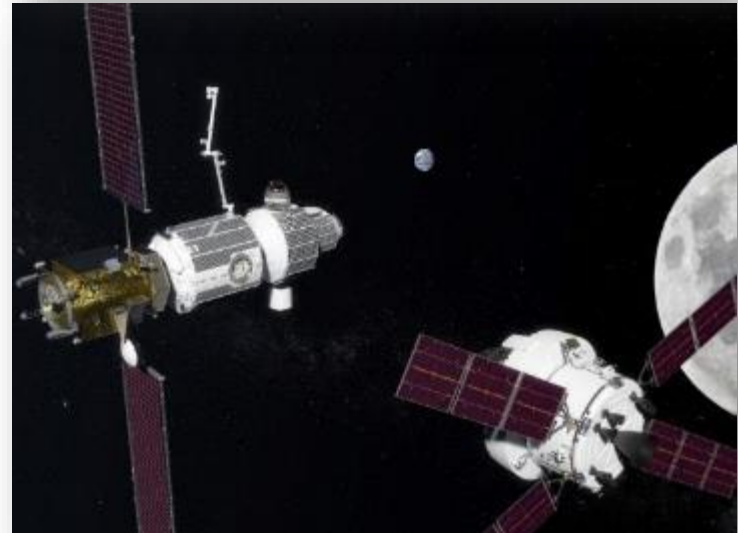
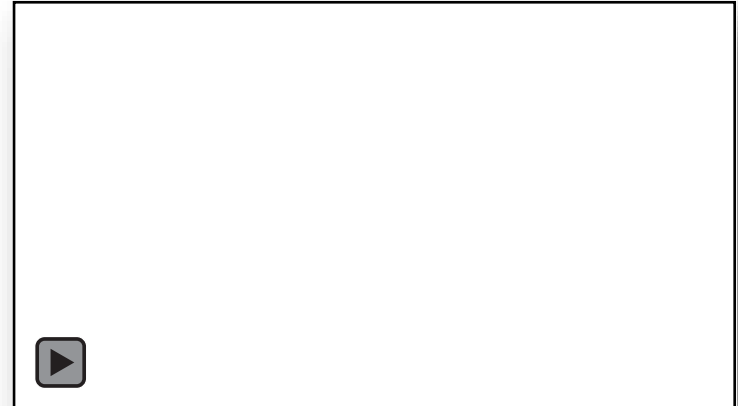
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# Introduction: HERMeS Development

- High-power (40-kW) SEP capability has been identified as enabling for near term and future NASA exploration architectures
  - Example: Power and Propulsion Element of NASA's Gateway
- Since 2012, NASA has been developing the Hall Effect Rocket with Magnetic Shielding (HERMeS) to serve as a SEP capability building block
- Technology development transitioned to Aerojet Rocketdyne via Advanced Electric Propulsion System (AEPS) contract
  - NASA continues to support AEPS development via mission risk reduction activities including wear testing of technology demonstration unit (TDU) thrusters





# Introduction: HERMeS Wear Tests

- 2016 TDU-1 Wear Test: AIAA Paper 2016-5025
  - Goal: provide first quantitative insight into wear and performance trends over an extended period of thruster operation
  - 1700 h of operation at 600 V/12.5 kW
- 2017 TDU-3 Short Duration Wear Test (SDWT): IEPC Paper 2017-207
  - Goal: quantify the impact of operating condition on thruster life
  - 200 h segments (7x) each performed at a different operating condition
- 2017-2018 TDU-3 Long-Duration Wear Test (LDWT)
  - Pathfinder test for the planned 23 kh AEPS life and qualification campaign intended to:
    1. Quantify the performance, stability, plume, and wear trends of TDU-3 over at least 3,000 hours of operation using methods planned for AEPS testing.
    2. Quantify the effect of back-sputtered facility material on TDU-3 over at least 3,000 hours of operation.
    3. Develop institutional guidelines and procedures for operation of long-duration tests in Vacuum Facility 5 (VF-5) at NASA GRC.



# Test Summary

- The TDU-3 LDWT was conducted between 10/23/2017 and 10/4/2018 and accumulated approximately 3,570 h of total operating time in six segments:
  - I: Repeat of the TDU-1 wear test
  - II-IV: Assess impact of discharge voltage and magnetic field strength on component wear
  - V: Assess performance and wear using an alternate pole cover material (carbon-carbon composite) with increased strength and crack resistance
  - VI: Assess the impact of facility pressure on performance and wear

\*All segments completed at a discharge current of approximately 20.8 A

Segment	I	II	III	IV	V	VI
Operating Condition	600 V/ 1 B	300 V/ 1 B	300 V/ 0.75 B	300 V /1.5 B	600 V/ 1 B	600 V/ 1 B
Facility Pressure ( $\mu$ Torr)	5.7	4.2	4.1	4.2	4.3	11.7
Duration (h)	1015	252	214	240	1579	270

AIAA Paper 2018-4645

This Work





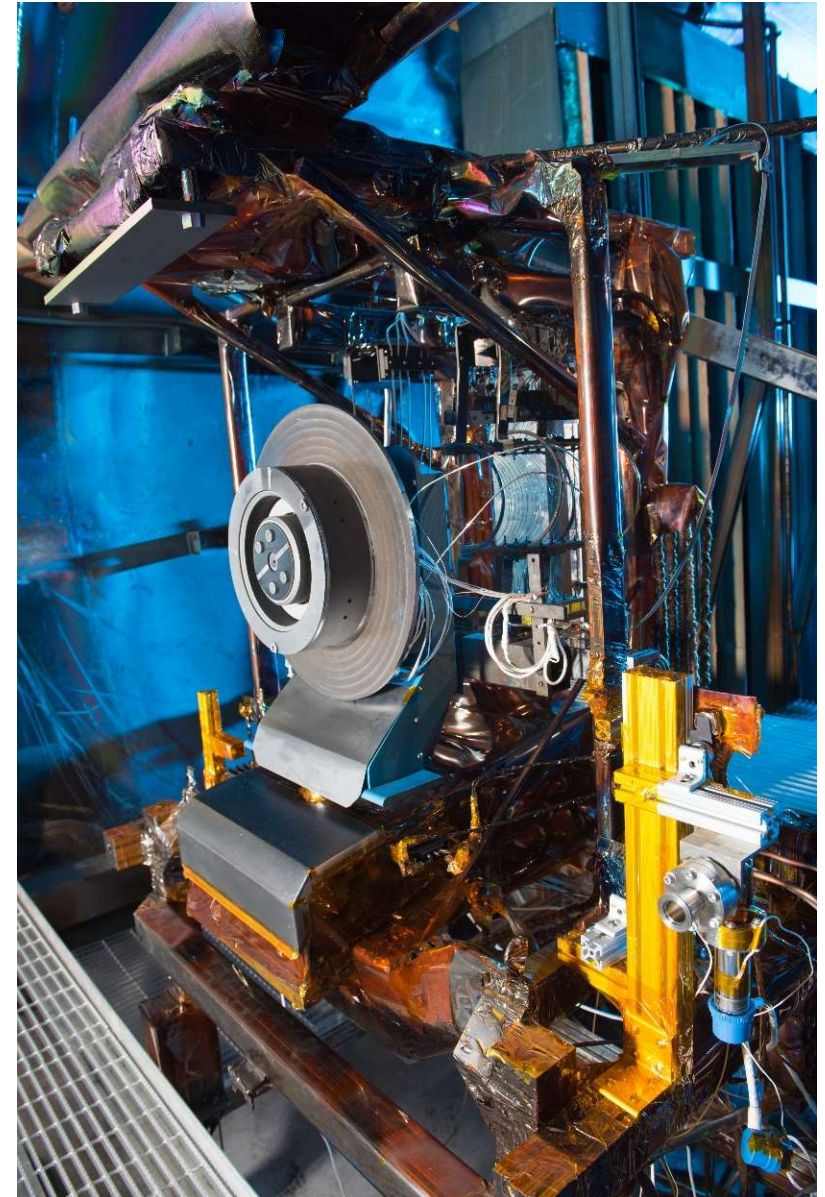
# Experimental Apparatus: Thruster and Facility

## HERMeS TDU-3

- Same thruster used for SDWT with minor modifications:
  - Thickness and position of cathode keeper
  - New magnet coils (field shape unaltered)
- Changes relative to TDU-1 detailed by Kamhawi et al. (IEPC Paper 2017-392)
  - Resulted in minimal variation in operating characteristics
- Thruster electrically configured per recommendations from Peterson et al. (AIAA Paper 2016-5027)
  - Thruster body electrically tied to cathode
  - Dielectric coating on all surfaces within 1 m of exit plane
- Power and propellant supplied using calibrated commercial laboratory systems
  - Flow rate uncertainty: 1%
  - Voltage uncertainty:  $\pm 0.06$  V
  - Current uncertainty:  $\pm 0.03$  A

## GRC VF-5

- Nominal pumping speed:  $\sim 700$  kl/s on xenon
- Nominal operating pressure:  $\sim 4.5$   $\mu$ Torr at 12.5 kW throttle point

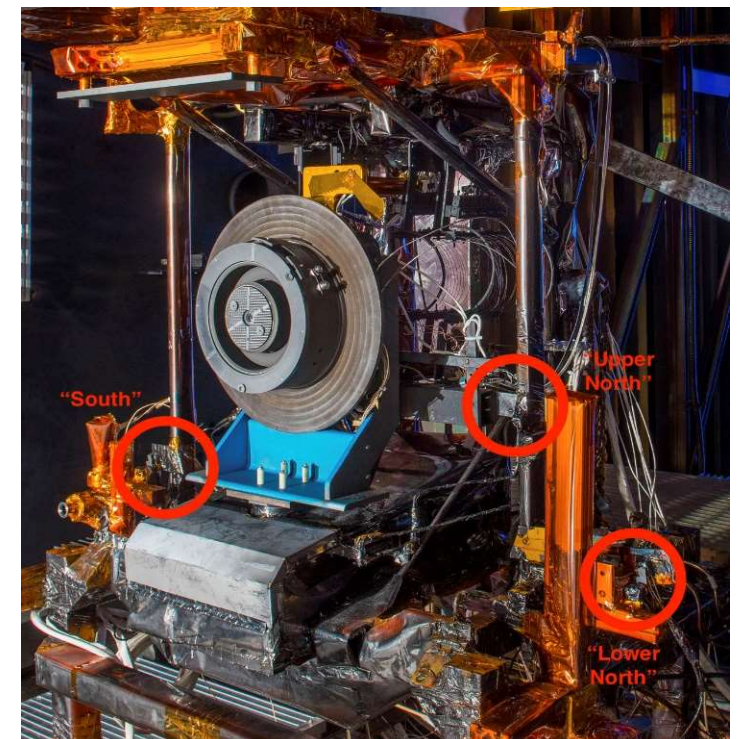
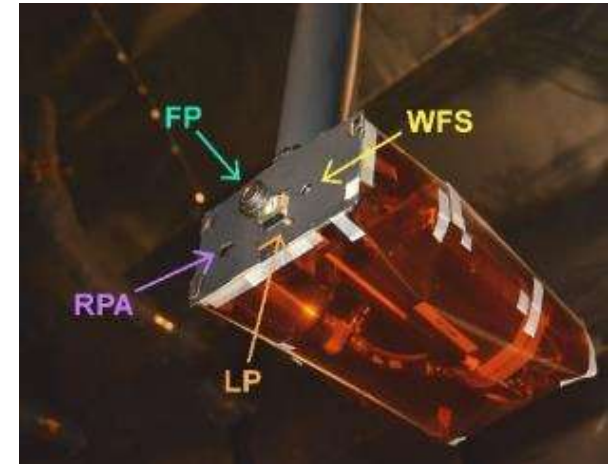




# Experimental Apparatus: Diagnostics

## Diagnostics

- Thrust measured with an inverted pendulum thrust stand ( $\pm 0.8\%$  uncertainty) (AIAA Paper 2018-4516)
- Plasma probe package mounted to a two-axis positioning system containing (AIAA Paper 2016-4828):
  - Faraday probe (FP) swept continuously over  $\pm 110^\circ$  at five distances from exit plane
  - Retarding potential analyzer (RPA) and Langmuir probe (LP) sampled at several polar angles at one distance
  - ExB (Wien filter spectrometer) sampled on thruster centerline at one distance
- Quartz Crystal Microbalances (QCMs) (AIAA Paper 2016-4941)
  - 3 mounted at a distance of 1 m radially outward from centerline in the thruster exit plane
- Pressure measured with a hot-cathode ionization gauge
  - EP configured: Xe-calibrated, elbow with additional plasma screen, and housing grounded to facility
  - Located 0.7 m radially outward, 0.08 m upstream, and 0.6 m below the thruster centerline
  - Two auxiliary gauges present

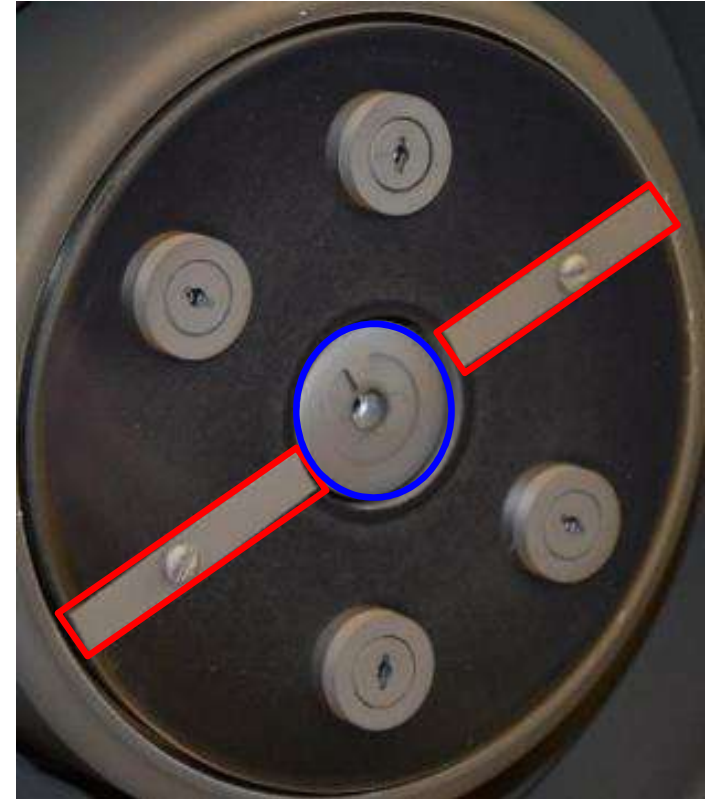






# Experimental Apparatus: Wear Measurements

- Inner front pole cover (IFPC), keeper, and outer front pole cover (OFPC) modified to enable wear measurements
  - Graphite components polished pre-test to maximize surface uniformity
    - Composite materials were not polished
  - Graphite masks installed to provide unexposed reference surfaces:
    - IFPC: two graphite strips covering approximately 95% of radius
    - Keeper: graphite ring with a tab protruding radially inward
    - OFPC: series of graphite strips covering approximately 95% of radius
- Erosion measurements made with a chromatic, white-light, non-contact profilometer
  - Data analyzed per ISO 5436-1 guidance for a type A1 step
  - Typical uncertainties  $\pm 2 \mu\text{m}$  accounting for:
    - Instrument error
    - Surface roughness
    - Non-flat surface geometry

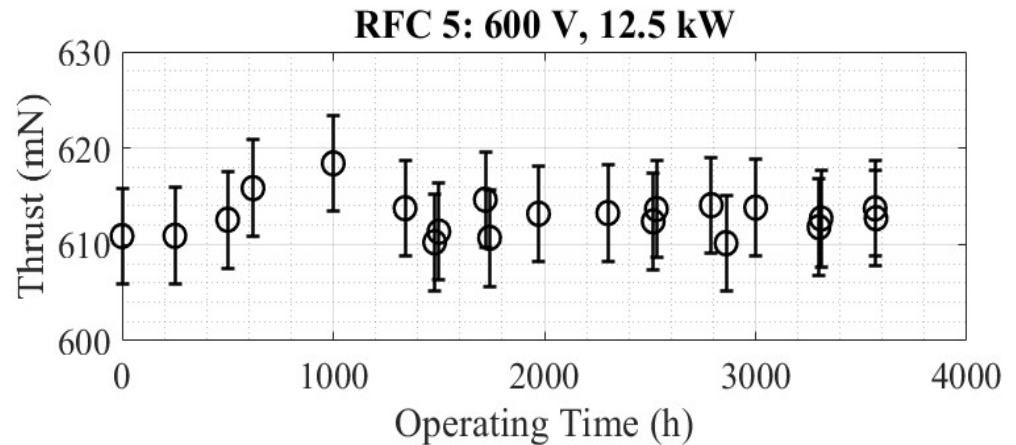




# Results: Performance

## Performance Results

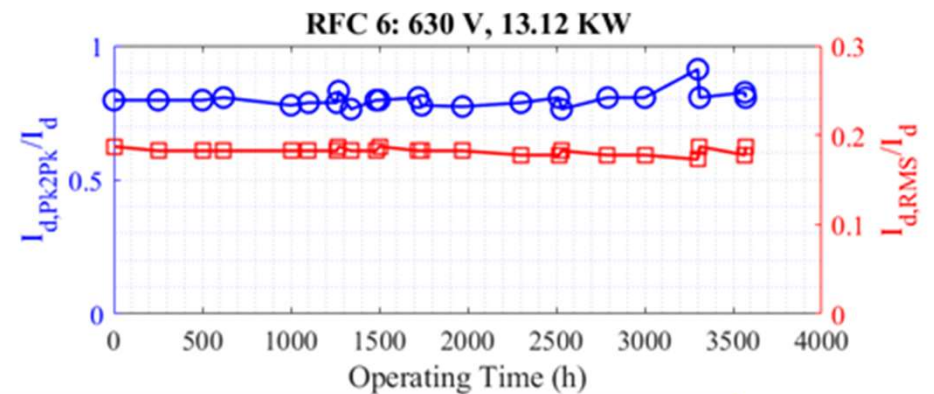
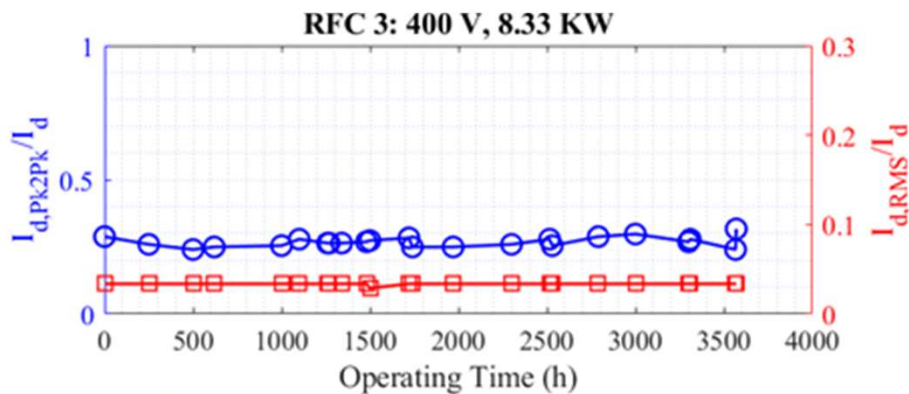
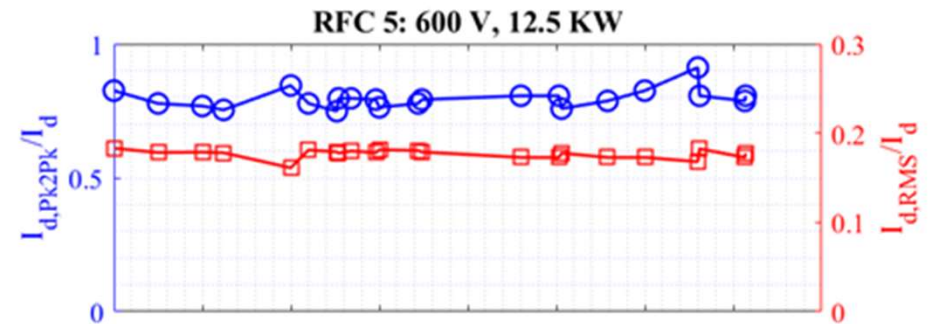
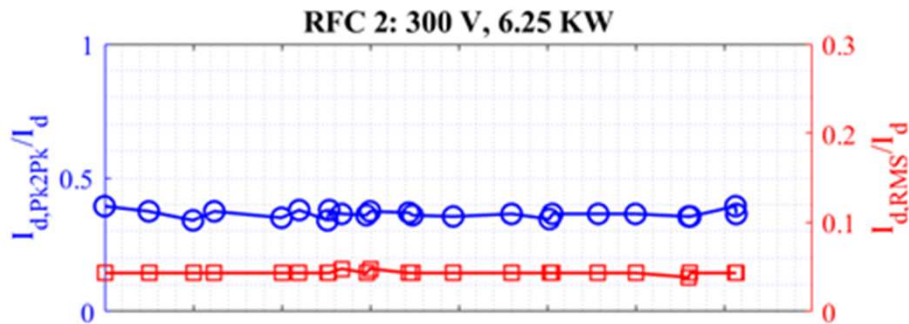
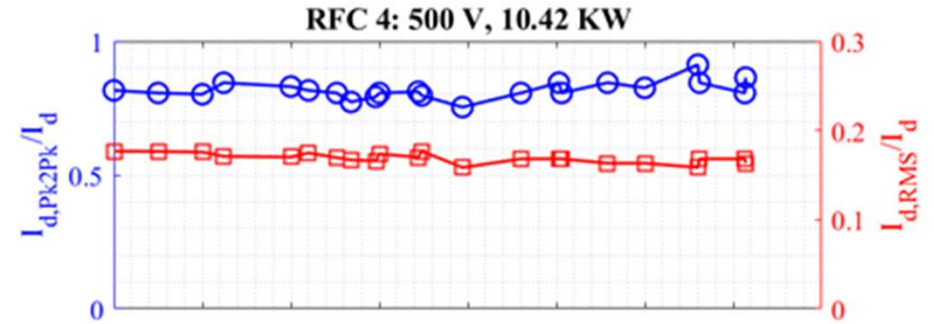
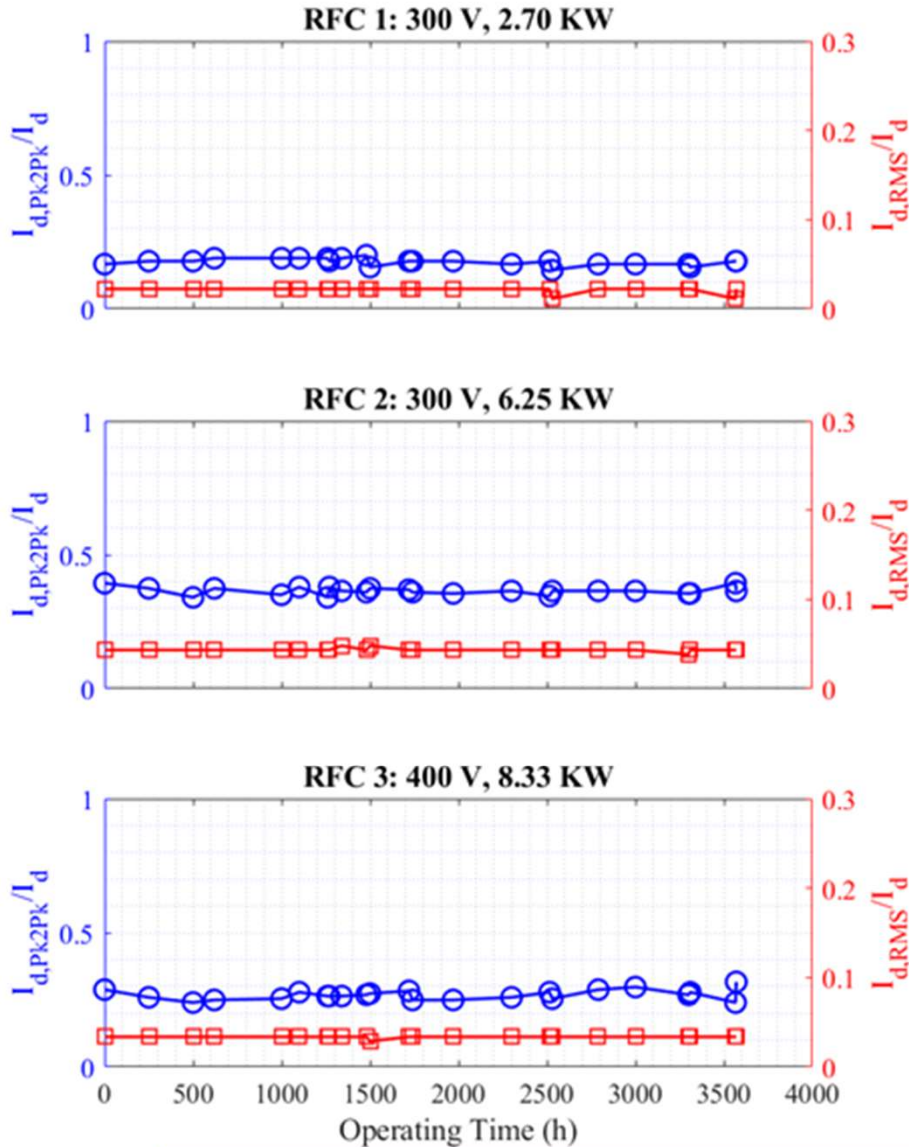
- Thruster performance and stability characterized periodically at 6 RFCs
  - Accounted for ~5% of total operating time
- Performance varied by less than the measurement uncertainty over the course of the LDWT
- TDU-3 performance matched results from previous wear tests to within the thrust measurement uncertainty ( $\pm 5$  mN)



RFC	TDU-1 Wear Test		TDU-3 LDWT	
	Thrust (mN)	Standard Deviation (mN)	Thrust (mN)	Standard Deviation (mN)
1 300 V, 2.7 kW	-	-	167.5	2.4
2 300 V, 6.3 kW	393.1	2.8	395.5	2.2
3 400 V, 8.3 kW	477.5	1.9	479.1	2.1
4 500 V, 10.4 kW	544.8	6.7	545.7	2.4
5 600 V, 12.5 kW	610.1	2.4	612.9	2.0
6 630 V, 13.1 kW	-	-	630.3	2.2



# Results: Discharge Current Oscillations



**Discharge current oscillations varied by less than the uncertainty during LDWT and when compared against previous TDU wear tests**

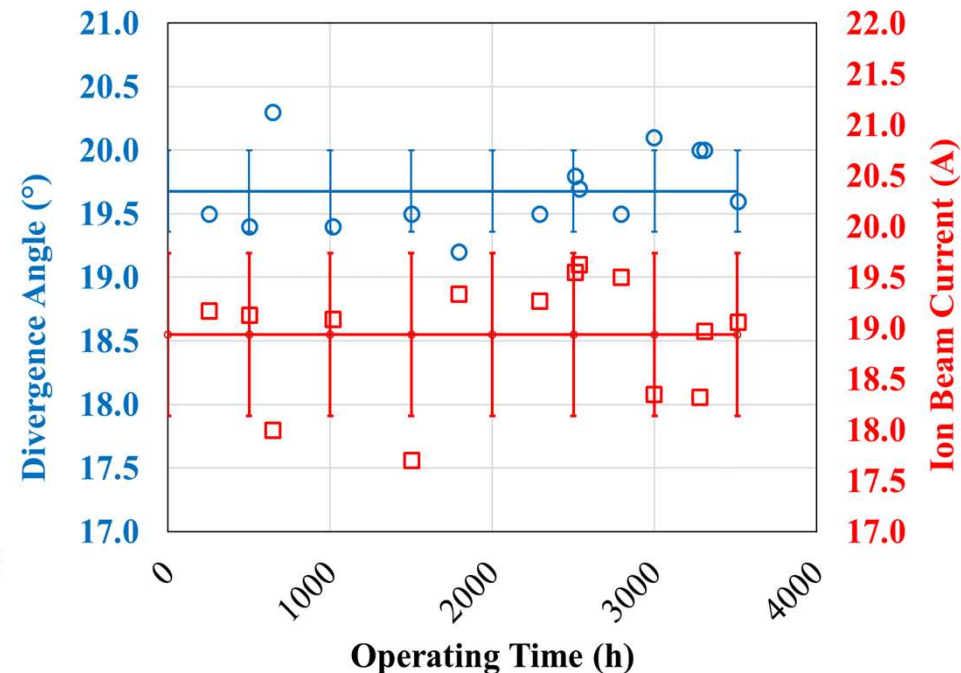




# Results: Plume and Backsputter

## Plume Properties

- The standard deviation of all measured plume properties was less than 5% over the course of the LDWT:
  - Charge-weighted Divergence Angle:  $19.7 \pm 0.3^\circ$  (1.6%)
  - Ion Beam Current:  $18.9 \pm 0.6$  A (3.2%)
  - High-energy Polar Angle:  $71.9 \pm 2.9^\circ$  (4%)
  - Most-probable Voltage:  $578 \pm 18$  V (3.2%)
- All plume measurements consistent with values obtained during previous TDU tests

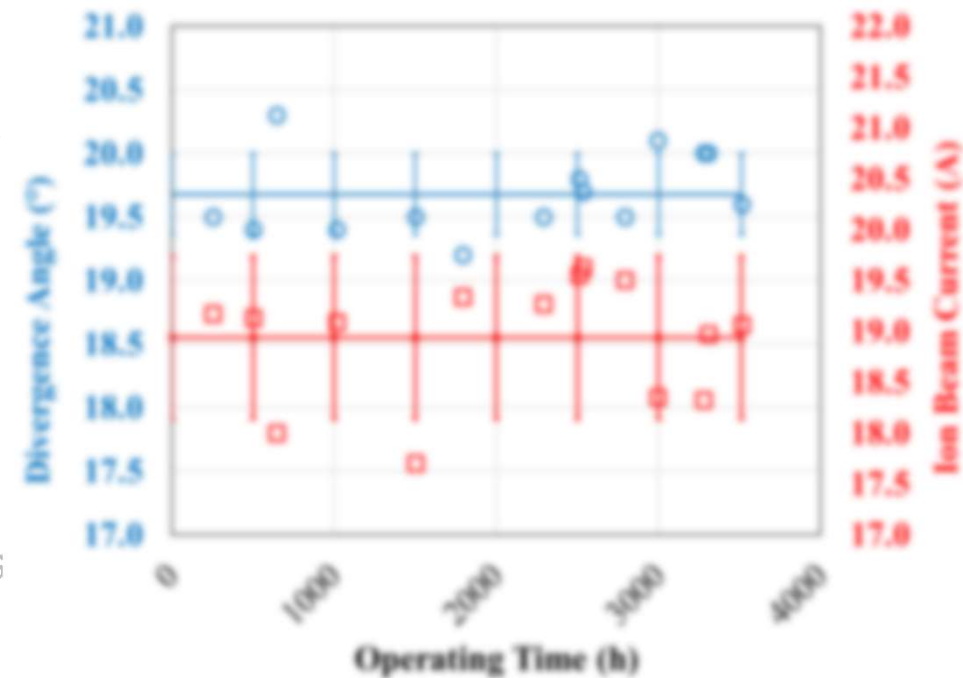




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## Facility Backsputter

- Consistent with previous tests, facility backsputter rates were at all times less than  $2 \mu\text{m/kh}$
- Operation at 300 V reduced backsputter rates by 10-15% relative to 600 V

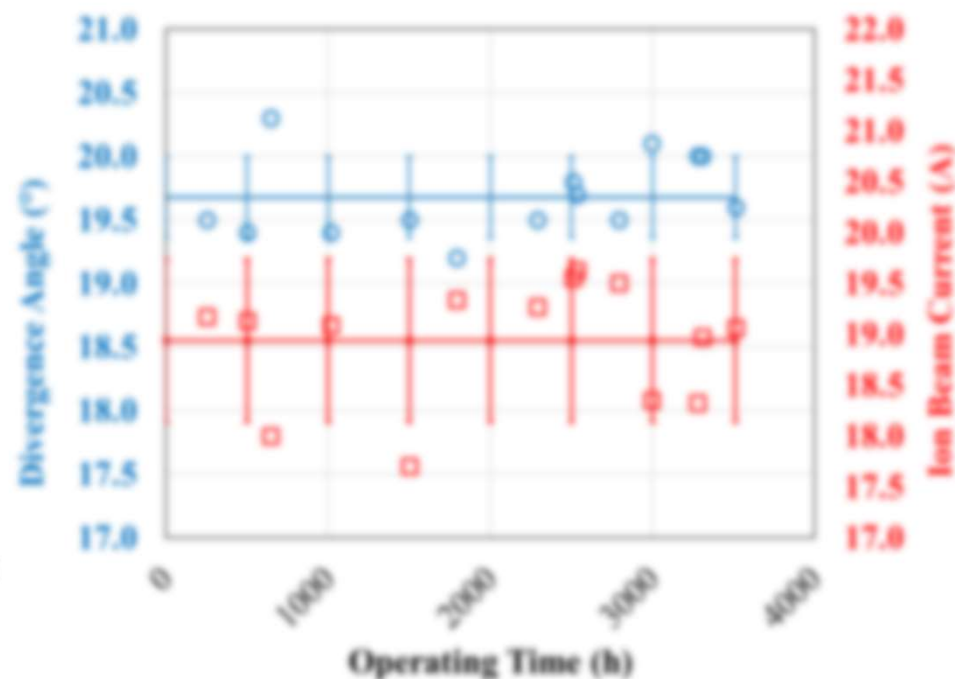
Location	300 V/6.25 kW		600 V/12.5 kW	
	Average ( $\mu\text{m/kh}$ )	$\sigma$ ( $\mu\text{m/kh}$ )	Average ( $\mu\text{m/kh}$ )	$\sigma$ ( $\mu\text{m/kh}$ )
Outer N	-	-	1.56	0.22
Inner N	1.14	0.13	1.24	0.28
S	1.40	0.17	1.67	0.12



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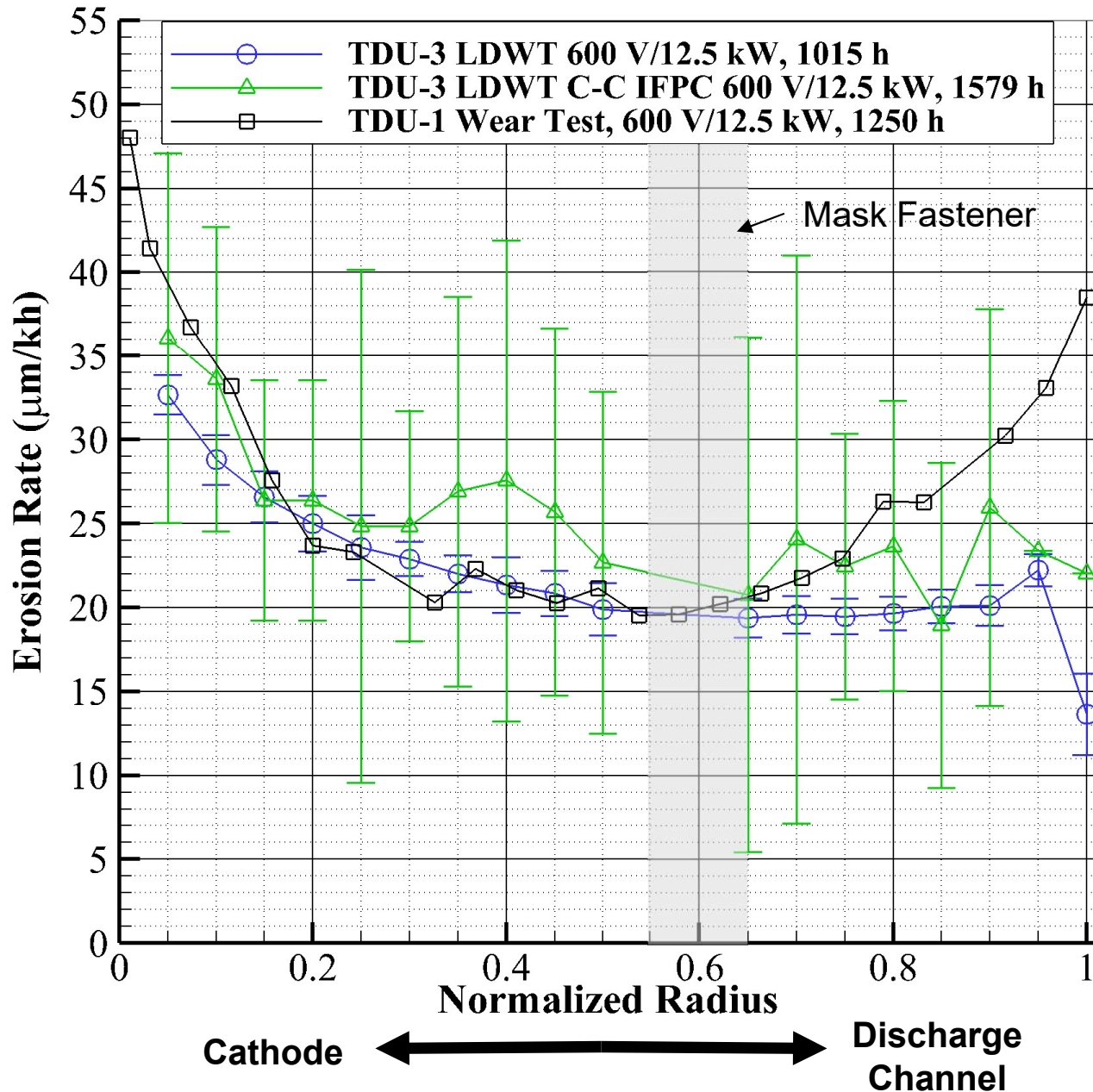
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**Performance, stability, and plume properties varied by less than the uncertainty during LDWT and when compared against previous TDU wear tests**



# Results: Carbon Composite IFPC Wear

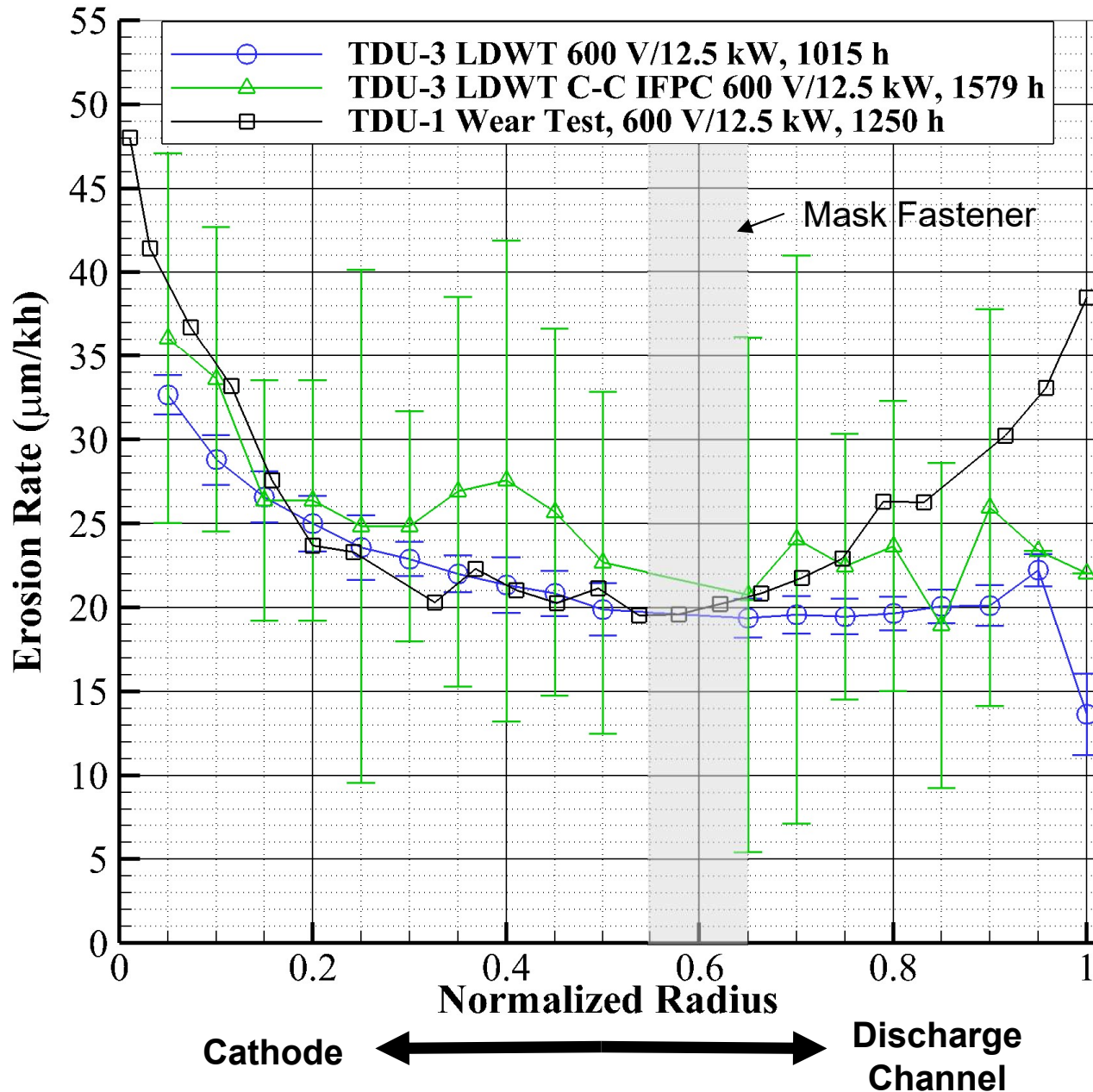


## Key Observations:

- 1) The erosion rates of the composite IFPC matched those obtained with graphite pole covers to within the uncertainty
- 2) Woven structure of the composite IFPC yielded increased surface roughness and the presence of surface features equal in dimension to eroded steps  $\rightarrow$  increased measurement uncertainty
- 3) Wear of composite IFPC maintains azimuthal symmetry



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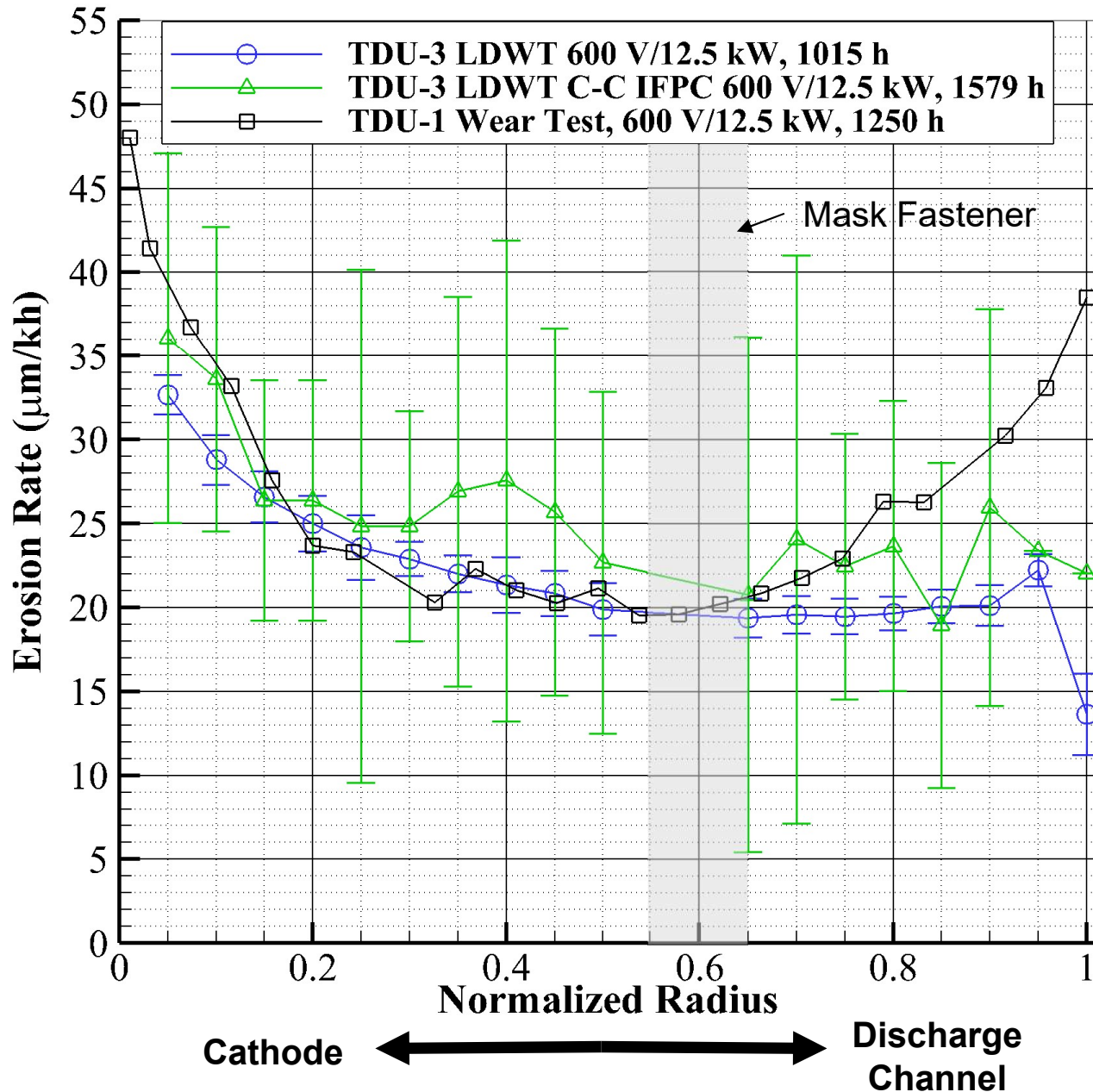
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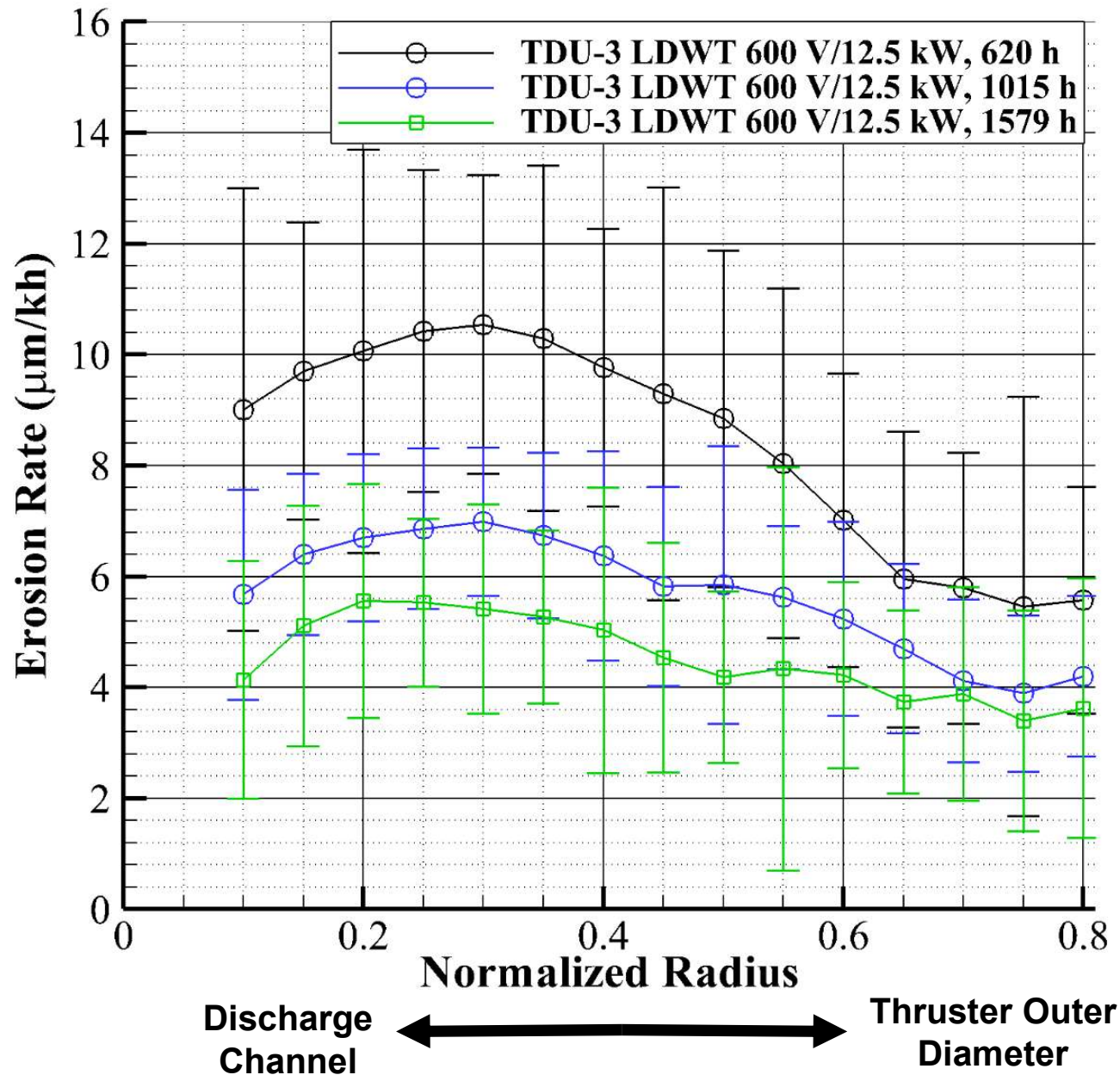


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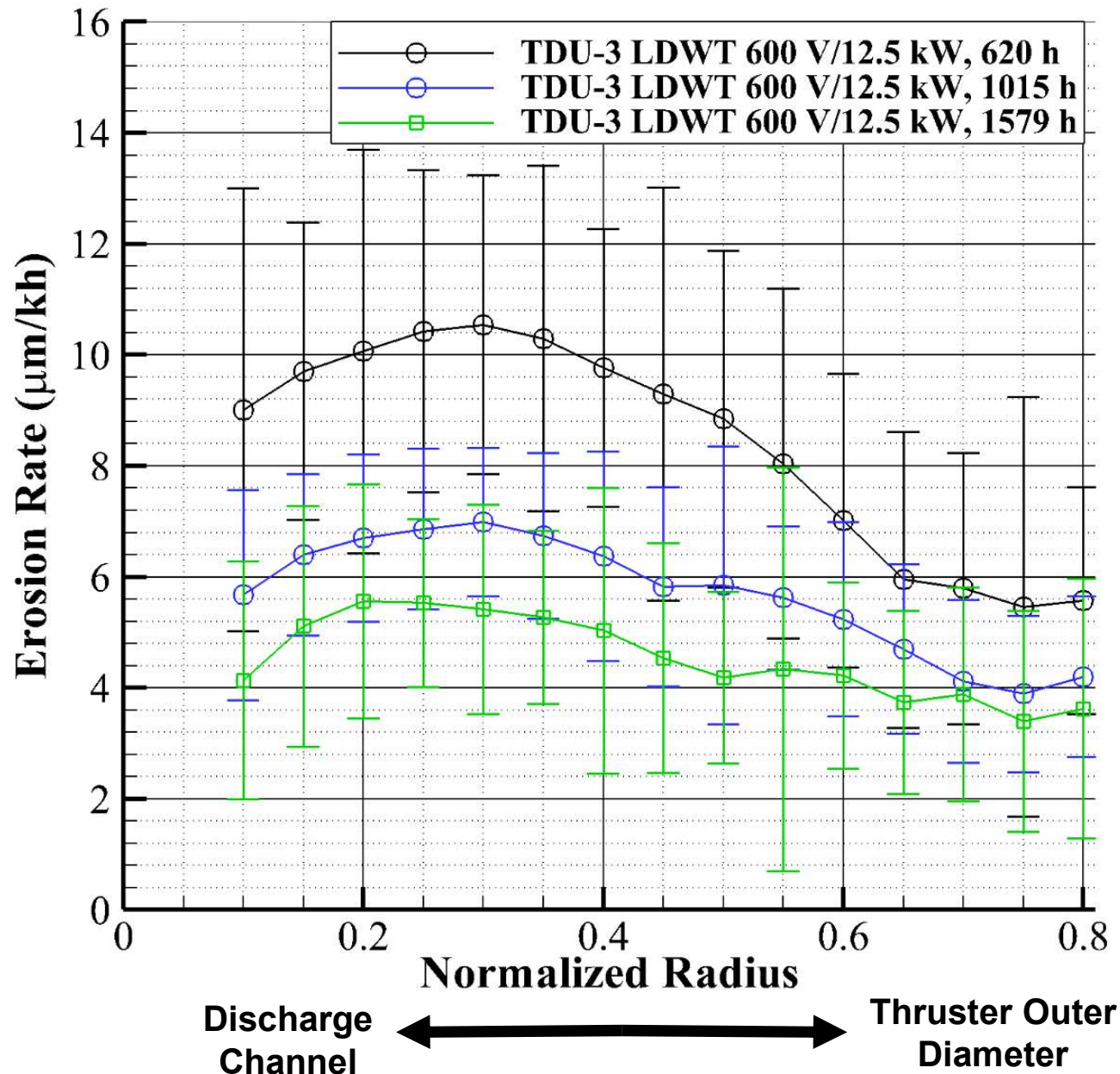


### Key Observations:

- 1) OFPC erosion rates appear to decrease with operating time
  - 46% reduction between 620 h and 1579 h
  - Matches trends previously observed with the IFPC
- 2) Wear rates impacted by pre-test surface finish
  - Plotted rates are for polished regions of OFPC
  - No measurable erosion detected on unpolished sections of OFPC
- 3) Results support hypothesis that apparent time variation in wear is driven by pole cover roughening during operation



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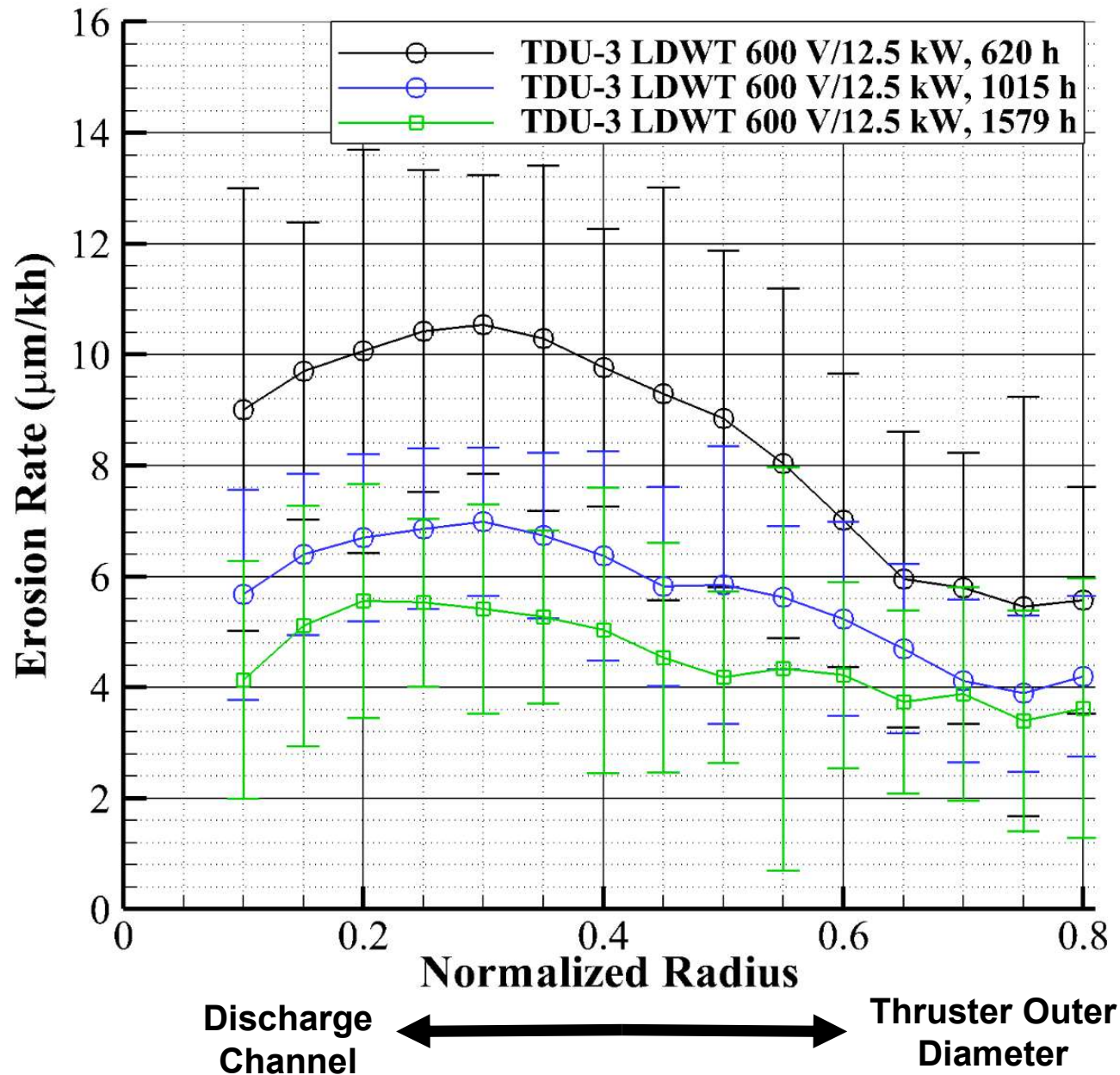
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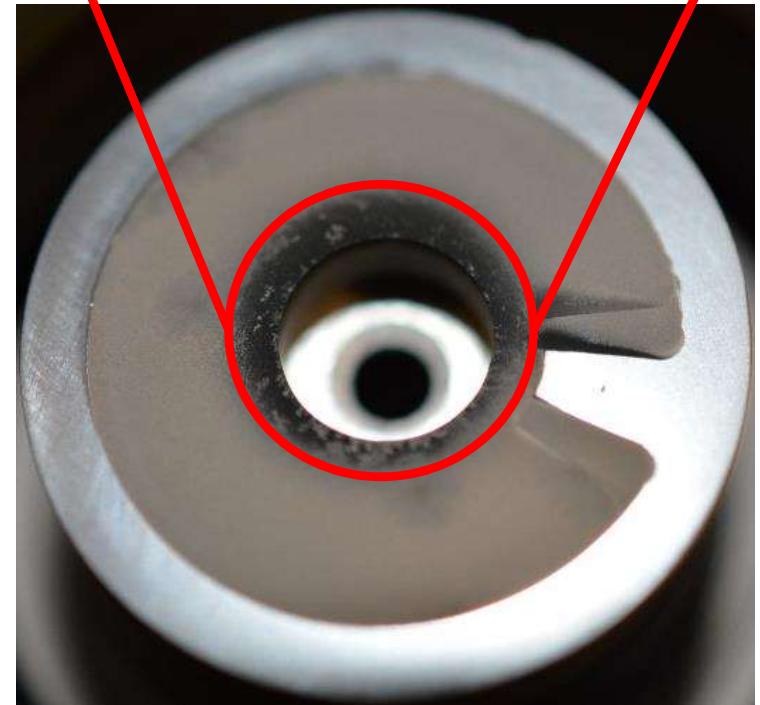
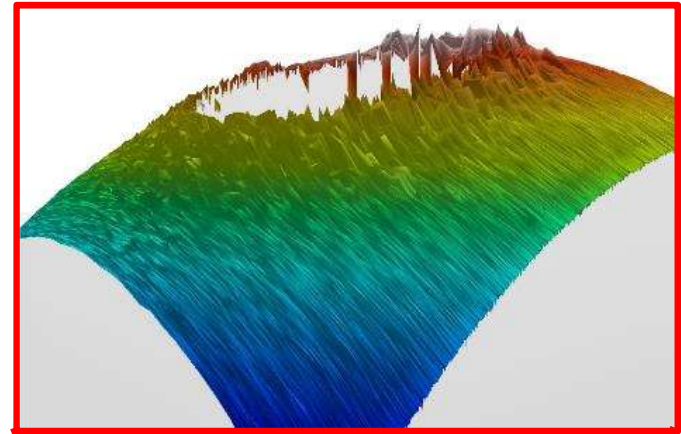
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## Results: Keeper Wear

- Net deposition with a thickness of  $\sim 1$   $\mu\text{m}$  observed around the keeper orifice
  - Net erosion observed at all other radii
  - Matches results from TDU-1 wear test

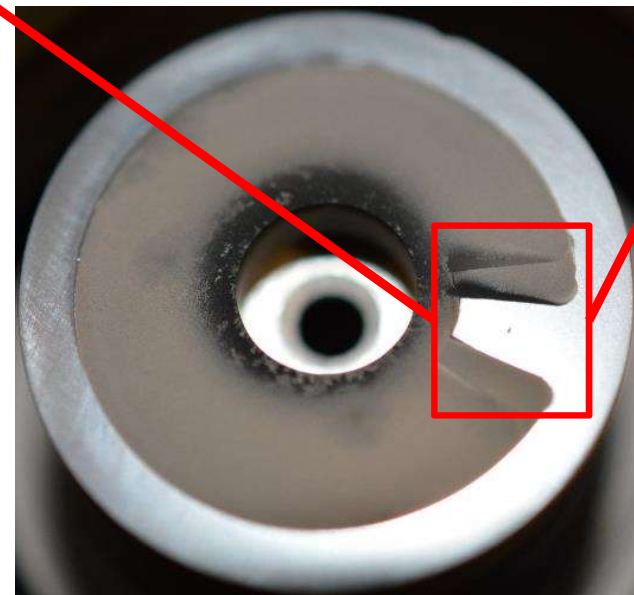
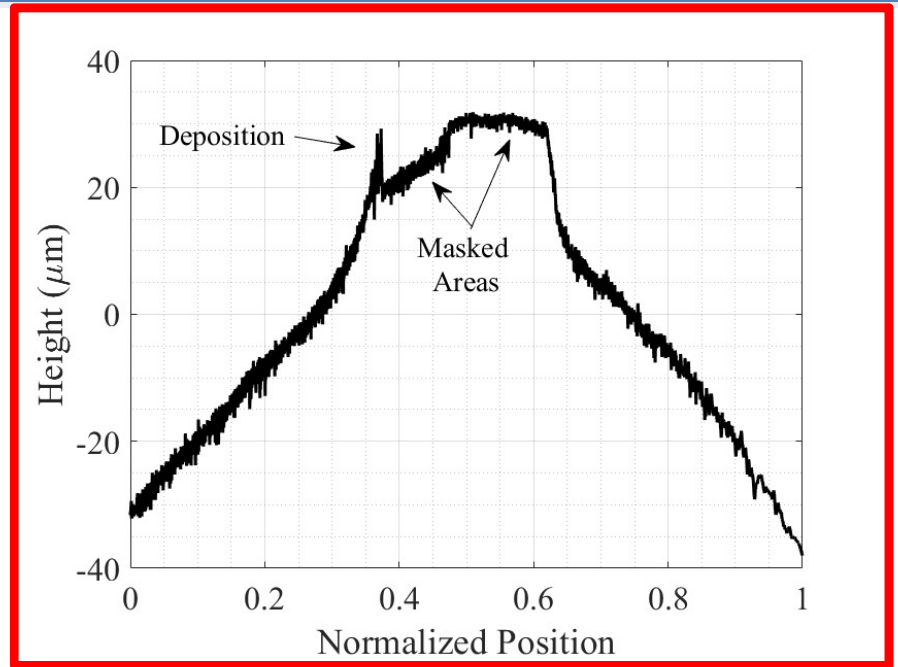






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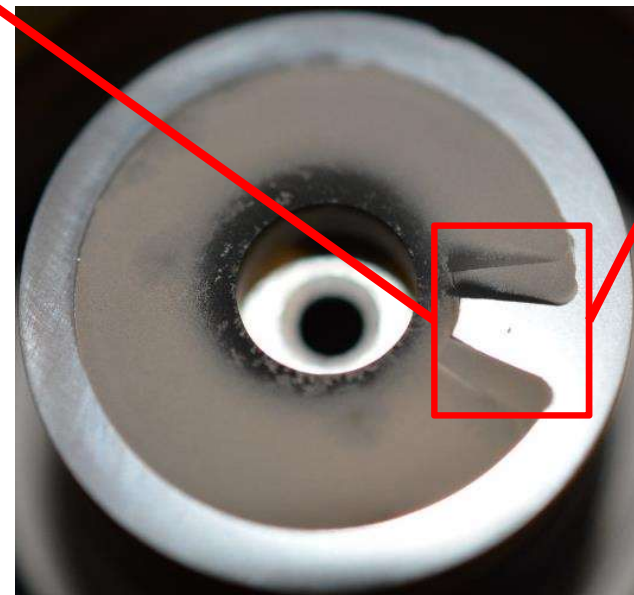
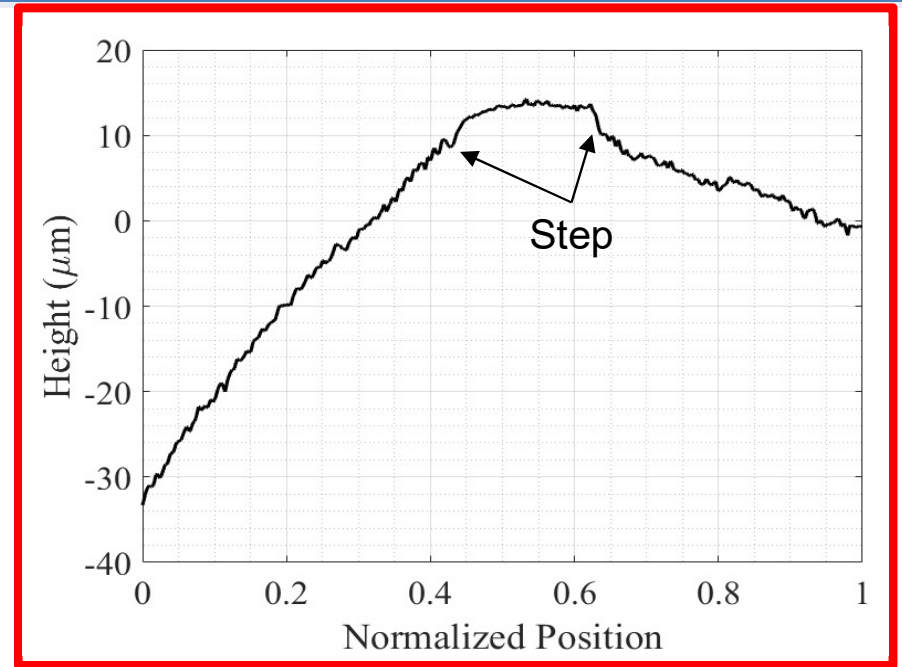
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- Net deposition also observed on one side of the keeper mask.





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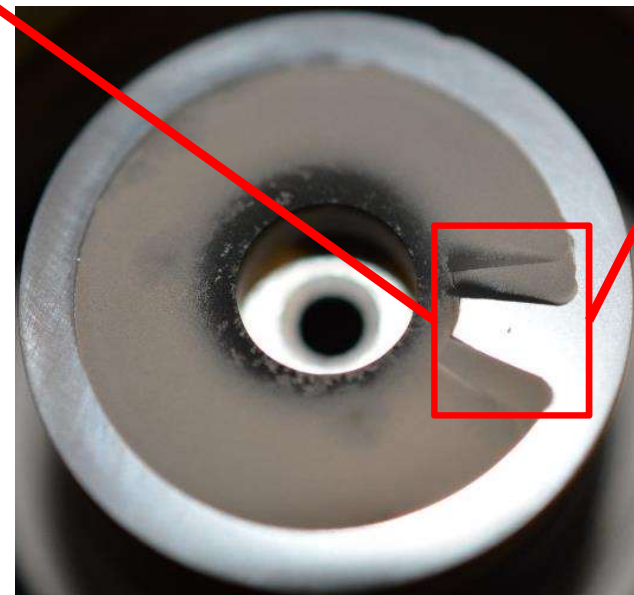
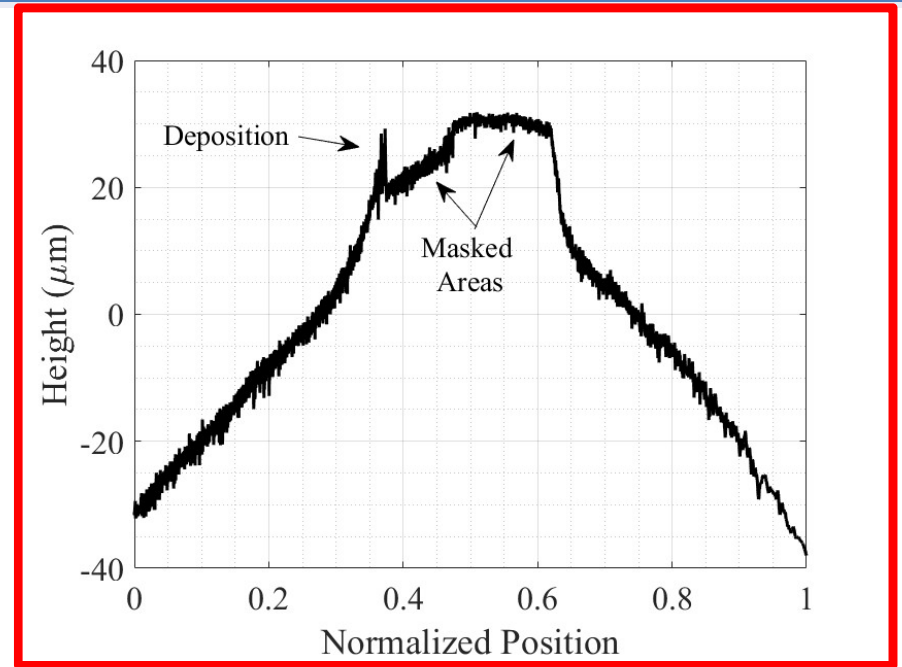
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- Net deposition also observed on one side of the keeper mask. **Possible causes:**
  - Azimuthal variation in process driving keeper erosion
    - Also explains step asymmetry observed during Segment I
  - Accumulation of facility backscatter on one side of the horizontal mask
    - Does not explain step asymmetry observed during Segment I (keeper mask oriented vertically)





# Conclusions

- The NASA HERMeS TDU-3 Hall thruster was successfully operated for 3,570 hours over six segments in a long duration wear test
- The TDU-3 demonstrated consistent performance, stability, and plume properties over the course of the LDWT and relative to previous wear tests
- Average erosion rates of a carbon-carbon composite inner front pole cover were found to match those obtained with graphite covers
- OFPC wear rates were shown to decrease with time and provided strong evidence linking this to pole cover roughening
- Regions of net deposition on the keeper suggests the presence of azimuthal variation in the process driving keeper erosion
- Overall, the TDU-3 LDWT successfully served as a pathfinder for the planned life and qualification testing of AEPS hardware by demonstrating facility readiness and component lifetimes margins of greater than 40% at the nominal 600 V/12.5 kW operating condition