

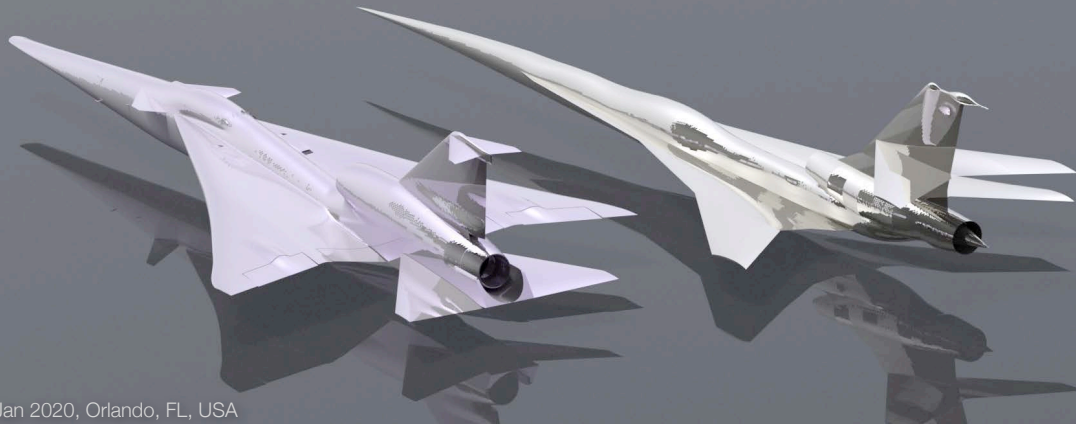
3rd AIAA Sonic Boom Prediction Workshop

# sBOOM Propagation for the Third AIAA Sonic Boom Prediction Workshop



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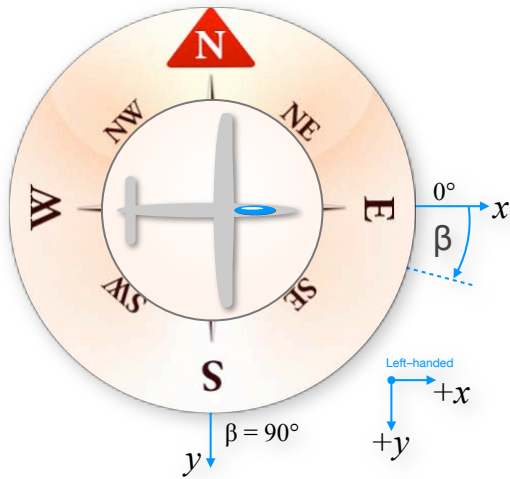
## Overview



- Preliminaries
  - Conventions & propagation primer
  - Mesh Convergence & oversampling
- Results for Cases 1 & 2
  - Ground signals for Standard Atm. & Required Atm.
  - Cutoff angles
  - Carpet noise metrics
  - Ground Intercepts, boom carpets & raytubes
- Summary & observations



# Wind Convention in sBOOM

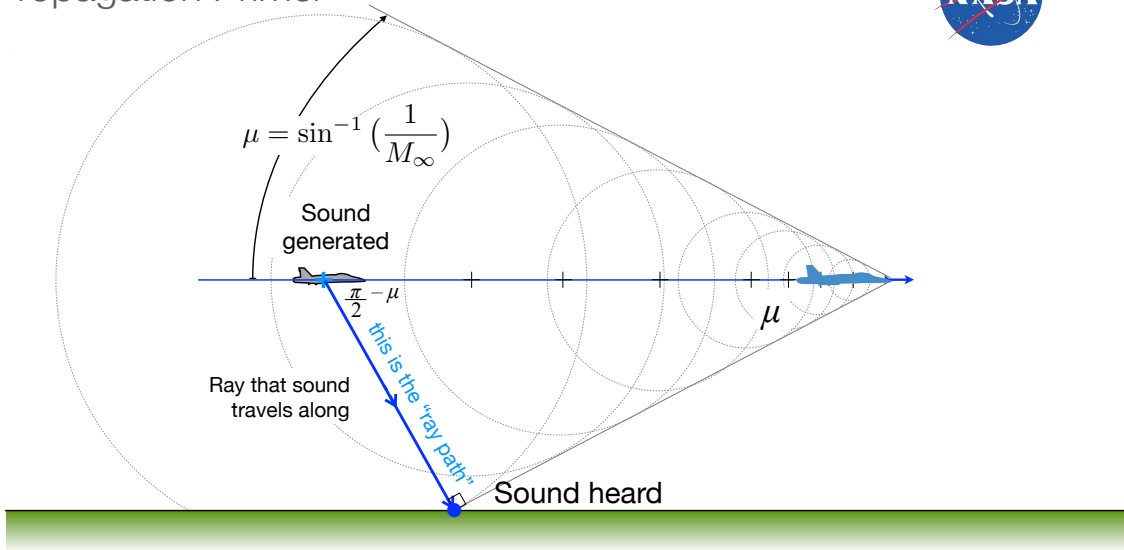


- sBOOM wind uses *left handed coord. sys.*
- $\beta$  = heading
- $\beta = 0^\circ$  A/C pointed East, cw+
- sBOOM wind tables are in meters vs m/s
- $x$  and  $y$  are wind components (“blows toward”)
  - $(x, y) = (1, 0)$  is tail wind if heading is East
  - ↓  $(x, y) = (0, 1)$  is tail wind if heading is South
  - ↘  $(x, y) = (1, 1)$  is tail wind if heading is SE

- Workshop has aircraft flying E,
  - This is  $0^\circ$  heading in sBOOM

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# Propagation Primer



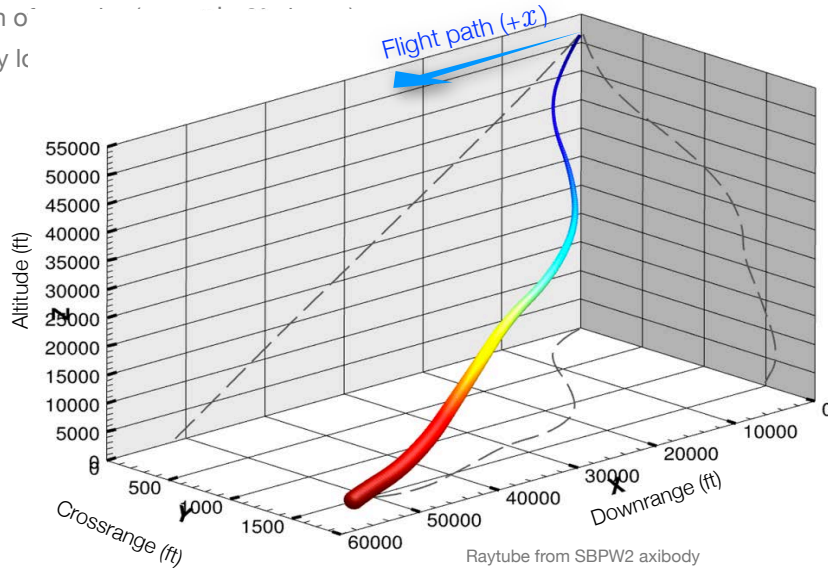
- Quasi-1D integration of Burger’s equations occurs in tube along the ray path
- Determines the ground intercept of sound emanating from given trajectory point & azimuth
- Ray path determines time required for signal propagation

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## Wind Effects

- Only consider crossrange and downrange winds (no up/down drafts)
- Wind can alter path of
- Paths are scaled by  $k$



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## Mesh Convergence

Sensitivity of noise output to discretization of near field signal

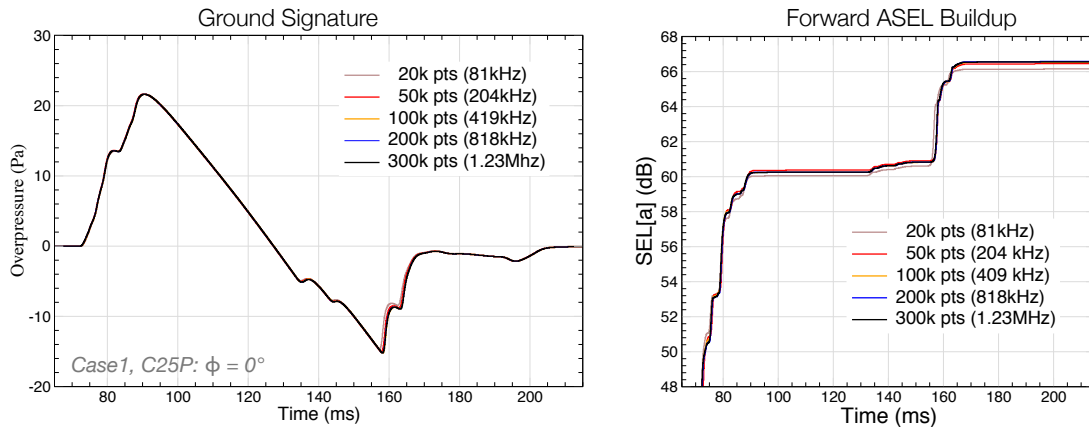
- Propagation code is solving augmented Burgers' via finite difference
- Need to make sure loudness metrics are sufficiently mesh converged
  - Mesh convergence of propagation is case dependent ( on signal, azimuth & atm.)
  - Mesh refinement study done for each near field signal (using Std. and Req'd. Atm.'s)
- Truncation error directly impacts accuracy, resolution requirements are driven by need to minimize error in propagation
  - Initial signal typically has < 2000 points
  - Propagation typically requires 40000-100000 points (oversampled by 20-50x)
  - Discrete ASEL filter can be poorly behaved at high sampling frequencies (> ~250kHz)
    - *this limits maximum allowable oversampling*
- How much accuracy is needed?
  - Atmospheric variability generally 2-5 dB, but may be ~10 dB in some cases
  - Generally tried to keep propagation error under  $\pm 0.2$  dB

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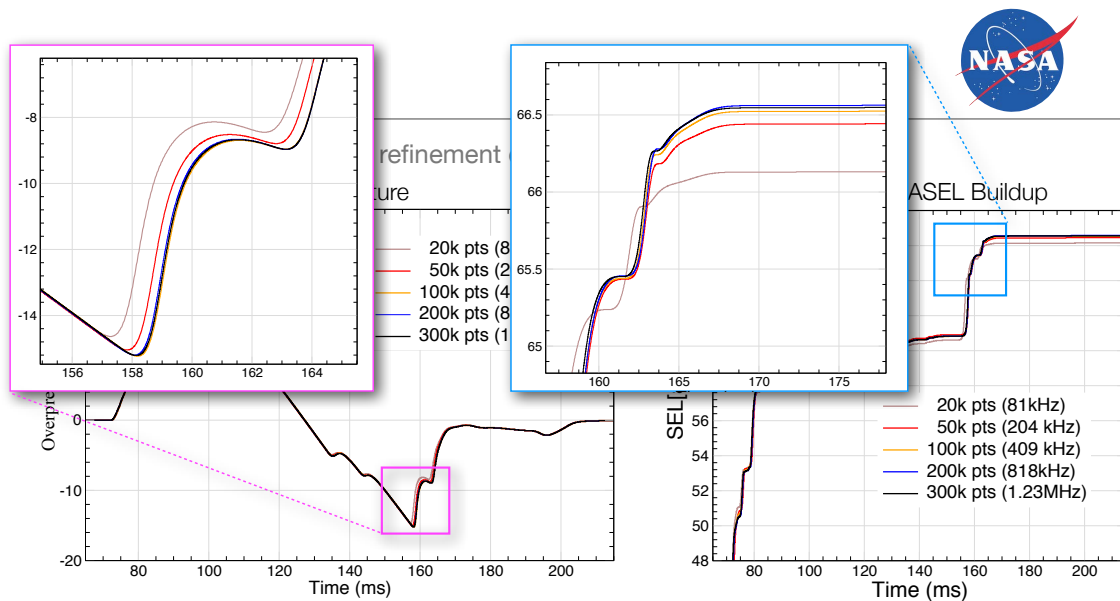
# Mesh Convergence

Sensitivity of noise outputs to refinement of the propagation mesh



- C25P signals at  $\phi = 0^\circ$ , using from 20k 300k points (80-1230 kHz) for propagation
- Despite similarities in ground signal, mesh convergence of ASEL is quite slow

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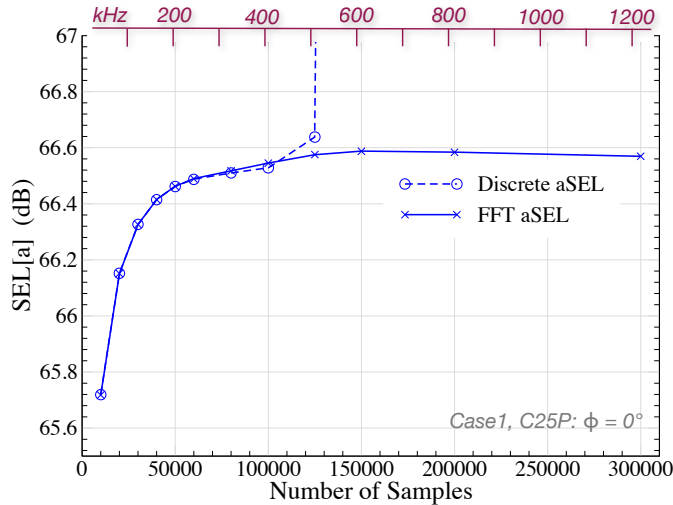
- C25P signals at  $\phi = 0^\circ$ , using from 20k 300k points (80-1230 kHz) for propagation
- Despite similarities in ground signal, mesh convergence of ASEL is quite slow

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# Mesh Convergence

Convergence ASEL noise metric with sampling frequency



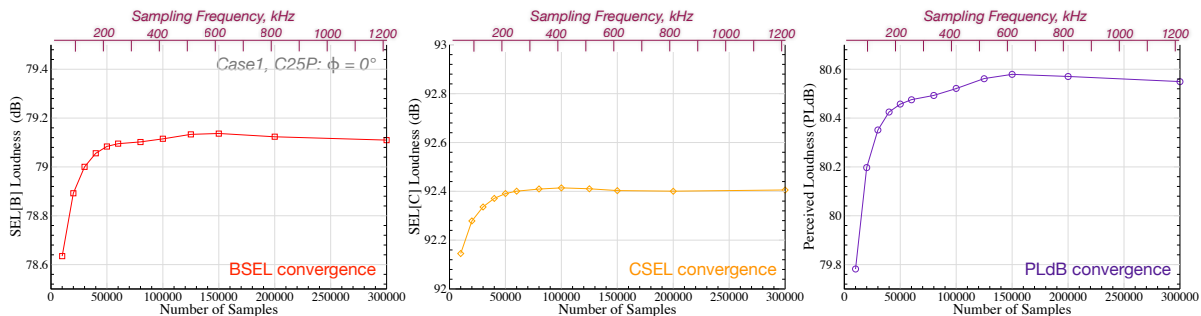
- ASEL converges slowly
  - Need ~600kHz (~150k pts) to converge ASEL to  $\pm 0.01$ dB
- However, discrete ASEL filter starts to have issues at ~250kHz, and blows up ~500kHz
- On this case (C25P) hard to guarantee ASEL error  $< \pm 0.1$ dB
- Discrete BSEL and CSEL remain well behaved till ~1 & 10 MHz (respectively), so generally easier to mesh converge

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# Mesh Convergence

Convergence of BSEL, CSEL & PLdB noise metrics with sampling frequency



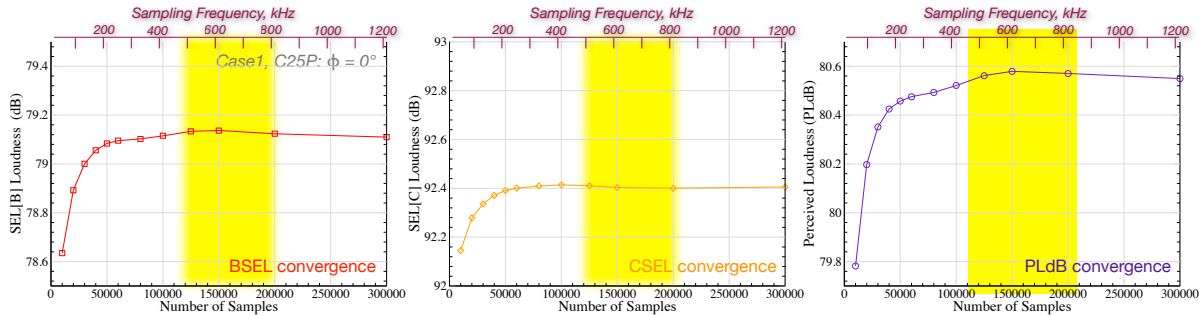
- BSEL, CSEL and PLdB all show good mesh convergence (all on 1 dB scale)
- FFT used for all metrics except for BSEL, but appears to be well behaved
- C-weighting converges fastest ( $\pm 0.02$  dB @ 200kHz)
- PLdB converges slowest (approx.  $\pm 0.1$  dB @ 200kHz)

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# Mesh Convergence

Convergence of BSEL, CSEL & PLdB noise metrics with sampling frequency



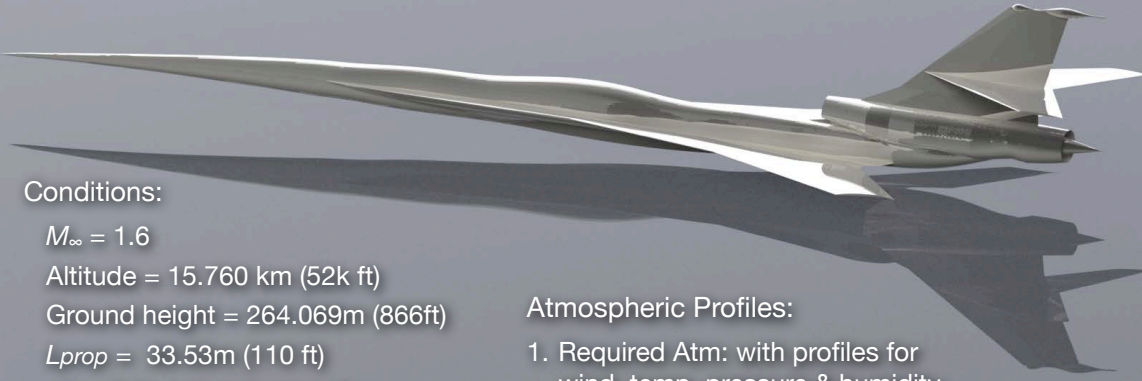
- To avoid excessive discretization error in propagation used 500-800kHz sampling frequencies for all workshop cases
- Computed noise metrics with FFT in LCASB (*adloud*) for ASEL, CSEL and PLdB noise metrics
- Used digital BSEL filter in sBOOM (well behaved at 500-800kHz)

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## Case 1: C25P

Powered version of the NASA Concept 25D



Conditions:

- $M_\infty = 1.6$
- Altitude = 15.760 km (52k ft)
- Ground height = 264.069m (866ft)
- $L_{prop} = 33.53\text{m}$  (110 ft)
- $r/L = 3.0$  at signal extraction
- Ground reflection factor = 1.9
- Heading East ( $\beta = 0^\circ$ )

Atmospheric Profiles:

1. Required Atm: with profiles for wind, temp, pressure & humidity
2. Standard Atmosphere

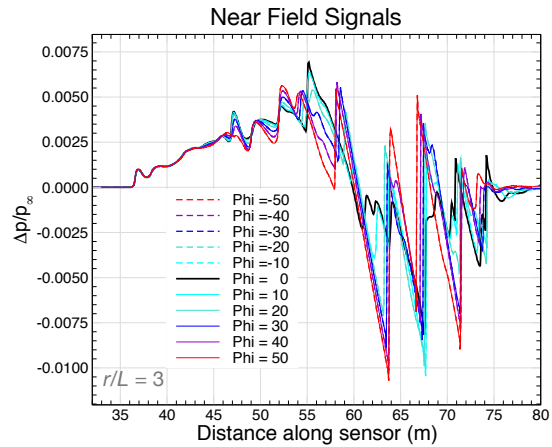
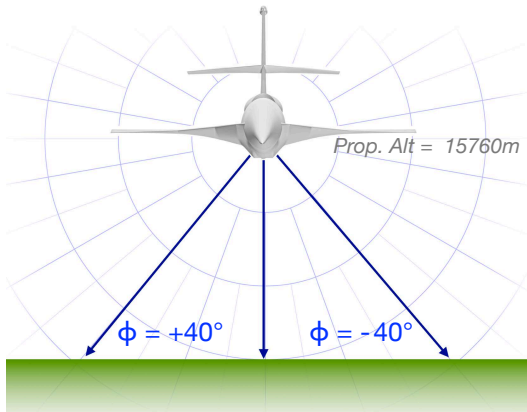
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## Case 1: C25P Standard Atmosphere

Near field and ground pressure signals

Sign Convention for Azimuth,  $\phi$



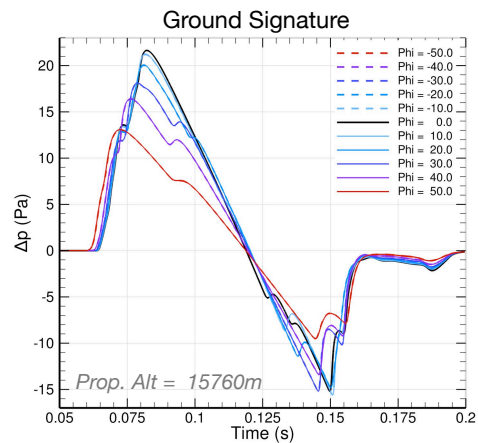
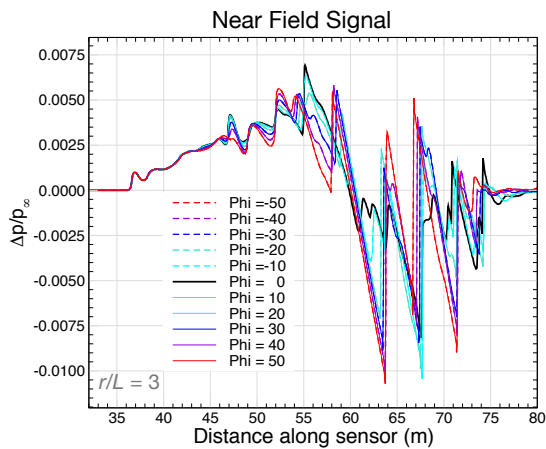
• Near field data provided for half-cylinder  $\{-90^\circ, 90^\circ\}$ ,  $\{-50^\circ, 50^\circ\}$  shown)

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## Case 1: C25P Standard Atmosphere

Propagation altitude = 15760m, ground height = 264m



• Near field data provided for half-cylinder  $\{-90^\circ, 90^\circ\}$ ,  $\{-50^\circ, 50^\circ\}$  shown)

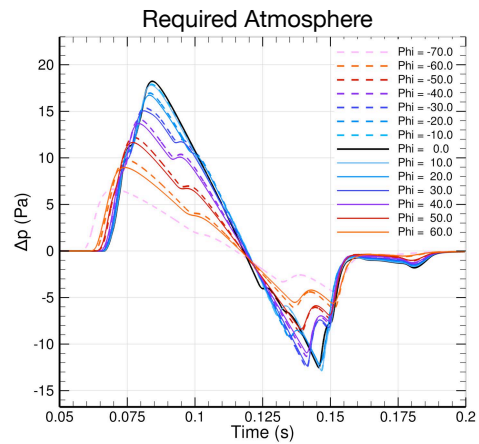
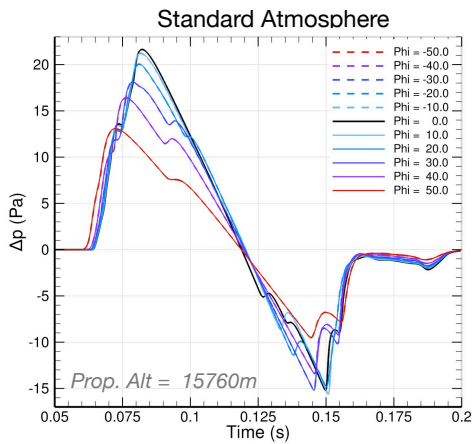
• Propagation shown used 500kHz sampling frequency (142k pts)

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## Case 1: C25P Ground Signatures

Propagation altitude = 15760m, ground height = 264m



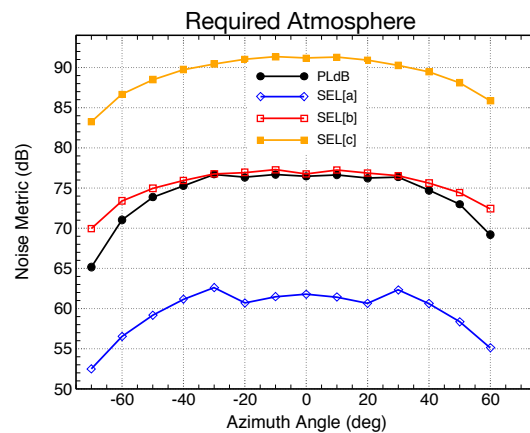
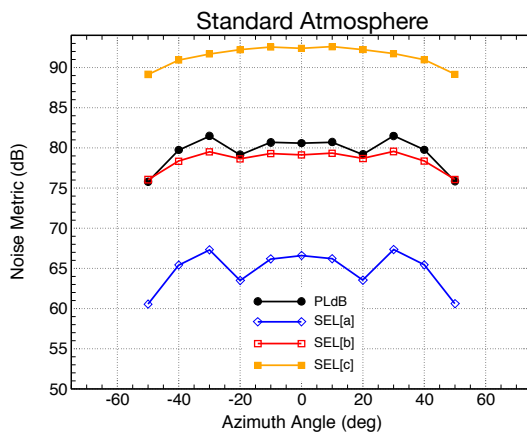
- Required Atm. has profiles of crosswind, temperature, humidity and pressure
  - Shows lots of asymmetry, and cutoffs are farther out on both sides

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## Case 1: C25P Ground Noise

Compare ground noise metrics across the carpet as a function of azimuth



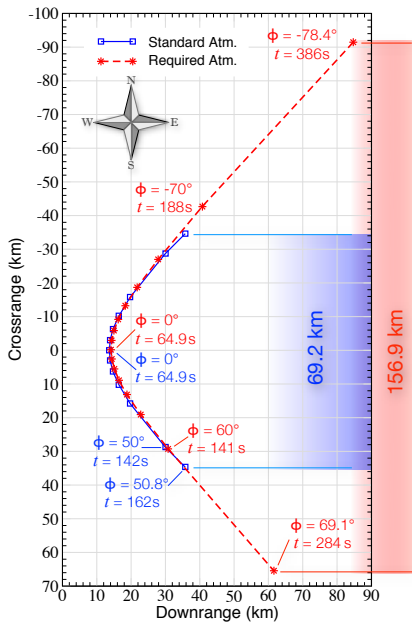
- Azimuthal range of carpet with real atm. is much wider than Standard Atm.
- Real atm. (with wind) reduces peak loudness by ~1dBA, ~0.5dBB, ~0.4dBC & ~0.7PLdB
- Noise at carpet edge drops, but can still be significant

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## Case 1: C25P Ground Carpet



### Project raytube ground intercepts on aircraft ground track

- Boom carpet computed from the intercepts of raytubes on the ground-plane projection of the trajectory. Showing both standard and required atmospheres
- Crossrange wind profile makes the required atm. asymmetric
- Cutoff angles: Std. Atm =  $[\pm 50.8^\circ]$ , Req. Atm =  $[-78.4^\circ, +69.1^\circ]$
- Long propagation distances near signal cutoff imply that these raytubes take a long time to reach the ground
  - Raytube for  $\phi = -78.4^\circ$  takes over 6 mins in Required atm.
  - Mesh convergence near signal cutoff is not nearly as good as at low azimuth angles
  - Higher discretization error due to much longer propagation
  - Propagation for signal cutoff used higher sampling frequency (800 kHz)
- Ground track for required atm is ~160 km, more than 2x as wide as standard atm. (~70 km)

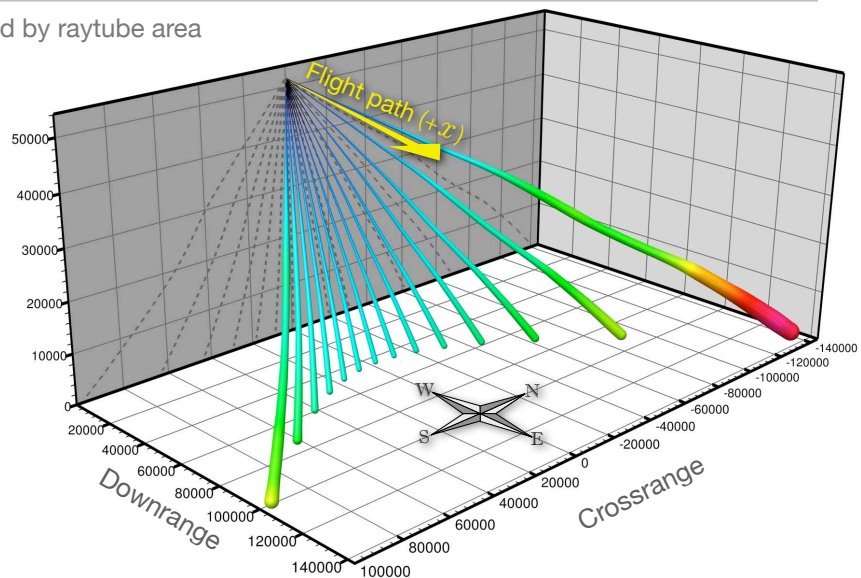
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## Case 1: C25P Raytubes for Required Atmosphere

Plot 3D raytubes colored by raytube area

- 3D plot of raytubes for real atmosphere
- Shows extremely long propagation times & large raytube areas near edges of the carpet



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## Case 2: C609

Preliminary design of X-59 Low Boom Flight Demonstrator



### Conditions:

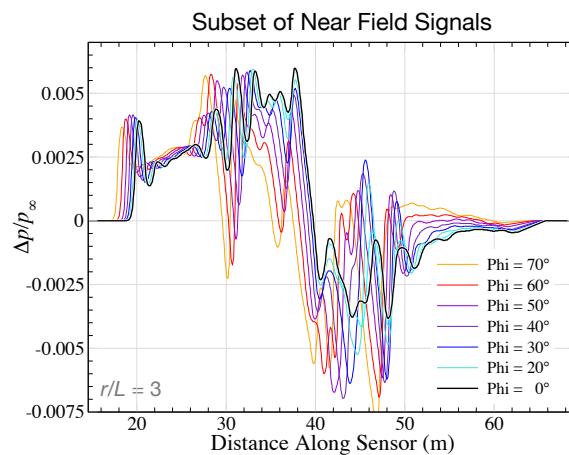
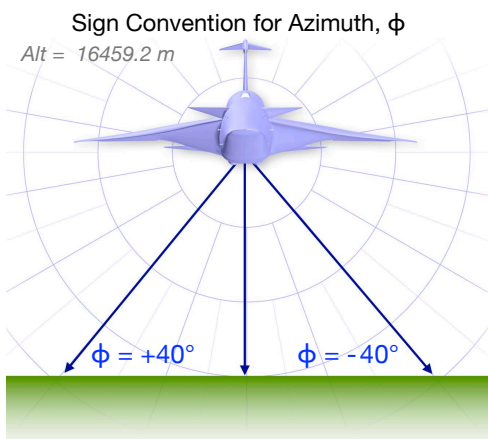
$M_\infty = 1.4$   
Altitude = 16.4592 km (54k ft)  
Ground height = 110.011 m (54k ft)  
 $L_{ref} = 27.43$  m (90 ft)  
 $r/L = 3$  at signal extraction  
Ground reflection factor = 1.9  
Heading East ( $\beta = 0^\circ$ )

### Atmospheric Profiles:

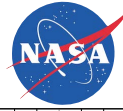
1. Required Atm: with profiles for wind, temp, pressure & humidity
2. Standard Atmosphere



## Case 2: C609 Near Field Signals

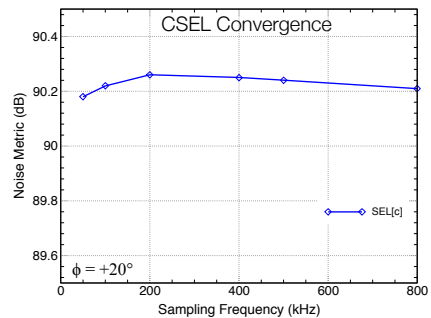
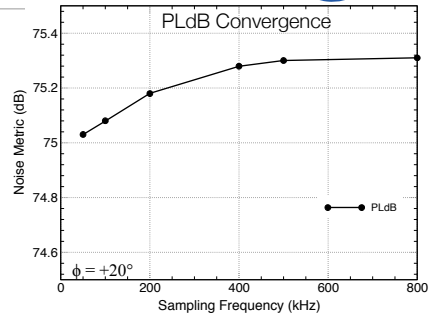
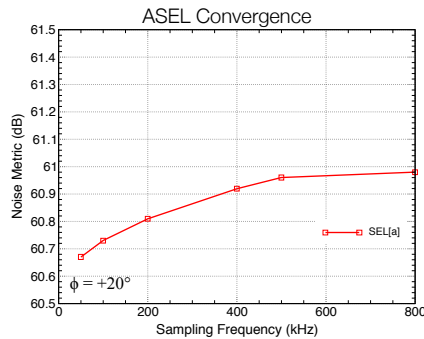


- Near field signals provided for 23 azimuths from  $-70^\circ$  to  $+70^\circ$   
 $\phi = [0, \pm 10, \pm 20, \pm 30, \pm 40, \pm 50, \pm 60, \pm 62, \pm 64, \pm 66, \pm 68, \pm 70]$
- Signals symmetric  $\pm \phi$



## Case 2: C609 Sampling Frequency

Metric convergence with sampling frequency (Std. Atm.)



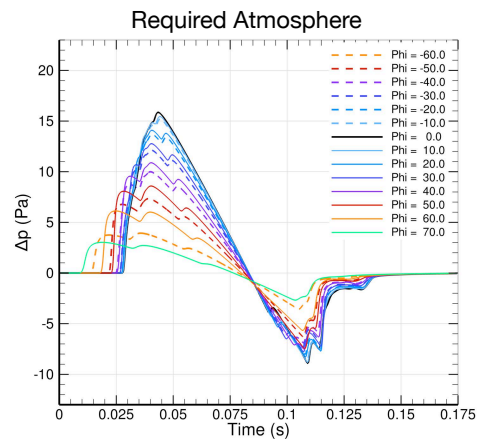
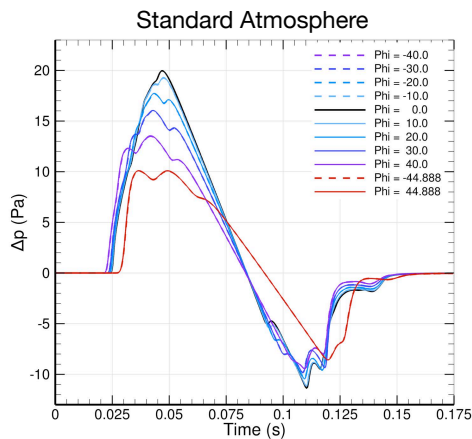
- Using FFT for metric computation get reasonable mesh convergence of ASEL, CSEL and PLdB by 500kHz.
- Discrete BSEL filter appears well behaved as well
- Similar mesh convergence behavior for other azimuths. Used 500kHz sampling frequency away from cutoff.

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## Case 2: C609 Ground Signals

Propagation altitude = 16460m, ground elevation = 110m



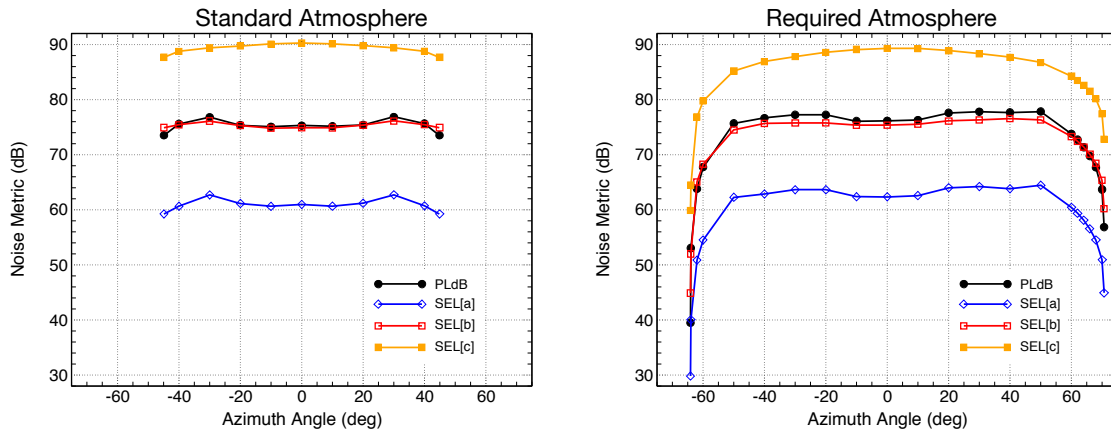
- Required Atm. includes profiles of crosswind, temperature, humidity and pressure
  - Very asymmetric, with much wider cutoffs on both sides
- Amplitude of ground signal in real atmosphere significantly reduced from Std. Atm.

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## Case 2: C609 Ground Noise

Compare ground noise metrics across the carpet as a function of azimuth

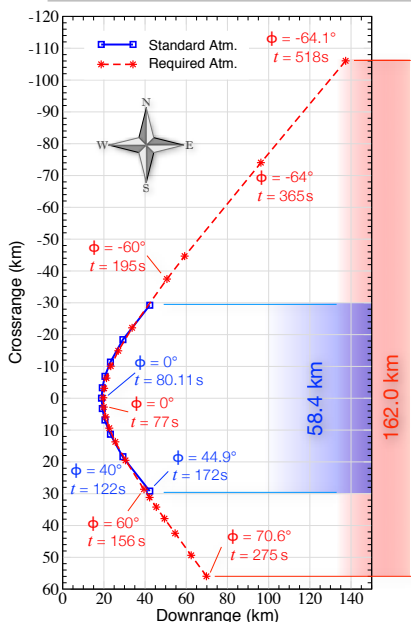


- Azimuthal range of carpet with Required Atm. is much wider than Standard Atm.
- Despite wind & reduced ground amplitude, Real Atm. and Std. Atm. have similar loudness
- Noise at carpet edge drops significantly in Required Atm.

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## Case 2: C609 Ground Carpet



Project raytube ground intercepts on aircraft ground track

- Boom carpet computed from the intercepts of raytubes on the ground-plane projection of the trajectory. Showing both standard and required atmospheres
- Crossrange wind profile makes the required atm. asymmetric
- Cutoff angles Req. Atm =  $[-64.1^\circ, 70.6^\circ]$ , Std. Atm =  $[\pm 44.9^\circ]$
- Long propagation distances near signal cutoff imply that these raytubes take a long time to reach the ground
  - Raytube for  $\phi = -64.1^\circ$  cutoff takes over 8.5 mins in Reqd. atm.
  - Mesh convergence near signal cutoff is not nearly as good as at low azimuth angles
  - Higher discretization error due to much longer propagation
  - Propagation for signal cutoff rays used higher sampling frequency (800 kHz)
- Ground track for required atm is ~160 km, more than 2.7x as wide as standard atm. (~60 km)

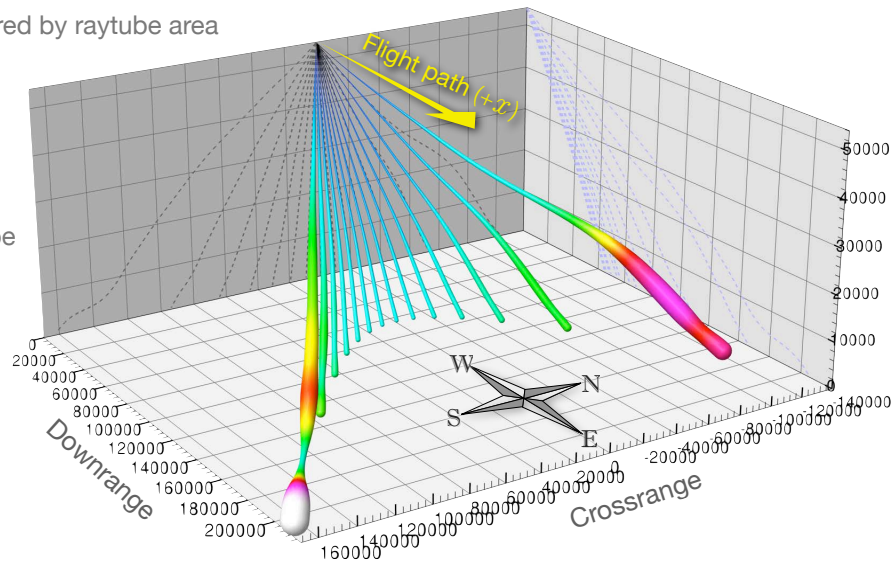
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## Case 2: C609 Raytubes for Required Atmosphere

Plot 3D raytubes colored by raytube area

- 3D plot of raytubes for real atmosphere
- Shows extremely long propagation times & large raytube areas near cutoff



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## Summary

- Applied sBOOM v2.82 & LCASB to all required and optional steady propagation cases
- Mesh convergence studies across the carpet to ensure accuracy of the ground signal and loudness metrics. Error in noise metrics can be 2-4x higher near signal cutoff.
- Mesh convergence is relatively slow on intricate non-smooth input signals
- Real atmosphere is *usually* quieter than Standard Atmosphere, (but not always - e.g. case 2)
- Ground track of real atmosphere can be nearly 3x wider than Standard day. Crosswinds generally increase track width and can result in large cutoff azimuths
- On windy days, boom may not arrive off-track for over 5 mins after a/c passes (case 2 took 8 mins!)
- Raytube visualization shows potential for loud off-track azimuths to be blown back under-track

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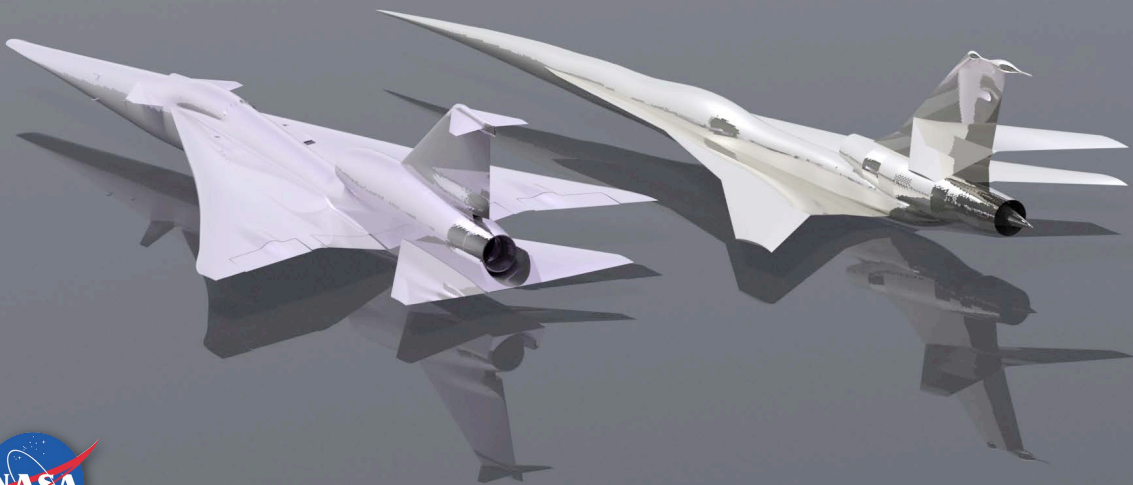


## Acknowledgments

- Thanks to Sriram Rallabhandi for developing and supporting sBOOM, and to Marian Nemeč and David Rodriguez for technical discussions on the various cases.
- SBPW3 organizers for their effort in organizing and coordinating the workshop, particularly Melissa Carter, Sriram Rallabhandi & Mike Park
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- NASA Advanced Supercomputing Division for providing computing resources
- NASA Ames Research Center contract NNA16BD60 and Science & Technology Corp. for supporting Wade Spurlock's involvement.

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Questions?



Backup

