Emission Characteristics of an Axially Staged Sector Combustor for a Small Core High OPR Subsonic Aircraft Engine

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NASA Advanced Air Transport Technology (AATT)

- Small core, high OPR (50+), engine
- gas-only and hybrid gas-electric aircraft
- Engine combustor, reduce Nitrogen Oxides (NOx) emissions to 80% below ICAO CAEP/6 standard (TRL 3)
- fuel-flexible combustors
- Cruise NOx reduced 80% below 2005 best-in-class





Contract or Space Act agreement

United Technologies Research Center

Axially Controlled Stoichiometry (ACS) combustor

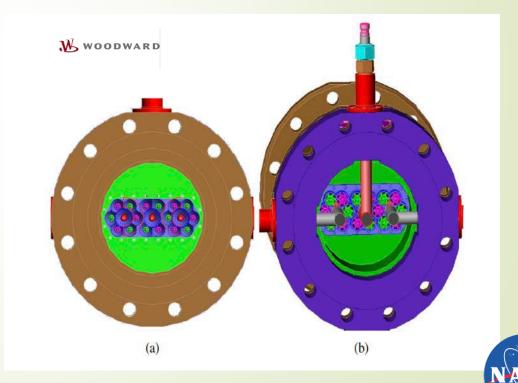
United Technologies
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MAIN STAGE

Report here

Woodward, INC

3-cups Lean Direct injection (LDI) combustor



Reported, > 80% NOx reduction

UTRC ACS combustor

PILOT STAGE

- ACS combustor concept used previously in NASA ERA project by P&W
- Single-cup combustor
 - one of 14 sector for core-size 2.0
 - rated 15,000 lbf thrust at sea-level take off.
- Two single-cup combustors were built under this contract.
 - One with water cooled combustor liners for UTRC HPHT rig
 - full engine power conditions
 - Screen injectors and other combustor feature.
 - One with air cooled combustor liners. NASA Glenn CE-5 rig.
 - Best configuration
 - More close to real engine combustor designs
 - Verify NOx emissions reductions
- NOx, CO and Particulate Matters (PM) emissions data of NASA CE-5 ACS combustor are reported



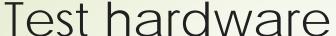
Test facilities

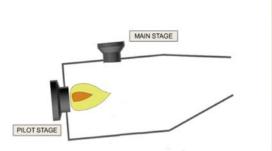
- NASA Glenn Research Center's CE-5 combustion rig
- Inlet air: up to 922 k and 19 bar
- fuel: Jet-A, and 50/50% GEVO/Jet-A alternative fuel (alt fuel data not report here)
- Traversing gas probe at combustor exit
- fixed particle probe 20 cm behind

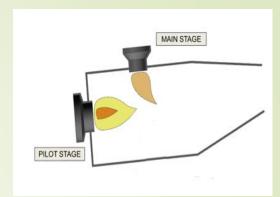


Low-power

High-power



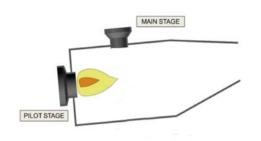




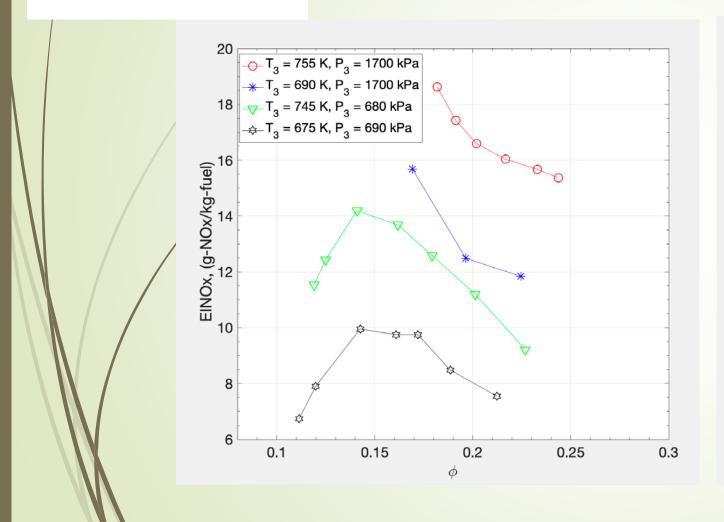


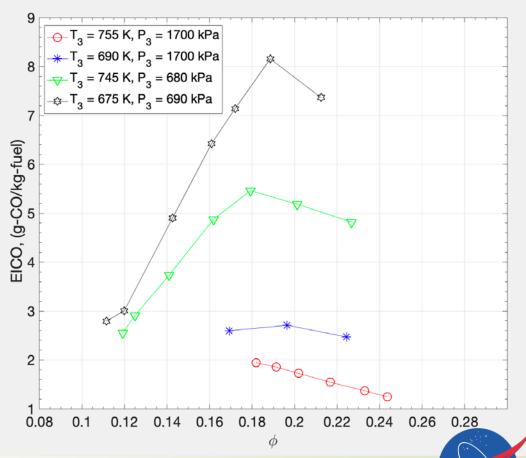
- Pilot injectors located front dome
- Main injectors on top liner downstream
- Combustion air cool liners top and bottom
- Left and right is metal plates
 - cooled by a separated source air
- Three fuel circuits
 - Two for pilot injectors.
 - One for main injectors.
- Two operational configurations
 - Low-power configuration (Pilot only)
 - High-power configuration (Pilot and Main)

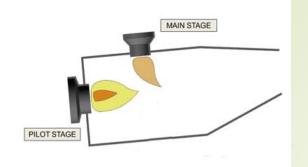




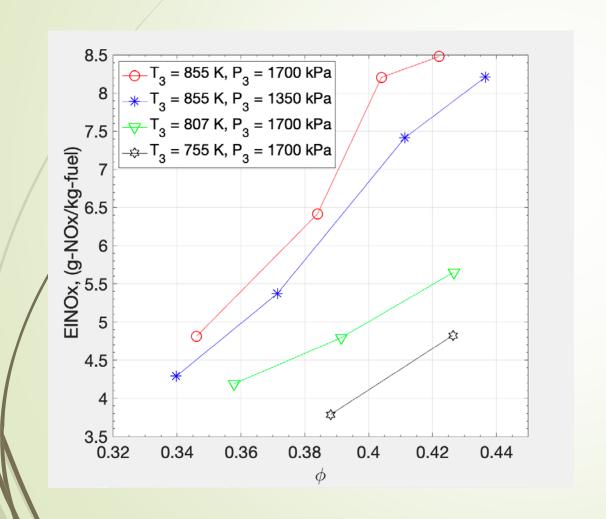
Results- NOx and CO emissions at Low-power configuration (pilot only)

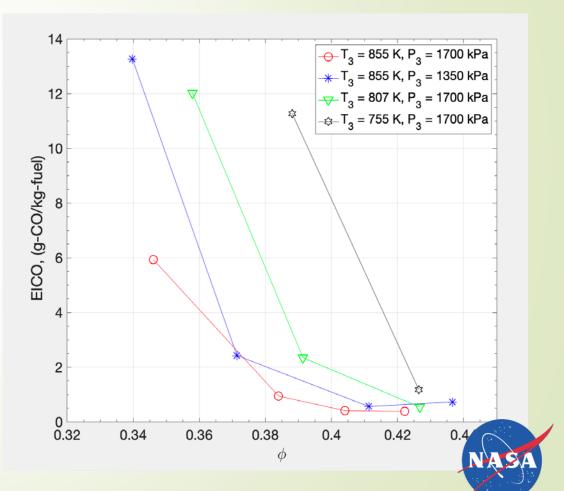




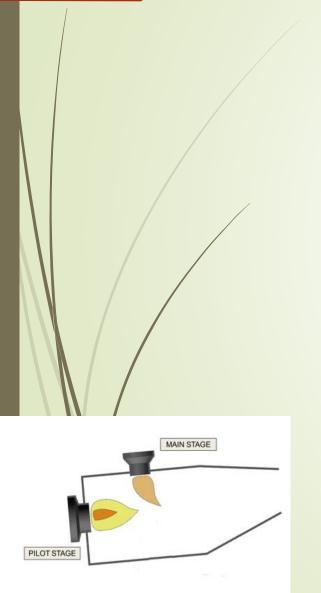


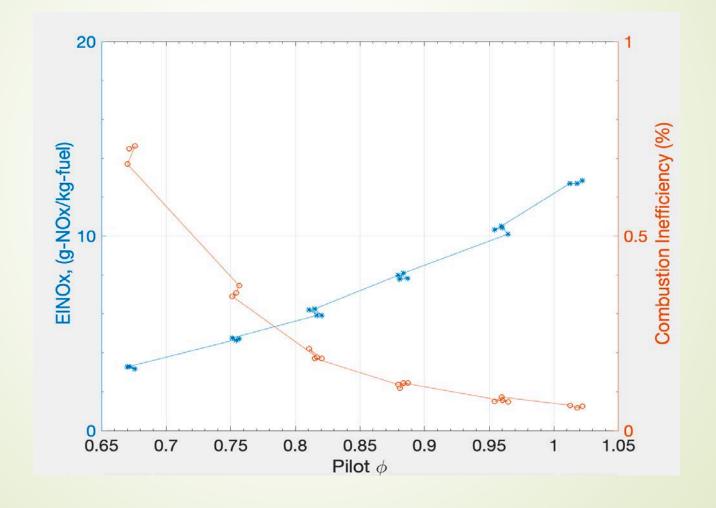
Results, NOx and CO emissions at High-power configuration (pilot and main)



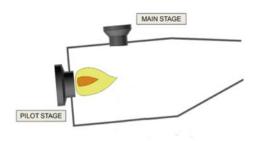


Fuel split between pilot and main injectors

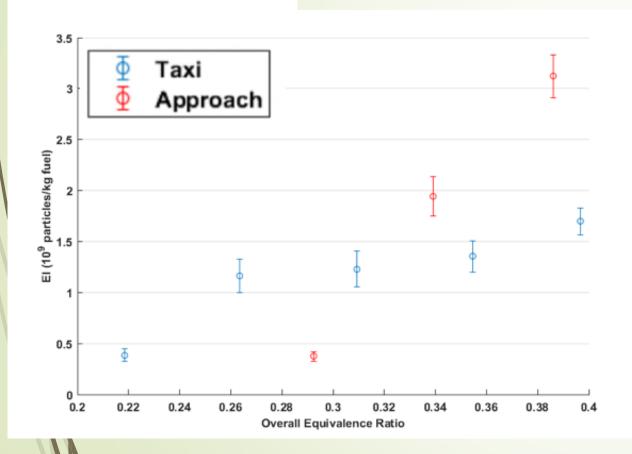


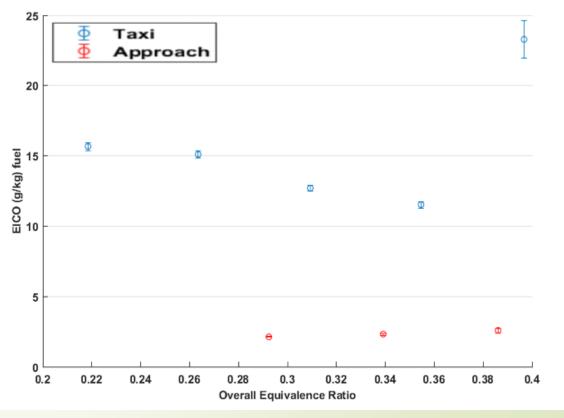




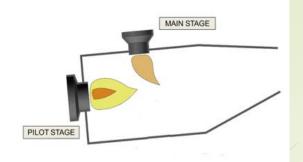


Particulate Matter (PM) and CO emissions —Low-power configuration

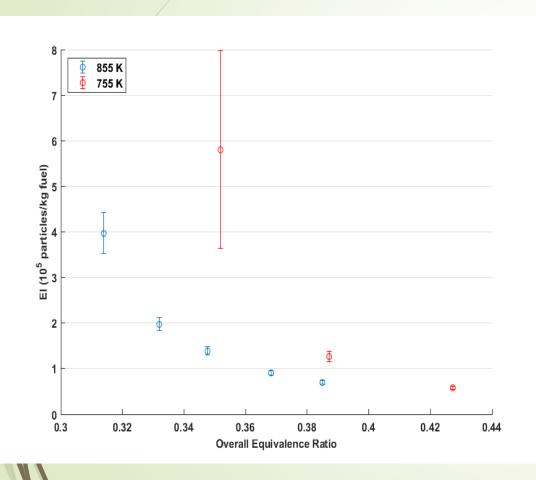


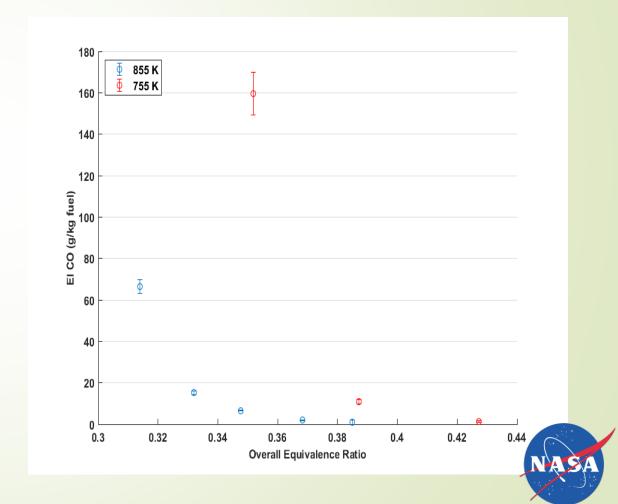






Particulate Matter (PM) and CO emissions —High-power configuration





EINOx correlation equations

Operational conditions

 \mathbf{NO}_{x} correlation equations

| Low-power configuration | $EINOx = 0.141 \times (-19.14 - \frac{4.411}{\emptyset} + \frac{0.07856}{\emptyset^2} + \frac{17.56}{\sqrt{\emptyset}}) \times P3^{0.515} \times e^{\frac{T3}{298}}$ | | | | |
|---------------------------|--|--|--|--|--|
| $0.07 < \emptyset < 0.15$ | ϕ ϕ^2 $\sqrt{\phi}$ ϕ^2 | | | | |
| Low-power configuration | $EINOx = 0.016 \times (21.7 + \frac{4.39}{\emptyset} + \frac{0.064}{\emptyset^2} - \frac{17.44}{\sqrt{\emptyset}}) \times P3^{0.327} \times e^{\frac{T3}{287}}$ | | | | |
| $0.35 > \emptyset > 0.15$ | | | | | |
| High-power configuration | $EINOx = 2.56e^{-3} \times P3^{0.48} \times \emptyset_{pilot}^{2.72} \times \emptyset^{0.11} \times e^{\frac{T3}{168}}$ | | | | |
| Ø > 0.30 | | | | | |

• P3 in kPa, T3 in K

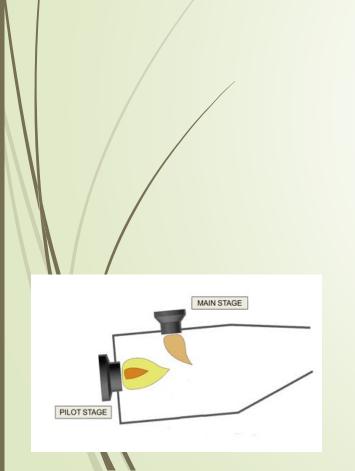


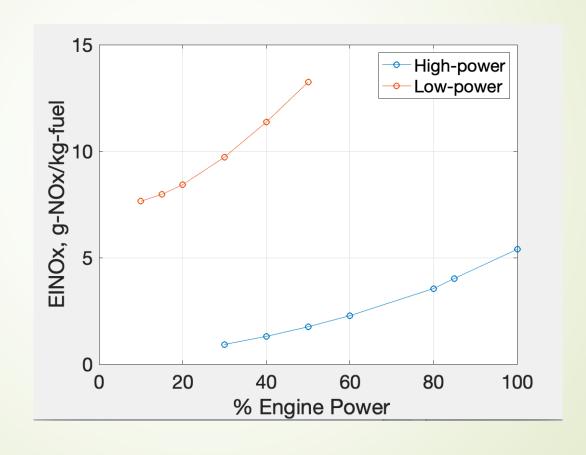
NASA N+3 engine LTO cycle for 120.4 kN, 37.6 OPR (sea-level) engine.

| % engine power | LTO condition | P3 (bar) | T3 (K) | Ø | Fuel (kg/s) |
|----------------|---------------|----------|--------|-------|-------------|
| 100 | SLTO | 38.0 | 870 | 0.354 | 0.585 |
| 85 | Climb | 32.7 | 835 | 0.325 | 0.479 |
| 30 | Approach | 14.1 | 661 | 0.185 | 0.147 |
| 7 | Taxi | 7.1 | 553 | 0.102 | 0.048 |



NOx emissions estimation over NASA's N+3 engine power setting.







ICAO NOx reduction in relative to CAEP-6

| % engine power | power conditions NASA N+3 cycle EI | | O _x UTRC N+3 cycle EINO _x * | |
|----------------|------------------------------------|------------------|---|--|
| 100 | SLTO | 4.65 | 4.02 | |
| 85 | Climb | 3.48 | 3.09 | |
| 30 | Approach | 10.2 | 10.7 | |
| 7 | taxi | 3.46 | 6.12 | |
| | cruise | 2.56 | 1.6 | |
| | | % ICAO reduction | % ICAO reduction | |
| | | 89% | 82% | |

^{*} Calculated from correlations developed from NASA test data.



^{*} The NO_x emissions results are humidity corrected

Conclusions

- NOx, CO, PM emissions of a small core high OPR ACS combustor are reported
- NOx and CO emissions characteristics are similar to a previous version of ACS combustor
- PM emissions data is not compared to most other PM data collected at the exit of the engine
- Low-power configuration (rich front end) is producing significant higher PM emissions that High-power configuration (lean front end)mode.
- 82% and 89% NOx reductions in relative to ICAO CAEP/6
- Over 80% reduction in Cruise NOx relative to a NASA-defined 2005 best-in-class



Acknowledgments

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Questions and Comments

