

Characterizing Damage Accumulation in CMCs

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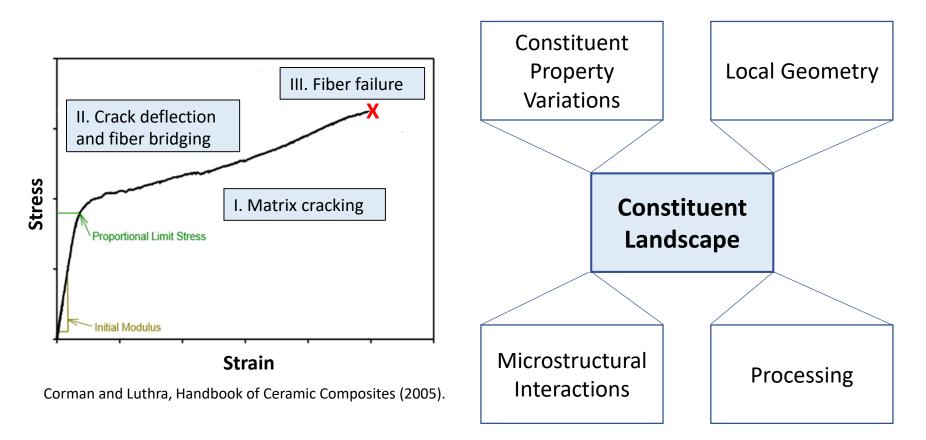
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CMC Damage Behavior is Influenced by Constituent Landscape Effects

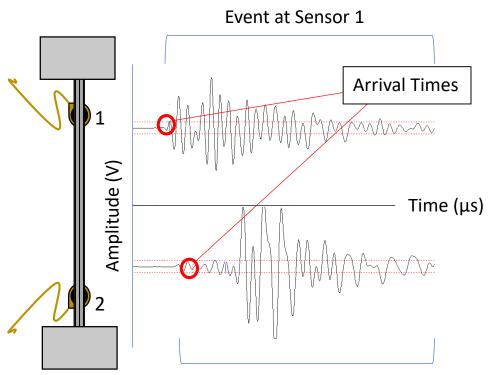
Hypothesis: Locally averaged structural features are significant drivers in the manner in which damage accumulates, moves, and interacts





Acoustic Emission (AE) Enables Real-Time Damage Assessment

AE can be used to locate event sources and characterize damage in the bulk





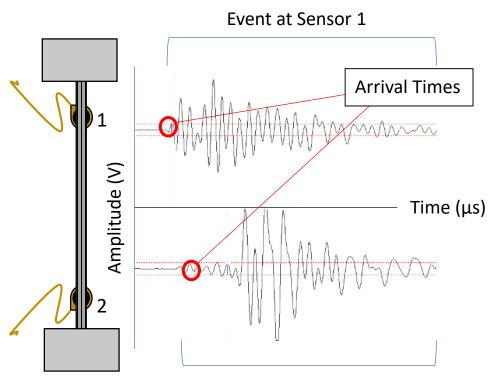
$$Location = \frac{x}{2} \cdot \left[\frac{\Delta t}{\Delta t_x}\right]$$

x = sensor separation
 Δt = arrival time difference
 Δt_x = difference in arrival times
across AE window



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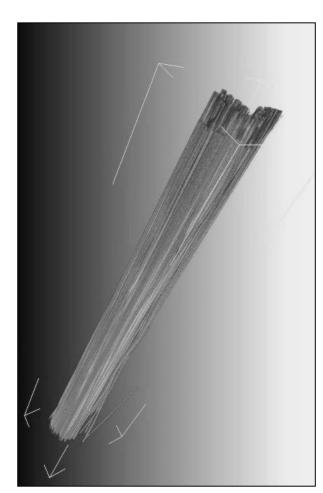
Event at Sensor 2

Advantages

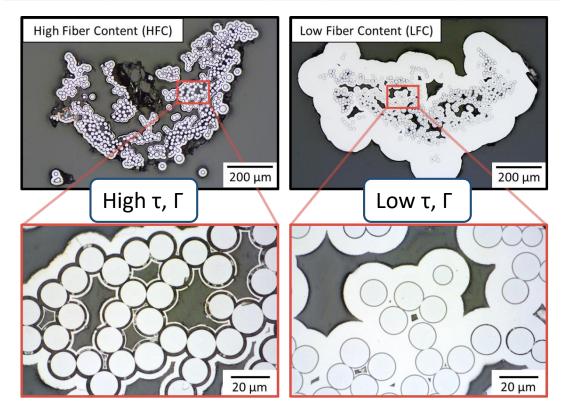
- In-operation monitoring
- Damage localization
- Volumetric inspection
- Early detection of damage



Minicomposites Provide Simplified Architecture Suited to Study Microscale Damage



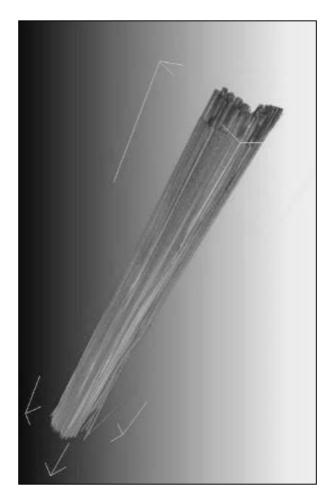
Specimen ID	BN Thickness (μm)	V _f (%)	V _{BN} (%)	V _m (%)	Area (mm²)
HFC	1.9 ± 0.6	33.5	24.6	41.8	0.167
LFC	0.3 ± 0.08	21.3	2.2	76.5	0.266



Courtesy of Richard Rauser (GRC)

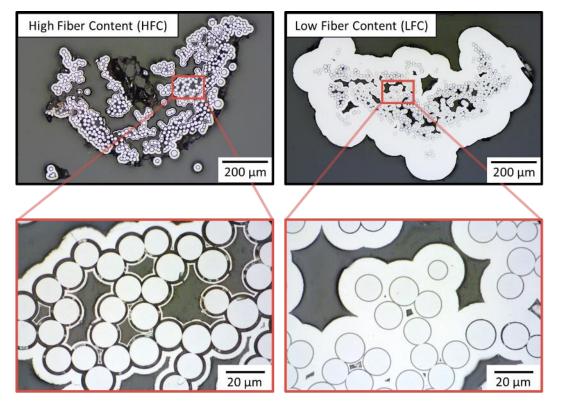


Minicomposites Provide Simplified Architecture Suited to Study Microscale Damage



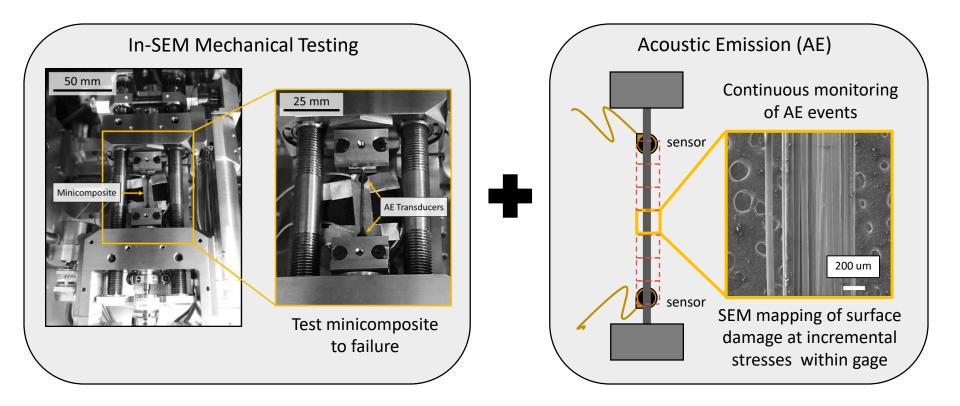
Courtesy of Richard Rauser (GRC)

Specimen ID	Sliding Stress (τ)	Debond Toughness (τ)
HFC	34.5 ± 13.0 MPa	5.5 ± 3.9 J/m ²
LFC	18.1 ± 4.8 MPa	$1.2 \pm 0.5 \text{ J/m}^2$



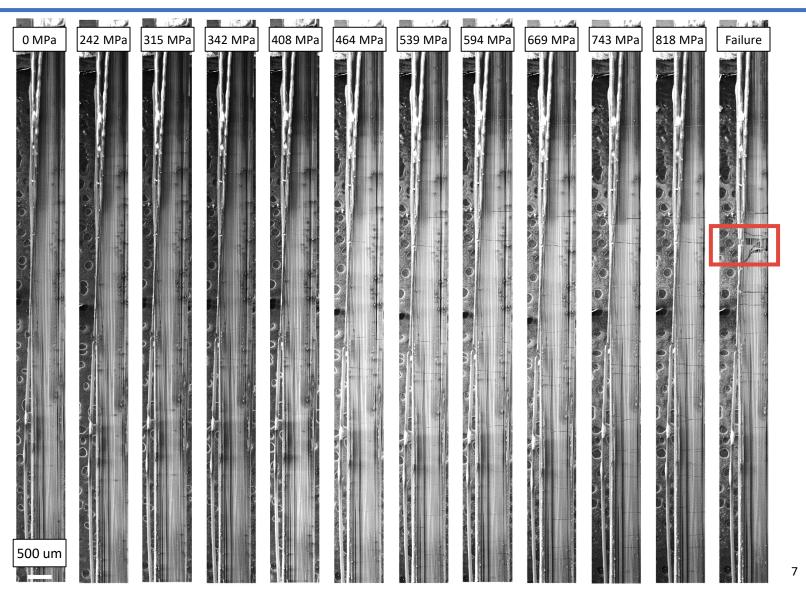


A Multi-Modal Approach for Damage Characterization



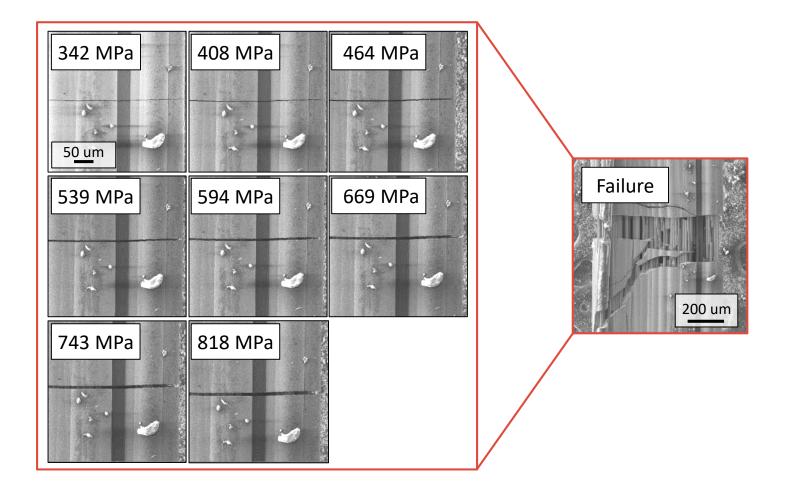


Incremental Loading to Capture Damage Progression





Incremental Loading to Capture Damage Progression





Two Domains: Matrix-Dominated and Fiber-Dominated Damage

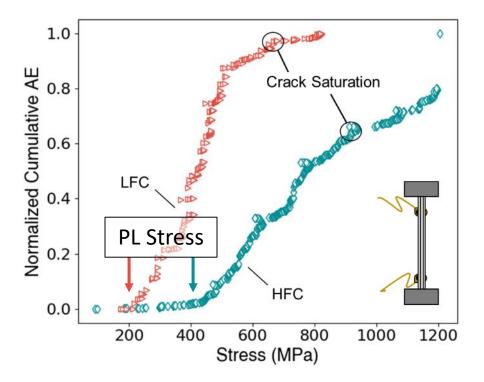
Matrix-Dominated Damage

- Matrix crack initiation
- Matrix crack propagation
- Interfacial debonding
- Fiber sliding
- Early fiber failures

Crack Saturation

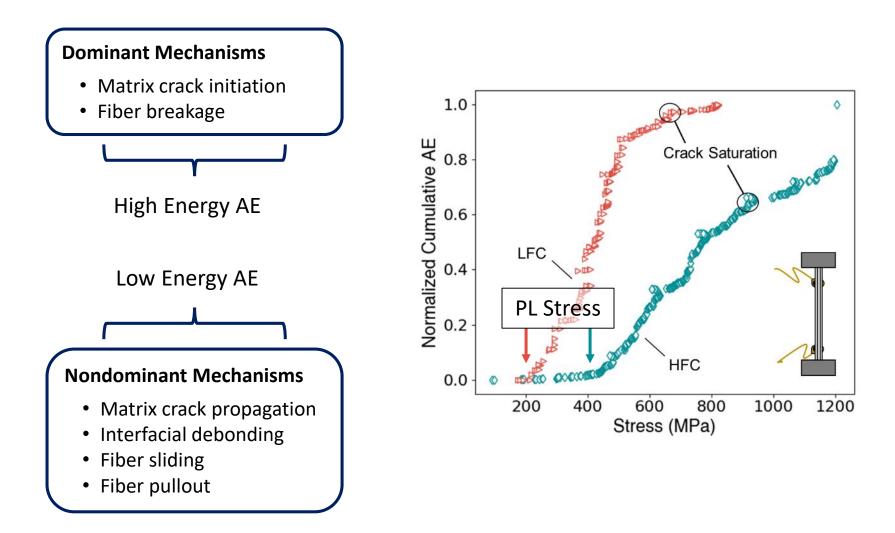
Fiber-Dominated Damage

- Fiber loading
- Fiber sliding
- Fiber breakage
- Fiber pullout



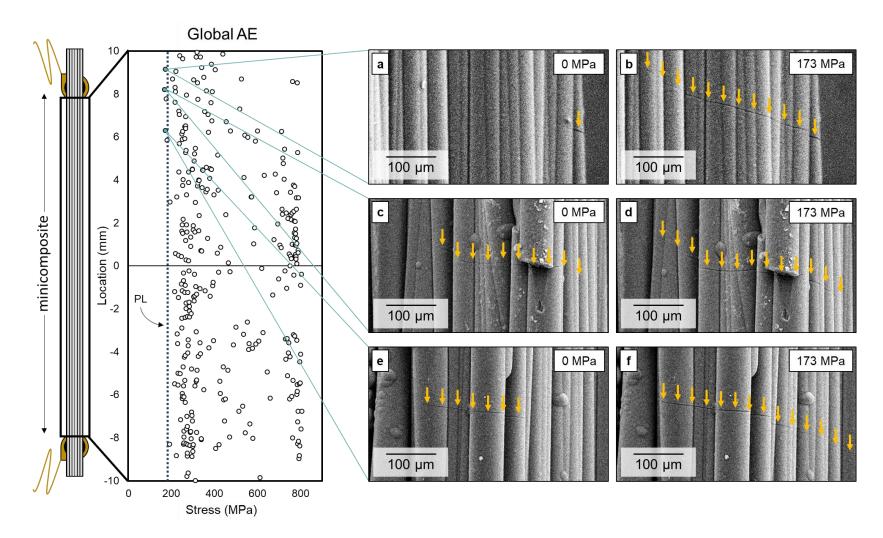


Two Domains: Matrix-Dominated and Fiber-Dominated Damage



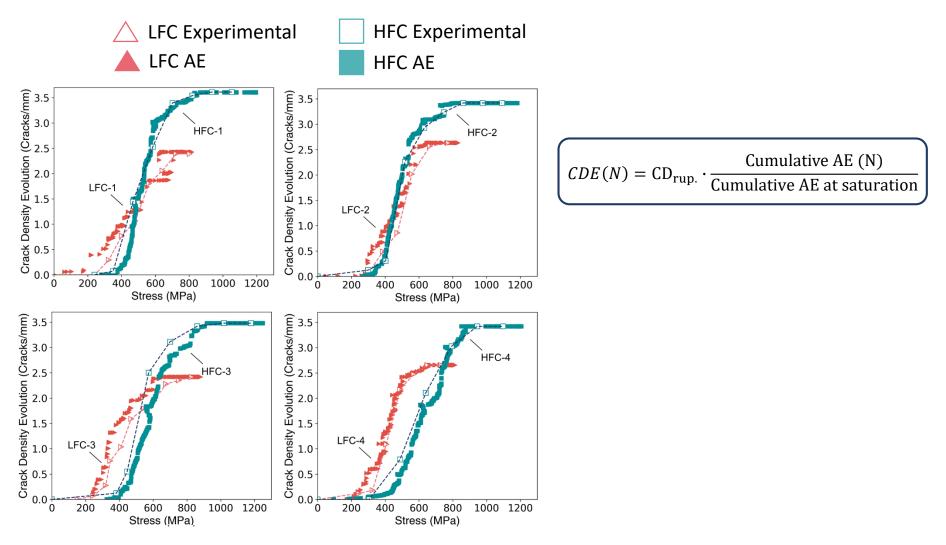


Damage Accumulation below PL due to Propagation of Flaws



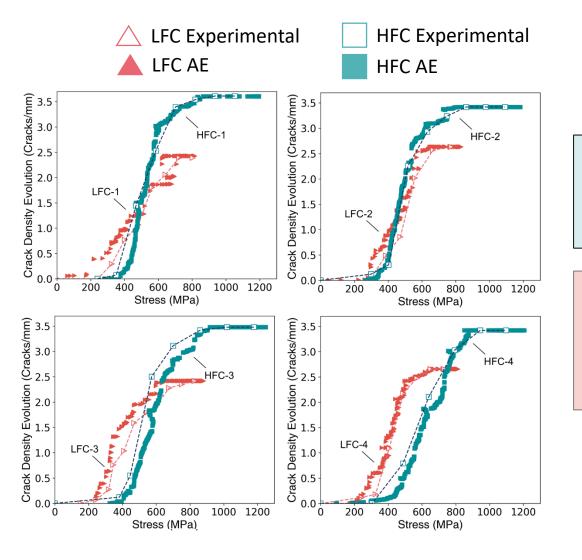


Agreement between In-SEM Measured and AE-Predicted Crack Density Evolution





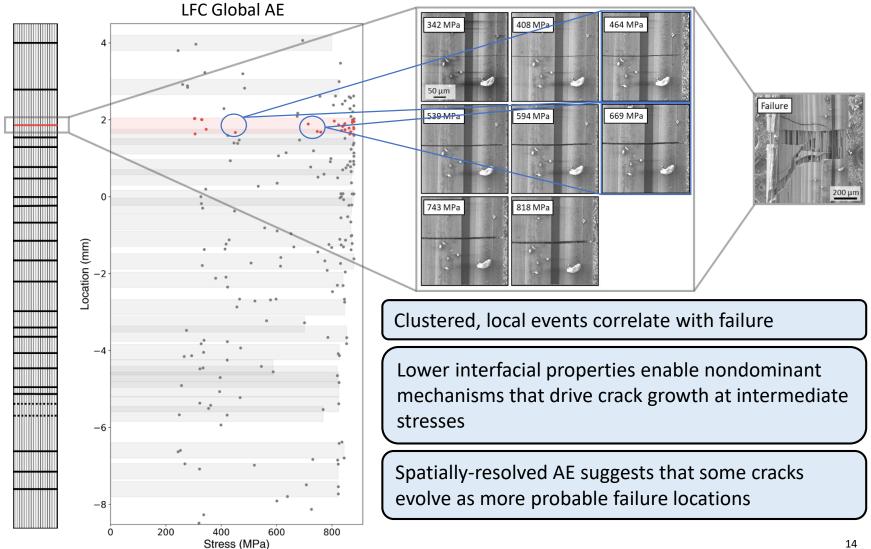
Agreement between In-SEM Measured and AE-Predicted Crack Density Evolution



- Agreement at early and intermediate stresses shows transverse matrix cracking dominance
- Agreement at early stresses shows transverse cracking
- Variations in real and predicted response[s] due to other phenomena detected by AE

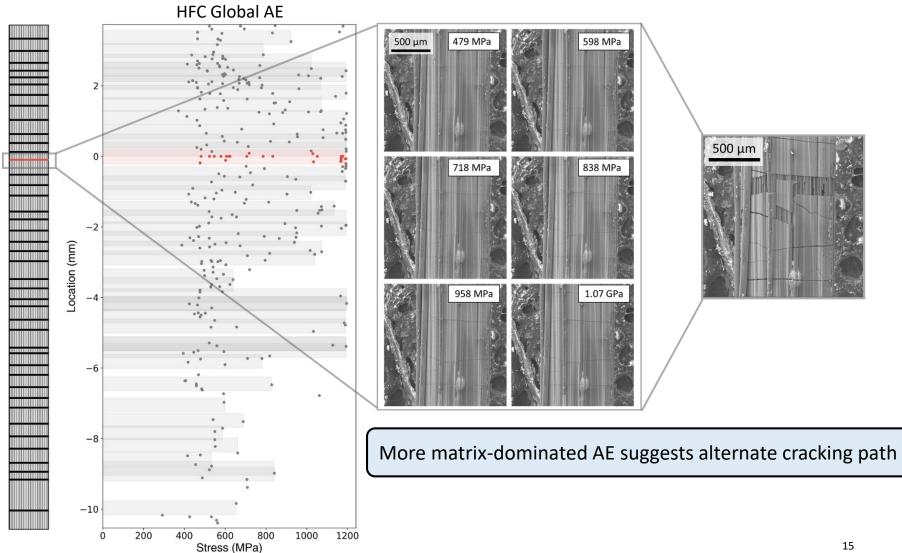


Correlation of Spatially-Resolved AE and In-SEM Observed Damage



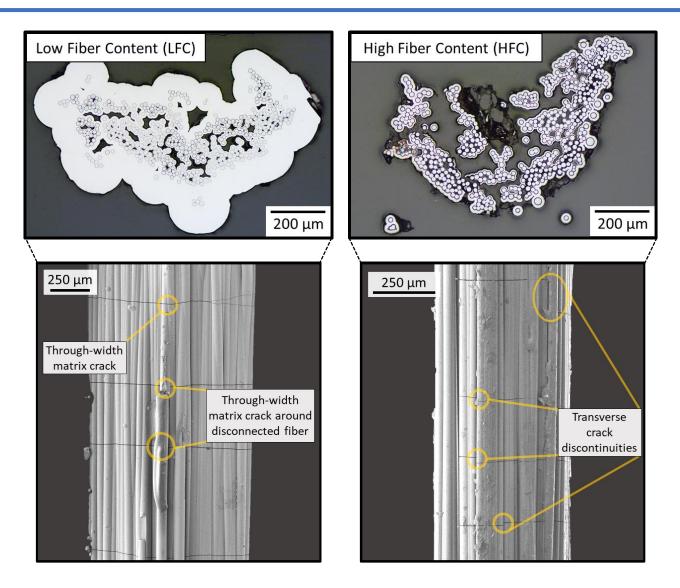


Correlation of Spatially-Resolved AE and In-SEM Observed Damage





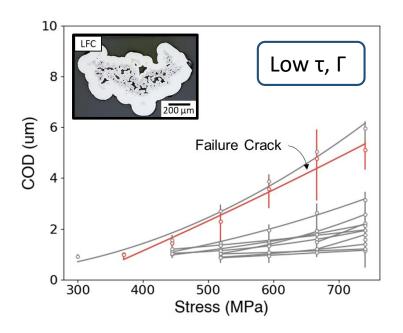
Incremental vs. Through-Thickness Crack Propagation



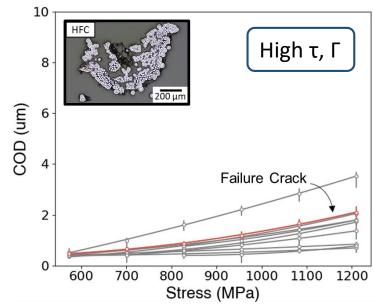


Local Microstructural Effects Influence Crack Opening Displacement (COD)

- Earliest crack openings: 600 nm
- Fiber sliding w/ larger debond lengths to accommodate opening
- Saturation of non-dominant phenomena prior to fiber breaks
- Fiber breaks redistribute load to tow



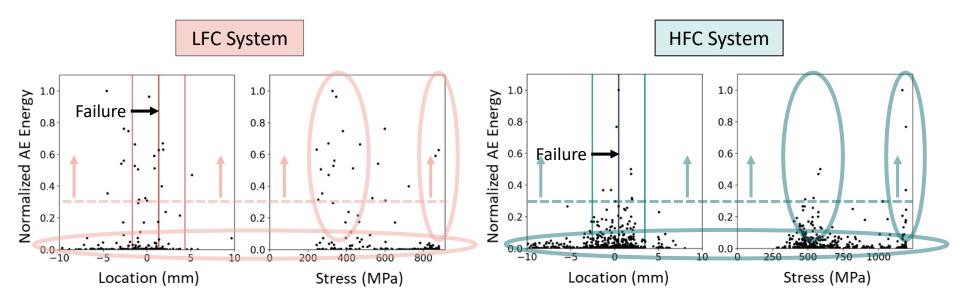
- Earliest crack openings: 300 nm
- High fiber content for initial crack bridging
- Fiber breaks redistribute load to pillar
- Fiber reloading through sliding





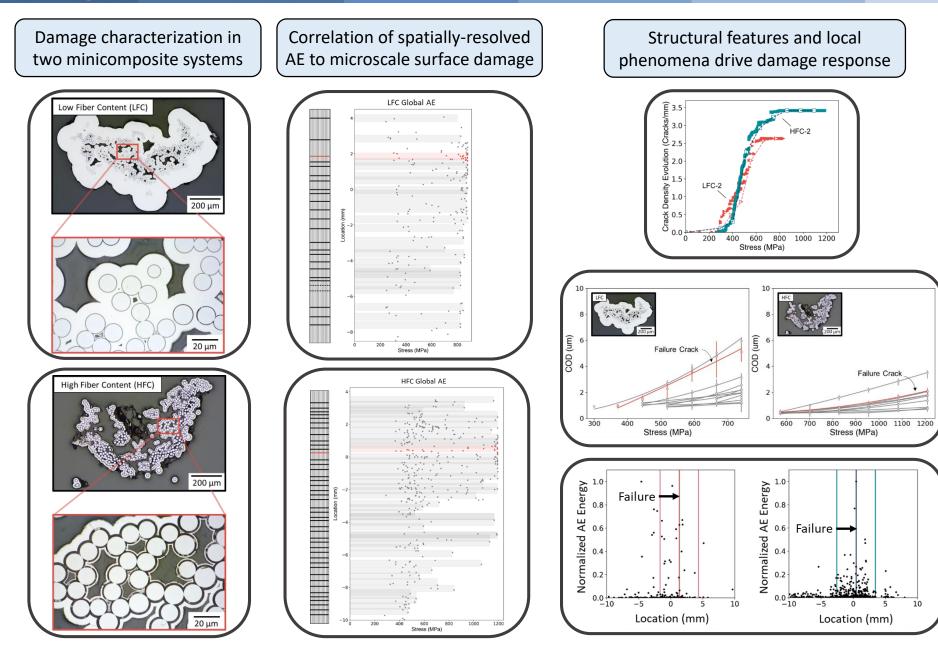
AE Event Energy May Correlate with Source Damage Mechanism

Correlation between high-energy AE and proximity to failure location



- High-energy AE activity from dominant damage mechanisms (matrix cracking / fiber breakage)
- Ultra-high-energy AE activity from large crack formation
- Low-energy AE activity from nondominant damage mechanisms





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