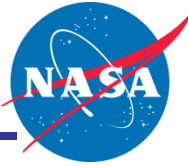




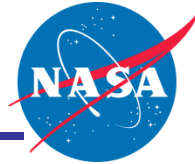
CFD for Aeroacoustics

David P. Lockard

Meelan M. Choudhari, Mehdi R. Khorrami,
Veer N. Vatsa

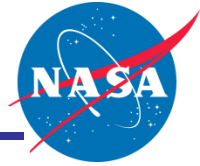


- Detailed study of the flowfield
 - Combined experimental / computational
 - Identify features in flowfield in which unsteadiness can develop
 - shear layers, vortices, separations
- Experimental measurement of source & noise details
 - Steady, unsteady surface pressure, hot-wire, PIV
 - Acoustic microphone arrays
 - Source location, spectra, directivity, amplitudes

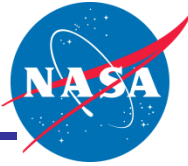


- Computational simulations of fluctuation-generating mechanisms
 - Computationally intensive prediction of source and resulting noise
 - Often gives a more detailed picture of the source than experiment alone
- Comparison / correlation
 - Understanding for noise reduction
 - Development of simplified models – based on flowfield features in common with actual configurations

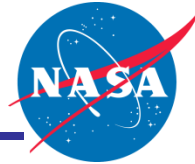
Why Unsteady Simulations?



- Acoustic source is inherently unsteady
 - Fourth space-time covariance of the Lighthill stress tensor $\sim \rho u_i u_j - \tau_{ij} + (p - c_o^2 \rho) \delta_{ij}$
 - Difficult to measure and model
- Steady RANS based noise prediction
 - Use the turbulence intensity and length scale as parameters in a model for the source
 - Efficient but highly dependent on modeling and calibration
- Unsteady simulations can be used to directly compute the noise source [for understanding and prediction] or to calibrate other methods

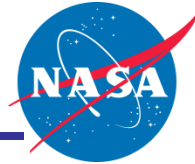


- Application of CFD tools to unsteady problems
 - Not involved with basic algorithmic development
 - Enhancements to collect data
 - Unsteady surface data
 - Time-averaged quantities
 - Evaluation of accuracy requirements
 - Time-step size & subiterations
 - Grid resolution
 - Testing of turbulence models
 - Validation studies
 - Analysis of configuration impacts on noise and performance

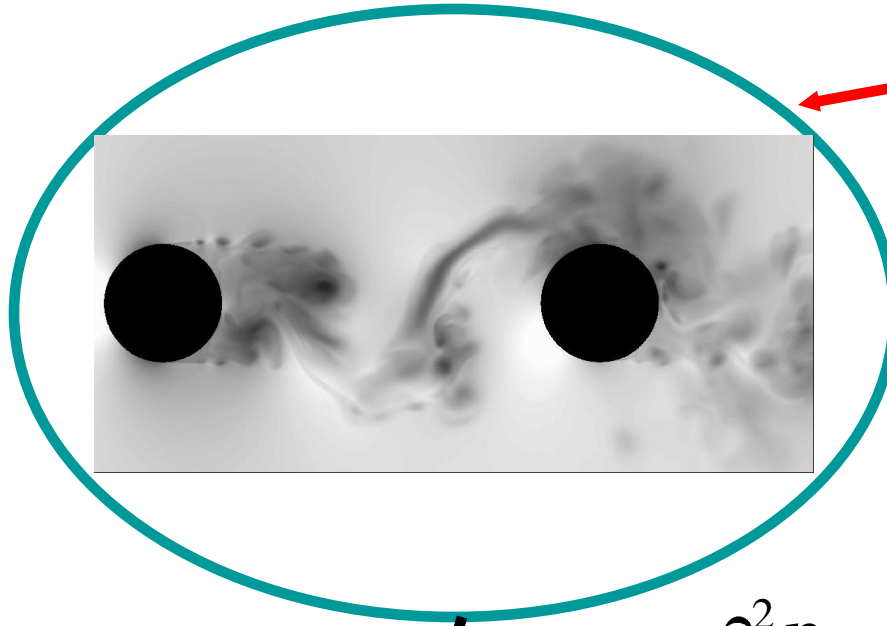


- Collaboration
 - NRA's
 - High-Fidelity Numerical Simulations in Airframe Aeroacoustics
 - Prof. Hussaini, Dr. Uzun of Florida State University
 - High-order LES on massively parallel computers
 - Space Act Agreements (SAA)
 - Gulfstream Partnership
 - Visiting researchers
 - ONERA
 - JAXA (awaiting final approval)
 - Sponsor workshops

How Do We Compute the Noise?



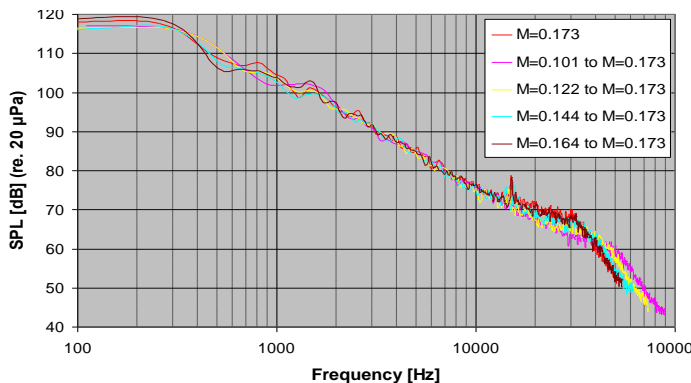
Unsteady
Numerical
Simulation



Accurately determine the unsteady noise source characteristics and account for near-field scattering.

$$\frac{\partial^2 p}{\partial t^2} - c_0^2 \frac{\partial^2 p}{\partial x_i \partial x_i} = \square^2 p = S(x_i)$$

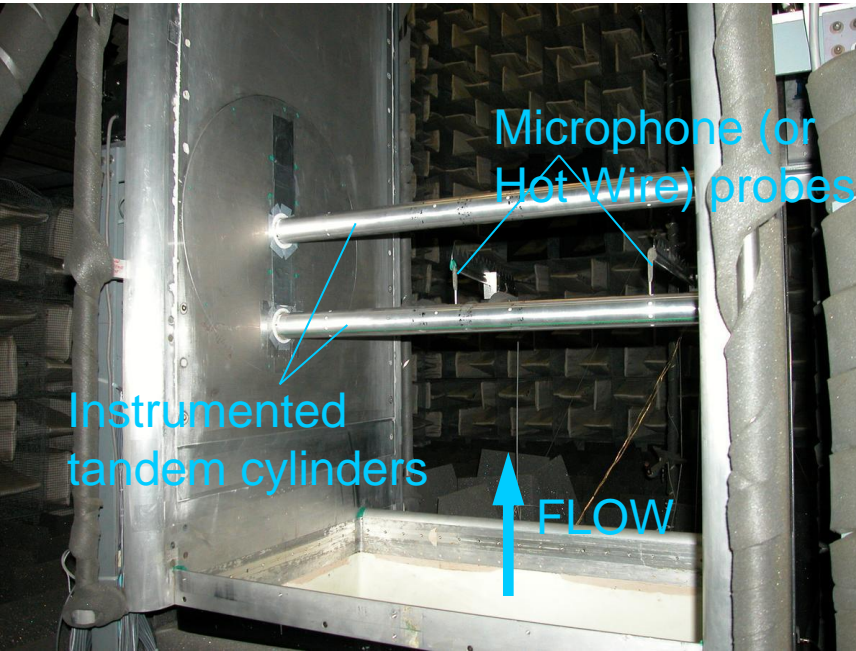
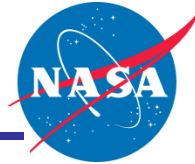
Experiment



Obtain the noise at far-field listener positions

- Physical insight
- Cause & effect relationships
- Detailed source description

Tandem Cylinders

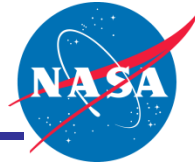


- BART + QFF measurements of tandem cylinders (prototype for landing gear interactions)
- Comparison with CFD+FWH computations

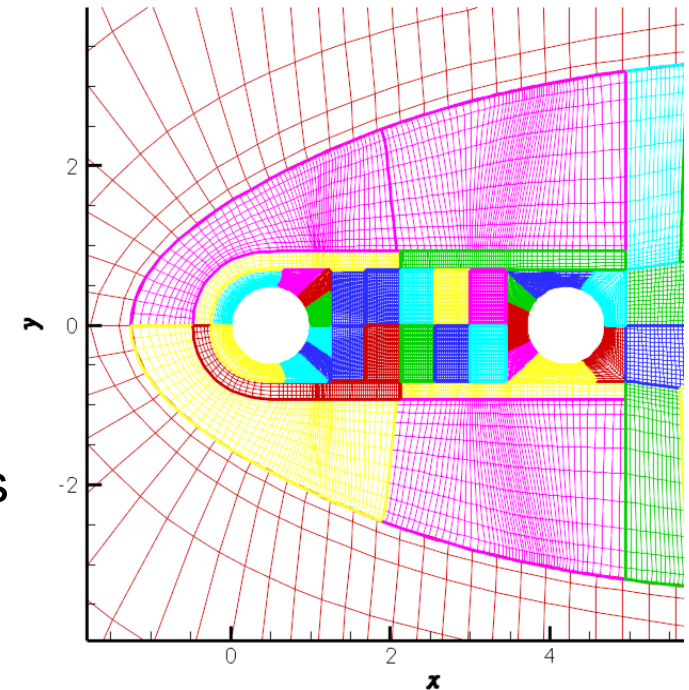


- Extensive aero comparisons
- Acoustics

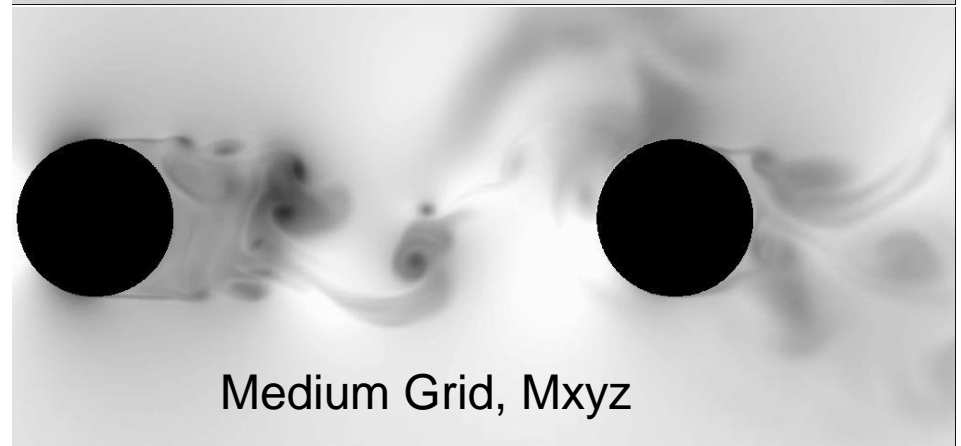
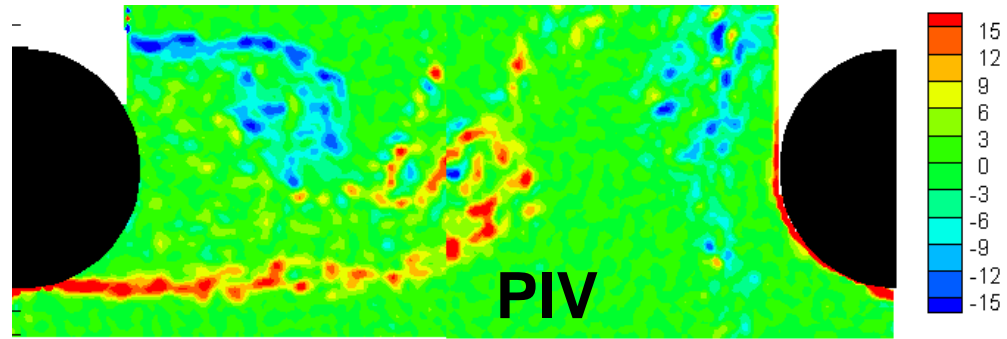
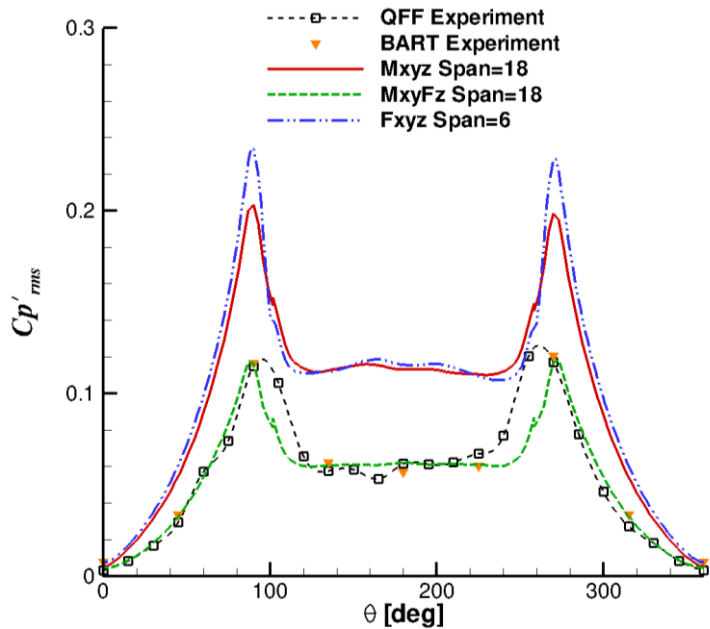
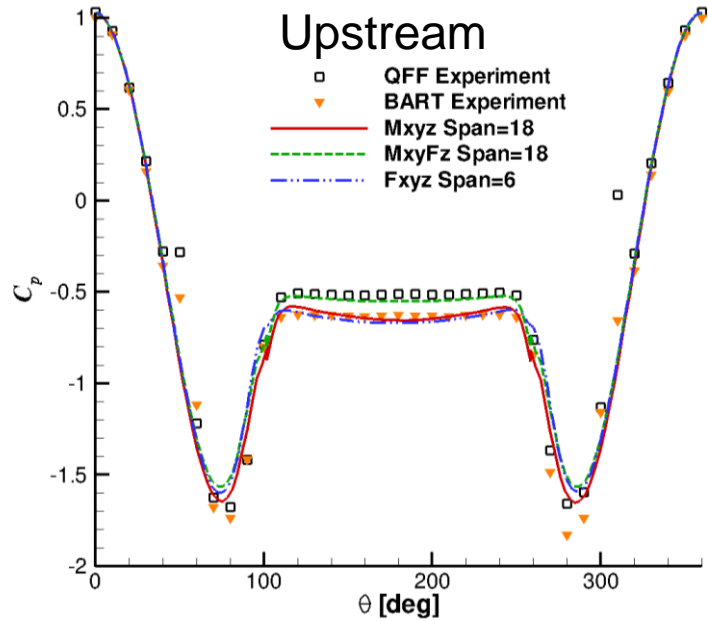
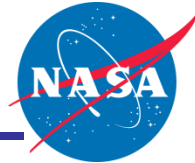
Computational Approach



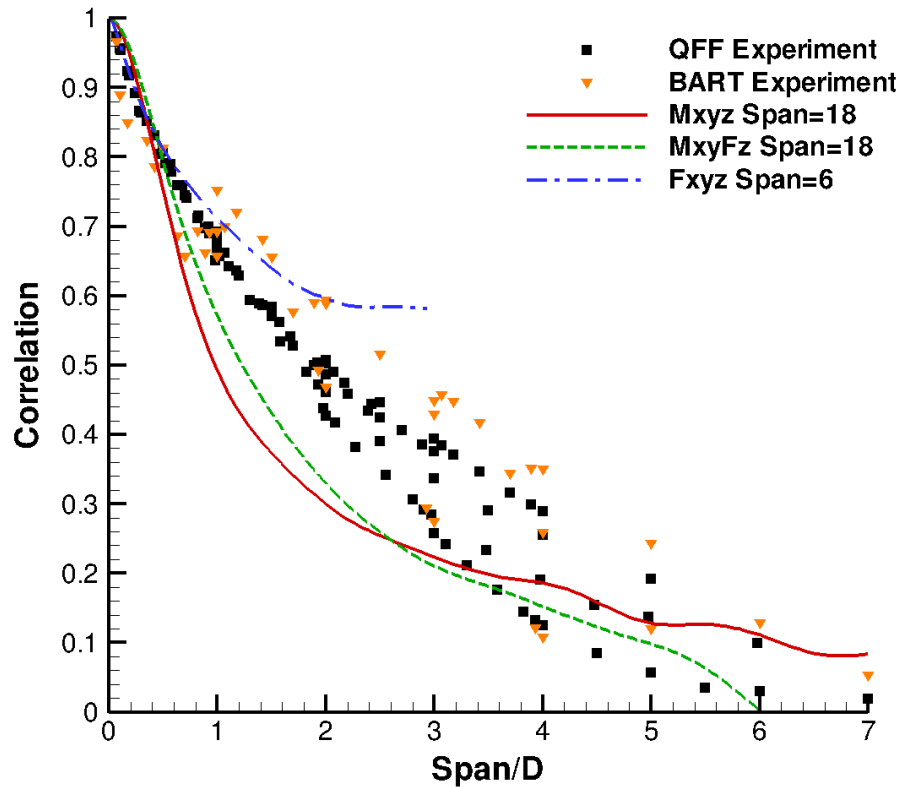
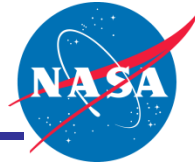
- Unsteady CFL3D Computations
 - 3D Navier-Stokes solver
 - Upwind, nominally 2nd order in space
 - 2nd order implicit time stepping (dual time)
 - Modified Menter's SST K- ω turbulence model
 - Production term turned off outside of boundary layers
- Block Structured Grids
 - Spans of 3, 6, 18
 - Grid refinement
 - 5M – 80M grid points
- Operating Conditions
 - Re=166E3
 - Fully turbulent simulations
 - Transition strip used in experiments
 - M=0.166



Tandem Cylinders

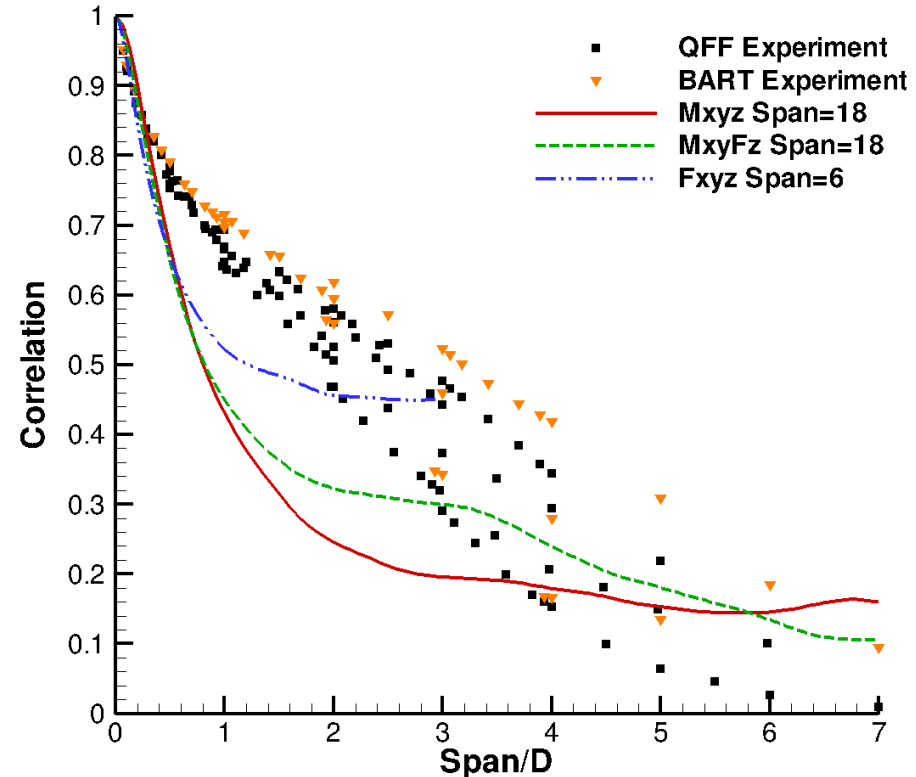


Spanwise Correlation



Upstream

135 deg

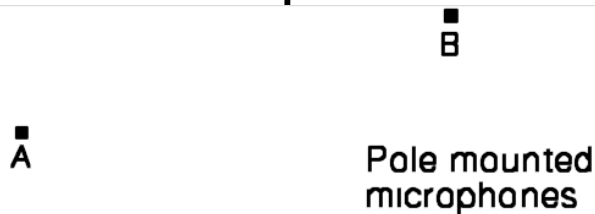


Downstream

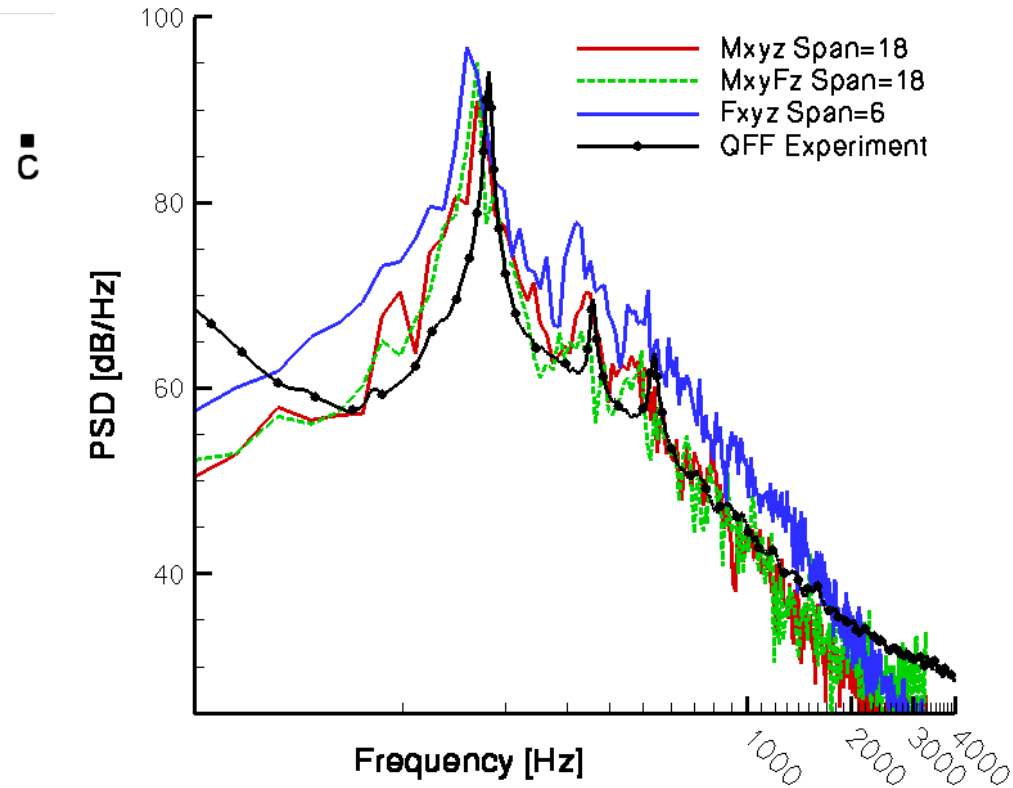
- Similar correlation on upstream and downstream cylinders
- Only span=18 calculations capture the complete decay

- Ffowcs Williams – Hawkings Noise calculations

- Integral technique derived from the Navier-Stokes equations

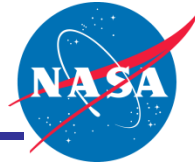


Tandem Cylinders

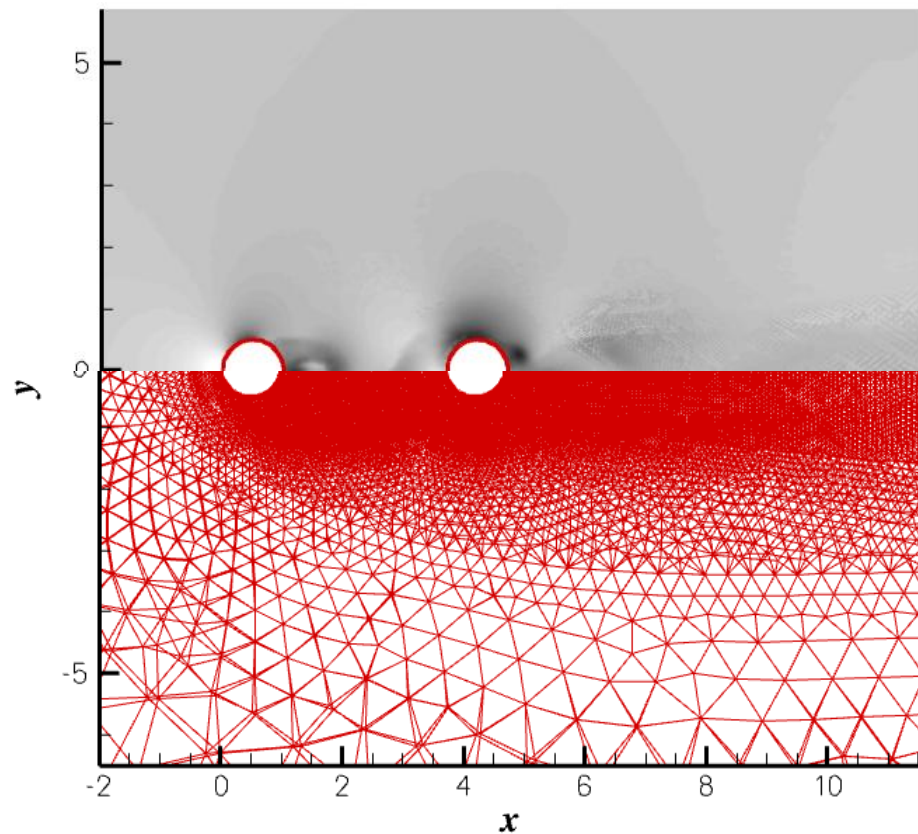


Spectra at A

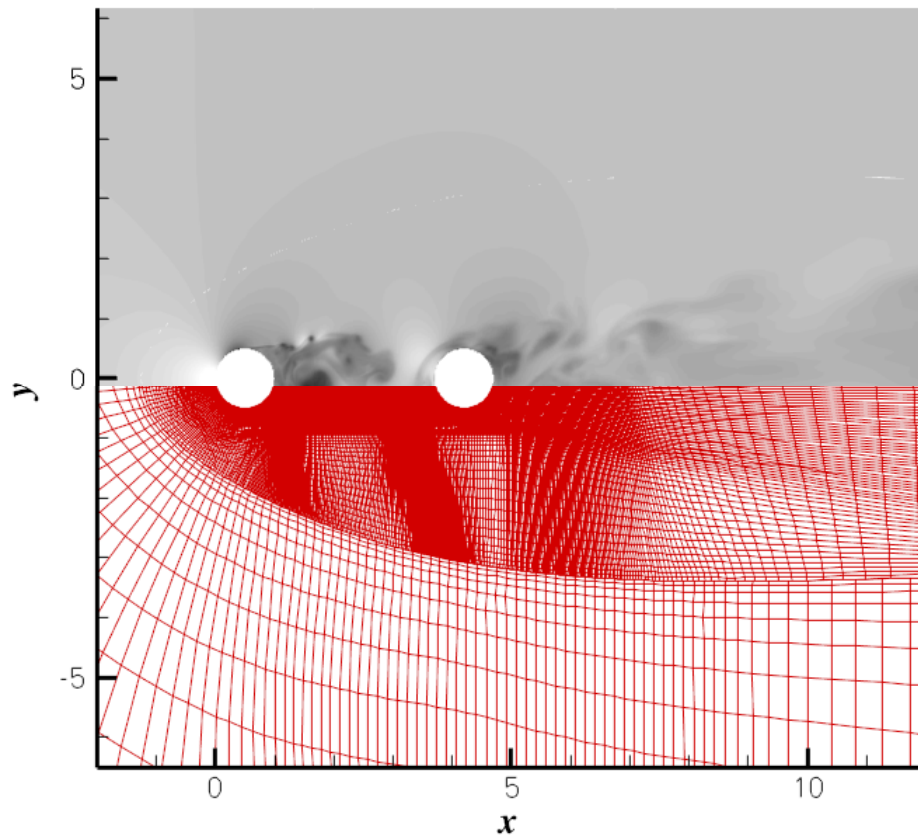
Tandem Cylinders



- Evaluating different numerical approaches using cylinder test cases
 - Hybrid RANS/LES turbulence models

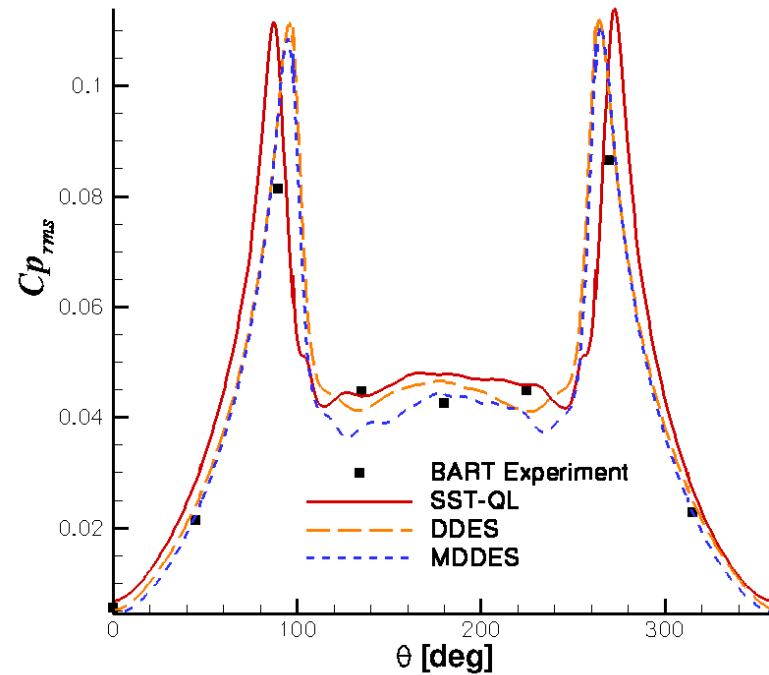
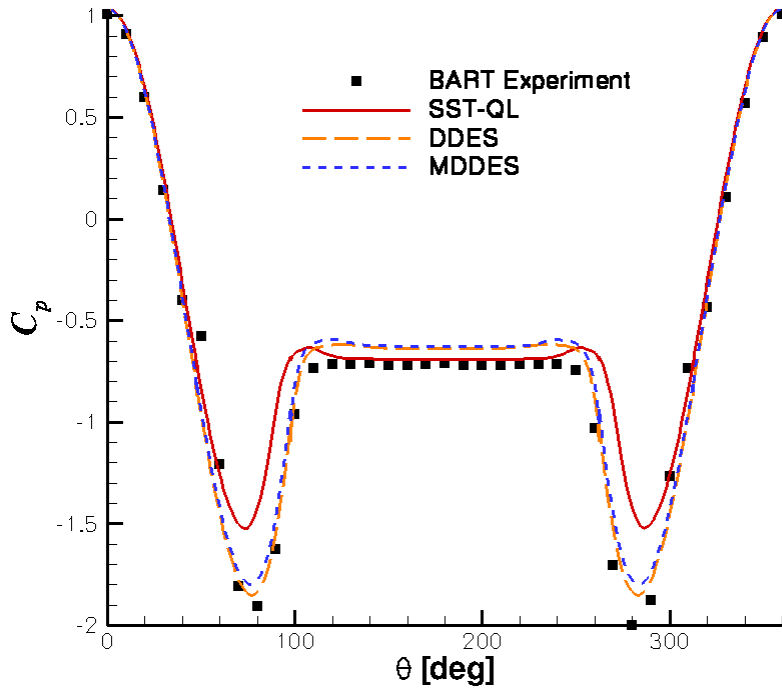
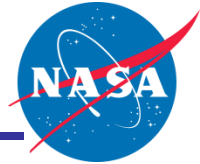


Unstructured Grid



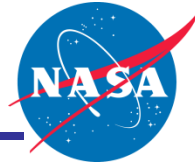
Structured Grid

Single Cylinder Results

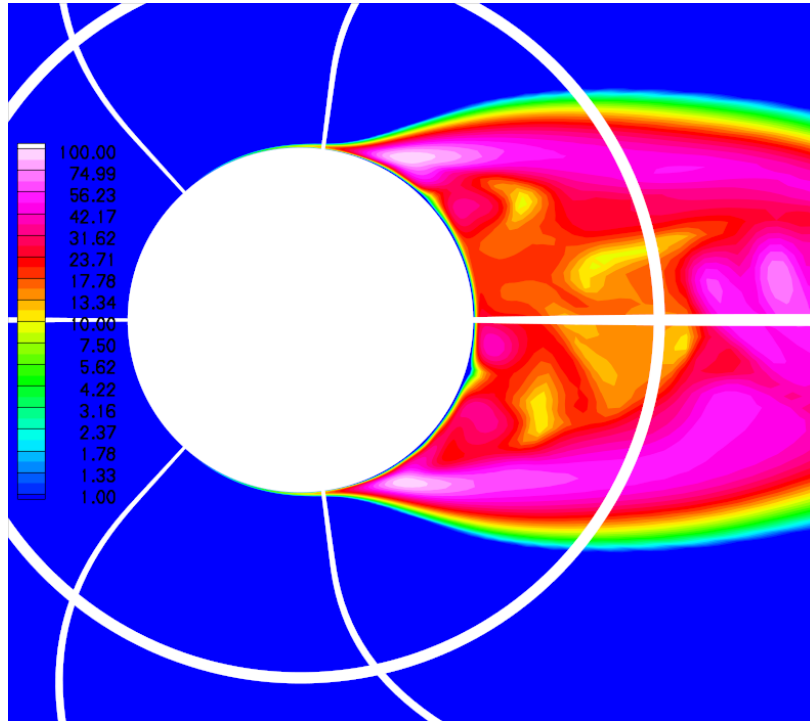


- Modified DDES (MDES) also changes the production term using the f_d function

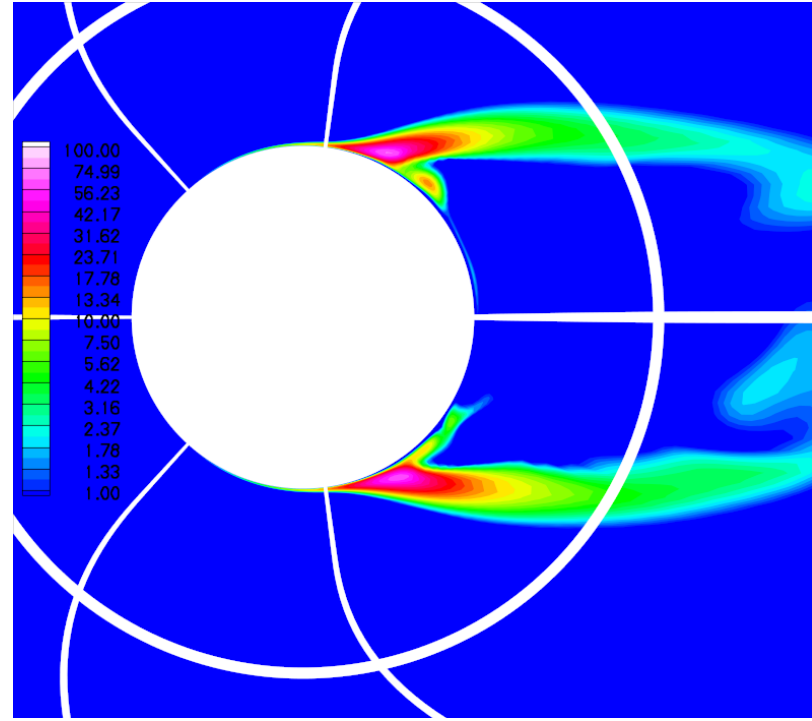
Single Cylinder Eddy Viscosity Results



DDES

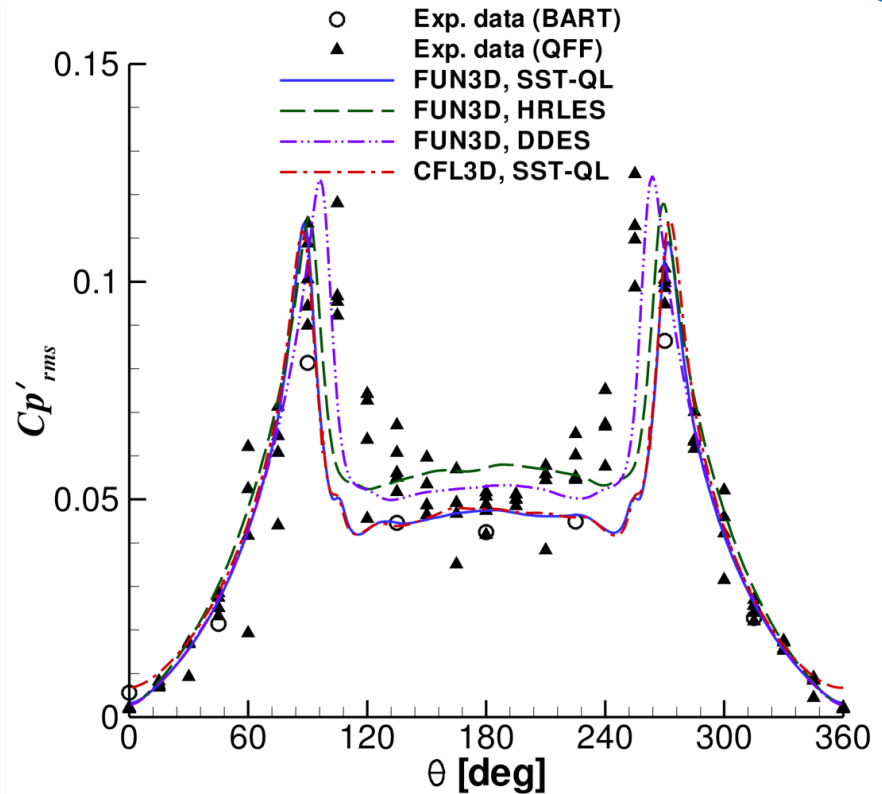
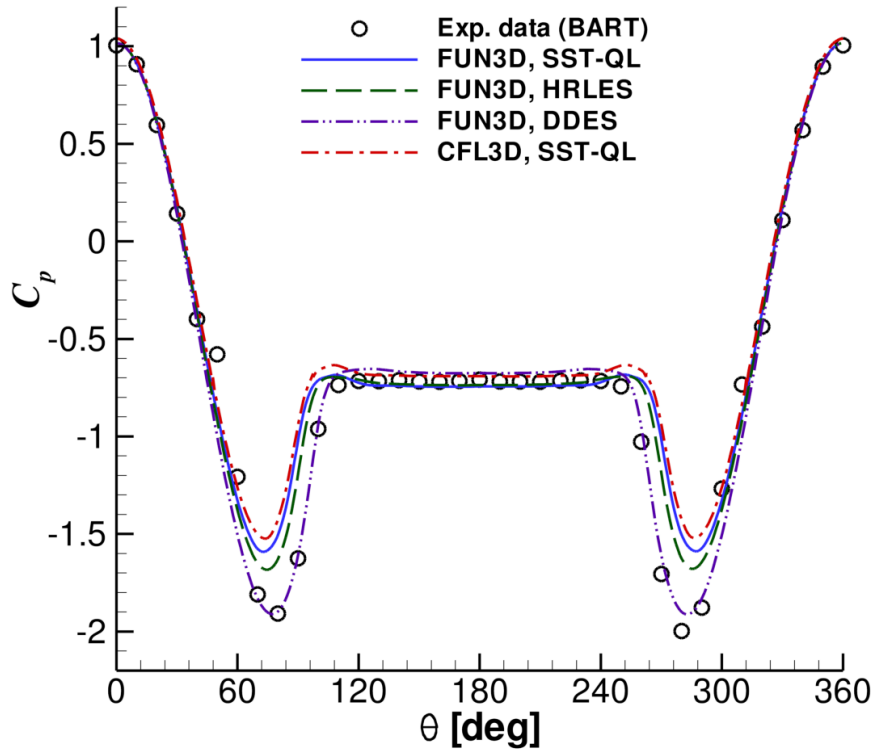
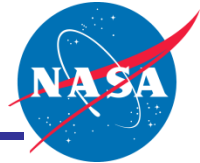


MDDES



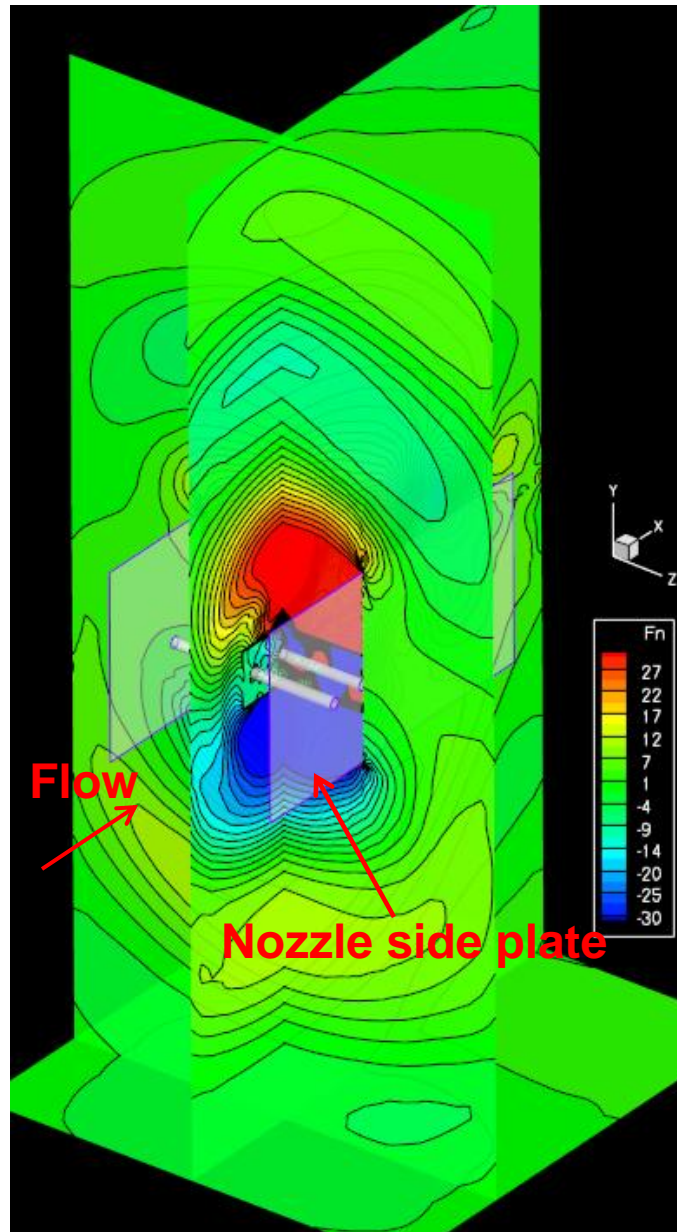
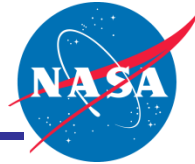
- MDDES maintains near wall behavior but decreases eddy viscosity that propagates into the field
 - Have not observed significant differences in measured quantities in any problem tested

Single Cylinder Results



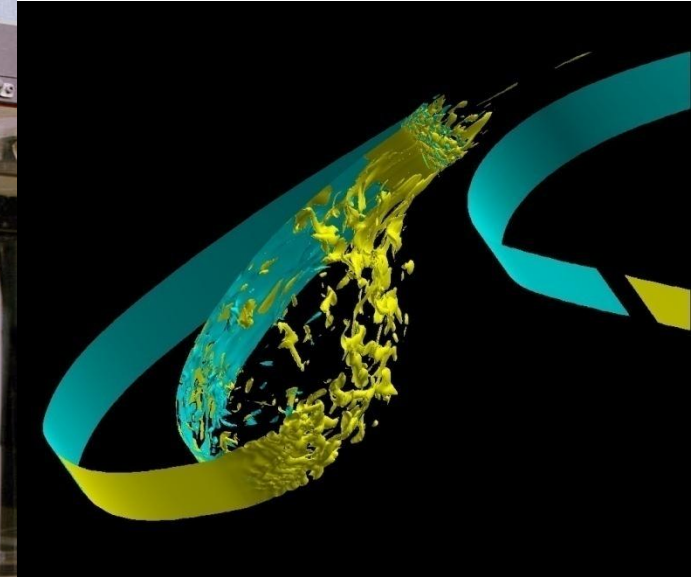
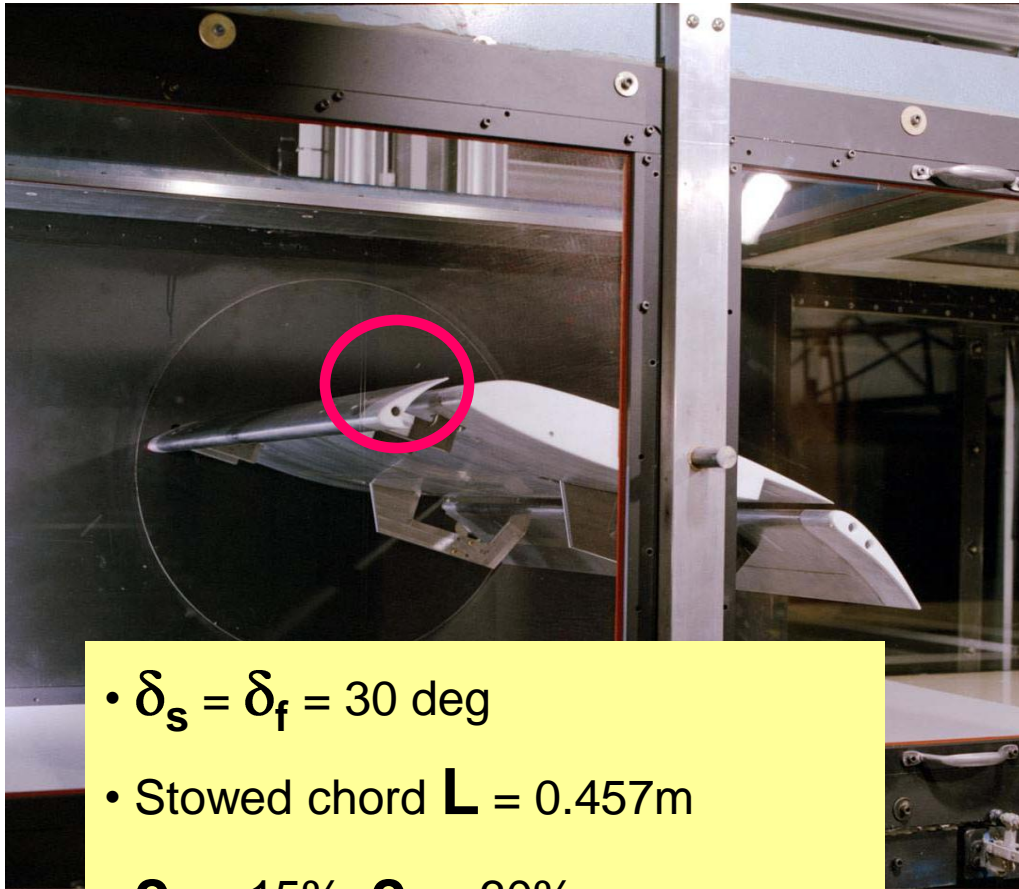
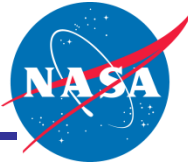
- Good agreement between CFL3D (structured) and FUN3D (unstructured)
 - Used same grid in both codes
- Most turbulence models produce early separation
 - High Re flows difficult to simulate

Installation Effects: Scattering Simulations



- Collaborative effort to quantify installation effects on acoustic experimental data
 - Space Act Agreement (SAA) between NASA and ONERA
- ONERA's high-order, overset grid CAA code used to compute acoustic propagation
 - Source imposed from near-field CFD simulation
 - Compare free-field results with case including scattering from nozzle side plates and collector

30P30N BART Configuration

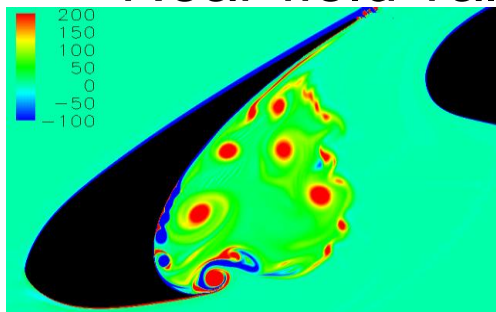


- $\delta_s = \delta_f = 30$ deg
- Stowed chord $L = 0.457$ m
- $C_s = 15\%$; $C_f = 30\%$
- $Re_L = 1.7$ M

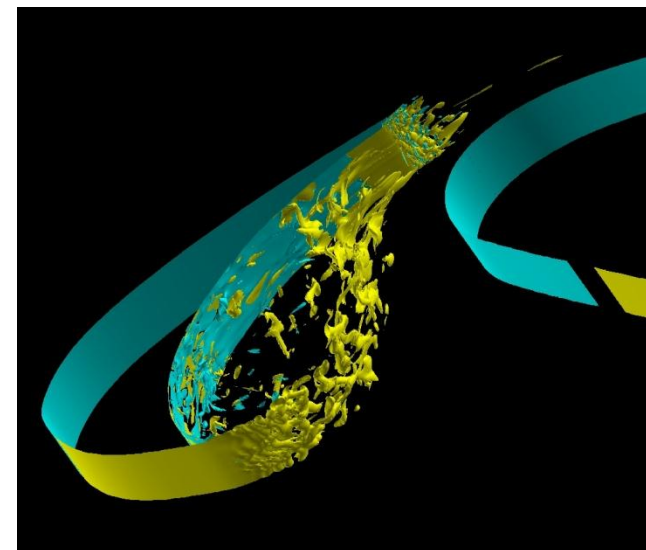
Investigating a span = $2.24 C_s$ using 186 million grid points

30P30N High-Lift in BART

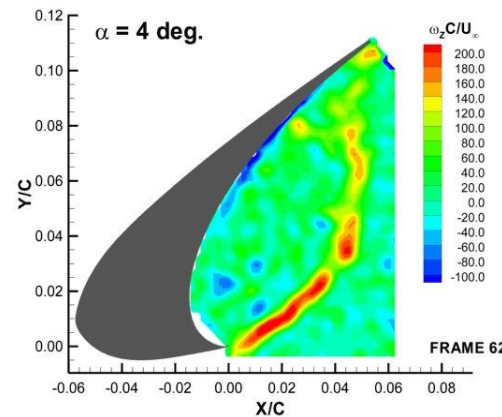
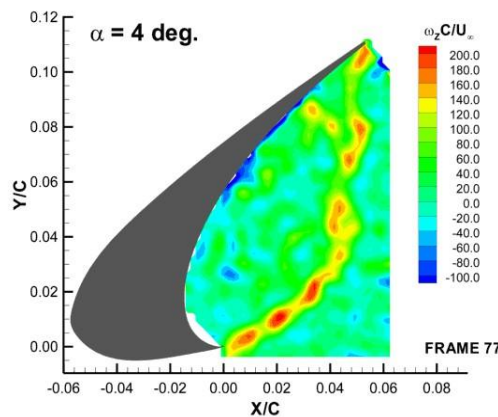
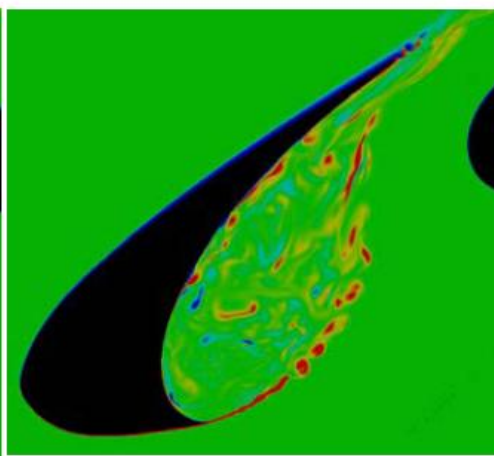
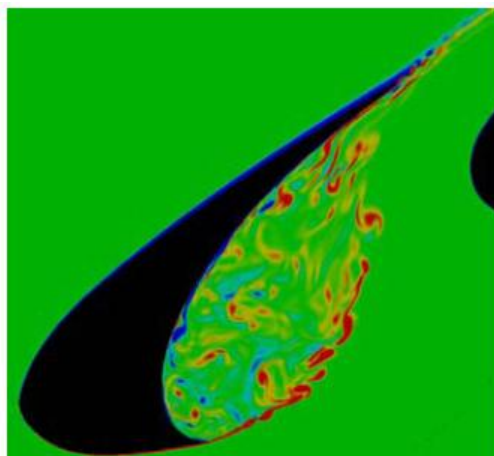
Near-field validation for Instantaneous vorticity-field



2D, in-tunnel CFD

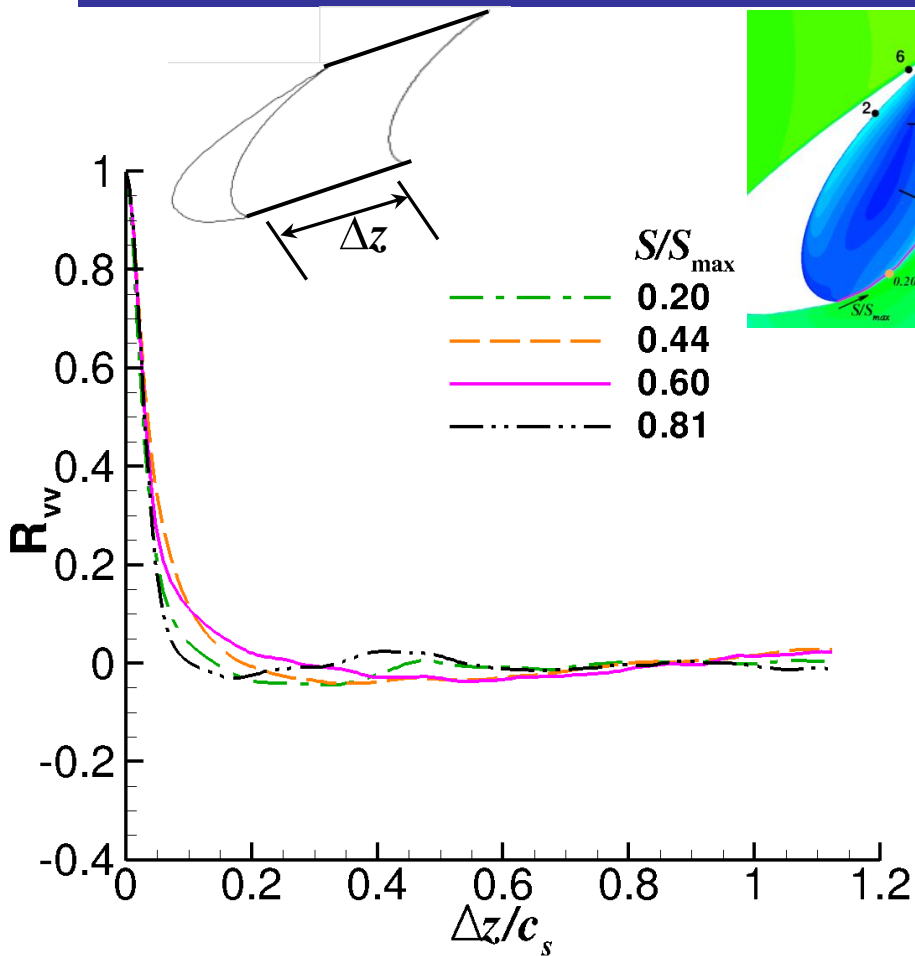
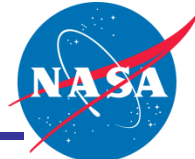


3D CFD

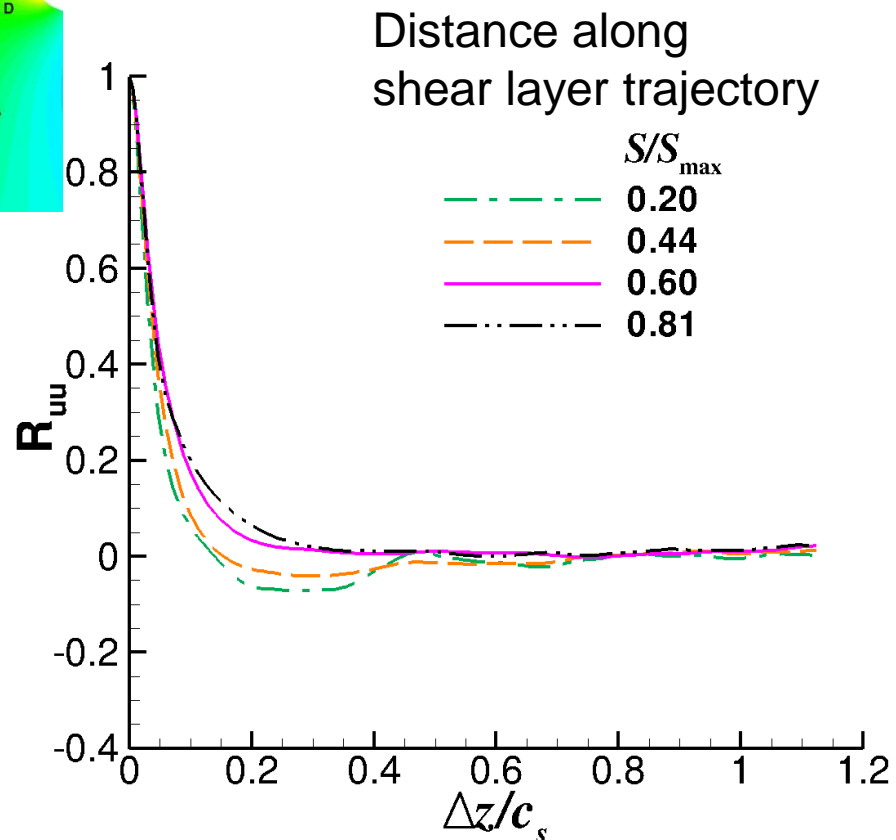


PIV
Jenkins '04

Spanwise Velocity Correlation



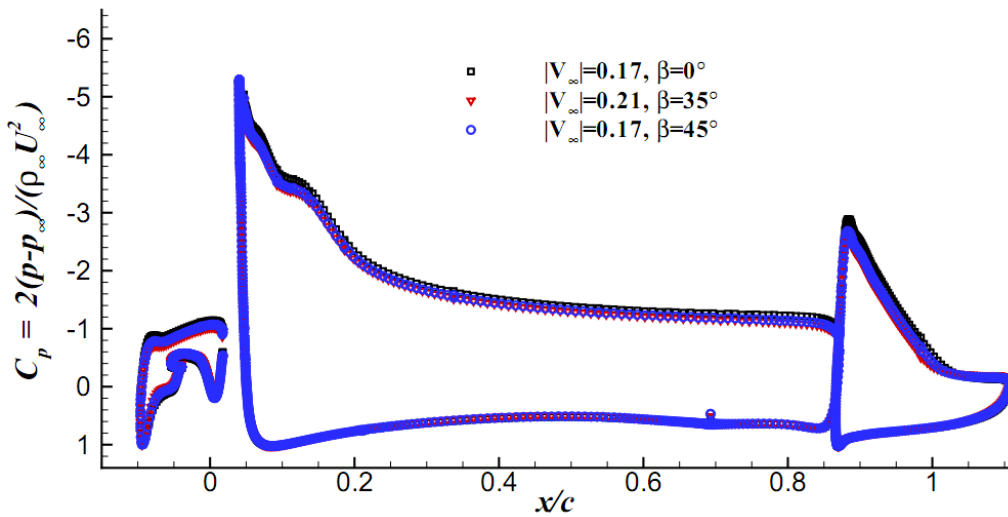
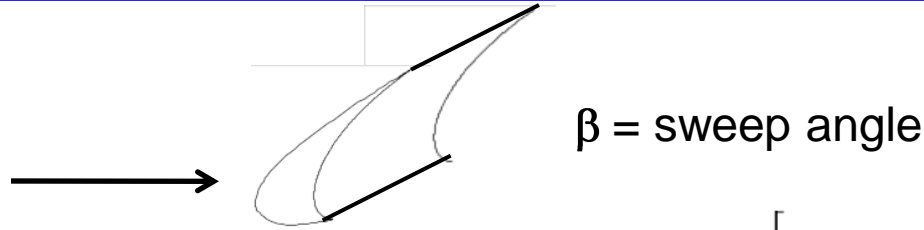
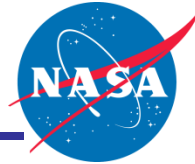
Correlation of v



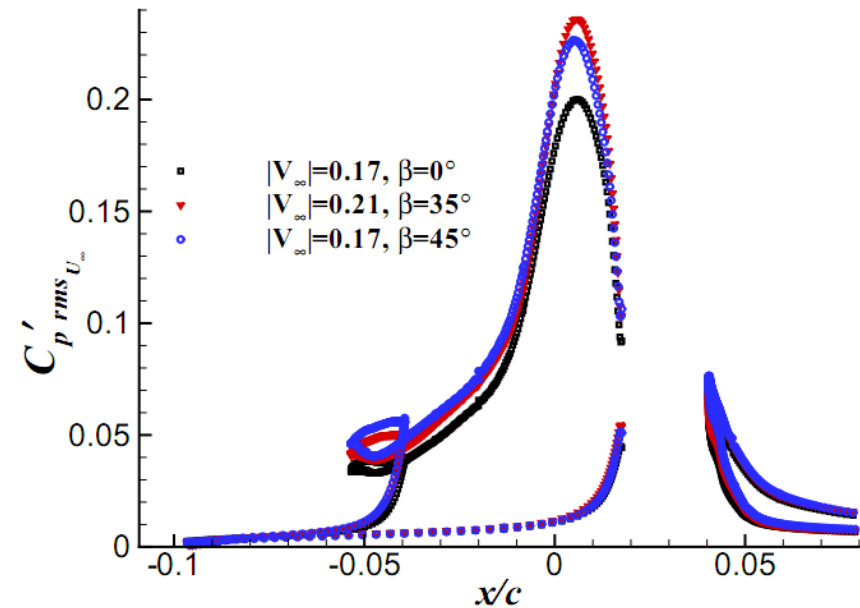
Correlation of u

- Appear to need a span of $2 \times 0.4 = 0.8 c_s$

Investigating the Effect of Sweep



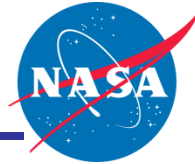
Time-averaged Surface Pressure



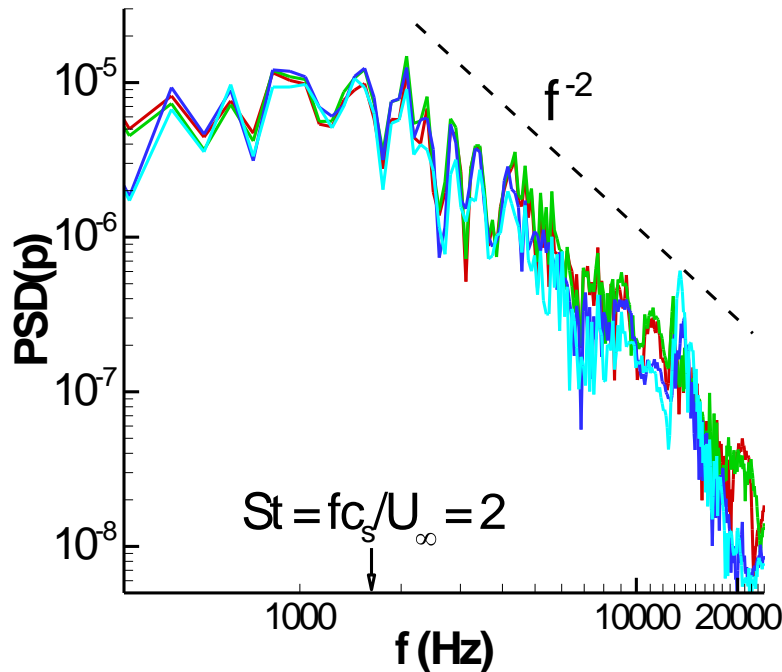
RMS Surface Pressure

- C_p collapses with velocity normal to leading edge
- Different behavior of rms of C_p

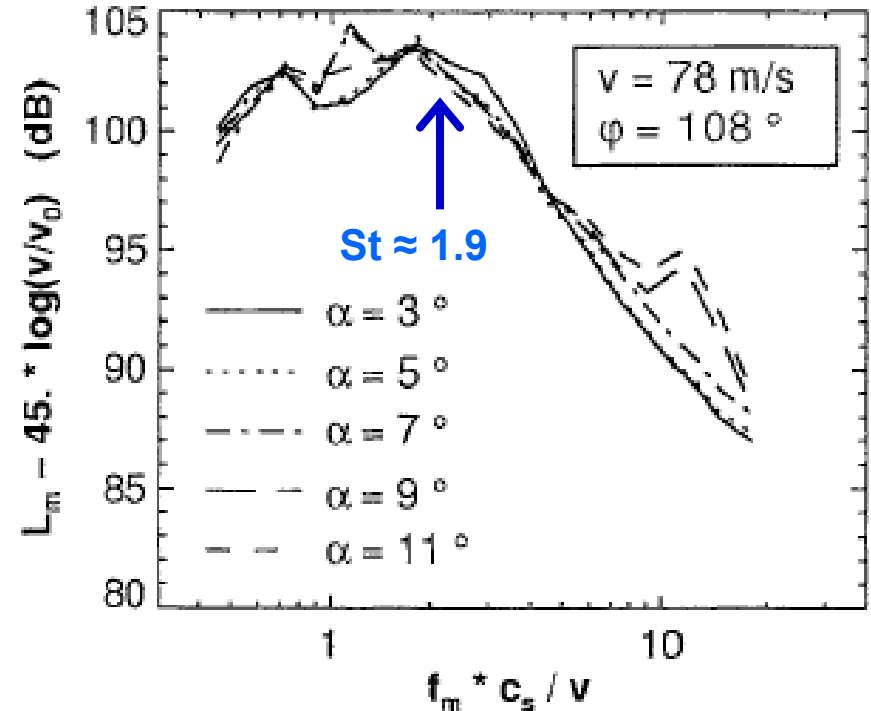
Acoustic Spectrum



CFD



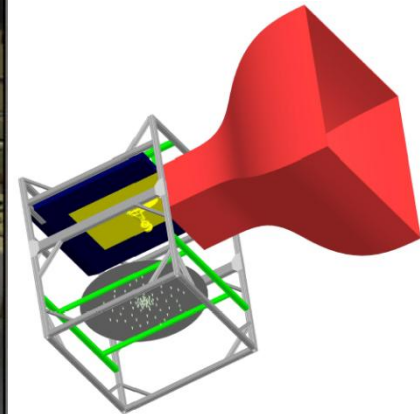
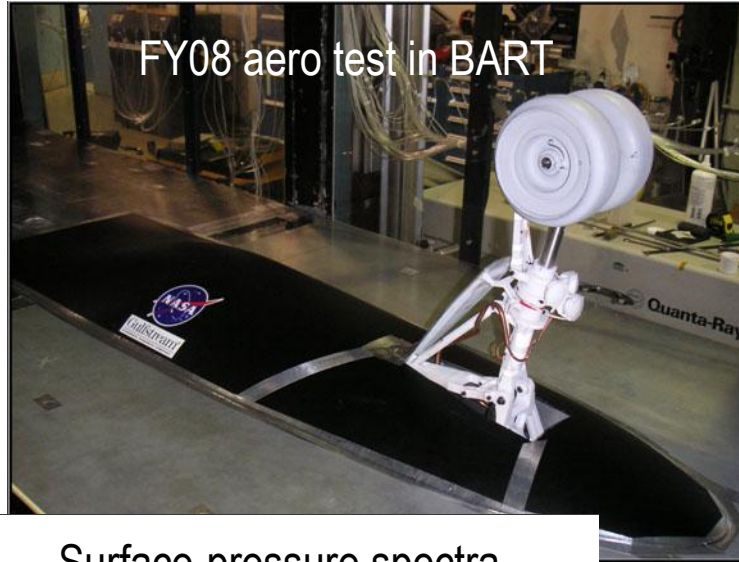
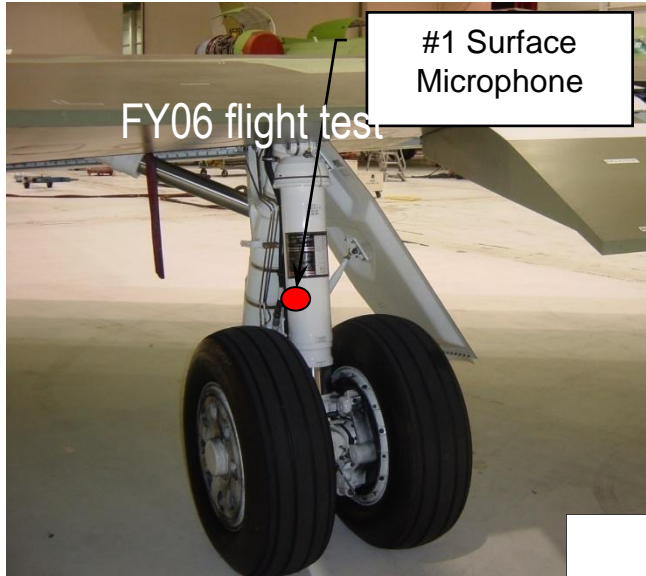
Dobrzynski+Pott-Pollenske (2001)



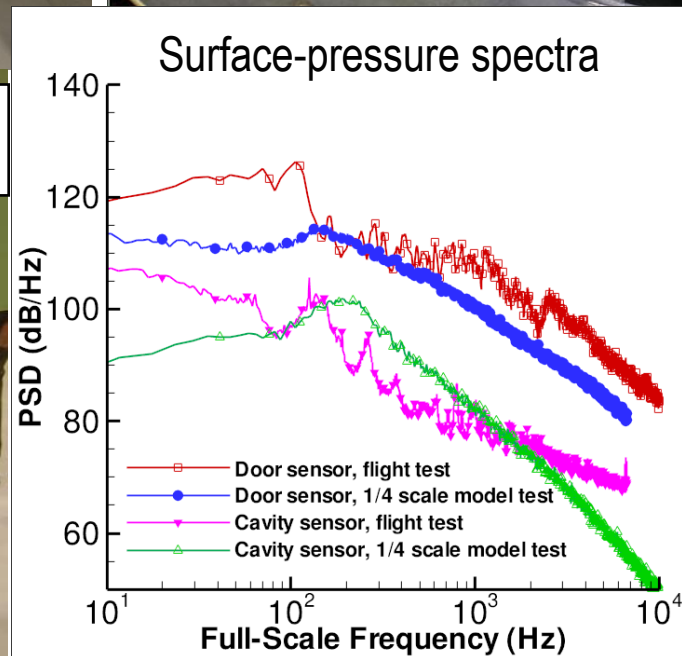
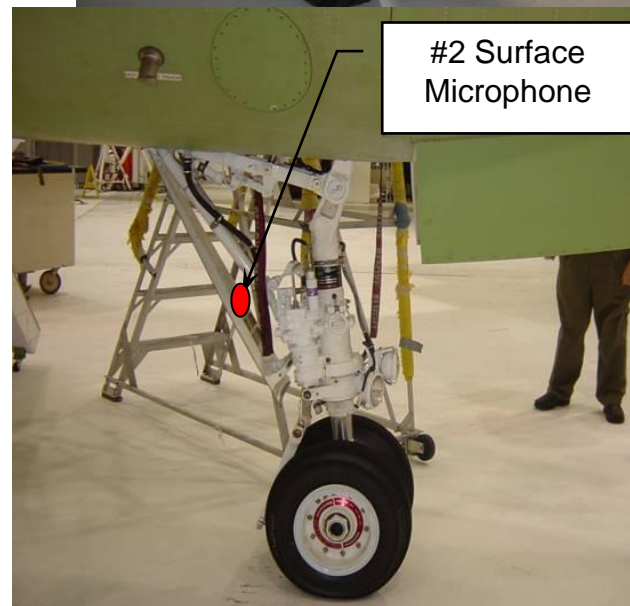
- Acoustic spectrum similar to p' spectrum near reattachment
- $St \equiv fc_s/U = 2-3 \Rightarrow f \approx 155-233$ Hz for $L = 5$ m ($M=0.17$)
- f^{-2} like roll-off similar to model (Guo), data (Mendoza+Brooks), and observations for other shear flows (Lilley)

NASA-Gulfstream Partnership: Nose Landing Gear

Comparison between model-scale and full-scale surface pressure fluctuations



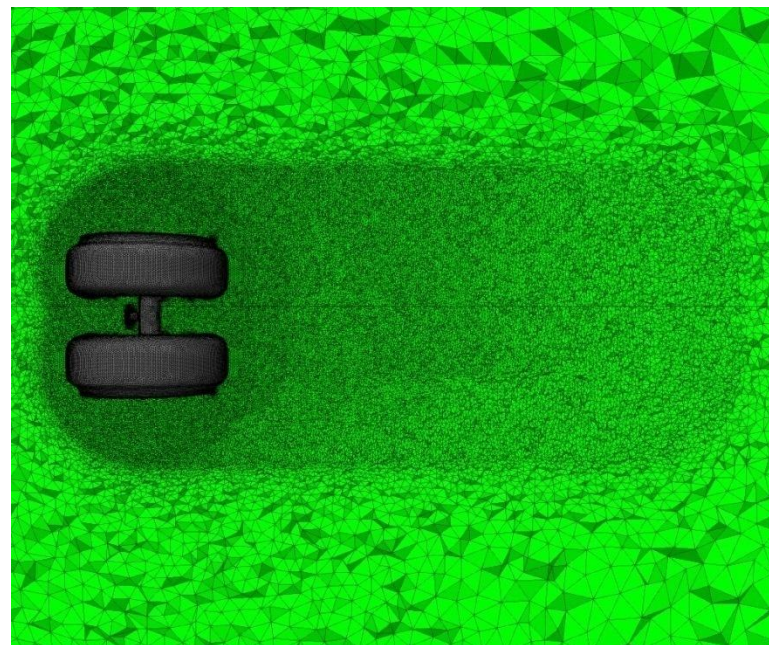
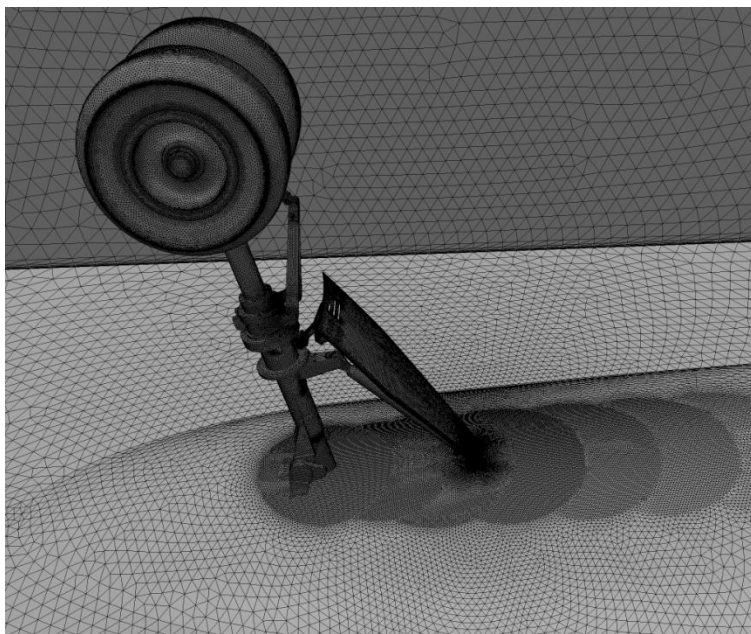
Acoustic Testing at UFL
Gulfstream funded



- SAA between NASA and Gulfstream
- Extensive experimental dataset from tunnel tests
- Connection to flight

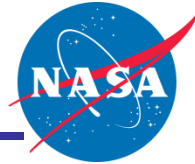
Nose Landing Gear

- Concurrent aeroacoustic simulations:
 - FUN3D unsteady simulations of partially dressed gear, no cavity
 - Generation of highly resolved grids
 - Tetrahedral and mixed-element grids
 - Required enhancements to the grid generation process
 - Consistent family of grids generated

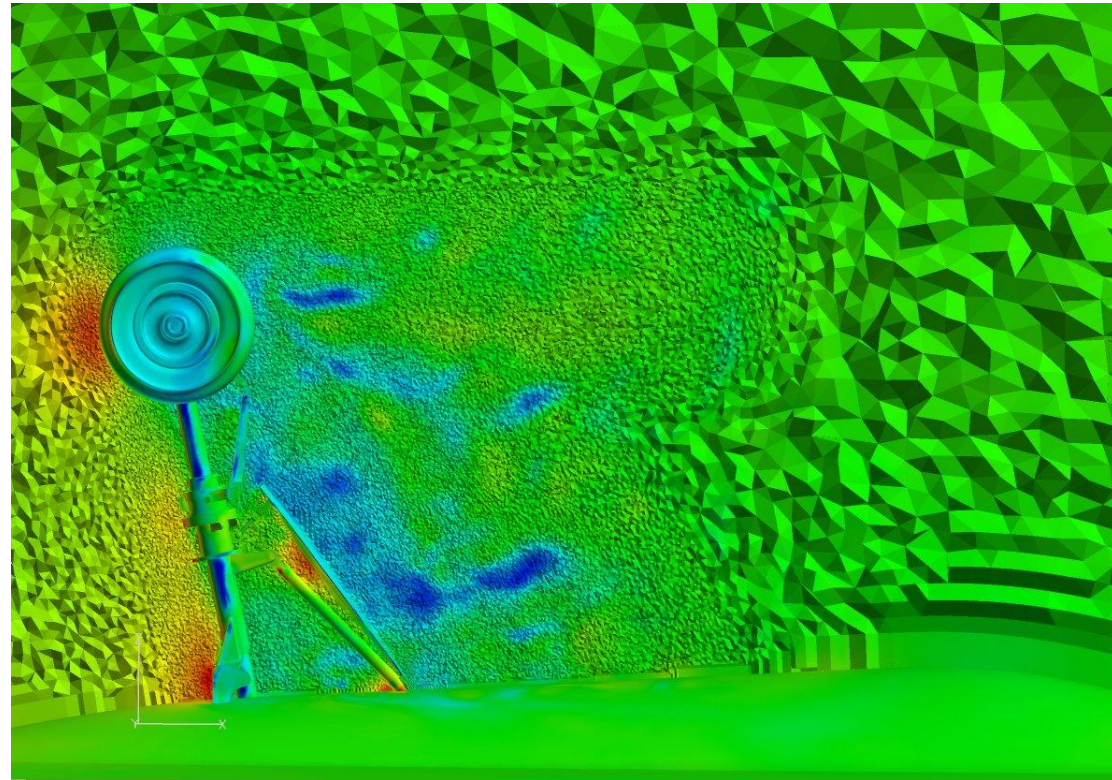
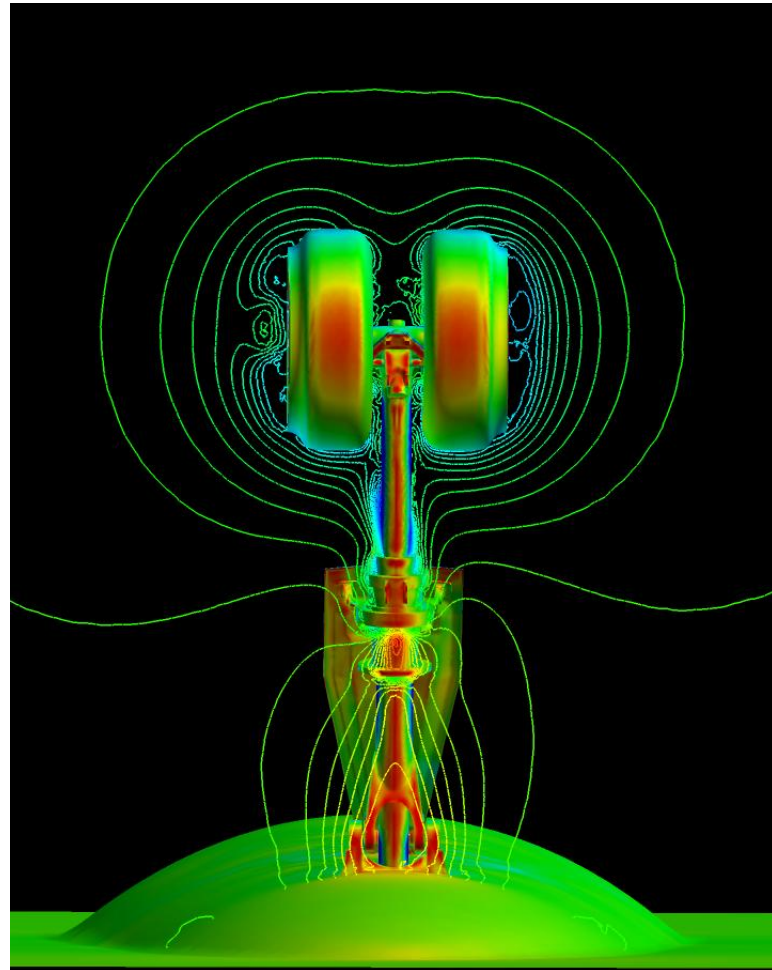


Critical to resolve gear wake

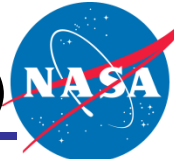
Nose Landing-Gear Configuration



Instantaneous pressure from FUN3D simulation

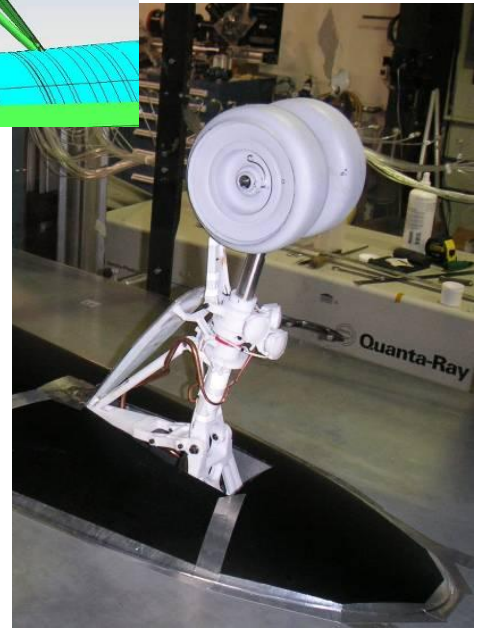
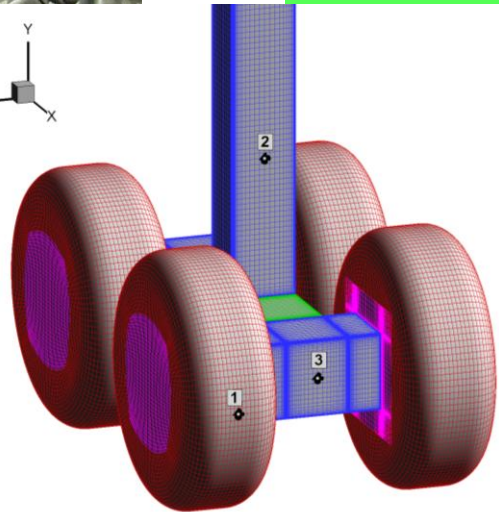
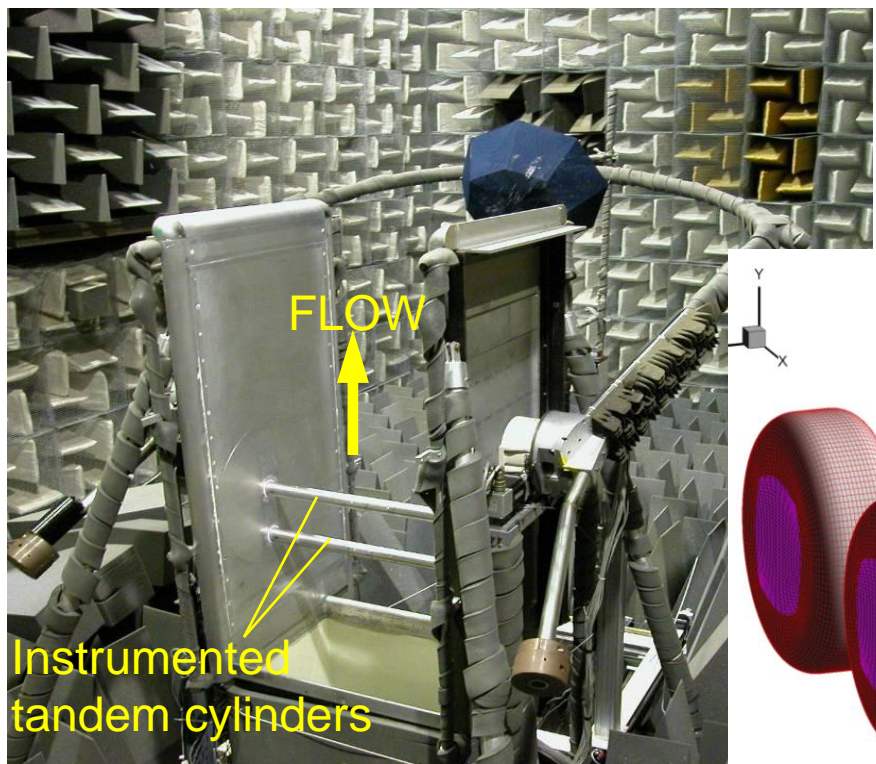
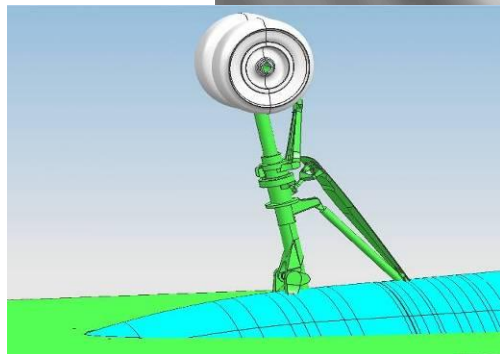
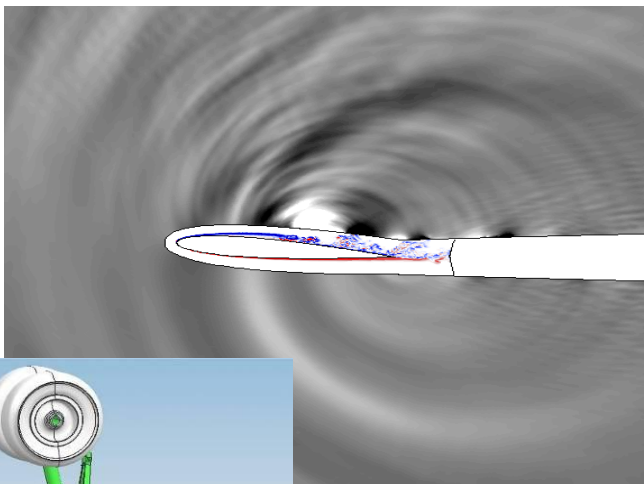


- Family of 3 meshes – 9, 25, 71 million nodes
 - Manually refined 48 million node mesh
- Two turbulence models

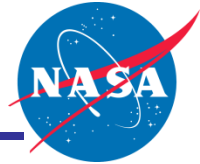


Benchmark problems for Airframe Noise Computations I (BANC-I)

- 2010 workshop following AIAA/CEAS Aeroacoustics conference in Stockholm
 - Tandem cylinders (NASA dataset)
 - Trailing-edge scattering (Multiple datasets)
 - Nose landing gear (NASA dataset)
 - Main landing gear (Boeing dataset)

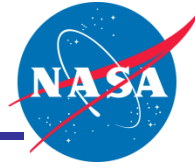


BANC Workshops



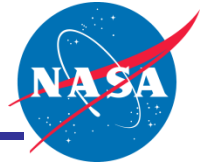
- Computational AeroAcoustics (CAA) community developed a set of verification and validation cases from a series of 4 CAA Workshops
- A new series of workshops (BANC) is being organized in coordination with the AIAA Aeroacoustics and Fluid Dynamics Technical Committees
 - Complex configurations for which no exact solutions are available
 - 2 of the 4 problems use NASA datasets
 - Holistic datasets from unsteady aero to acoustics, with a thorough quantification of the individual stages or links
 - Also valuable for the unsteady CFD community
 - Collective efforts (computations AND experiments) for common configurations
 - Develop validation cases for airframe noise applications
 - Iterative process refining computations and experimental data

BANC Summary



- Collective effort to develop validation cases for complex airframe noise configurations
 - Develop confidence and identify problems more rapidly
 - Leverage different expertise / distribute the expenses
 - Formation of AIAA Discussion Group on Benchmark Experiments and Computations for Airframe Noise
(<https://info.aiaa.org/tac/ASG/FDTC/DG/BECAN.aspx>)
- Several BANC workshops envisioned
 - BANC I: June 10-11, 2010
 - 55+ Notices of Intent (NoI) to participate in workshop
 - 12 countries represented (US, UK, France, Germany, Belgium, Sweden, Netherlands, Italy, Japan, Brazil, Australia), 5 airframers, 6 government agencies, 5 software vendors, 3 research consortia, 18+ universities
 - Other datasets for following workshop (besides continued consideration of BANC-I configurations) currently under consideration and/or development

Summary



- Unsteady simulations are enhancing our understanding of acoustic sources
 - Computations are expensive
 - Errors can be large and are unknown without experimental data
- Using a collaborative, community oriented approach
 - Collecting high-quality experimental data
 - Assessing different models and numerical techniques

