



Sublimation Protection Coatings for Thermoelectric Materials for Space Power Applications

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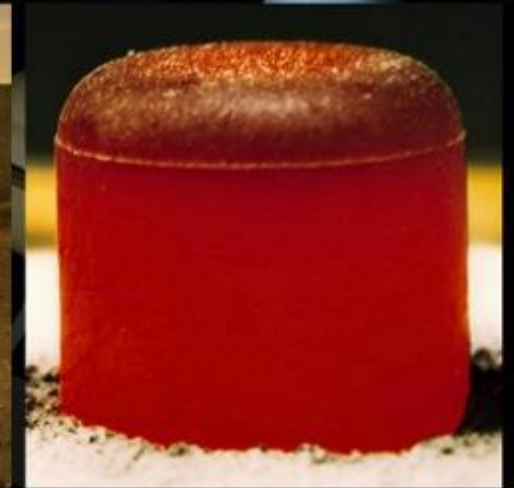
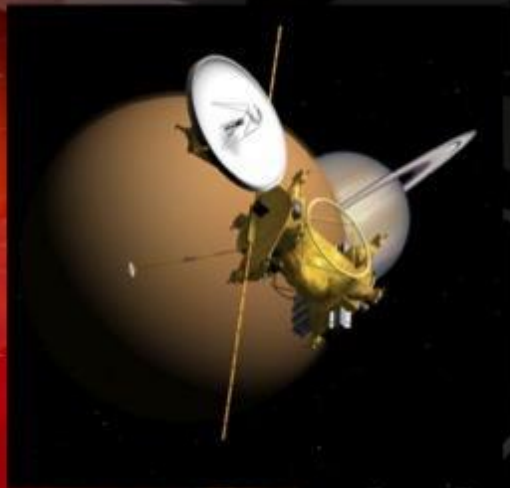
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MS&T2019, Portland OR

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Radioisotope Power Systems



- Enable and enhance missions by providing electrical power to explore remote and challenging environments where solar power is unavailable
 - Spacecraft operation
 - Instrumentation
- Converts heat from a Radioisotope into electricity
 - Heat is the product of the natural decay process of the isotope



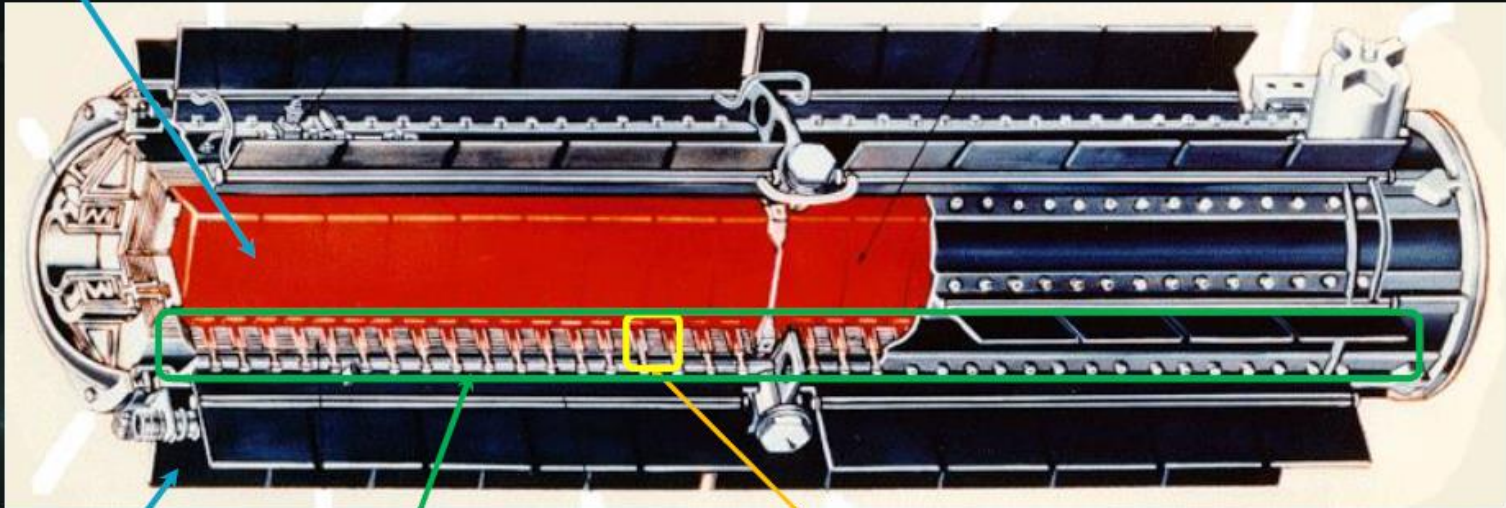
RTG (Radioisotope Thermoelectric Generator)

- An electrical generator that uses an array of thermocouples to convert the heat released by the decay of a radioactive material into electricity.
- Radioactive decay of the fuel produces heat. The temperature difference between the fuel and the heat sink allows the thermocouples to generate electricity.
- Si-Ge is current state-of-the-art thermoelectric material in current RTGs
- The compound $\text{Yb}_{14}\text{MnSb}_{11}$ is a thermoelectric material of interest to NASA as a candidate replacement for Si-Ge.
- $\text{Yb}_{14}\text{MnSb}_{11}$, however, suffers from a high sublimation rate at elevated temperatures (up to 1000°C)
 - Requires a sublimation protection in order to survive the required RTG lifetime of 14 years.

RTG: Thermoelectric Technology Nomenclature

1961
1971
1981
1991
2001
2011
2021

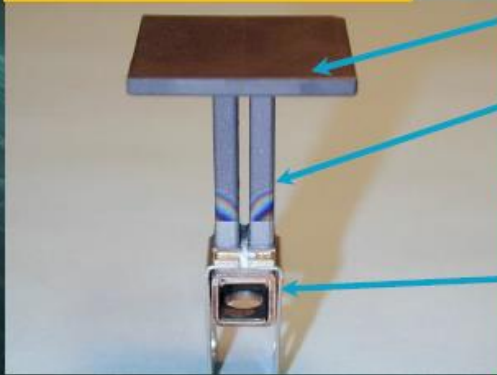
Heat source



Radiator

Thermoelectric Converter
(array of couples and its support structure/interfaces to heat source and radiator)

Thermoelectric Couple

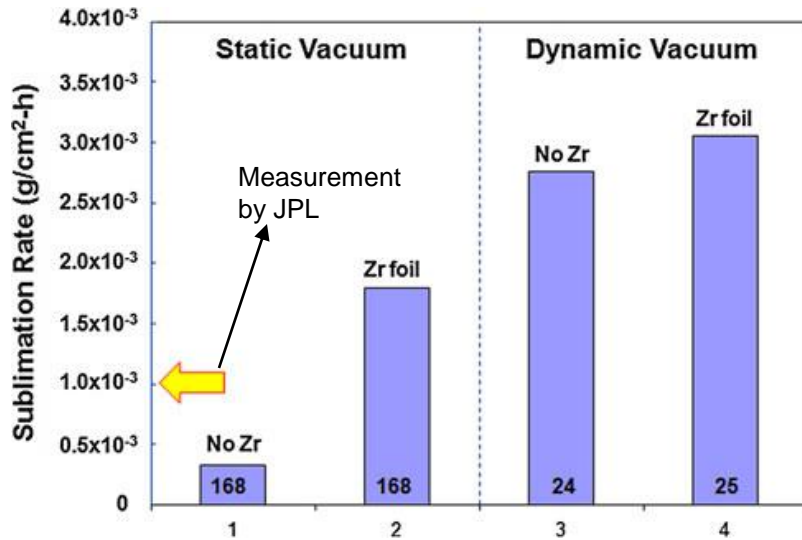


Hot Shoe
(Heat collector, electrical interconnect)

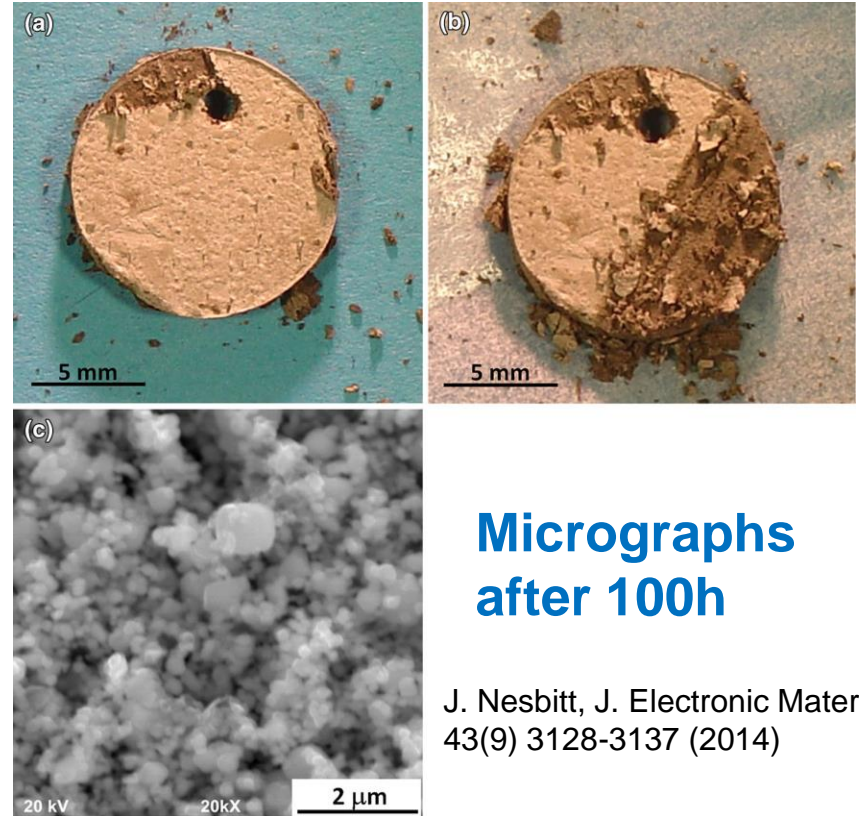
TE elements
(TE materials, metallizations, diffusion barriers)

Cold Shoe
(Electrical interconnect, Dielectric layer, cold side attachment)

Sublimation of $\text{Yb}_{14}\text{MnSb}_{11}$ (1000°C, 4 - 6 x 10⁻⁶ Torr)



J. Nesbitt et al, J. Electronic Materials, 41(6) 1267-1273 (2012)

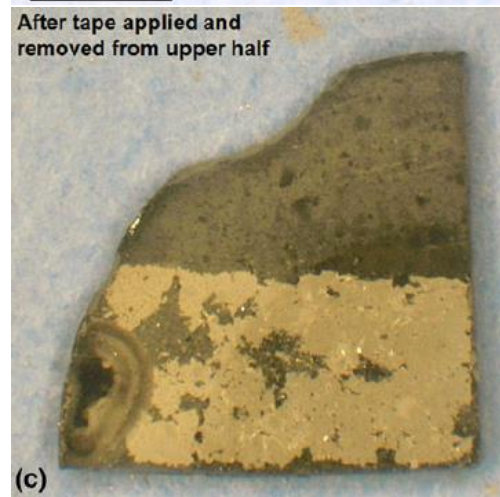
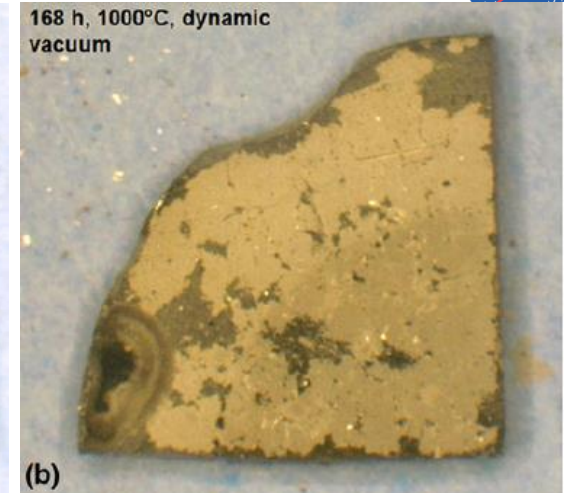
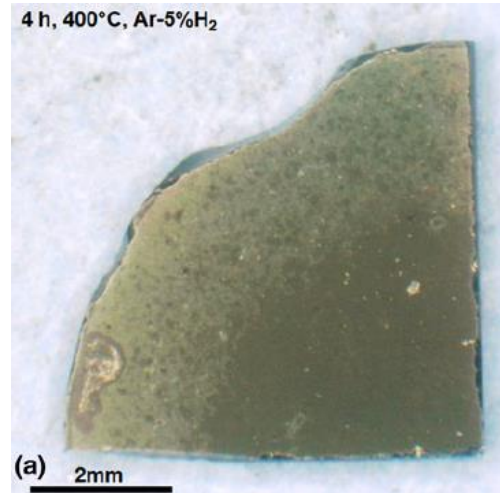
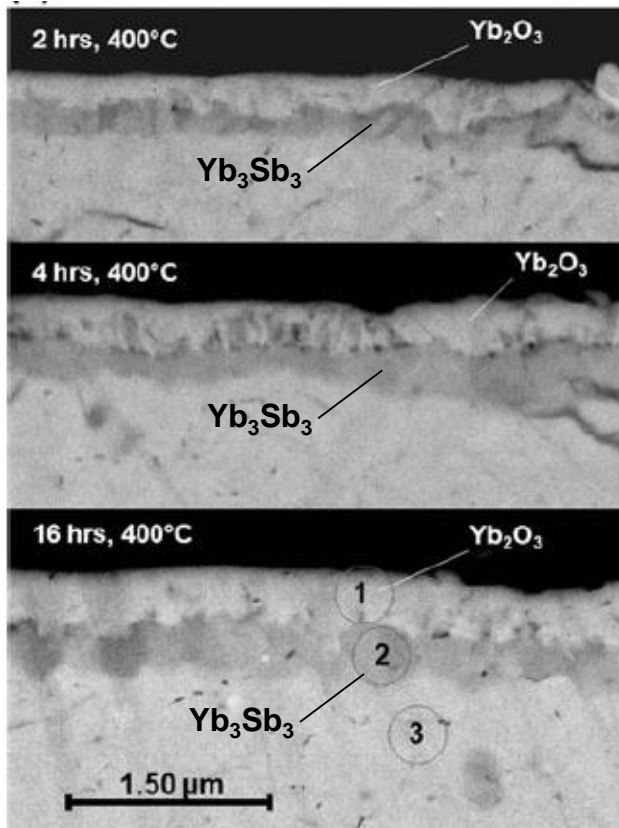


Micrographs after 100h

J. Nesbitt, J. Electronic Materials, 43(9) 3128-3137 (2014)

- Sublimation rates: 0.3 x 10⁻³ g/cm² - 3 x 10⁻³ g/cm²
 - Three orders of magnitude higher than the target rates (1 x 10⁻⁶ g/cm²)
- White, powdery oxide on the surface, which was identified by XRD as Yb_2O_3

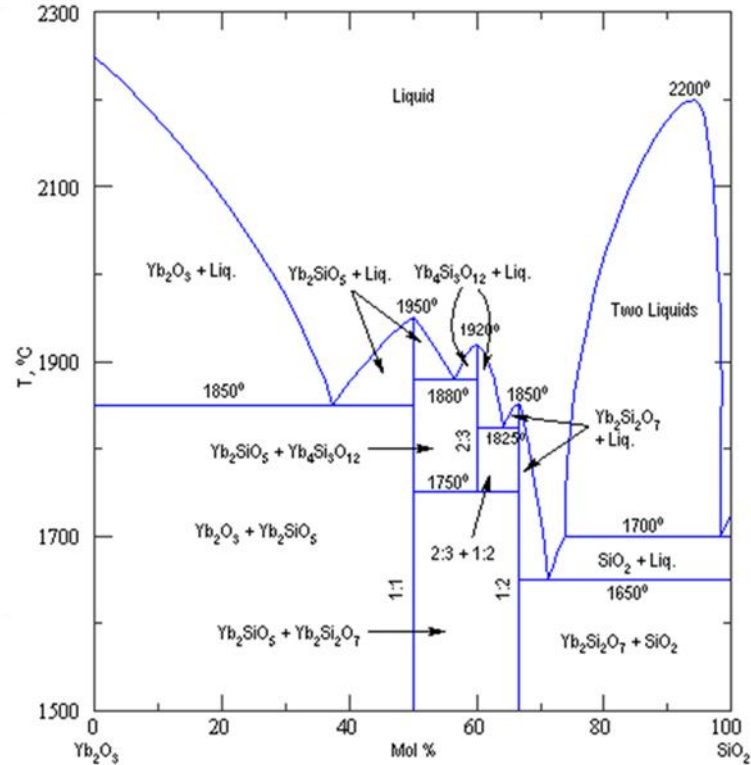
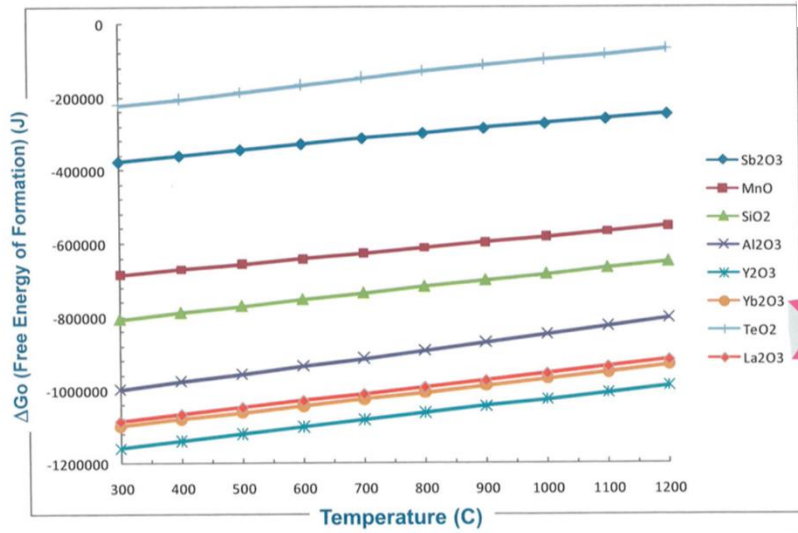
Pre-oxidation (400°C, Ar-5% H₂)



J. Nesbitt et al, J. Electronic Materials, 41(6) 1267-1273 (2012)

- In Ar-5% H₂, there was sufficient oxygen present in the furnace system to form thin, transparent, adherent scale
- After 168h at 1000°C in vacuum, the scale became opaque, friable, and detached
 - Not effective as sublimation barriers

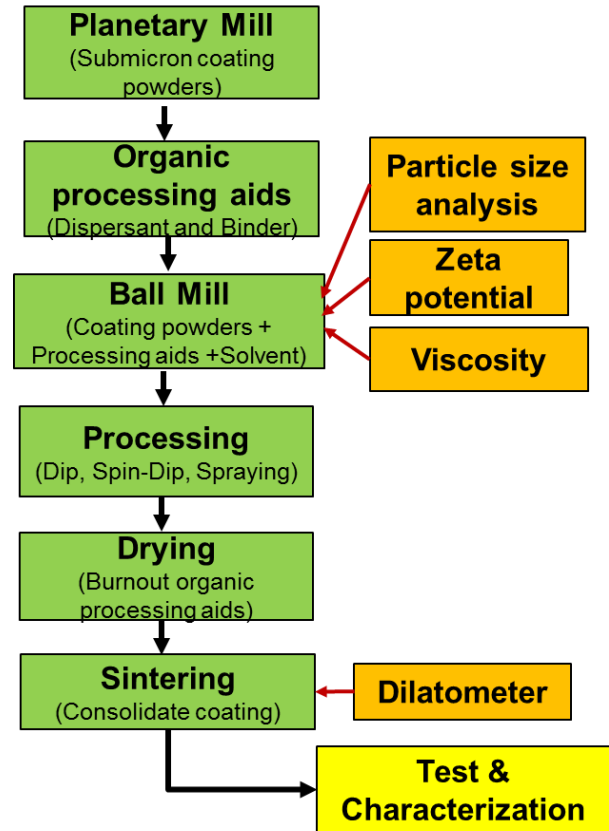
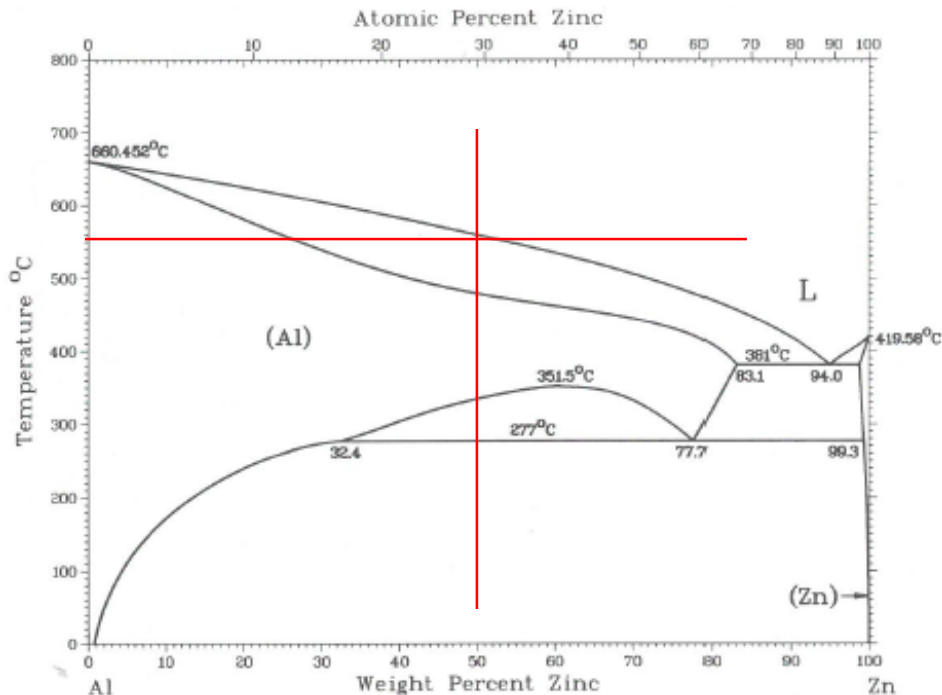
Rare Earth Oxide and Rare Earth Silicates are Thermodynamically Compatible with $\text{Yb}_{14}\text{MnSb}_{11}$



- Most oxides are reduced by Yb_2O_3 because of its very low free energy of formation
- Yb_2SiO_5 is thermodynamically stable in contact with Yb_2O_3
- Other rare earth oxides should be stable in contact with Yb_2O_3 as long as they do not form a solid solution

Objective

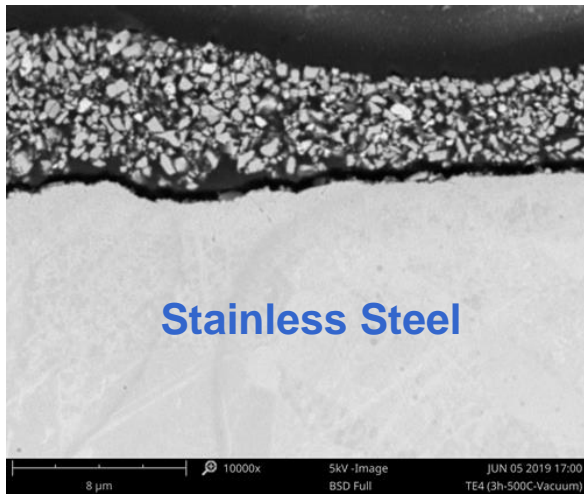
- Develop a sublimation protection coating for $\text{Yb}_{14}\text{MnSb}_{11}$ via slurry process
 - Derived from our experience with slurry-based EBCs (environmental barrier coatings)
 - Candidate coating material: Y_2O_3 , Yb_2SiO_5 , 7YSZ ($\text{ZrO}_2 + 7\text{wt}\% \text{Y}_2\text{O}_3$)
 - Sintering temperature $< 1000^\circ\text{C}$
 - Sintering aids: Al, Al + Zn (50 wt% + 50 wt%)
 - Sintering: 2-3 hr @ $< 1000^\circ\text{C}$, vacuum
 - Durability Test: 100 hr @ 1000°C , vacuum



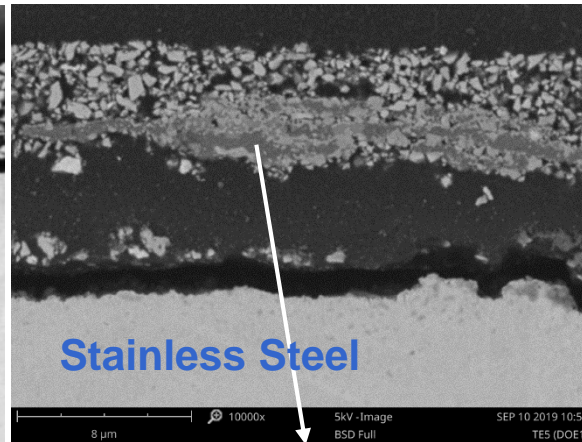
Y₂SiO₅ + Al Slurry Coating on Stainless Steel

Sintered at 700°C for 3 hr in vacuum (10⁻⁶ ~ 10⁻⁷ Torr)

Y₂SiO₅ + 2 wt% Al

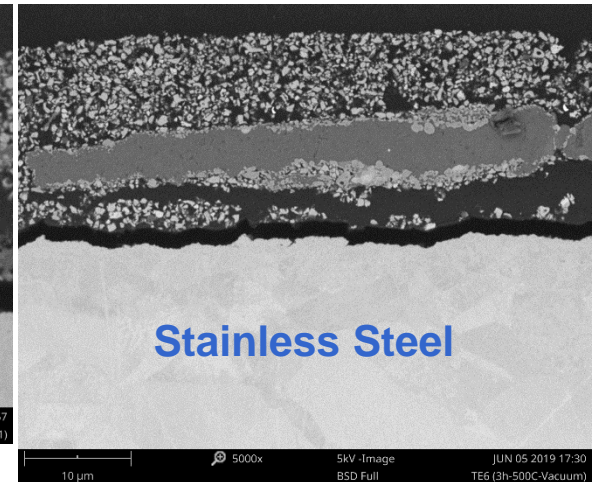


Y₂SiO₅ + 5 wt% Al



	Al	Fe	Cr	O	Si
Wt%	29.4	36.0	26.6	7.0	1

Y₂SiO₅ + 10 wt% Al

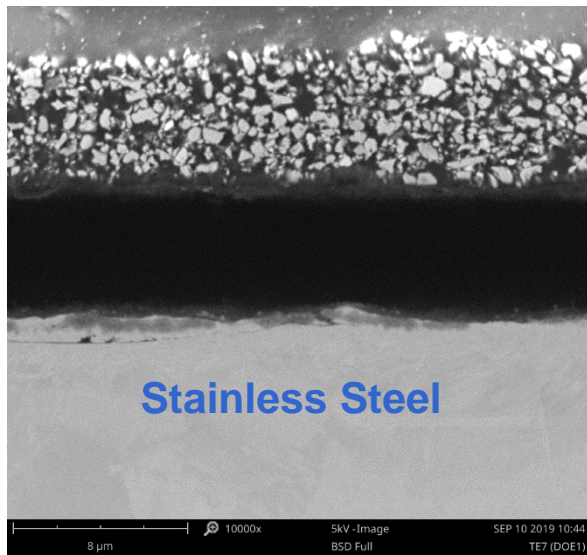


- Excess Al (Al = 5 wt% & 10 wt%) leads to coating debonding and spallation
- No excess Al visible with 2 wt% Al, however coating is not well bonded

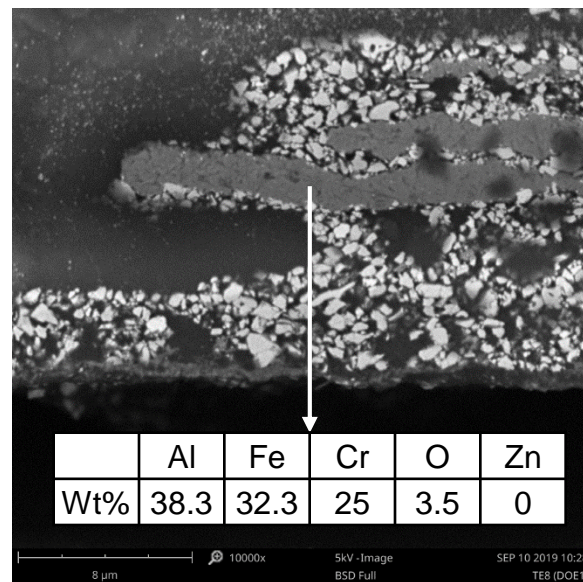
$Y_2SiO_5 + (Al + Zn)$ Slurry Coating on Stainless Steel

Sintered at 500°C for 3 hr in vacuum ($10^{-6} \sim 10^{-7}$ Torr)

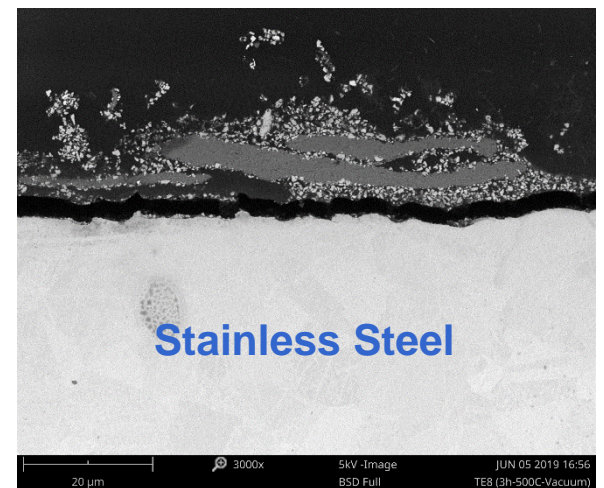
$Y_2SiO_5 + 2 \text{ wt}\% \text{ Al} + 2 \text{ wt}\% \text{ Zn}$



$Y_2SiO_5 + 5 \text{ wt}\% \text{ Al} + 5 \text{ wt}\% \text{ Zn}$



$Y_2SiO_5 + 5 \text{ wt}\% \text{ Al} + 5 \text{ wt}\% \text{ Zn}$



- Excess Al + Zn (Al + Zn = 5 + 5 wt% & 10 + 10 wt%) leads to coating debonding and spallation
- No excess Al visible with 2 wt% + 2 wt% Zn, however coating is completely debonded

Slurry Coatings on $\text{Yb}_{14}\text{MnSb}_{11}$ (Sintering Aid = 2 wt% Al + 2 wt% Zn)



Y_2O_3

Yb_2SiO_5

$\text{ZrO}_2 + 7 \text{ w\% } \text{Y}_2\text{O}_3$



Sintering in vacuum ($10^{-6} \sim 10^{-7}$ Torr)

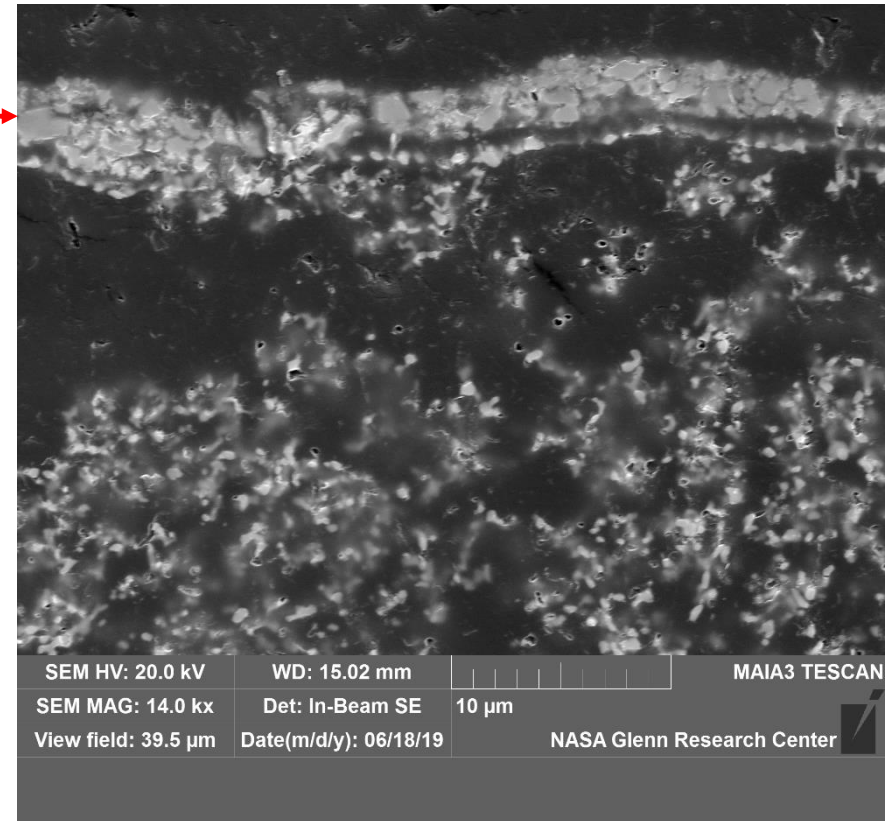
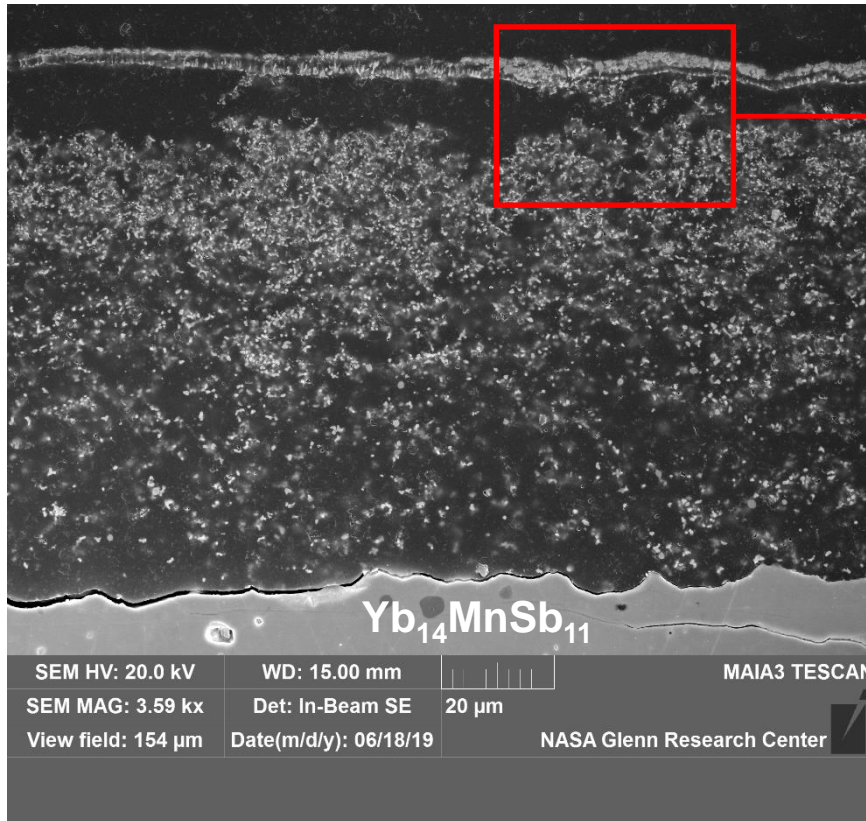
- Ramp to 500°C (4°C/min)
- Dwell at 500°C for 3 hr
- Cool down to RT (5°C/min)

Oxidation in vacuum ($10^{-6} \sim 10^{-7}$ Torr)

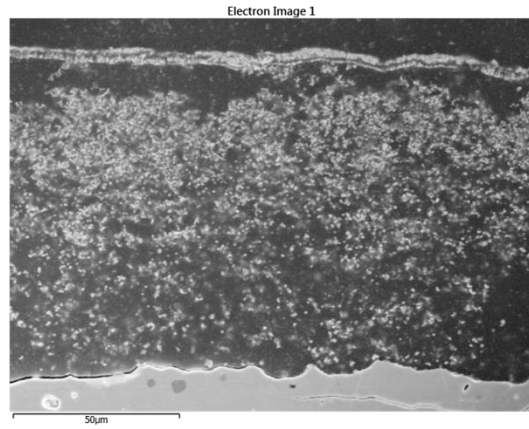
- Ramp to 1000°C (4°C/min)
- Dwell at 1000°C for 100 hr
- Cool down to RT (5°C/min)

- Y_2O_3 was powdery: Crumbled on handling (darker gray edges are spalled areas)
- Yb_2SiO_5 looked best: Edges damaged by tweezers, indicating the coating is friable
- 7YSZ spalled: Black is remaining coating and gray is exposed substrate after spall

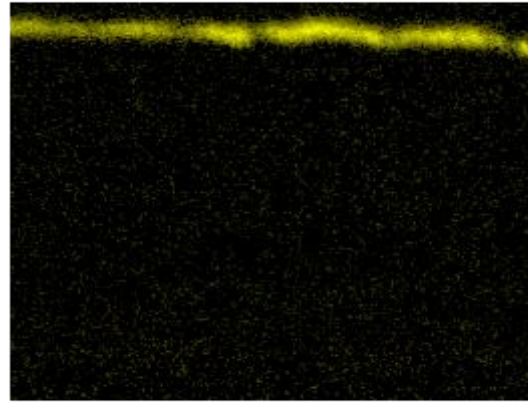
$Y_2O_3 + 2 \text{ wt\% Al} + 2 \text{ wt\% Zn}$



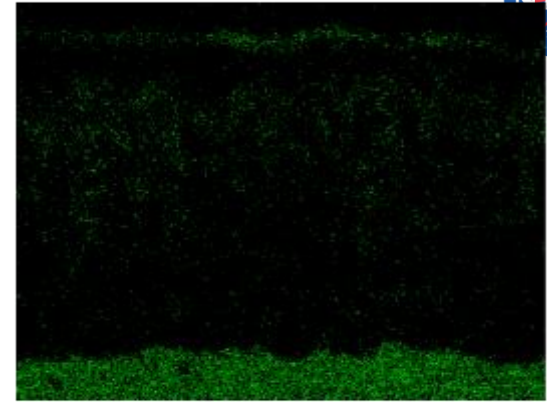
- An outer layer separated from the substrate by cloud of particles



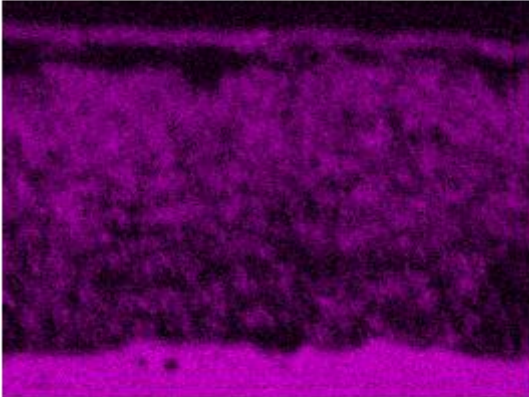
Y L series



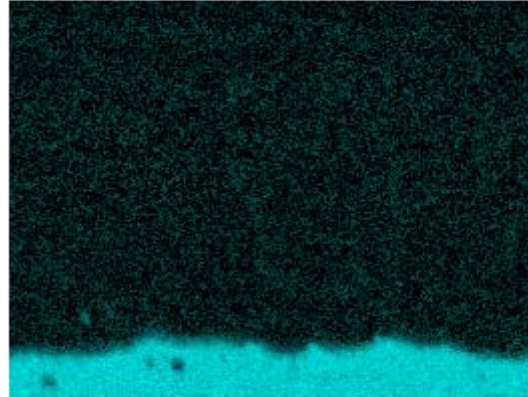
O K series



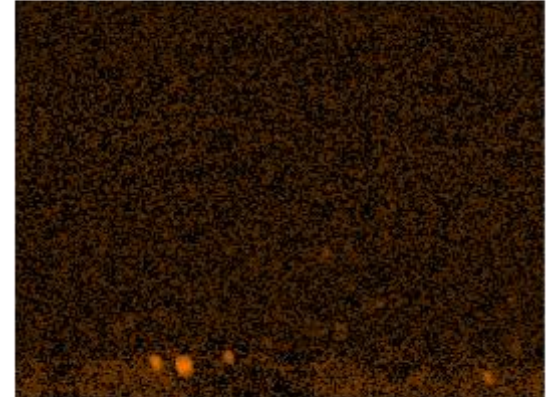
Yb L series



Sb L series



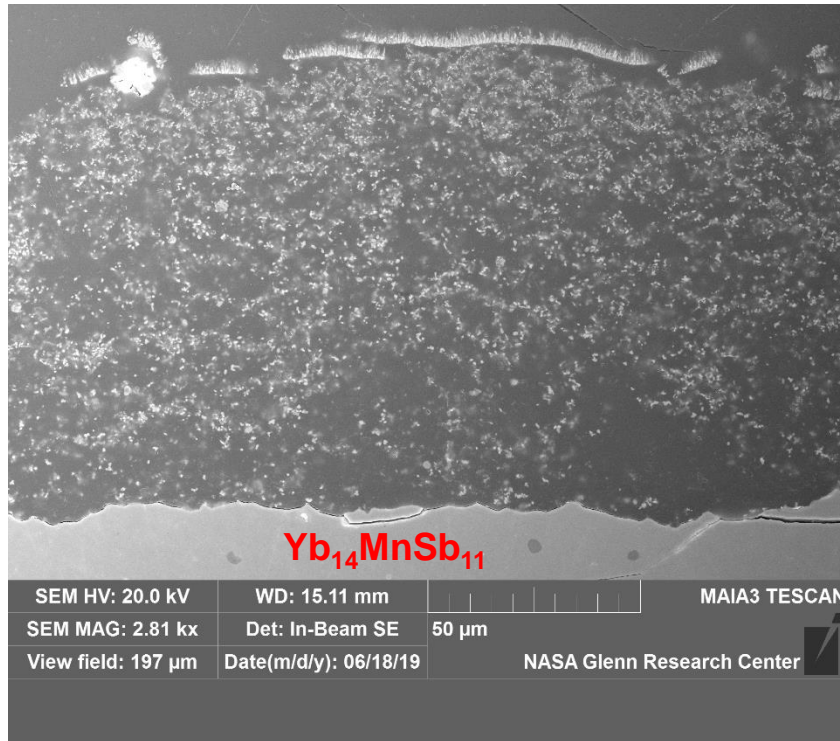
Mn K series



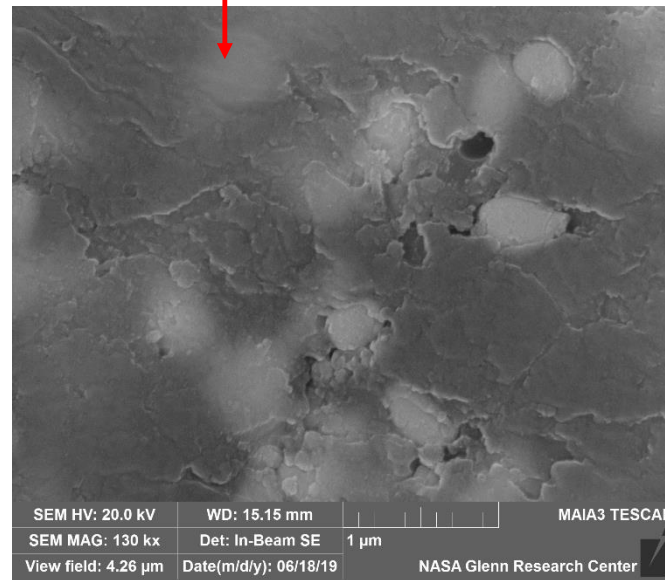
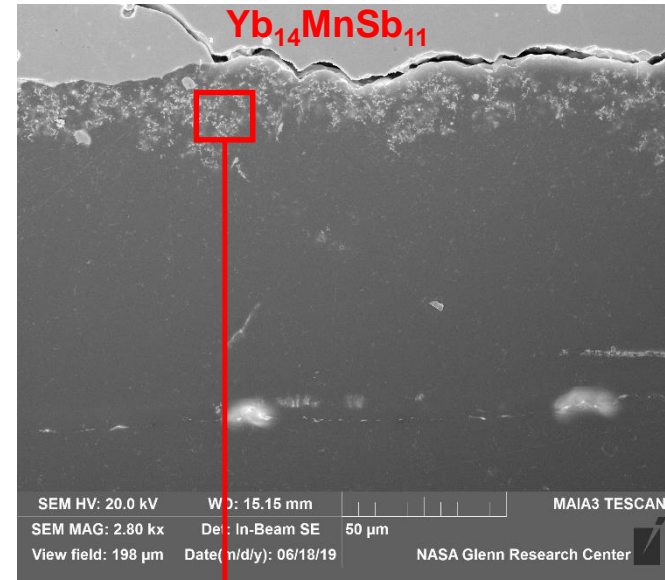
- The outer layer appears to be a $Y_2O_3 + Yb_2O_3$ solid solution
 - No Al and Zn detected in the coating by EDS – presumably dissolved in the substrate
- Cloud of particles is Yb_2O_3 due to the oxidation of substrate
 - Yb_2O_3 is thermodynamically more stable than Sb_2O_3 and MnO

Yb₂SiO₅ + 2 wt% Al + 2 wt% Zn

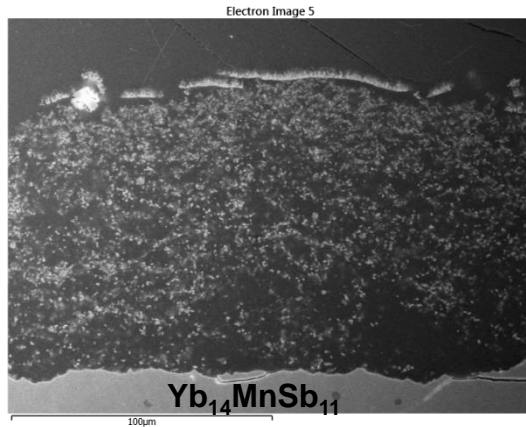
Coated Side



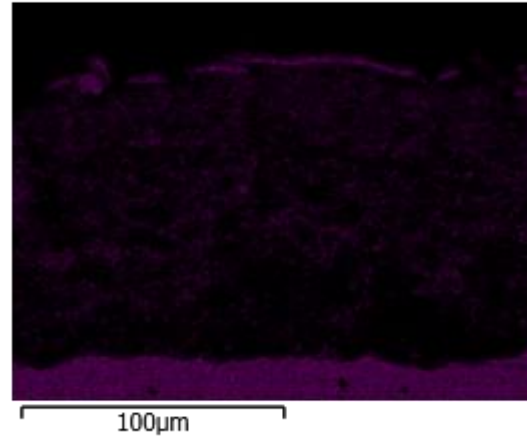
Uncoated Side



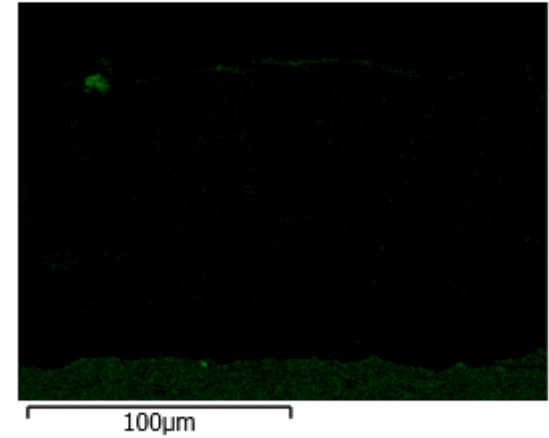
- Similar microstructure to Y₂O₃ coating
- Uncoated side has cloud of particles only



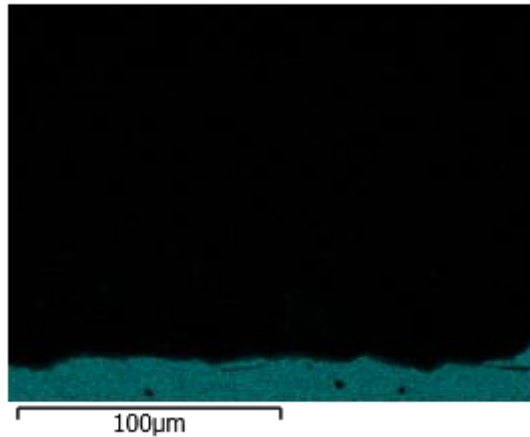
Yb L series



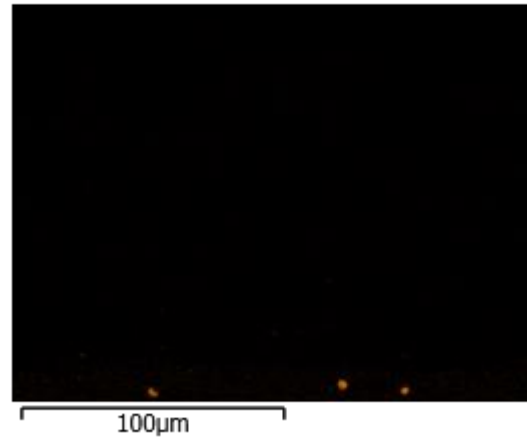
O K series



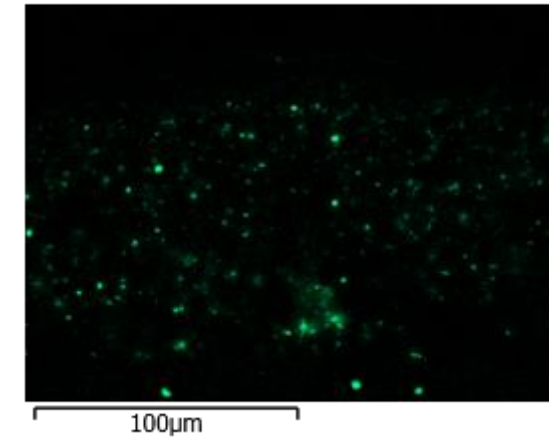
Sb L series



Mn K series



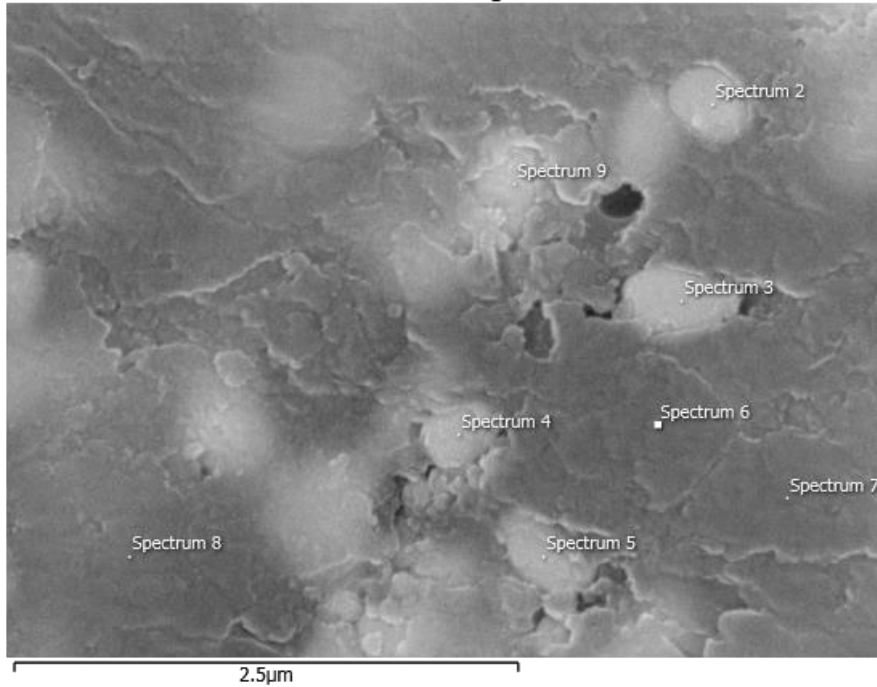
Si K series



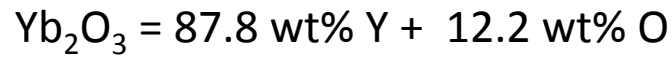
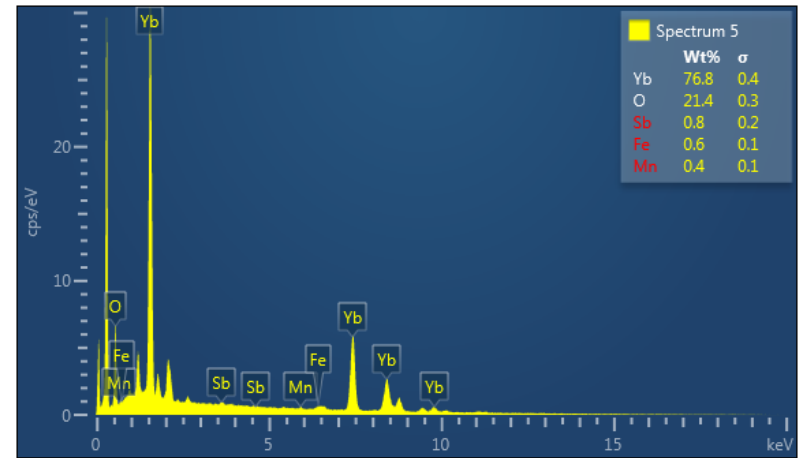
- No Si in the outer layer, but Si in the cloud of particles
 - Need further investigation to understand this
- No Al and Zn detected in the coating by EDS – presumably dissolved in the substrate

Particles on the Uncoated Side

Electron Image 8

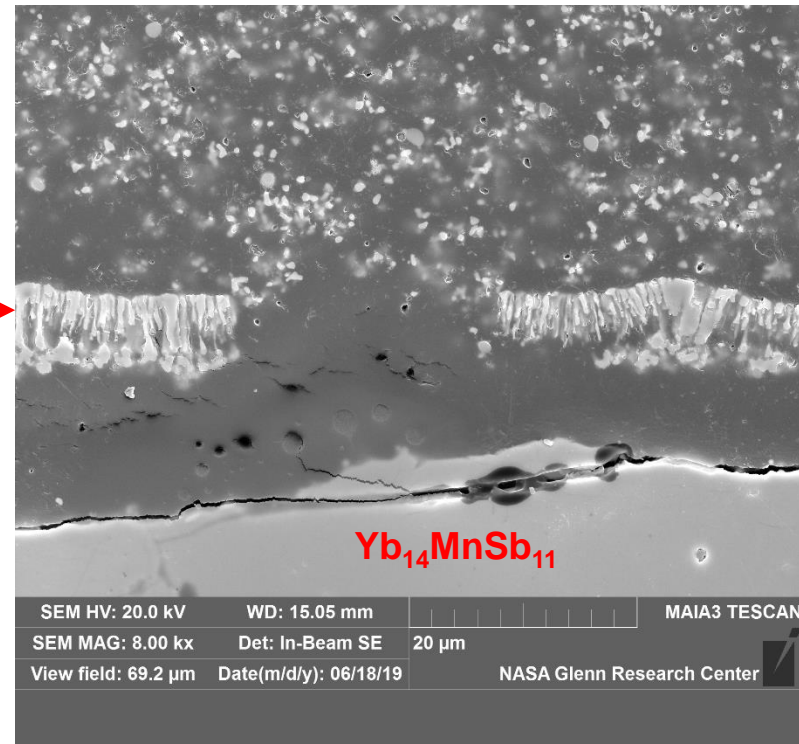
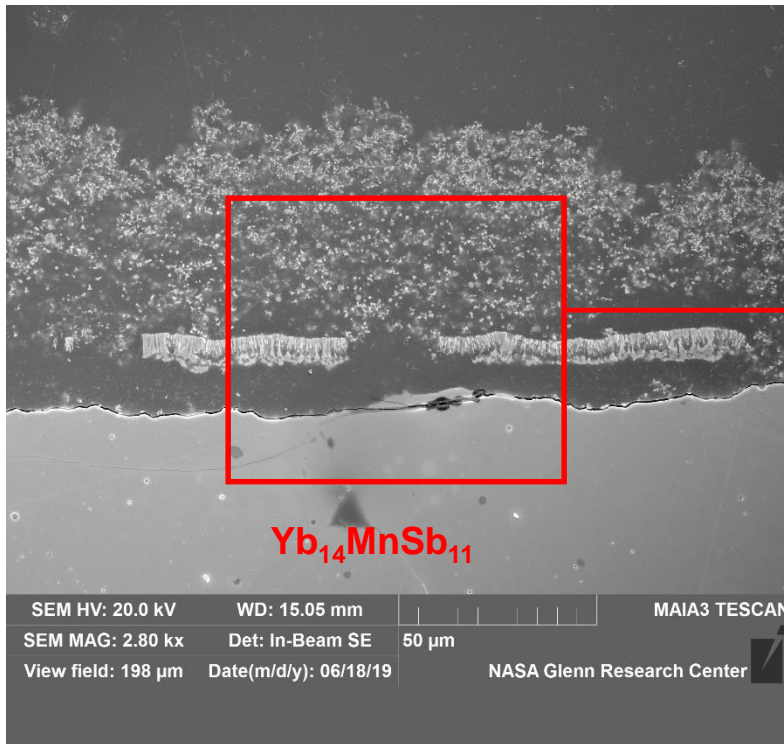


Spectrum 2, 3, 4, 5, 9

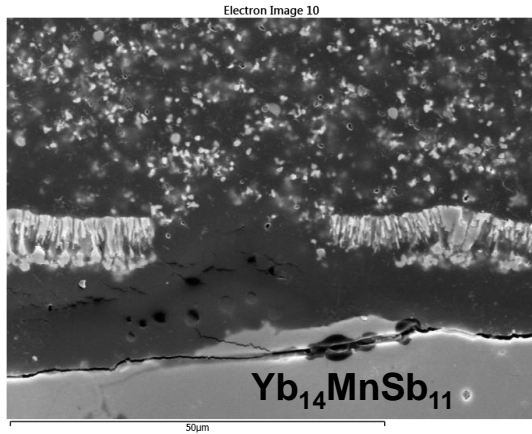


- Particles are likely Yb_2O_3

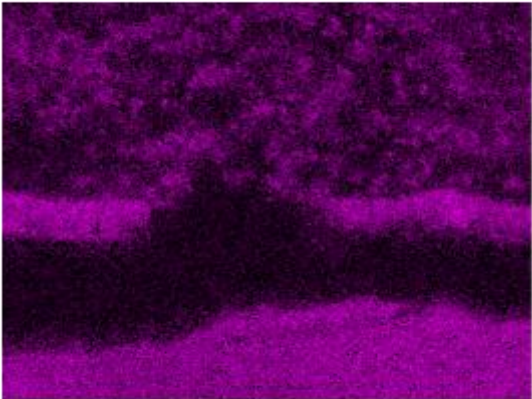
YSZ ($\text{ZrO}_2 + 7 \text{ wt\% Y}_2\text{O}_3$) + 2 wt% Al + 2 wt% Zn



- YSZ coating is buried in the cloud of particles

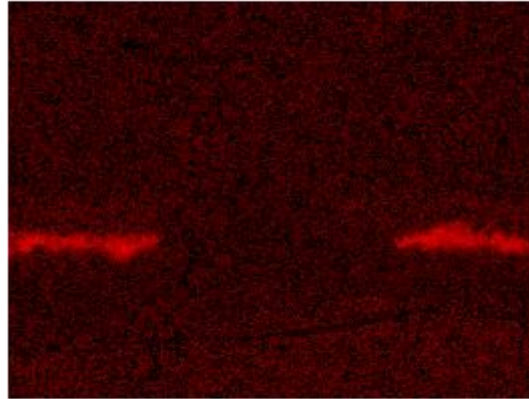


Yb L series



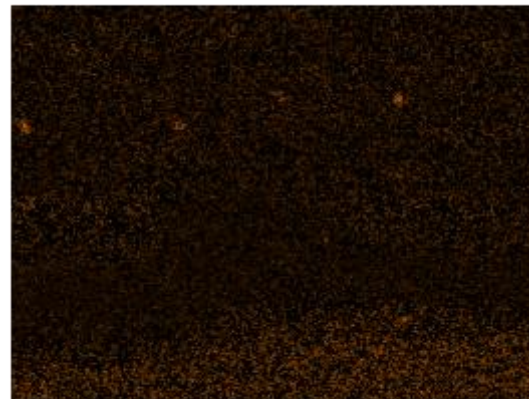
50µm

Zr L series



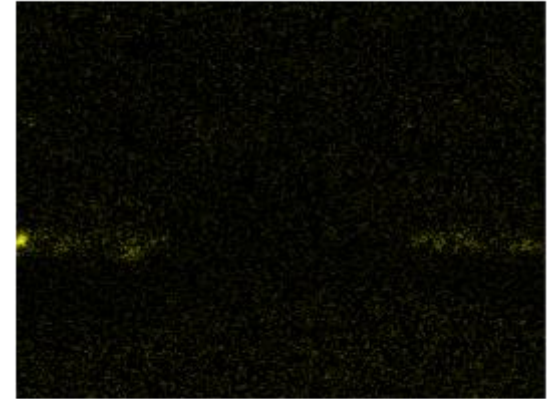
50µm

Mn K series



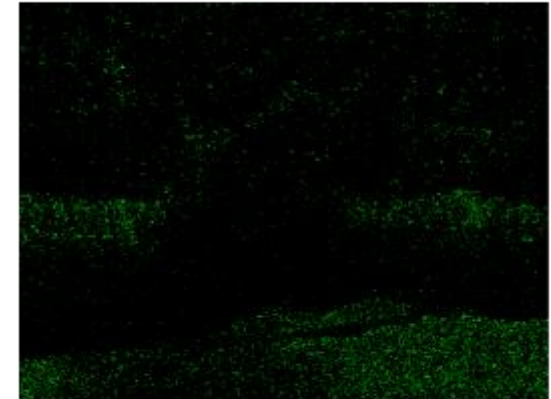
50µm

Y L series



50µm

O K series



50µm

- Yb_2O_3 layer grew on YSZ layer
- Cloud particles is Yb_2O_3

$\text{Yb}_2\text{SiO}_5 + 2 \text{ wt}\% \text{ Al}$



Sintering in vacuum ($10^{-6} \sim 10^{-7}$ Torr)

- Ramp to 700°C (4°C/min)
- Dwell at 700°C for 3 hr
- Cool down to RT (5°C/min)

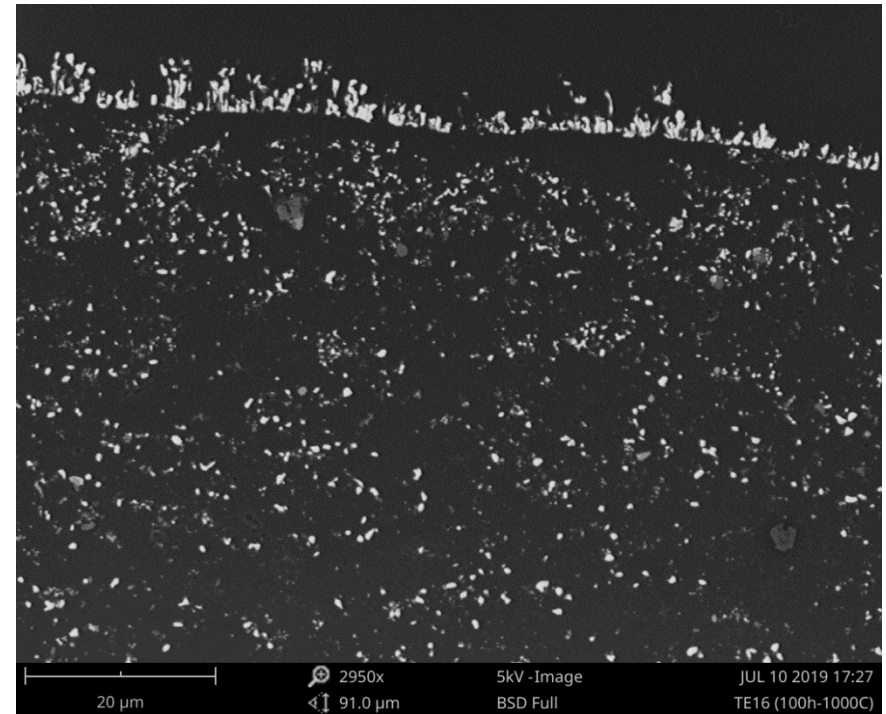
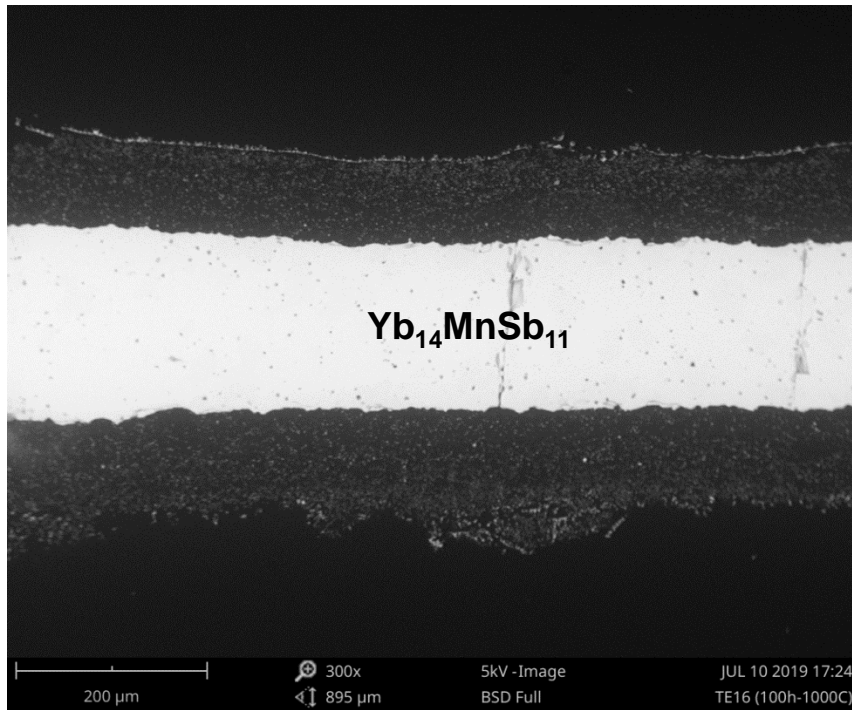


Oxidation in vacuum ($10^{-6} \sim 10^{-7}$ Torr)

- Ramp to 1000°C (4°C/min)
- Dwell at 1000°C for 100 hr
- Cool down to RT (5°C/min)

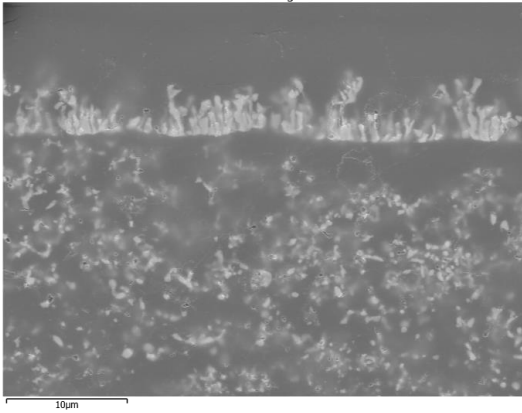
- Coating stayed on after 100h / 1000°C exposure, however, it was friable

$\text{Yb}_2\text{SiO}_5 + 2 \text{ wt}\% \text{ Al}$ after Oxidation

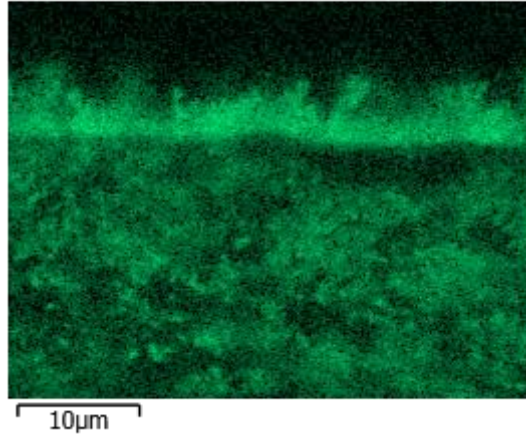


- Similar microstructure to Yb_2SiO_5 coating with Al + Zn sintering aid

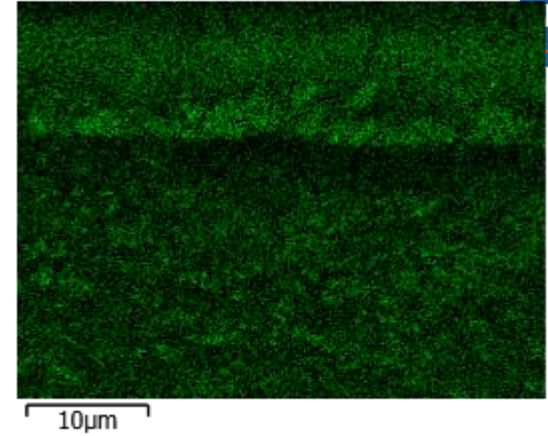
Electron Image 5



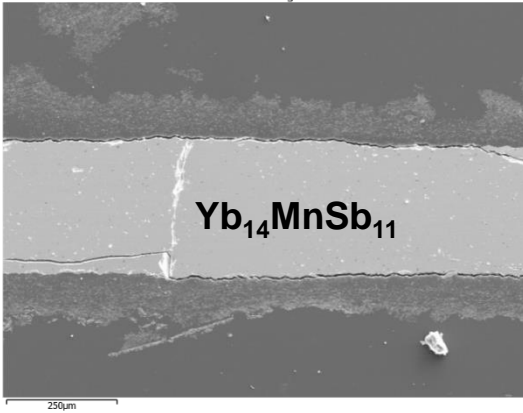
Yb L series



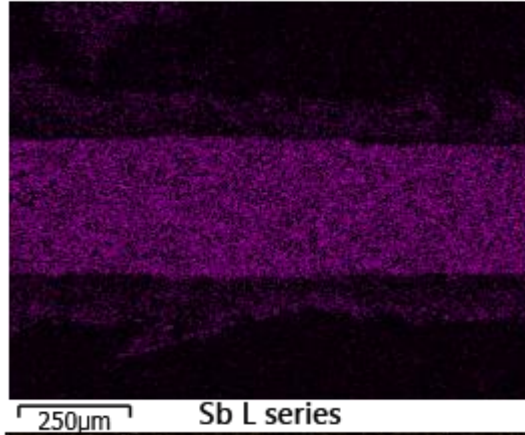
O K series



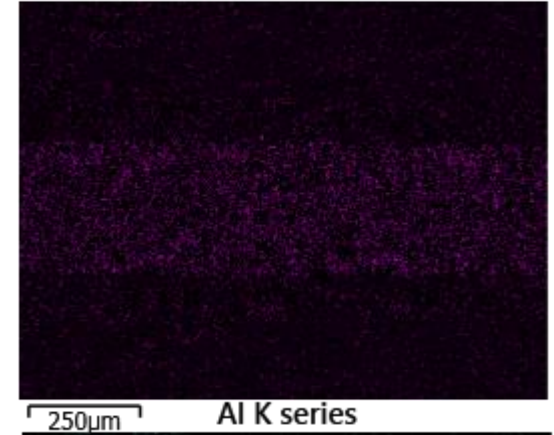
Electron Image 1



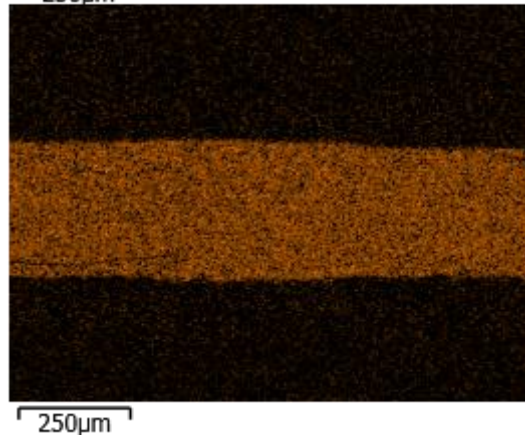
Yb L series



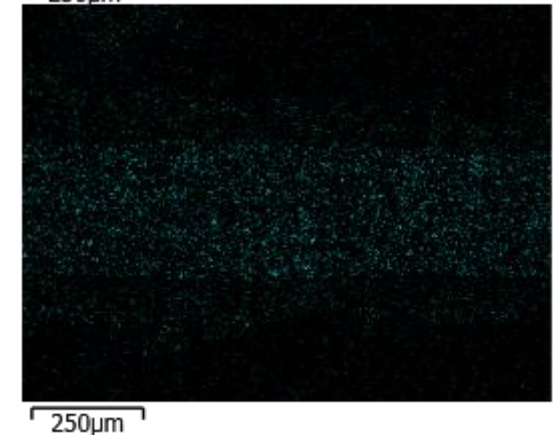
Mn K series



Sb L series



Al K series



- No Al in the coating detected by EDS
- Al presumably dissolved in the substrate

Conclusion

- $\text{Yb}_{14}\text{MnSb}_{11}$ requires sublimation protection coating to be useful as a thermoelectric material for next gen Radioisotope Thermoelectric Generator (RTG)
- Rare oxides, rare earth silicate, and $\text{ZrO}_2 + 7 \text{Y}_2\text{O}_3$ (YSZ) are promising coating candidates because they are chemically compatible with the substrate
 - Yb_2O_3 is very stable, due to its very low free energy of formation, however, is friable, causing the coating to debond
 - Debonded coating was weak and friable, presumably because Al and Al + Zn are not effective sintering aids as they dissolve into the substrate
- Alternative sintering aids that do not react with the substrate required
- Even with a better sintering aid, debonding may be unavoidable due to the weak and friable nature of Yb_2O_3 oxide
 - Alternative strategy is to develop a coating with strong cohesive strength that can be physically harnessed to the substrate to mitigate sublimation



Acknowledgements

- Wayne Jennings (NASA Glenn) – SEM analysis