



Influence of Thermally-Grown Oxide (TGO) Layer on the Driving Forces Associated with Failure in Environmental Barrier Coating (EBC) Systems

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Courtesy of GE Aircraft Engines

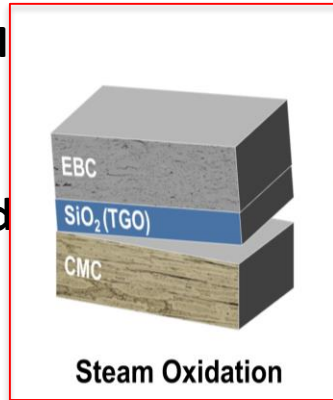
Benefits:

- Enabling for high OPR engines (high turbine inlet temperatures)
 - 200 to 500+ °F temperature advantage over metals
 - Reduce cooling air
 - Reduce fuel burn (up to 6%) - NO₂ emissions
- Weight – 1/3 of metals and 1/2 titanium aluminides
- CMC combustor liner and first stage turbine vane reduce NO_x
- **An external environmental barrier coating (EBC) made of layers of oxides/silicates is required to achieve long-term stability and component life.**

- 1st Gen of EBCs were developed in 1990s under NASA's HSCT-EPM (High Speed Civil Transport – Enabling Propulsion Materials) program consisting of mullite and BSAS materials.

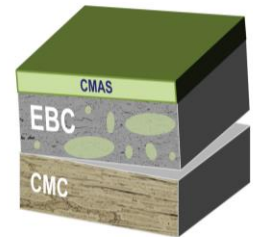
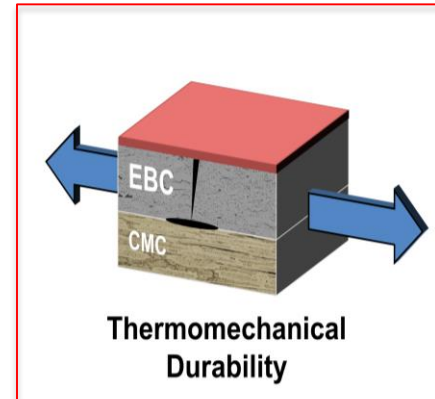
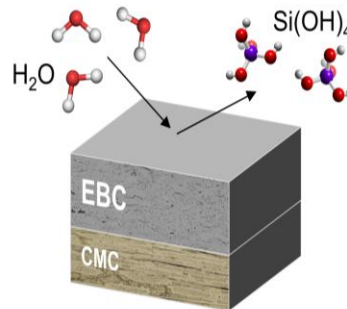
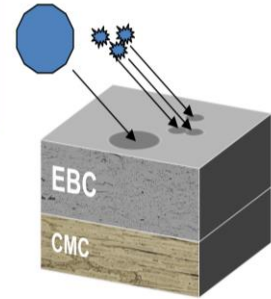
- 2nd Gen EBCs were developed under NASA's UEET (Ultra Efficient Engine Technology) program in early 2000s. Most of the current EBCs are some variation of 2nd Gen EBCs.

EBCs have various failure modes.



Synergies between extrinsic failure modes determine EBC lifetime and design requirements

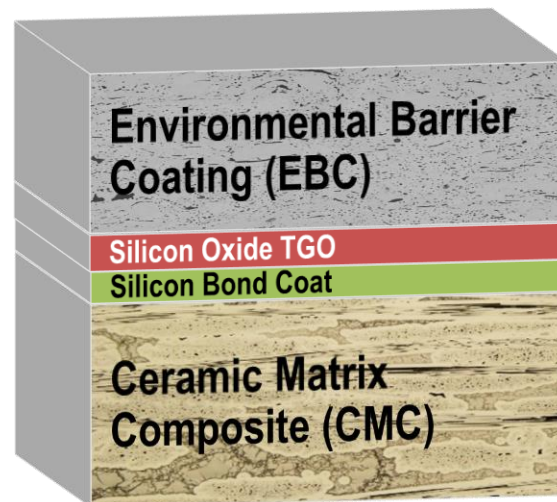
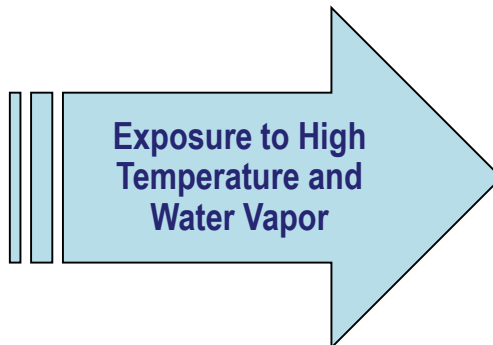
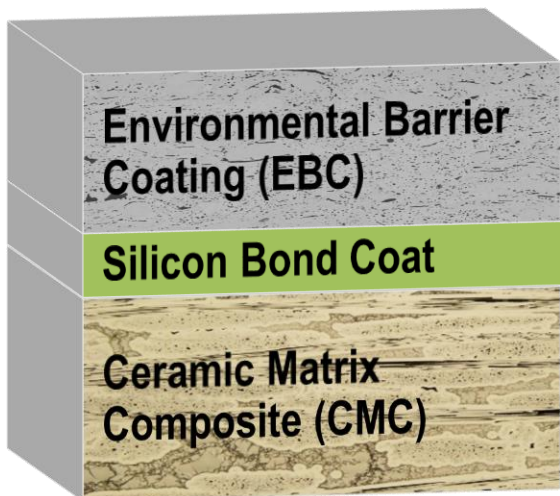
EBC Intrinsic Requirements
CTE match, isotropic CTE
Phase stability
No EBC/CMC interaction



K. N. Lee, "Environmental Barrier Coatings for CMC's"; in *Ceramic Matrix Composites*, Wiley, New York (2015)

K. N. Lee, *J Am Ceram Soc.* 2019:1507-1521

Low Temperature System (< 1316°C)

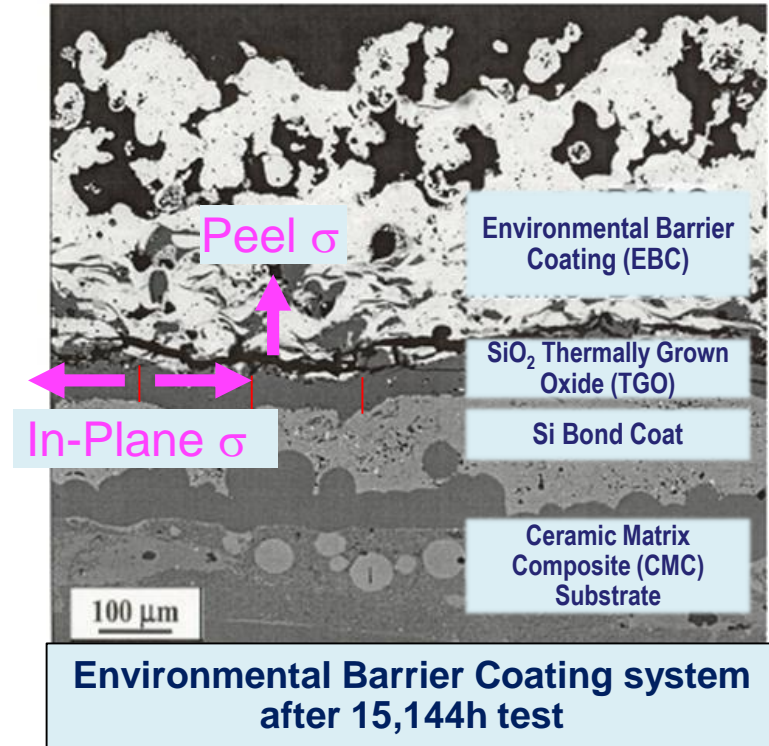


High Temperature System (> 1316°C)



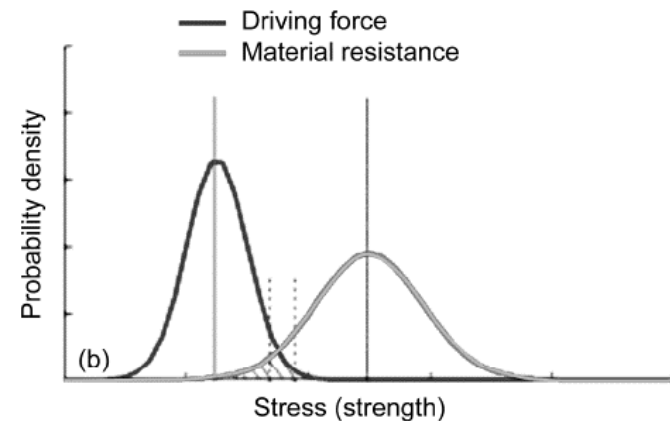
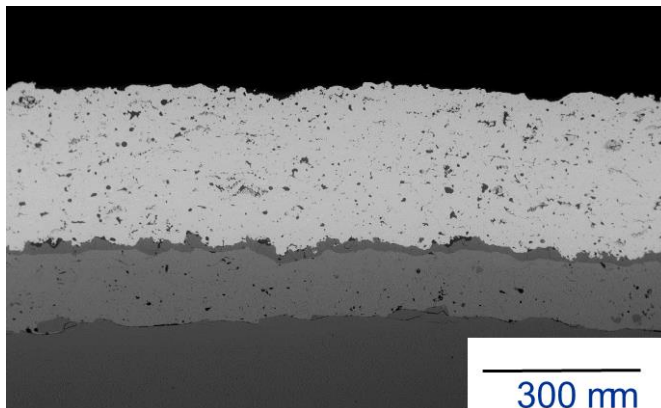
Thermally Grown Oxide (TGO) is the Observed Point of Failure

- Although durable, EBC systems must survive for 10,000+ hours
- Lifetime of EBC/CMC systems is limited by the formation of a thermally grown oxide (TGO)
 - SiO_2 TGO can grow on either silicon bond coat or SiC substrate
- Observed failures
 - Vertical Cracks (**$\sim 10 \mu\text{m}$ spacing at failure**).
 - Horizontal Cracks (Delamination)
- EBC fails when TGO reaches some critical thickness ($\sim 20\text{-}40$ microns)
 - Can vary due to exposure temperature, microstructure, composition, etc.



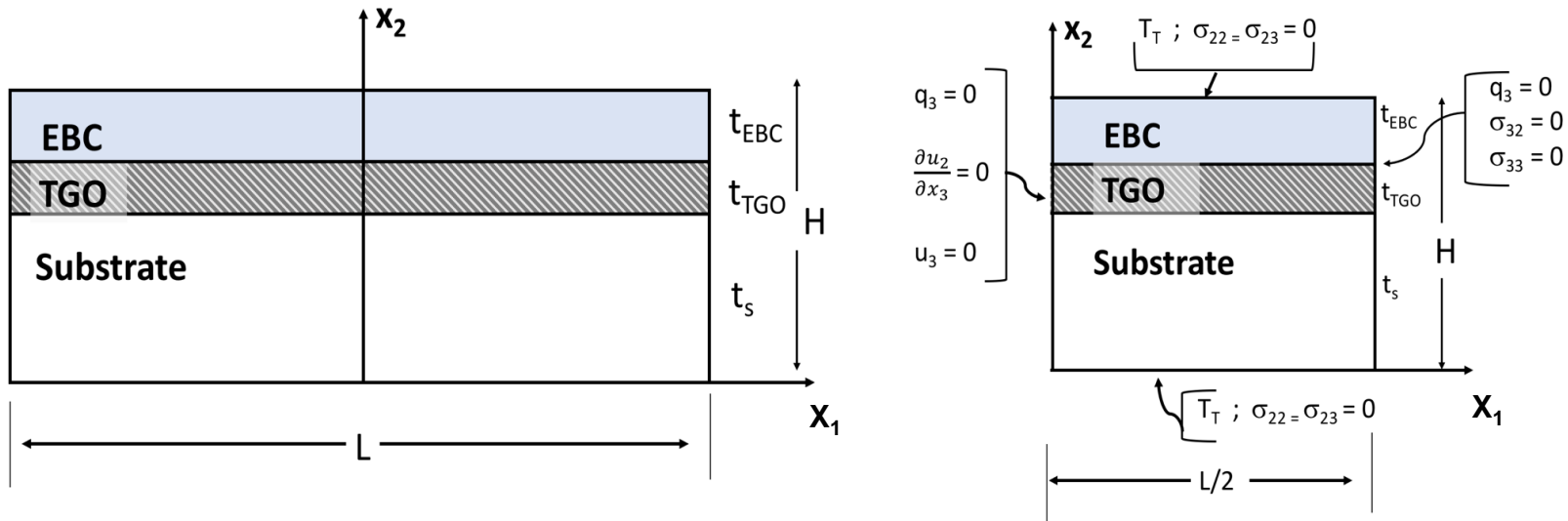
Ultimate Goal: Predict the durability of EBC/CMC system when subjected to harsh environments

- Perform **finite element analyses** to examine the influence of uniformly and nonuniformly grown oxide layers on the associated driving forces leading to mechanical failure (spallation) of EBC layer when subjected to isothermal loading
- **Assess the effect of damage** in the TGO layer in the form of vertical cracks for both uniform and non-uniform TGO layers.
 - Ignore residual stresses due to processing, cyclic loading effects, growth rate of TGO as well as any time dependent behavior (creep/relaxation)
 - **Qualitative** not quantitative study
 - What influences critical TGO thickness
- Examined 3 layer and 4 layer systems



With Geometry And Applied Thermal And Mechanical Boundary Conditions

Boundary Conditions



- Global loading is cool-down from 1482°C to 38.7°C (2700 °F to 102 °F)
- Applied in one step since material assumed to be linearly elastic
- Stress state is generated due to geometry and mismatch in constituent material properties

Two-dimensional finite element analyses are performed using ABAQUS finite element program.



Constituent's Material Parameters



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- Assume isotropic thermoelastic properties

Material	Thickness (mm)	Modulus (GPa)	Poisson Ratio	CTE ($\times 10^{-6} \text{ K}^{-1}$)	Strength (MPa)
$\text{Yb}_2\text{Si}_2\text{O}_7$ (EBC)	0.175	200*	0.27	4.5	45-65 (?)
SiO_2 (TGO)	0.001 0.002 0.004 0.008 0.016	35*	0.17	10	45-75 (200)
Si ** (Bond Coat)	0.075	97*	0.21	4.5	40-55 (?)
Hexoloy SiC (Substrate)	3.000*	400	0.17	5.25	380-550

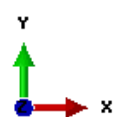
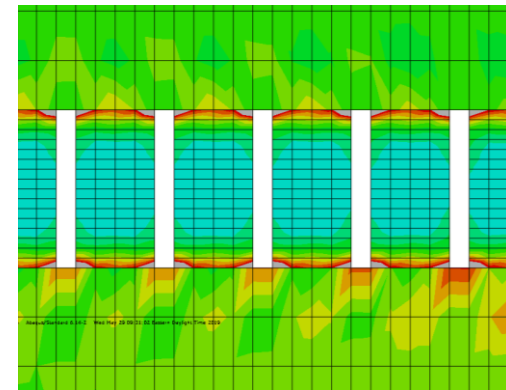
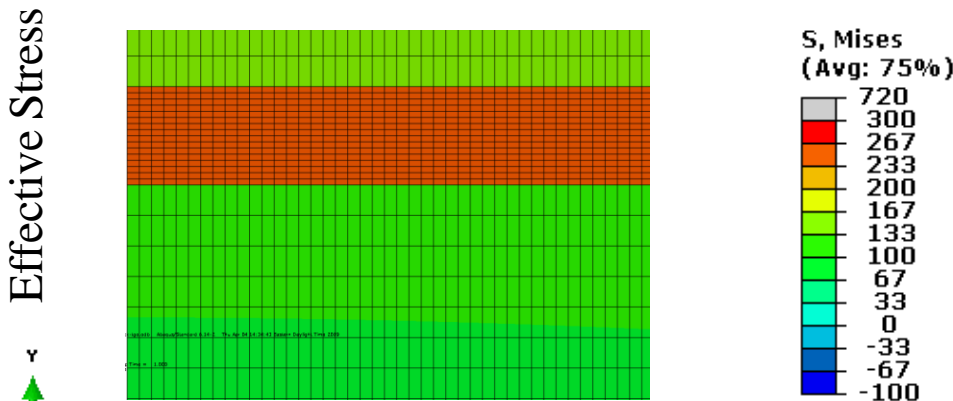
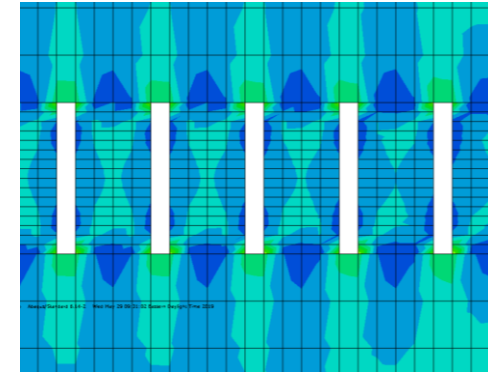
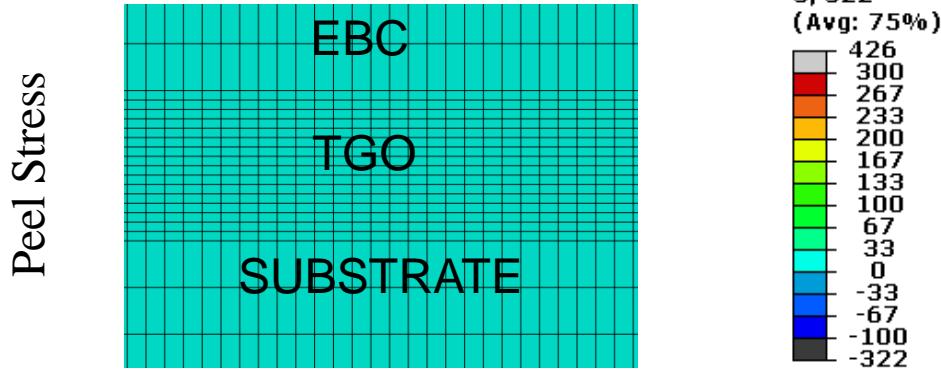
* Initial thickness assuming no TGO, bond coat

** If present

Two TGO thicknesses (4 and 16 μm) have been analyzed here with both uniform and non-uniform TGO layer thickness.

Undamaged (16 μm TGO Layer)

Damaged (16 μm TGO Layer)



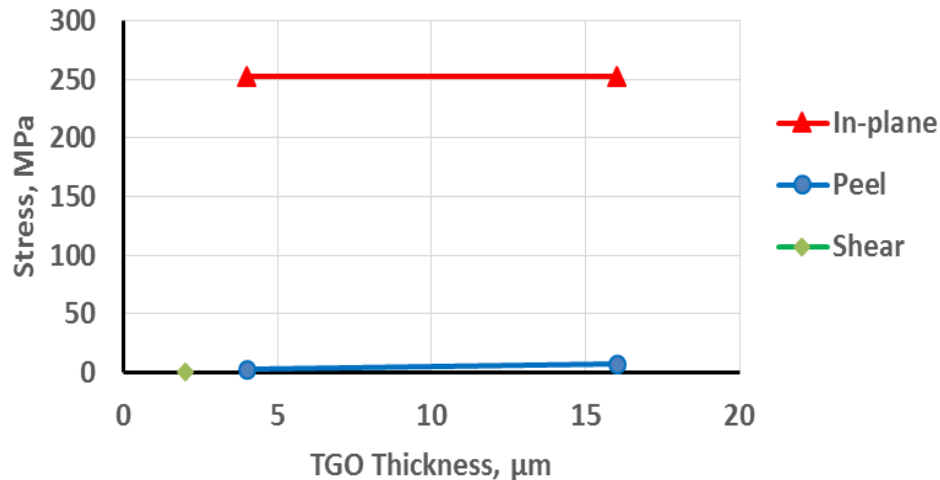
- Significant increase in peel and Von-Mises stress as damage is introduced. Peel stress increases from a negligible value when there is no damage to **~100 MPa** at EBC/TGO interface **when damage is present.**



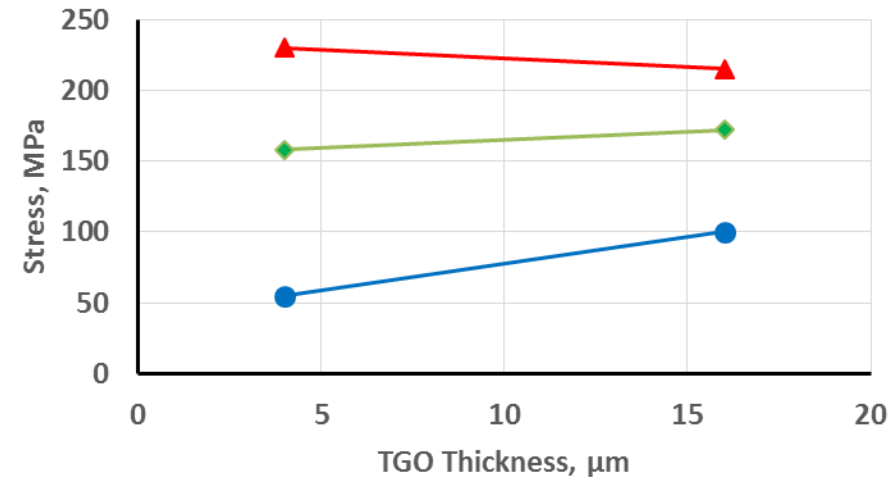
Maximum Stresses in Uniform TGO Layer 3-layer System



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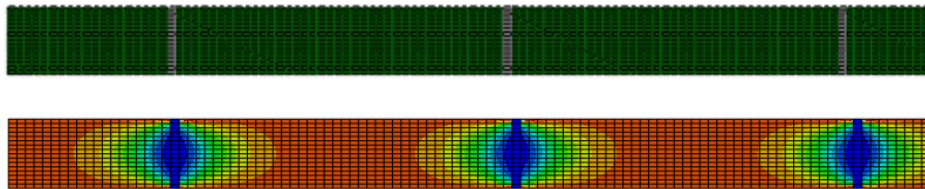
No Damage



Vertical cracks @10 μm spacing

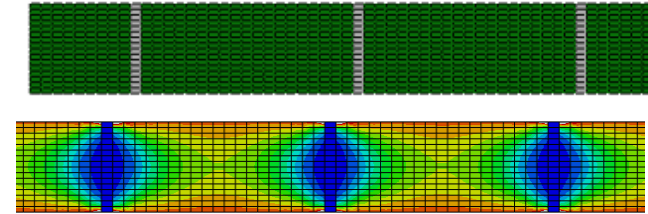
- TGO thickness has **no significant (< 1%) effect** on the resulting stress state in the system when there is **no damage**. Only significant stresses are in-plane stresses that cause vertical cracks
- When **damage is present**, *peel and shear stresses increase with increase in TGO layer thickness*

80 μm spacing



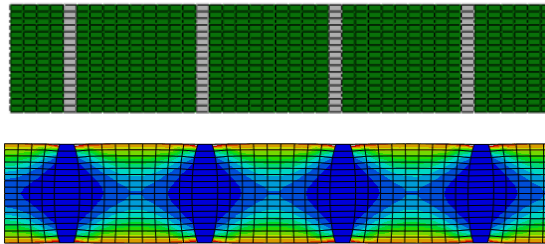
In-plane stress

40 μm spacing

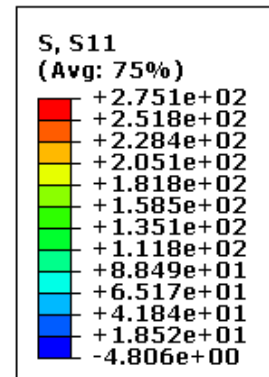


In-plane stress

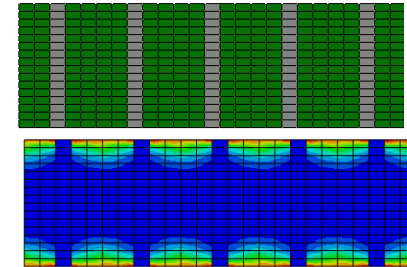
20 μm spacing



In-plane stress



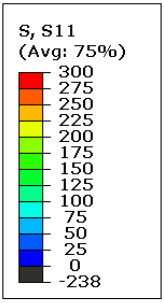
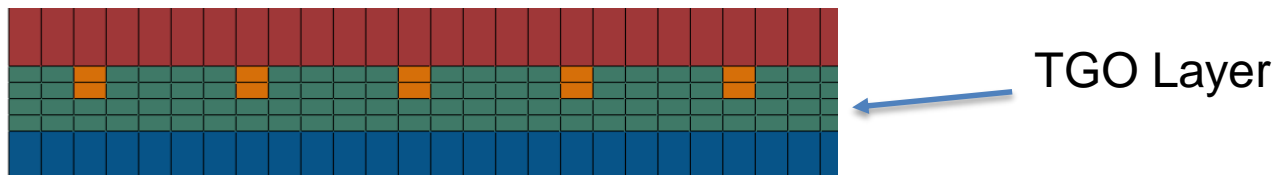
10 μm spacing



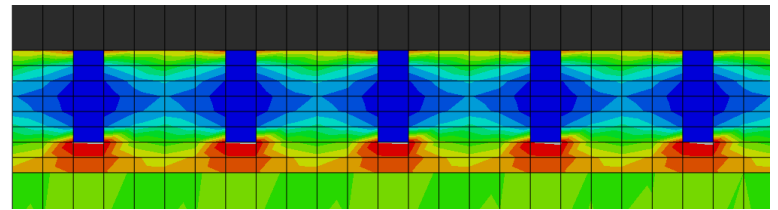
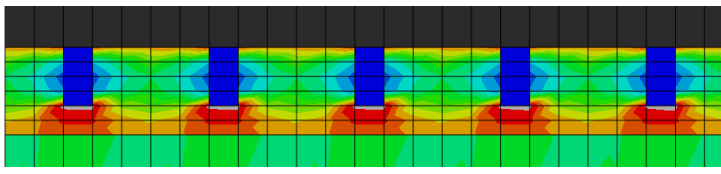
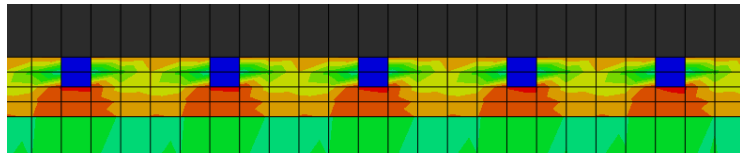
In-plane stress

- Elements representing cracks are shown in gray
- TGO has a Uniform thickness of 16 μm
- Current idealization suggests that strength of pristine TGO material should be ~ 200 MPa

Geometry



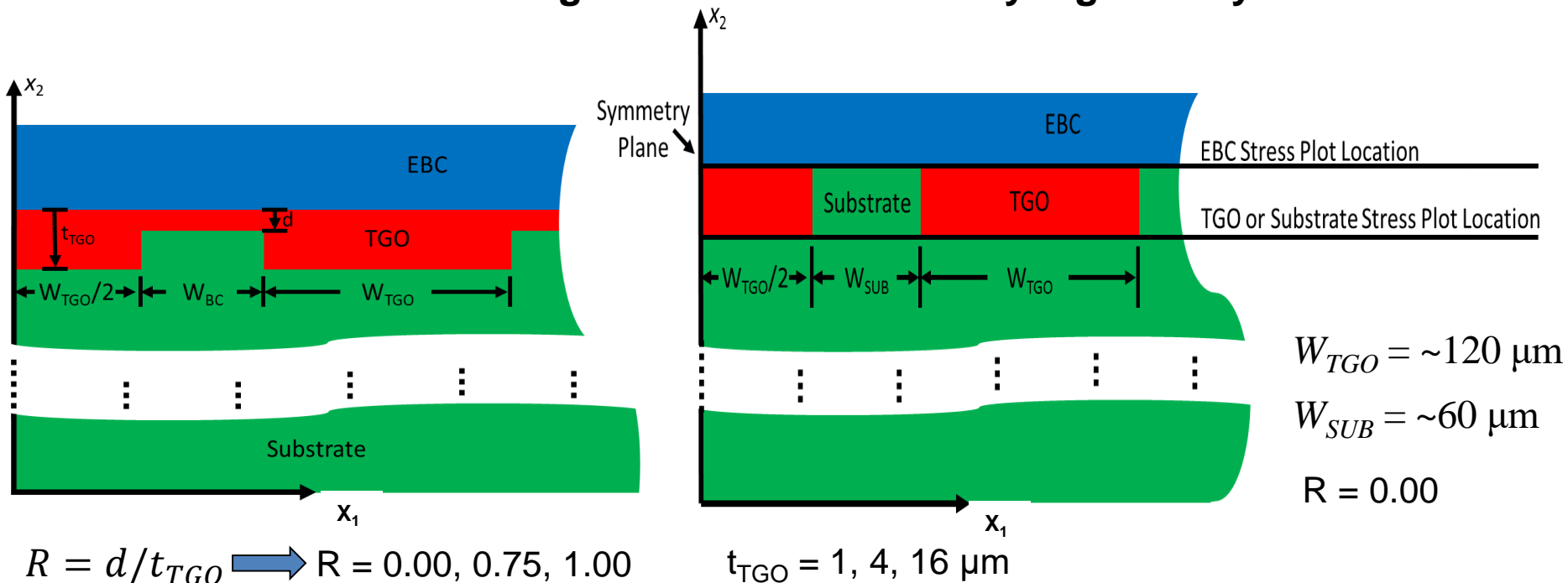
In-plane stress



Increasing
TGO
Thickness

- In-plane stress at the tip of the partial cracks is very high (> 300 MPa), suggesting that partial cracks are likely to propagate and coalesce into a full vertical crack almost instantaneously.

Schematic showing discontinuous TGO layer geometry



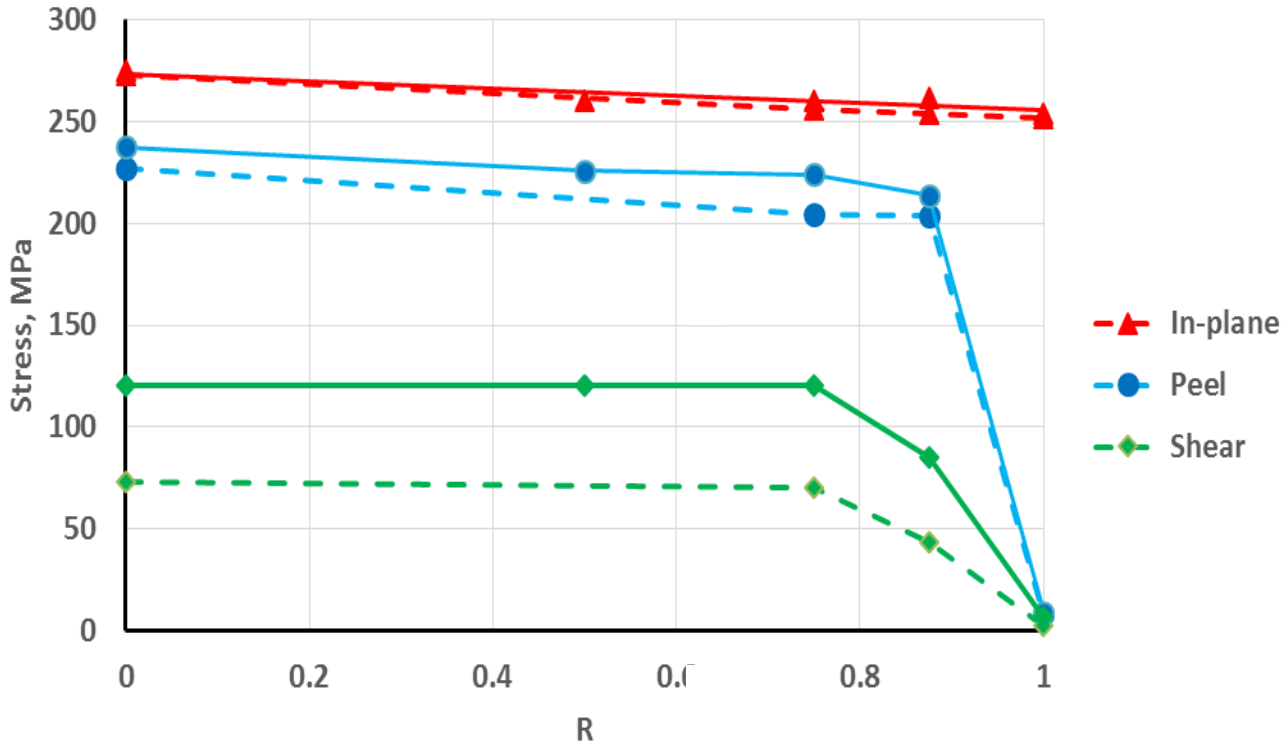
- EBC, TGO, and CMC substrate involving only the first $\sim 550 \mu\text{m}$ out of $5000 \mu\text{m}$ ($L/2$) in the x_1 -direction
- Discontinuous TGO “islands” inserted between the substrate and EBC interface
- Severity of nonuniformity considered by adjusting R factor
- Initial TGO island width was set to half its full width (symmetry boundary conditions)



Maximum Stresses in TGO Layer with No Damage Three-Layer System (EBC/TGO/Substrate)

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Solid lines represent thick (16 μm) TGO
Dash lines represent thin (4 μm) TGO



- Significant peel and shear stresses develop even at slight non-uniformity.
- Magnitude of stress is independent on the severity of non-uniformity
- As the TGO thickness grows, peel and shear stresses will cause initiation and propagation of delamination/horizontal cracking leading to EBC spallation.
- Change in shear is greater than peel with TGO growth

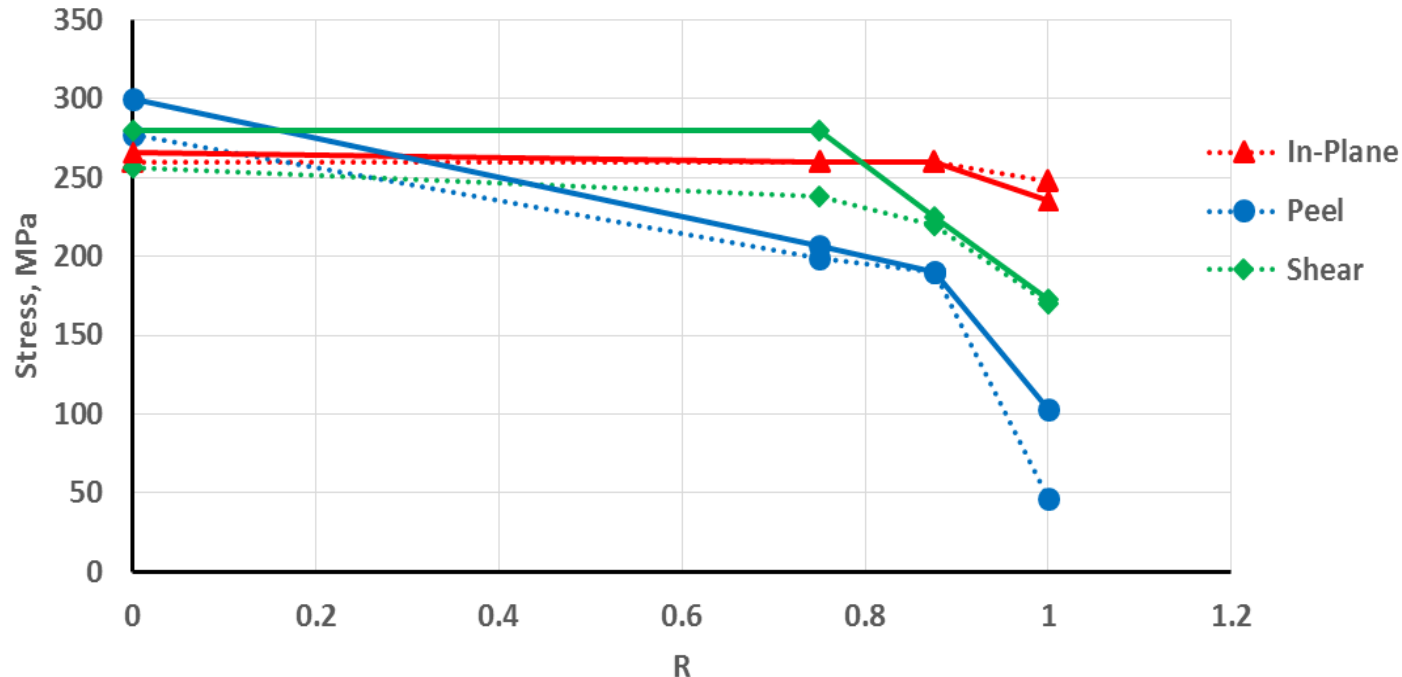


Max. Stresses in Non-uniform TGO Layer Vertical Cracks @ 10 μm Spacing; 3 Layer System

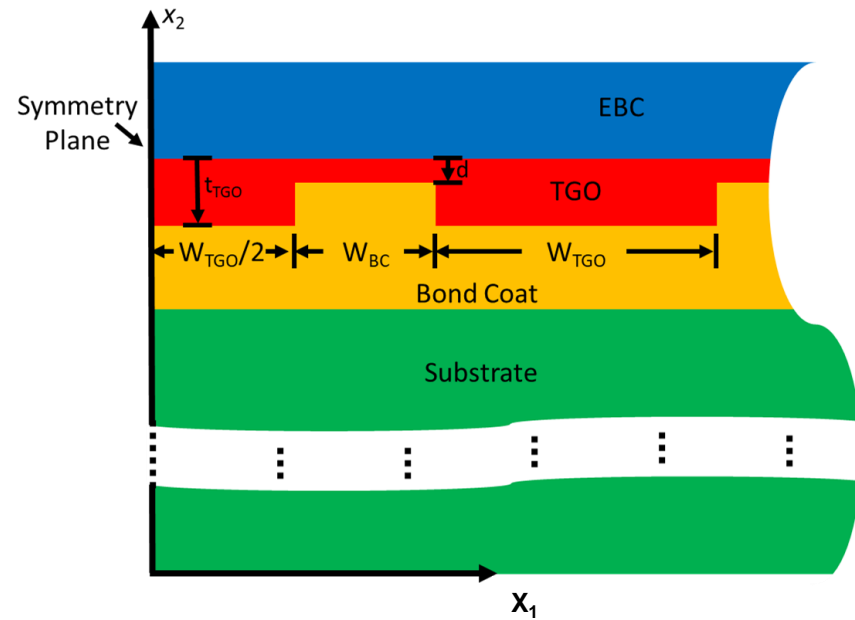


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Solid lines represent thick (16 μm) TGO
Dash lines represent thin (4 μm) TGO



- In the presence of **damage and non-uniformity**, there are significant shear and peel stresses for delamination to initiate and propagate causing spallation of the coating (particularly when the TGO becomes thick, e.g., 16 μm (solid curves)).
- Nonuniformity magnifies residual stress by up to a factor of 5-6x.



Lower temperature system

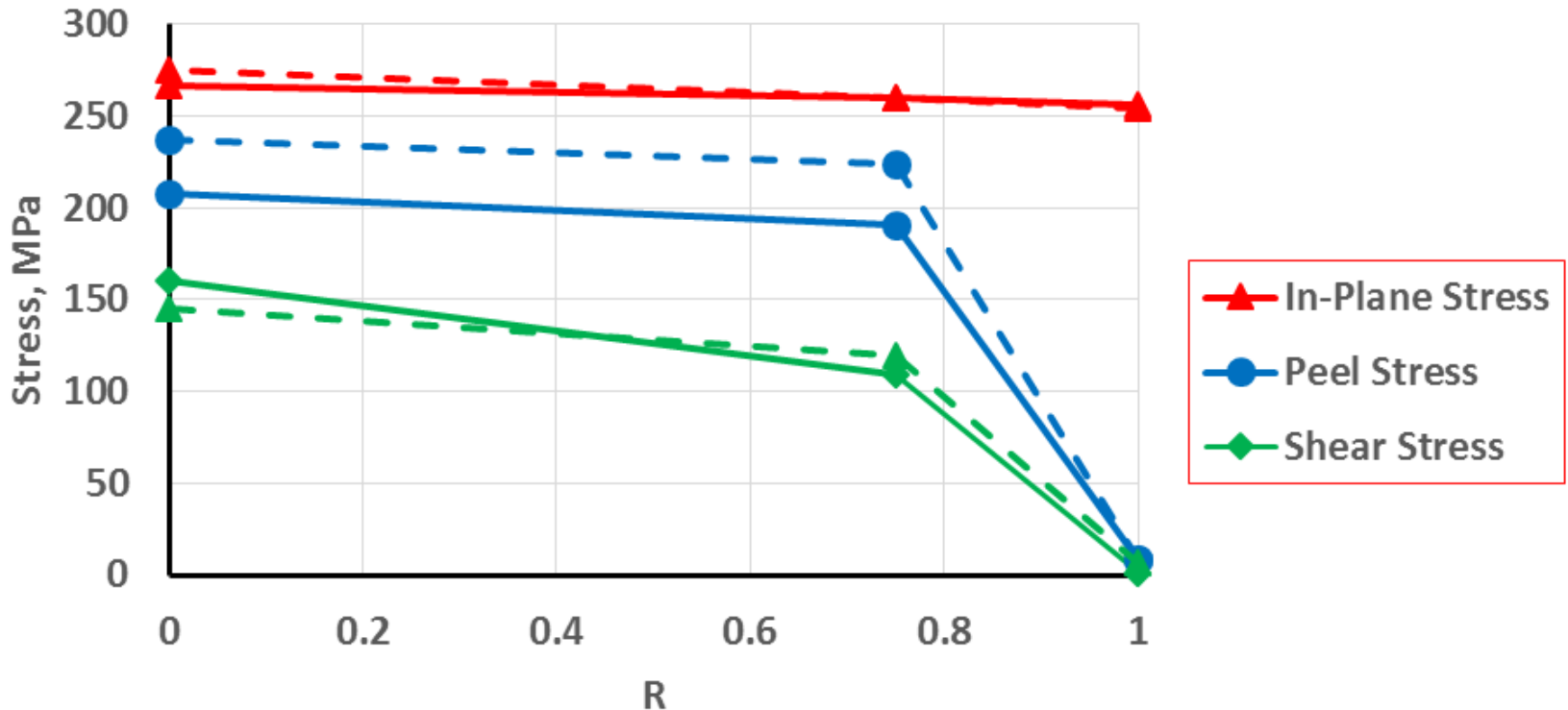
$$t_{TGO} = 1, 4, 16 \mu\text{m} \quad R = d/t_{TGO}$$

$$W_{TGO} = \sim 120 \mu\text{m} \quad R = 0.00, 1.00$$

$$W_{BC} = \sim 60 \mu\text{m}$$

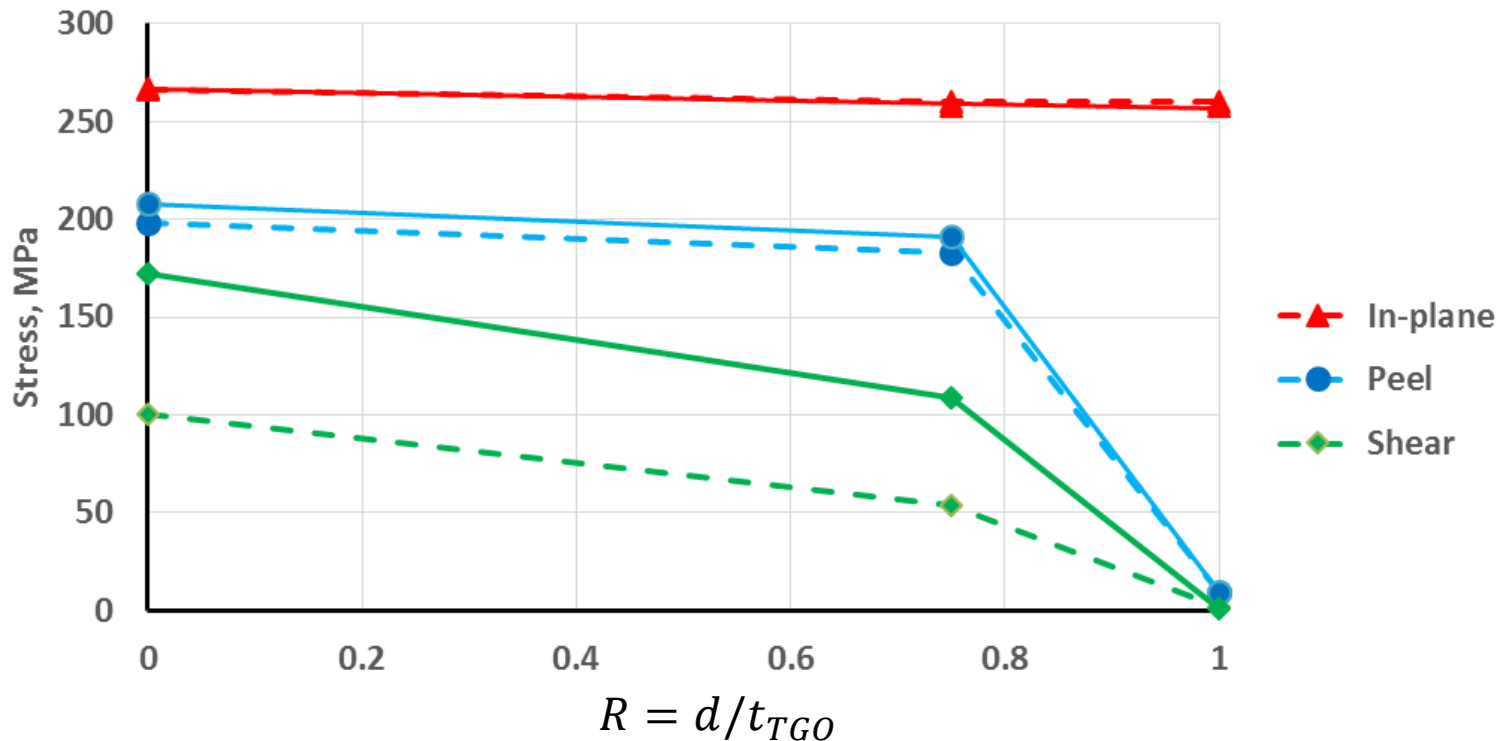
- Discontinuous TGO “islands” inserted between the substrate and EBC interface
- Severity of nonuniformity considered by adjusting R factor

Solid lines represent **4 layer** EBC system (Low Temp System)
 Dash lines represent **3 layer** EBC system (High Temp System)



- Stresses are lower overall for 4 layer system compared to 3 layer
 - Peel stresses significantly lower (10%)
 - In-plane and Shear stresses are similar but slightly lower

Solid lines represent **thick** (16 μm) TGO
Dash lines represent **thin** (4 μm) TGO



- $R=0$ (island); $R=1$ (uniform); $R=0.75$ (step island)
- Similar trends in peel and shear as with 3 layer system – yet sensitivity to nonuniformity appears greater

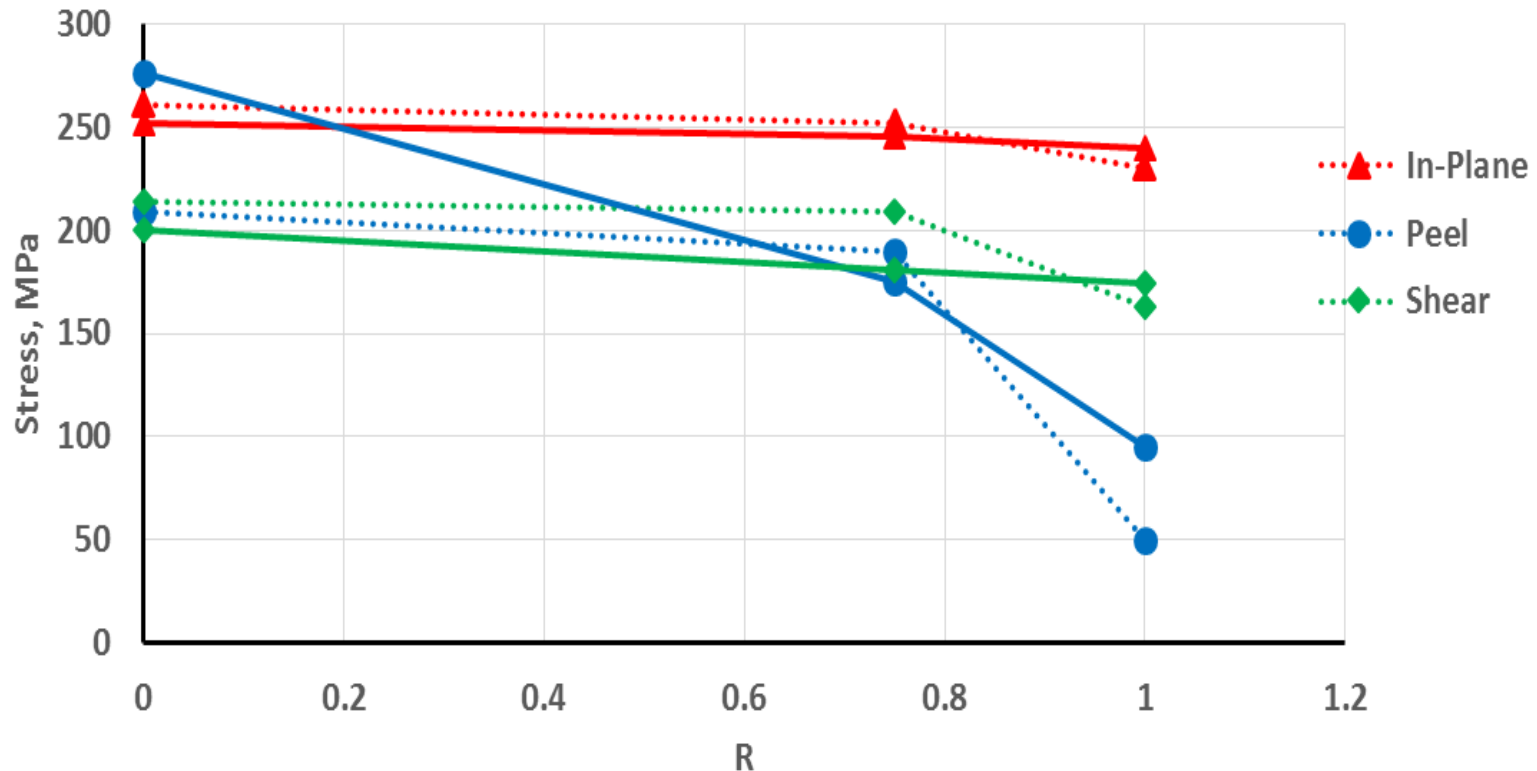


Maximum Stresses in Damaged TGO Layer 10 μm Spaced Cracks; 4 Layer System



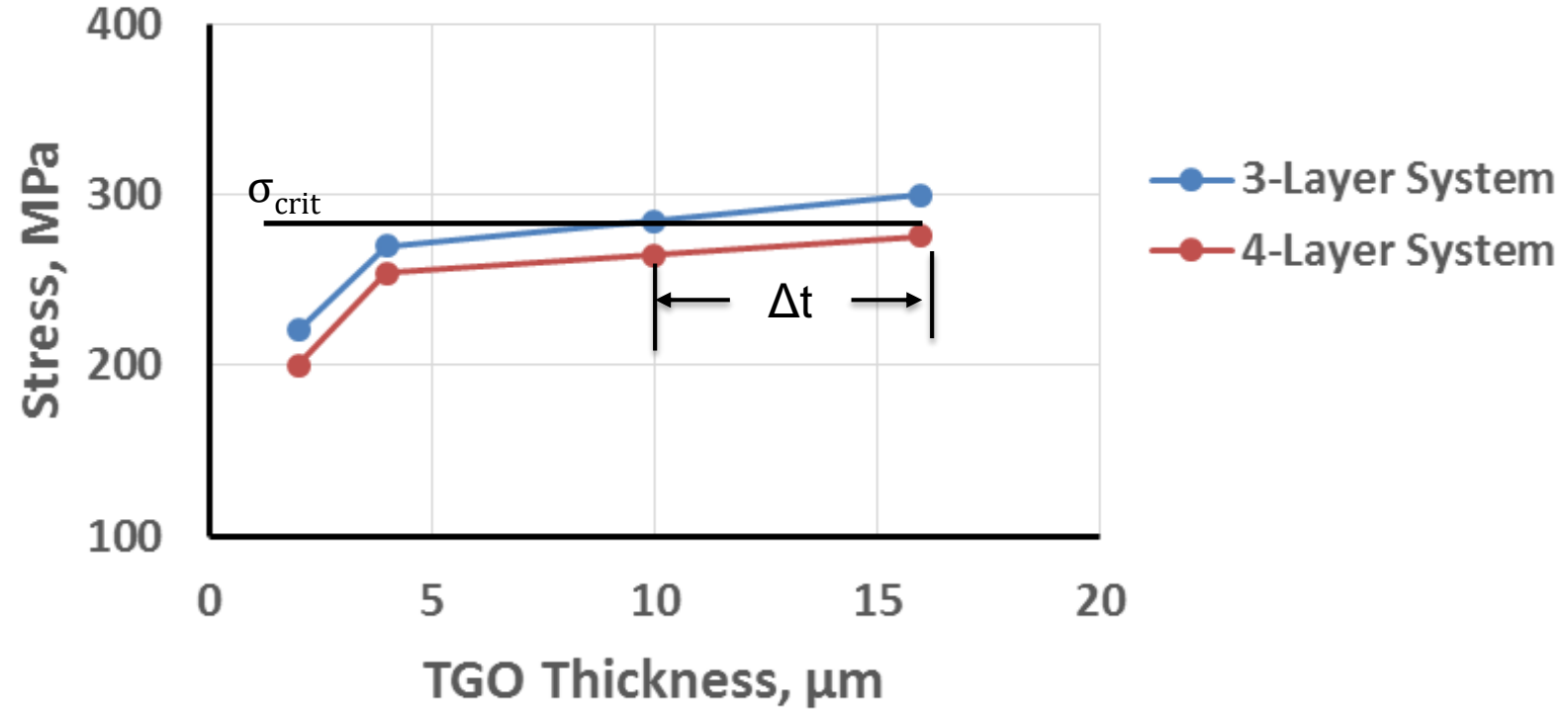
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Solid lines represent **thick** (16 μm) TGO
Dash lines represent **thin** (4 μm) TGO



- Uniform ($R=1$), damaged system has nonzero peel and shear stresses
- Peel significantly increases with increasing TGO
- Shear slightly decreases with increasing TGO

Peel stress ; 10 μm Spaced Cracks; R=0 (island)



- Decrease in peel stress when bond coat added
- **Given critical failure stress, Si bond coat (i.e., four layer system) enables thicker TGO layer prior to failure**
- **Suggests bond strength between EBC and TGO >290 (MPa)**
- Shear stresses similar but reduction in magnitude larger !



- A three layer (EBC/TGO/Substrate) and a four layer (EBC/TGO/Bond coat/Substrate) were analyzed subjected to an isothermal cooldown.
- The influence of damage in the TGO layer in the form of vertical cracks and two thicknesses for both uniform and non-uniform TGO layer were examined.

Uniform TGO layers

- With no damage, the stress state is independent of TGO layer thickness.
- When damage was introduced in the form of vertical cracks, **significant peel and shear stresses** developed.
- Given an average experimentally observed crack spacing in the TGO layer of 10 μm ; suggests the tensile strength of the pristine TGO material should be around 200 MPa.

Non-uniform TGO layers

- **Even a slight non-uniformity in the TGO thickness resulted in significant peel and shear stresses** increasing the possibility of delamination and spallation of EBC when a critical thickness is reached.
 - When damage is introduced, there was an increase in peel and shear stresses.
- The presence of damage (vertical cracks caused by in-plane stresses) enhances the stresses that are present due to non-uniformity. However, the presence of non-uniformity itself is still the main factor influencing the magnitude of peel and shear stresses.



Summary (contd.)



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- As TGO thickness increases with exposure time; peel and/or shear stresses will exceed the material resistance (strength) and lead to EBC failure. That is a critical thickness will be reached whereupon delamination/spallation will occur.
- Presence of a bondcoat layer reduces the driving forces. For a given critical failure stress, silicon bondcoat in four-layer system enables a thicker critical TGO and thus increased life prior to failure.
- Note when characterizing constituent, interface, etc. strengths it's important to account for localization features such as damage, microstructure, residual, etc.!!

Future Work

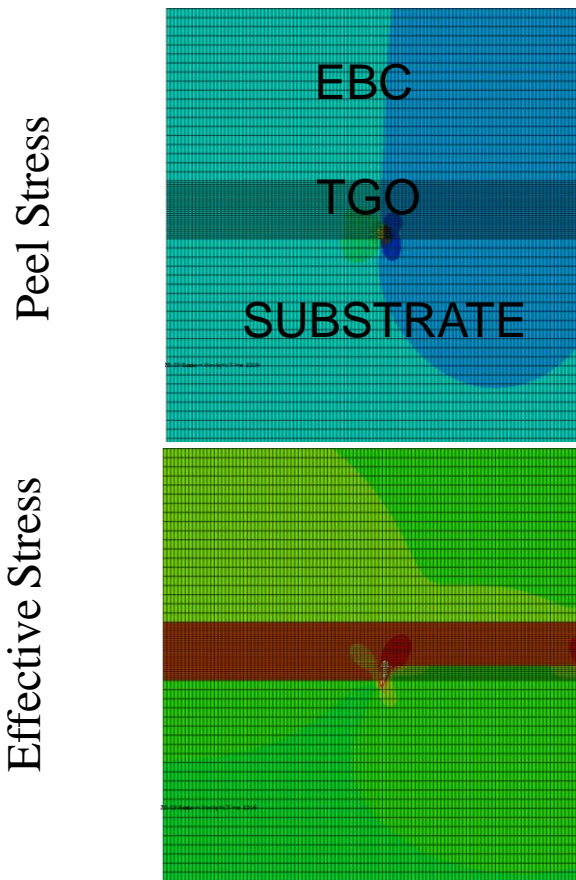
- Material behavior (e.g. creep/relaxation), TGO growth rate
- Constituent material and interfacial bond strength



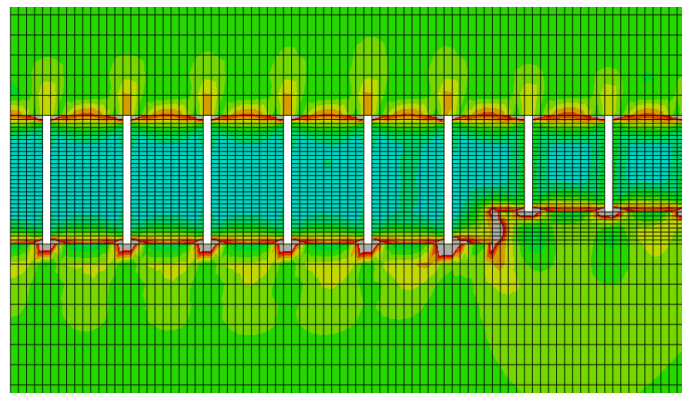
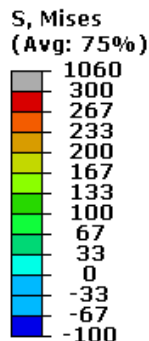
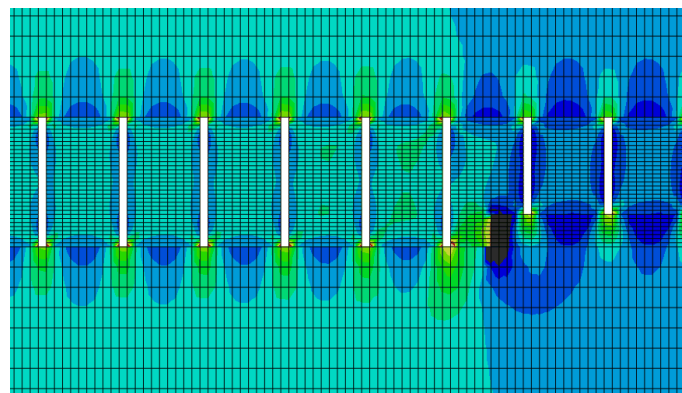
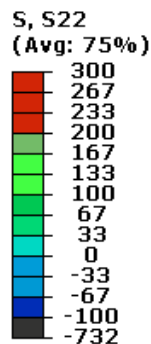
Backup Charts

R=0.75

Undamaged (16 μm TGO Layer)

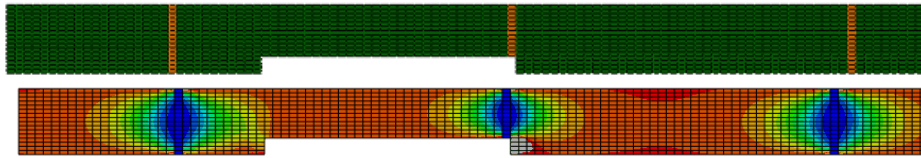


Damaged (16 μm TGO Layer)



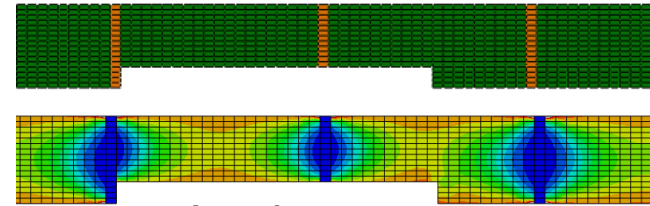
- Significant increase in peel and Von-Mises stress as damage is introduced. Peel stress at undulation is similar to crack tips. TGO/Sub interface higher values than TGO/EBC interface.

80 μm spacing



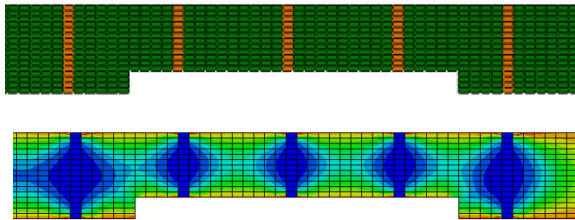
In-plane stress

40 μm spacing



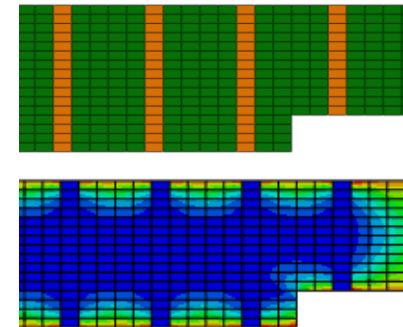
In-plane stress

20 μm spacing

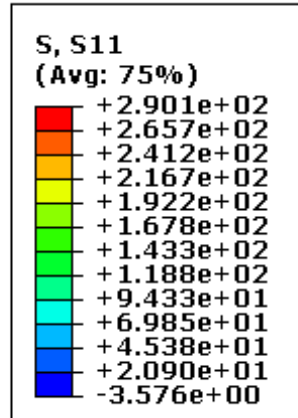


In-plane stress

10 μm spacing



In-plane stress



- Elements representing cracks are shown in gray
- **TGO has a Non-uniform thickness of 16 μm ; R=0.75**
- At 10 μm crack spacing observed experimentally, maximum in-plane stress in the TGO material is ~ 190 MPa

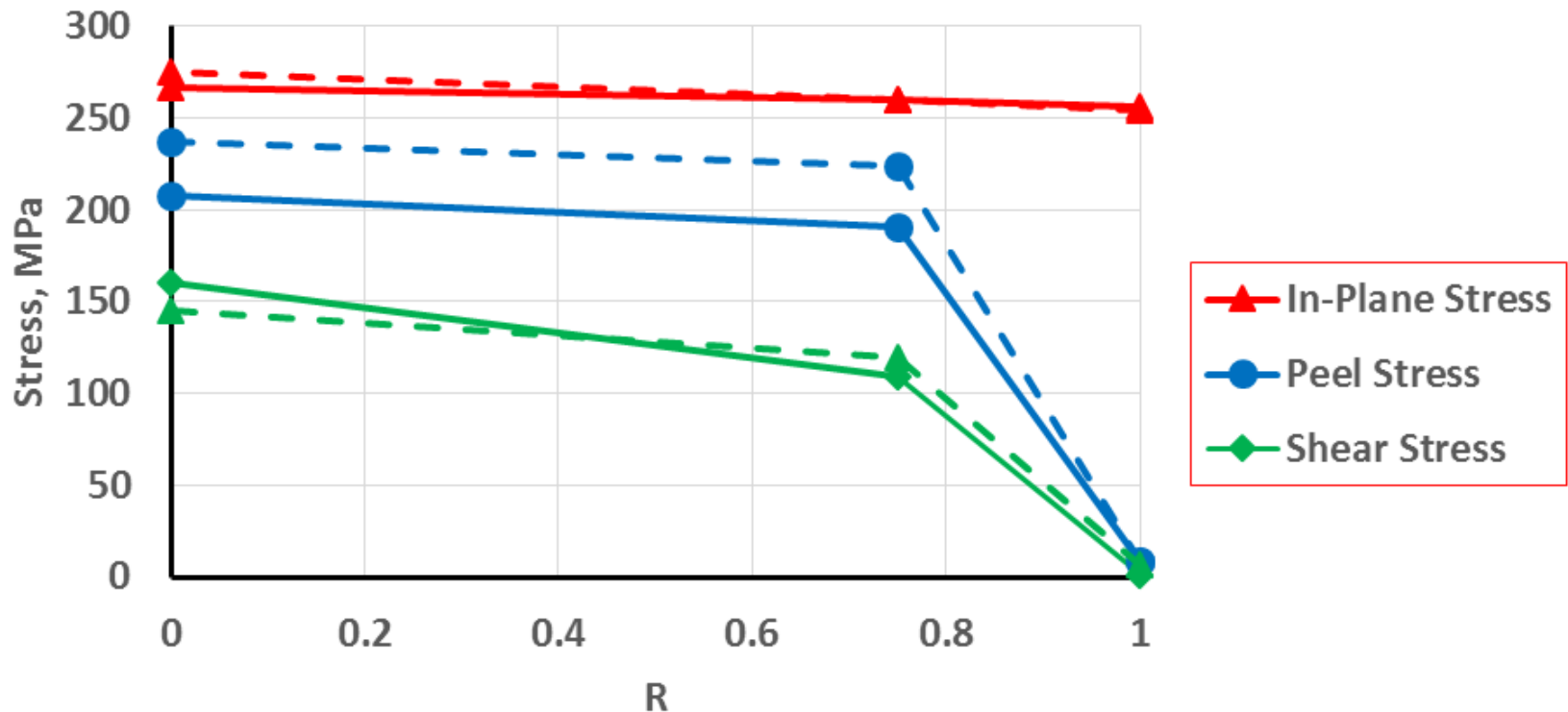


Comparison of Max Stresses in 3 and 4 Layer Systems with Undamaged TGO Layer (16 μm)



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Solid lines represent **4 layer** EBC system (Low Temp System)
Dash lines represent **3 layer** EBC system (High Temp System)



- Stresses are lower overall for 4 layer system compared to 3 layer
 - Peel stresses significantly lower (10%)
 - In-plane and Shear stresses are similar but slightly lower

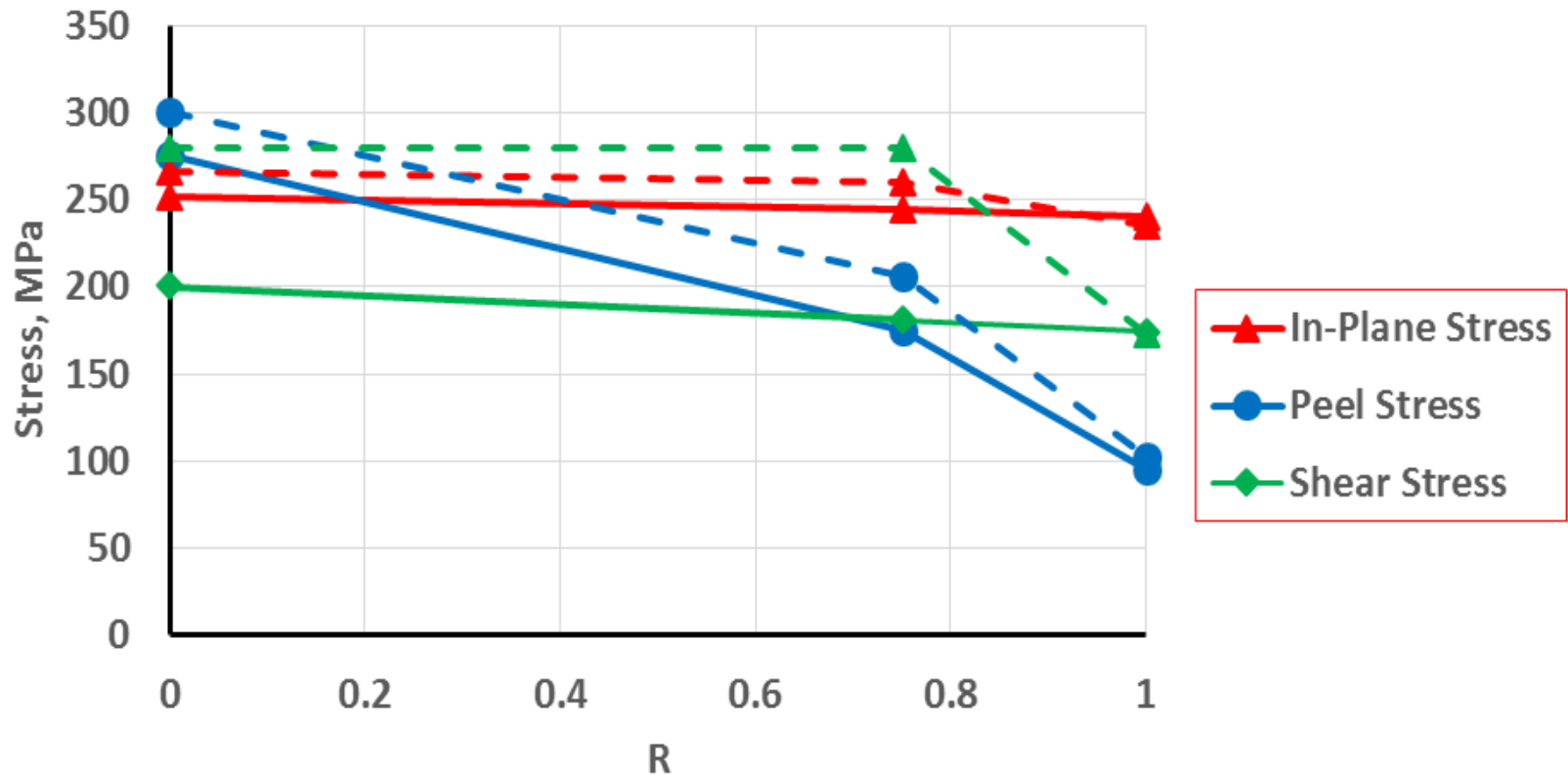


Comparison of Max Stresses in 3 and 4 Layer Damaged Systems; 16 μm TGO Layer, 10 μm Cracks



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Solid lines represent **4 layer** EBC system (Low Temp System)
Dash lines represent **3 layer** EBC system (High Temp System)



- Stresses are lower overall for damaged 4 layer system compared to 3 layer
 - Shear stresses significantly lower (~30%)
 - Peel stresses lower (~10%)