



Optimizing a Coupled Solution for the Orion MPCV Using DPLR and NEQAIR

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TSA

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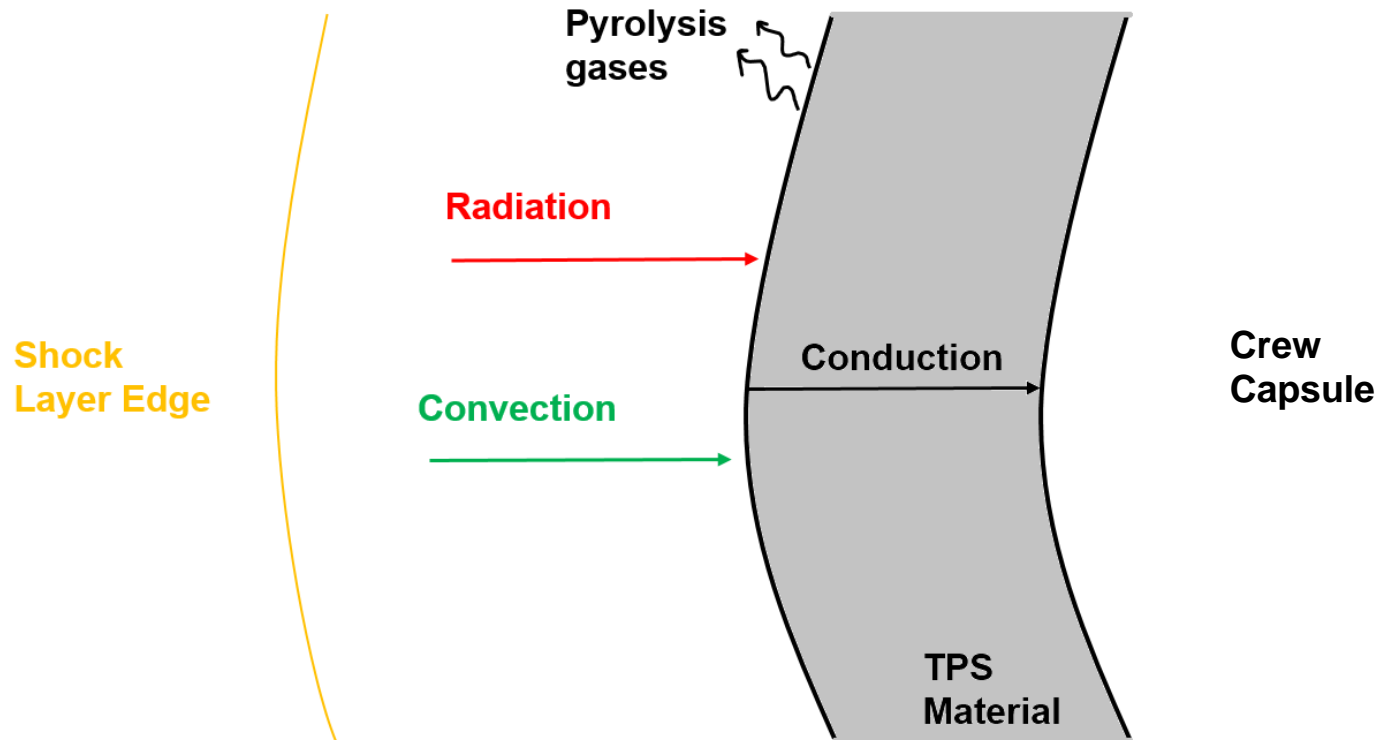


- **Background**
- **Significance**
- **Approach**
- **Data**
- **Results & Future Work**

Background



- Aerothermal CFD has shown that there are two important types of heating on Hypersonic Entry
 - **Radiative** and **Convective** Heating

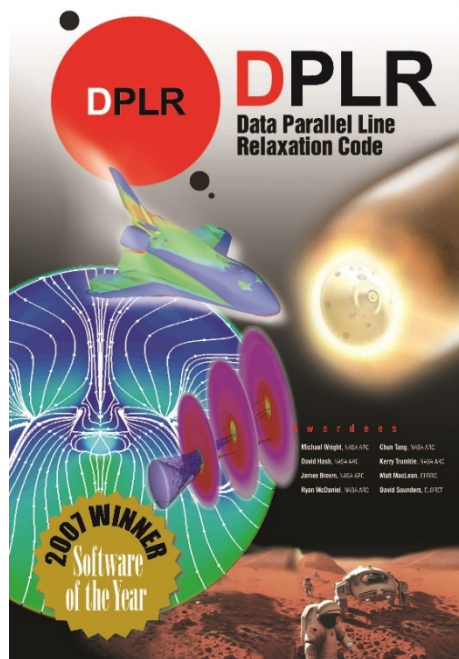


Background (cont.)

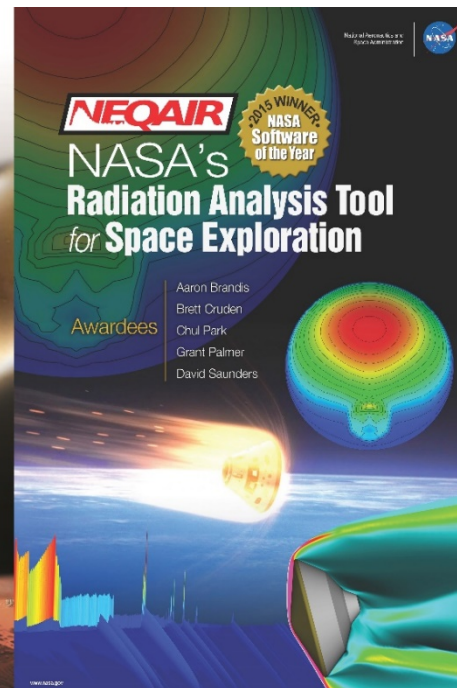


- Normal CFD solvers can only solve for convective or radiative heating one at a time
 - Few are able to “couple” the two accurately
 - But a production ready tool is under way...

**DPLR – Data Parallel
Line Relaxation Code**



**NEQAIR – Nonequilibrium
Air Radiation Code**



Background (cont.)



DPLR

Initial DPLR grid and solution files **copied** from external location to a local working directory.

DPLR - LOS

The 'dplr_los' program **partitions DPLR data into HDF5 files** for NEQAIR. Each HDF5 file has a series of wall-normal lines for NEQAIR to calculate.

NEQAIR

The 'postflow' program is run on the stored files to **extract species number densities, T_{tr} , and T_v** from the cell centers, which is output on the grid vertices.

Repeat for each iteration

DPLR is run again to **re-converge the flow field** with the NEQAIR-derived radiation source term.

The 'dplr_los' program is run again to **reassemble radiation source data** into a single file for use with DPLR, 'grad.prda'.

For each HDF5 file, a NEQAIR job is executed. NEQAIR outputs the **net energy lost/gained along a given line** and appends it to the original HDF5 file.

Coupler Iteration	1	2	3	4	5
Radiation Source Term Scaling	0.6	0.8	0.9	1	1

Background (cont.)



- The Coupling Setup script enables the user to easily control parameters
- Each iteration can be tailored with the number of CFD iterations and coarsening of the “radiation grid”

```
[COUPLER_SETUP]
iterations = 5
prefix = run

[DPLR_SETUP]
input_dir = inputs
inputfile = dplr.inp
gridfile = cev.111.pgrx
flowfile = cev.111.pslx
prefix = dplr
dimension = 2
normal_line = j

[NEQAIR_SETUP]
input_dir = inputs
inputfile = neqair.inp
prefix = neqair
batch_jobs = 16

[OPTIONS]
# All items are list with 1 entry per coupling iteration
dplr_igalign = 0, 0, 1, 1, 1
dplr_istop = 5000, 5000, 3500, 3500, 3500
coupler_iskip = 2, 1, 1, 1, 1
coupler_jskip = 2, 1, 1, 1, 1
coupler_scale_divq = 0.6, 0.8, 1.0, 1.0, 1.0

[DPLR_BATCH]
nprocs = 100
walltime = 03:00:00
jobname = couple_dplr
queue = batch
stdout = run_dplr.out

[NEQAIR_BATCH]
nprocs = 64
walltime = 04:00:00
jobname = couple_neqair
queue = batch
stdout = run_neqair.out

[D2N_BATCH]
walltime = 00:30:00
jobname = couple_d2n
stdout = run_d2n.out

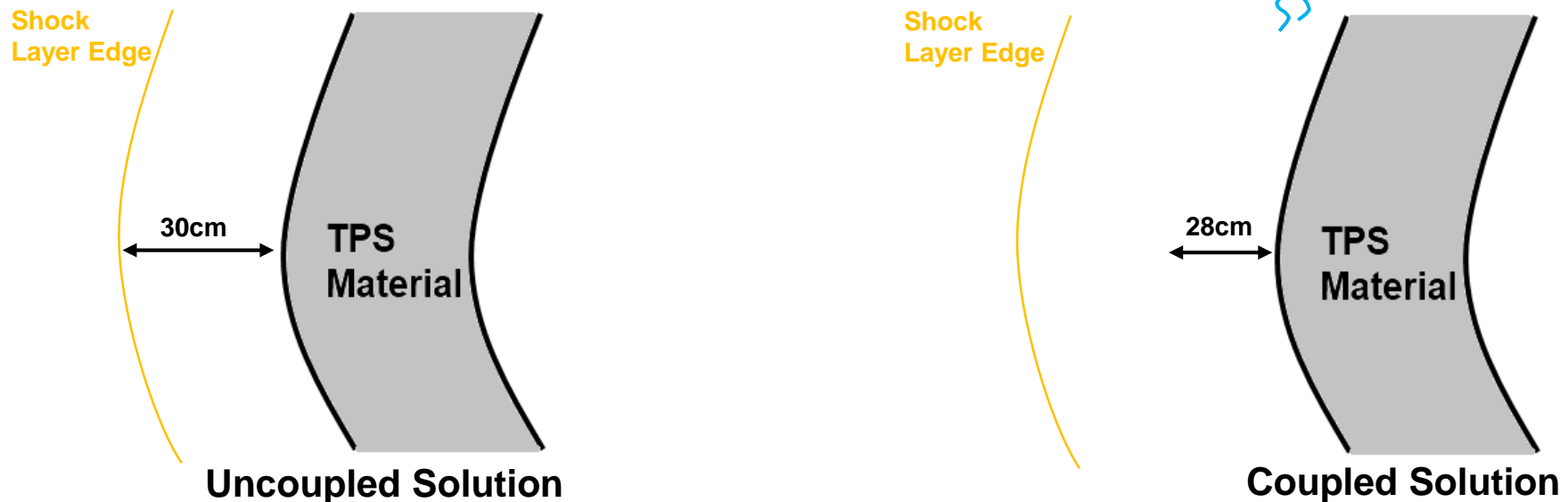
[N2D_BATCH]
walltime = 00:30:00
jobname = couple_n2d
stdout = run_n2d.out

[SYSTEM_SETUP]
setup_commands = ulimit -s unlimited
```

Significance



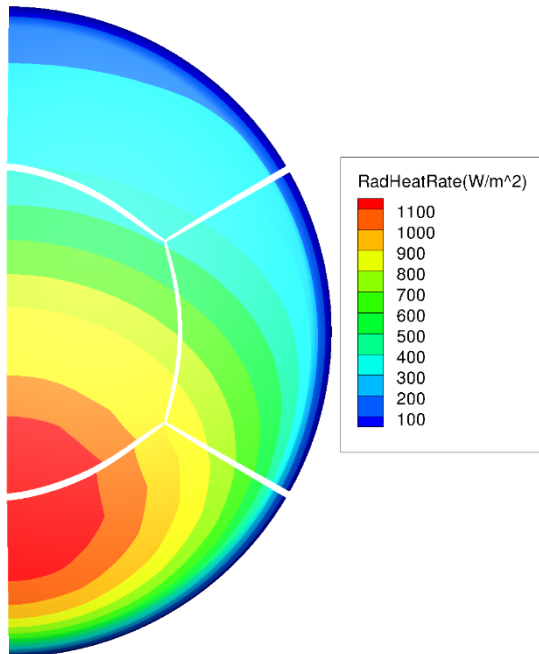
- Most flow simulations can get away with being uncoupled or loosely coupled because the radiative energy is minimal compared to the total energy of the gas
 - However, for high-speed entries, radiative energy is a major sink in the shock layer and a source in the boundary layer, which reduces the bow shock standoff distance and reduces the convective and radiative heating rates at the wall
 - This phenomenon is known as *radiative cooling*



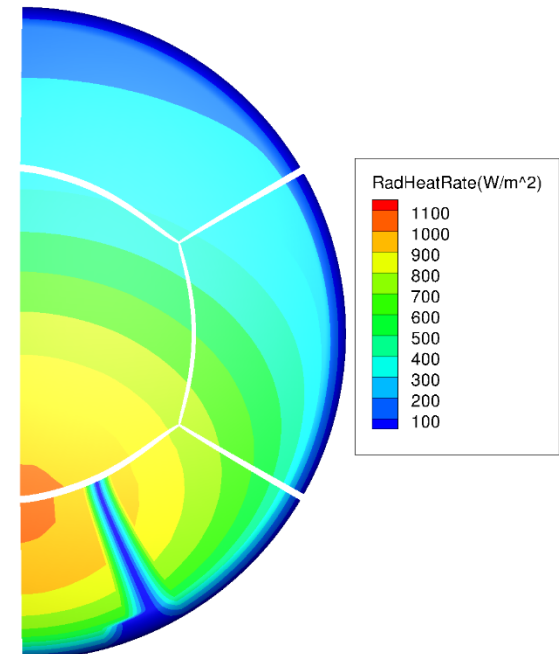
Significance



- Another way to show the effect of *radiative cooling* is on the forebody surface. For uncoupled solutions, the implied margin is higher and so a more conservative estimate is required.



Uncoupled Solution



Coupled Solution

Significance



More accurate modeling
of the heating effects



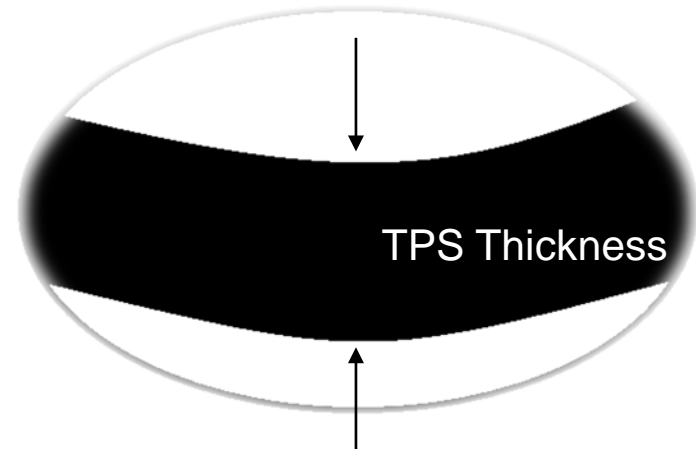
Slimmer Design Margins



Thinner TPS/Reduced weight



More weight for mission critical elements
(science instruments, food, sensors, etc.)

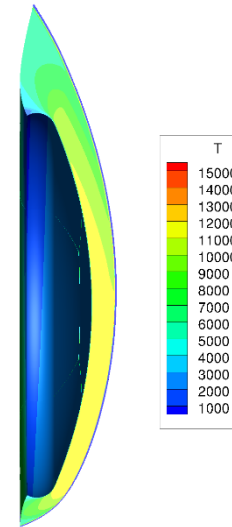


My Objectives



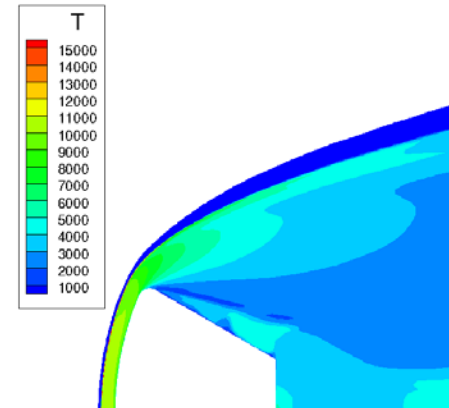
Objective 1:

Successfully run a 3D Orion MPCV simulation through the coupler



Objective 2:

Optimize run time of Orion MPCV by testing run time of 2D case through the coupler

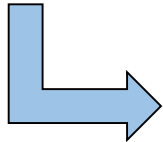


My Approach

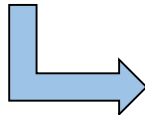


Started with a low velocity (5km/s) 2D axi-symmetric case to validate coupler would work

Coupler Bug Found:
wouldn't write out all 'grad' lines for multi-block problems

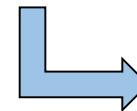


After coupler fixed, ran 3D half body case at 5km/s to ensure 3D could work in coupler



Went back to 2D and began running at peak heating condition (10km/s)

NEQAIR Update:
"Ill-conditioned" math lines were hung, fix put in to skip hanging

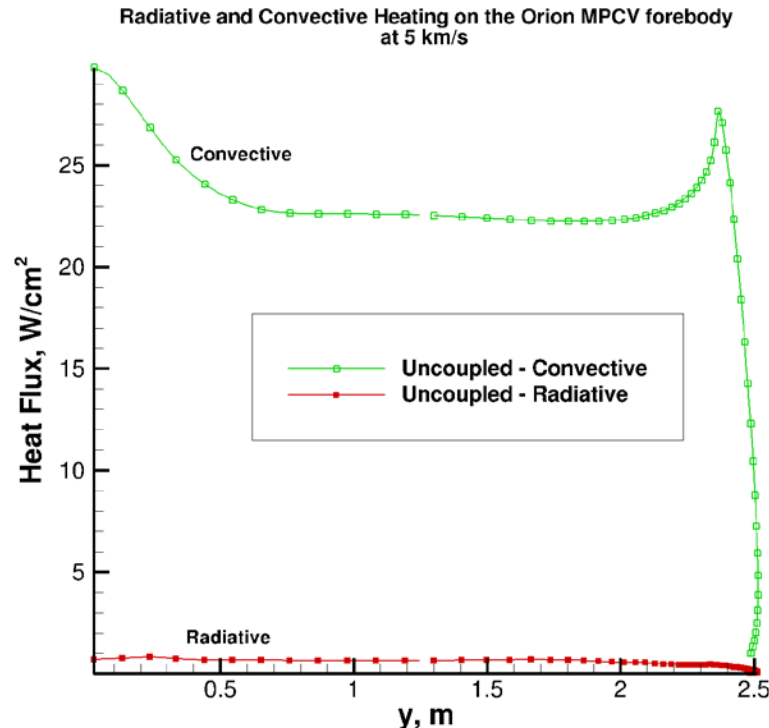


Began running 3D case at peak heating conditions (10km/s) and examined forebody conditions

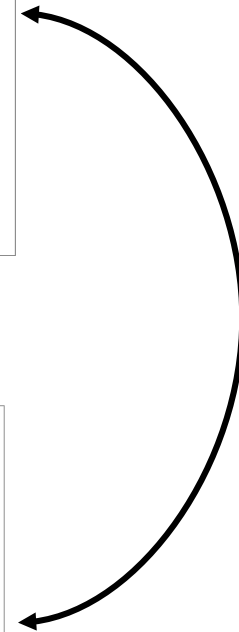
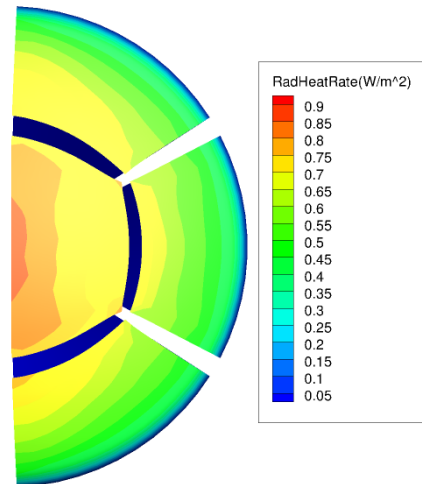
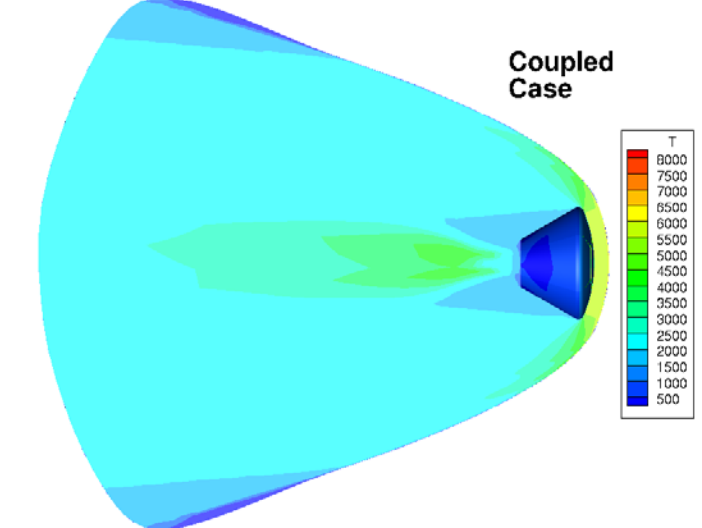
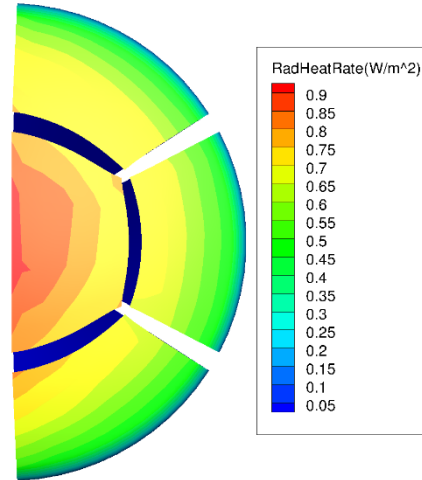
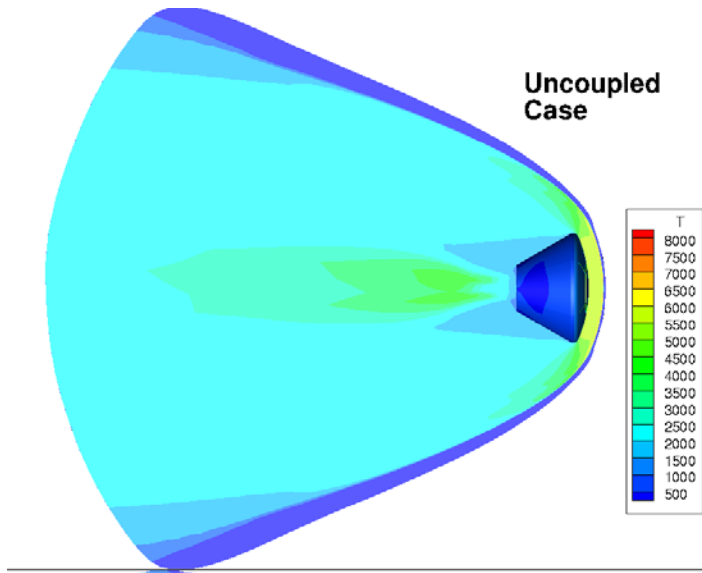
2D Axi-Symmetric Case (5km/s, 54.6km)



- In order to sort out bugs in the coupler, a 2D case was ran through
 - Several bugs were found in the coupler source code that prevented NEQAIR from working
 - Note how the **Radiative Heating** is much lower than the **Convective Heating** at 5 km/s



3D Half Body (5km/s, 54.6km, 0' AoA)



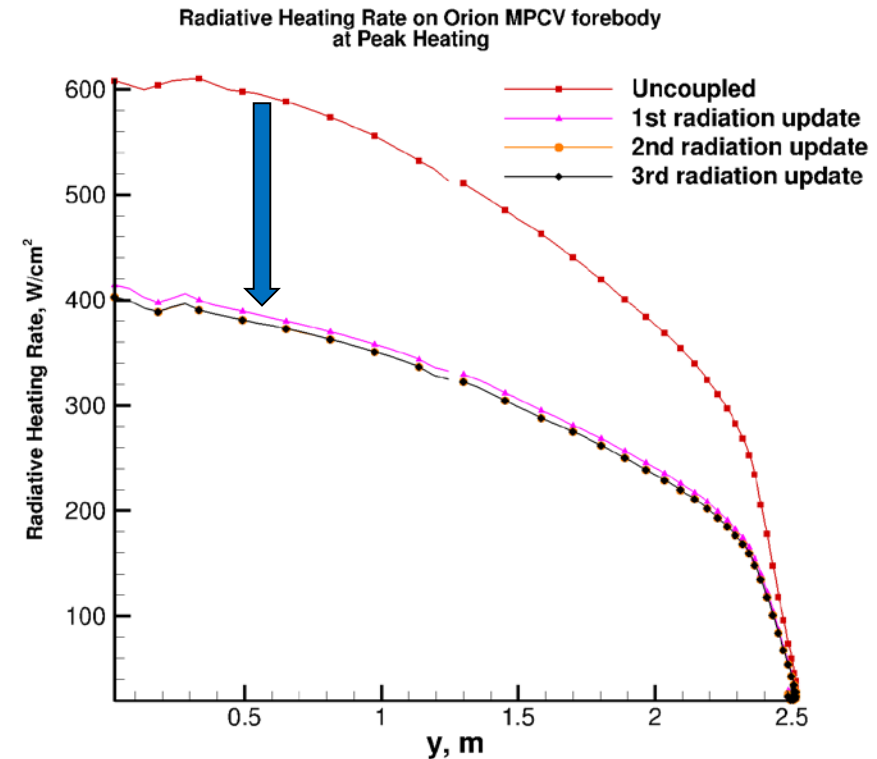
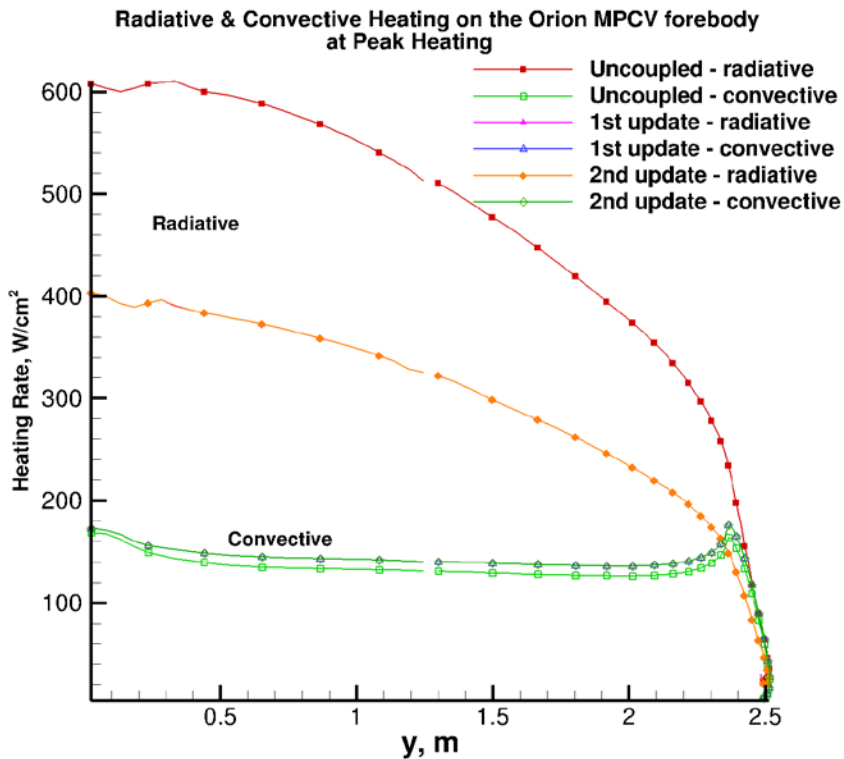
Note - the Coupled Case has **lower** radiative heating than the Uncoupled

2D Peak Heating (10.5km/s, 61km)



At high entry speeds, the **radiative** heating becomes **much greater** than the **convective** heating

As progressive runs are done, the **radiative** heating on the forebody converges to a **lower value**

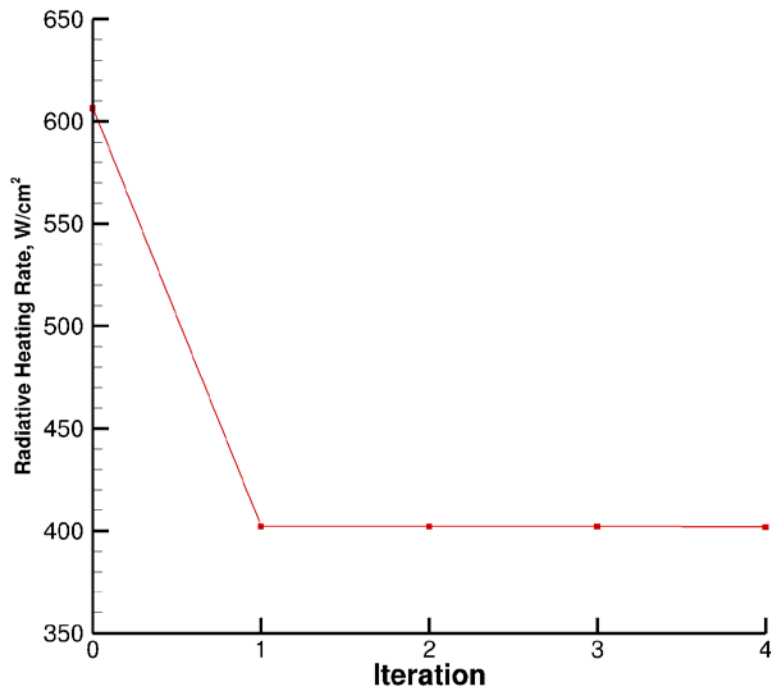


2D Peak Heating (10.5km/s, 61km)

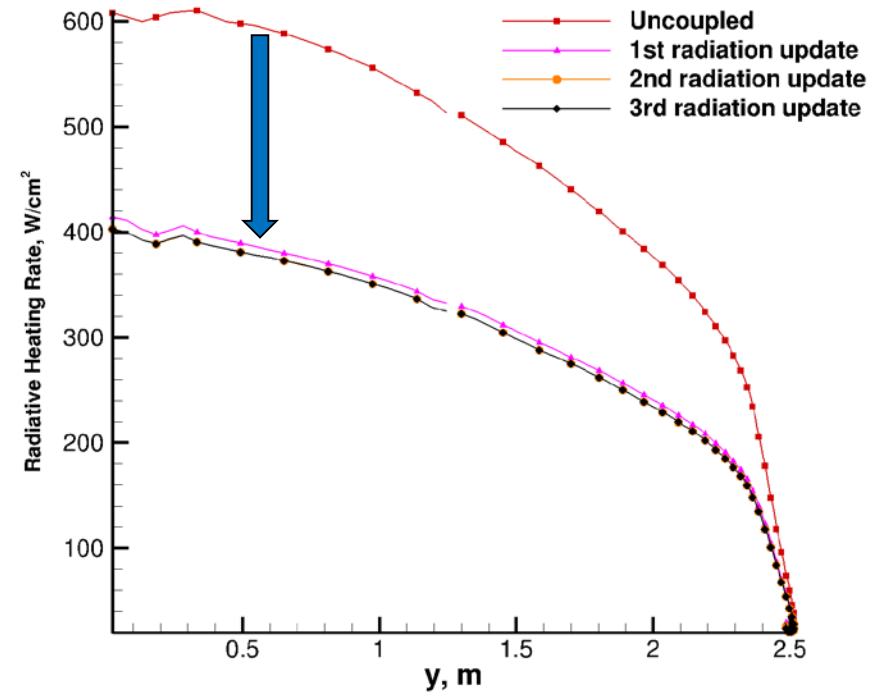


As progressive runs are done, the **radiative** heating on the forebody converges to a **lower value**

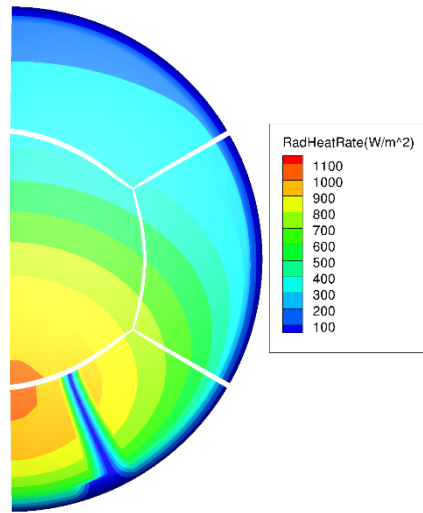
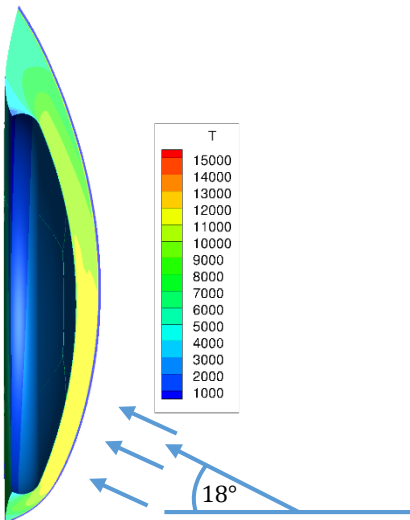
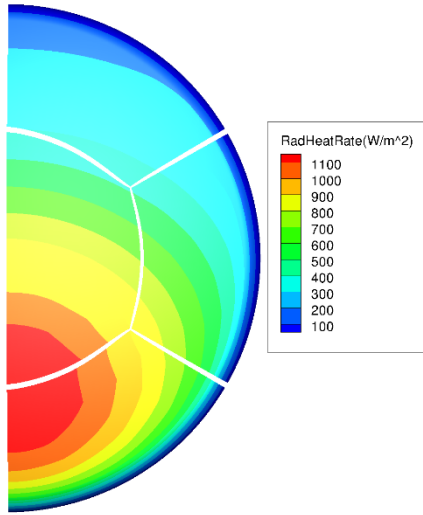
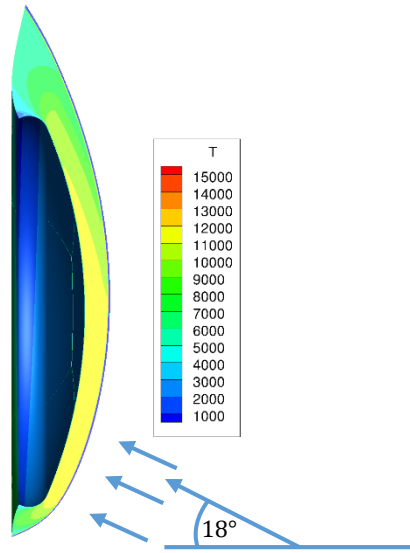
Radiative Heating Convergence on the Orion MPCV through the Coupler



Radiative Heating Rate on Orion MPCV forebody at Peak Heating



3D Peak Heating (10.5km/s, 61 km, 18' AoA)



Note - the Coupled Case has **much lower** radiative heating than Uncoupled

Discussion/Conclusions



- The 3D case is set up and can run several steps through the coupler
 - Recommend that # of batch jobs be split up to 32 and the number of NEQAIR lines be coarsened from 8, to 4, to 2
 - Computational Time: running with 256 processors per NEQAIR file and 300 processors for DPLR
 - Switch from Cedar to Pleiades will speed this up dramatically
- Still errors with some of the NEQAIR lines

```
slurmstepd: error: Exceeded job memory limit
slurmstepd: error: *** JOB 3919 ON c3 CANCELLED AT 2019-07-16T15:41:32 ***
```



- Tweak the 3D coupled case further in order to fix NEQAIR stability issues
 - Move from Cedar to Pleiades
- Set up the 3D case to run through a database of entry conditions
 - Varying entry speeds, angle of attack, and altitudes
 - Already done for 2D, still needs to be done for 3D

Lessons Learned



Start Small

- Work from a simple 2D case and troubleshoot errors before running a larger case

Adapt First

- Adapt the uncoupled solution before running it through the coupler

Boundary Conditions

- Check that your boundary conditions are correct *before* starting or else your solution will not converge

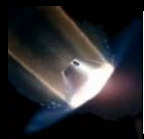
Works Cited & Acknowledgements



Glass, David. "Ceramic Matrix Composite (CMC) Thermal Protection Systems (TPS) and Hot Structures for Hypersonic Vehicles." *15th AIAA International Space Planes and Hypersonic Systems and Technologies Conference*, 2008, p. 6., doi:10.2514/6.2008-2682.

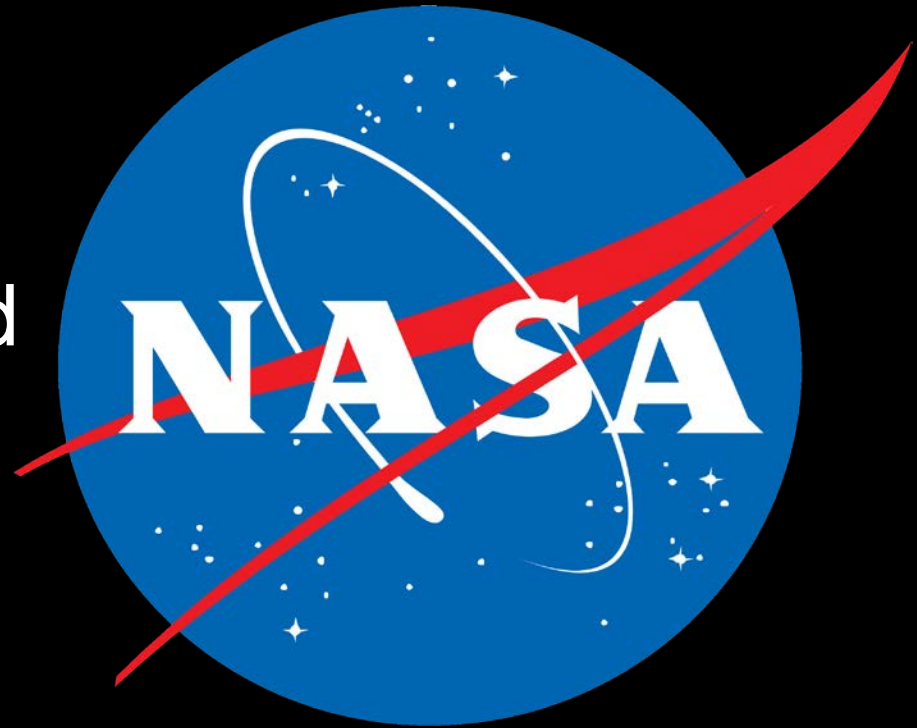
Palmer, Grant E., et al. "Direct Coupling of the NEQAIR Radiation and DPLR CFD Codes." *Journal of Spacecraft and Rockets*, vol. 48, no. 5, 2011, pp. 836–845., doi:10.2514/1.52043.

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Questions?

National Aeronautics and
Space Administration



Ames Research Center
Entry Systems and Technology Division