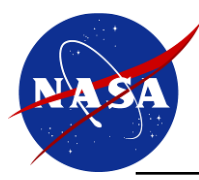


CFL3D and FUN3D Analysis of HiLiftPW-1 Workshop Cases

Elizabeth M. Lee-Rausch & Christopher L. Rumsey
NASA Langley Research Center

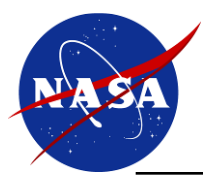
1st AIAA CFD High Lift Prediction Workshop (HiLiftPW-1)
Sponsored by the Applied Aerodynamics TC
Chicago, IL

June 27-27, 2010



CFD Code Descriptions

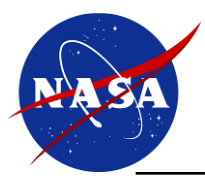
- CFL3D Structured-Grid Code
 - Thin-layer Navier-Stokes equations in all coordinate directions
 - Parallel 3D compressible cell-centered finite-volume RANS
 - Implicit local time-stepping using AF relaxation for linear system
 - Upwind Roe flux-difference splitting for inviscid fluxes
 - Spalart-Allmaras and SST turbulence models, fully-turbulent
- FUN3D Unstructured-Grid Code
 - Full Navier-Stokes equations-node centered
 - Parallel 3D compressible finite-volume RANS for mixed-element meshes
 - Implicit local time-stepping using multi-color point Gauss-Seidel relaxation for linear system
 - UMUSCL 0.5 scheme (Averaging + Upwind) for inviscid fluxes with Venkatakrishnan limiter
 - Combined Green-Gauss and edge-based gradients for viscous fluxes
 - Spalart-Allmaras turbulence model, fully-turbulent



Cases and Grids

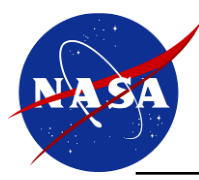
- Required Case 1 and Case 2
- Optional Case 3 not done

	Struct. 1 to 1 – A (Boeing)	Strut. 1 to 1 – B (Pointwise)	Unst. Tet NC - A (UWYO)	Unst. Mixed NC - B (DLR-Solar)
FUN3D			SA (Mixed)	SA (not finished)
CFL3D	SA SST	SST		

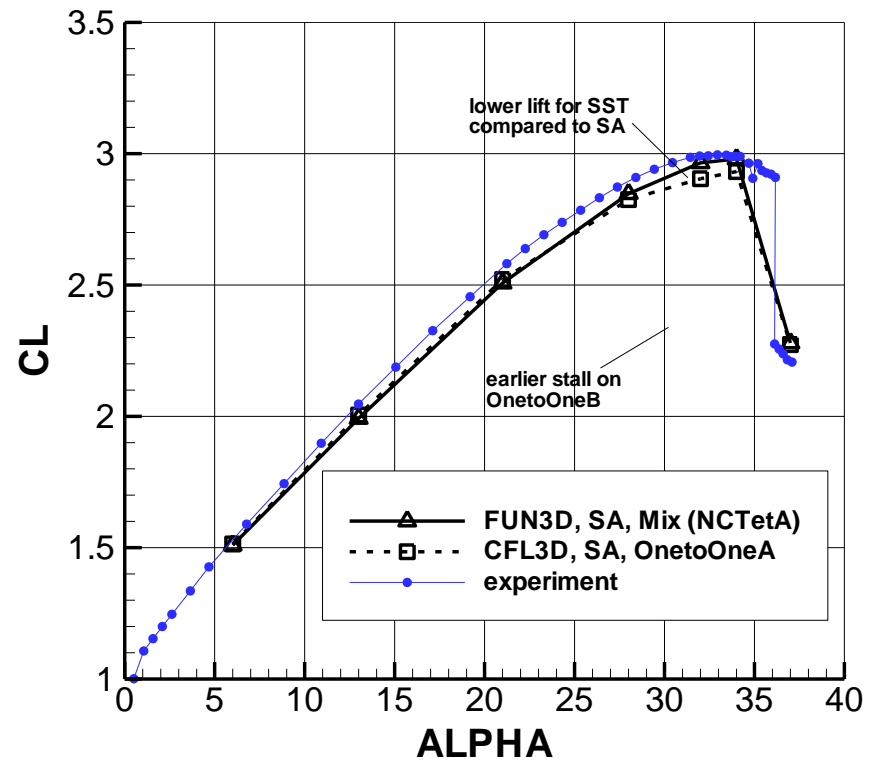
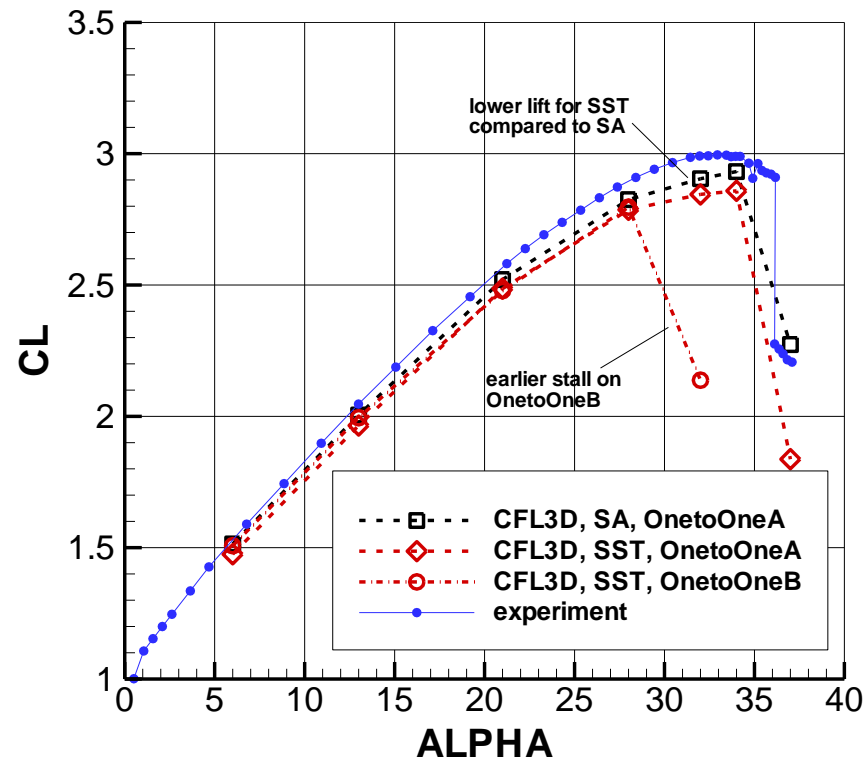


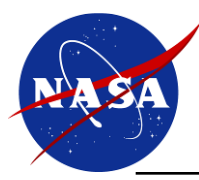
Comparison of Grid Sizes

	Extra-Coarse	Coarse	Medium	Fine	Extra-Fine
Struct. 1-to-1 A Boeing	7.1M	22.6M	52.1M	171M	
Stuct. 1-to-1 B Pointwise	3.8M	11.2M	28.7M	85.5M	
Mixed ver. Unst. Tet. NC A VGRID		3.7M	11.0M	32.4M	
Mixed NC B Solar		12.3M	37.0M	111M	

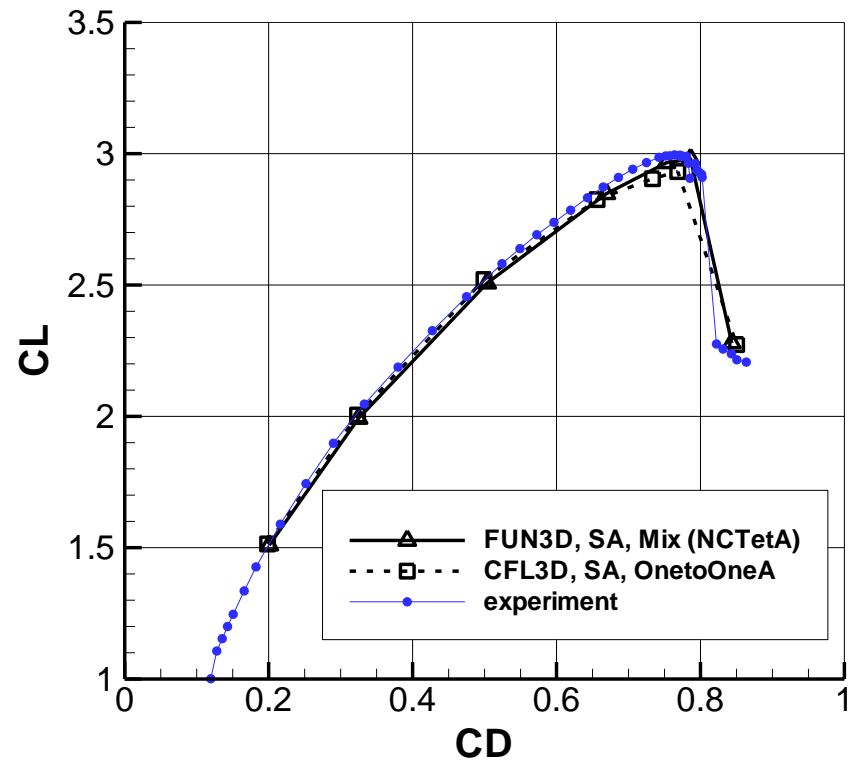
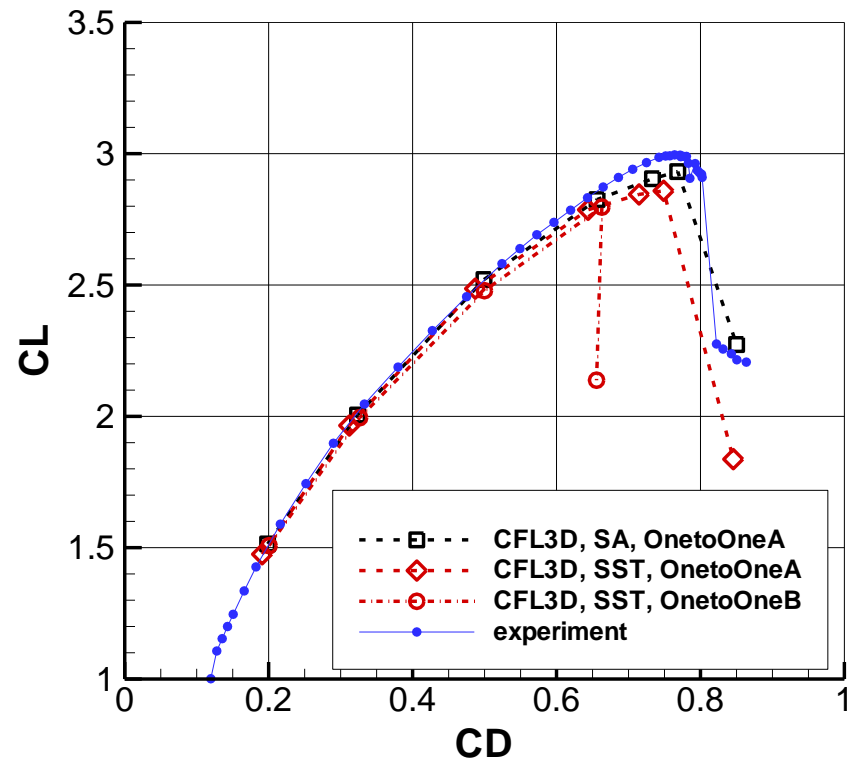


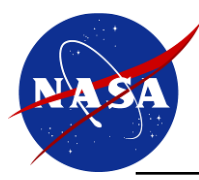
Configuration 1 – Lift Polar



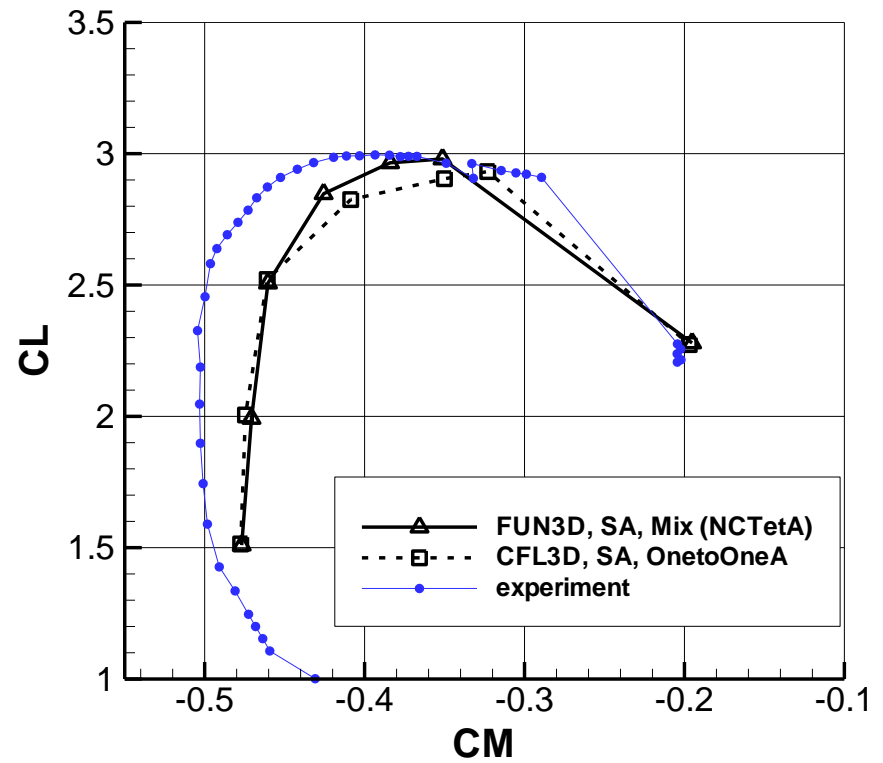
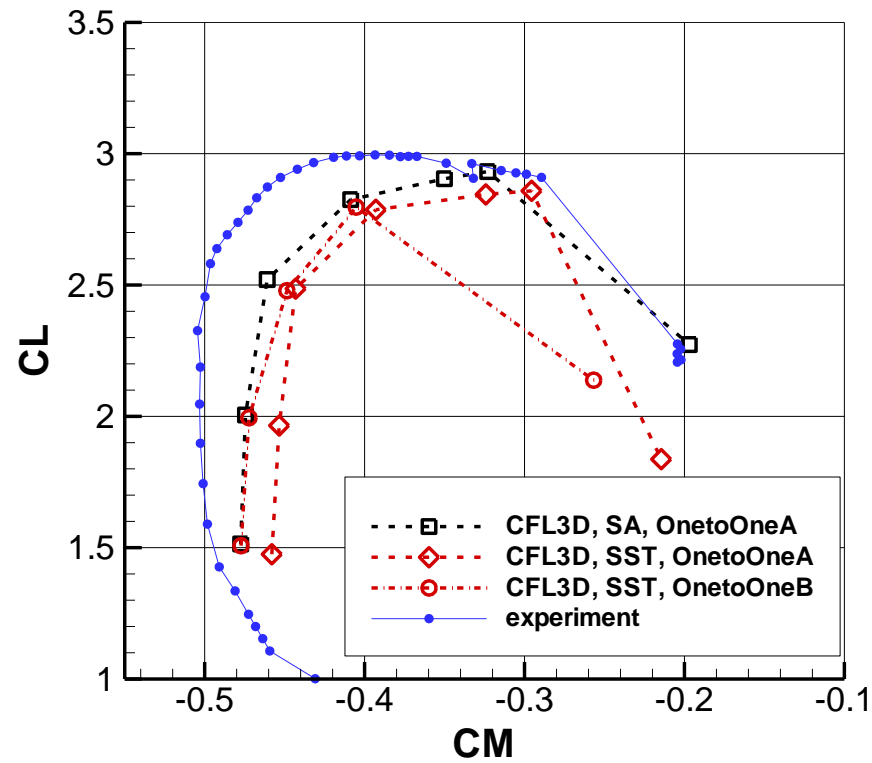


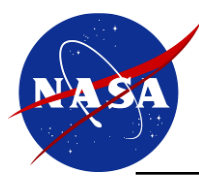
Configuration 1 – Drag Polar



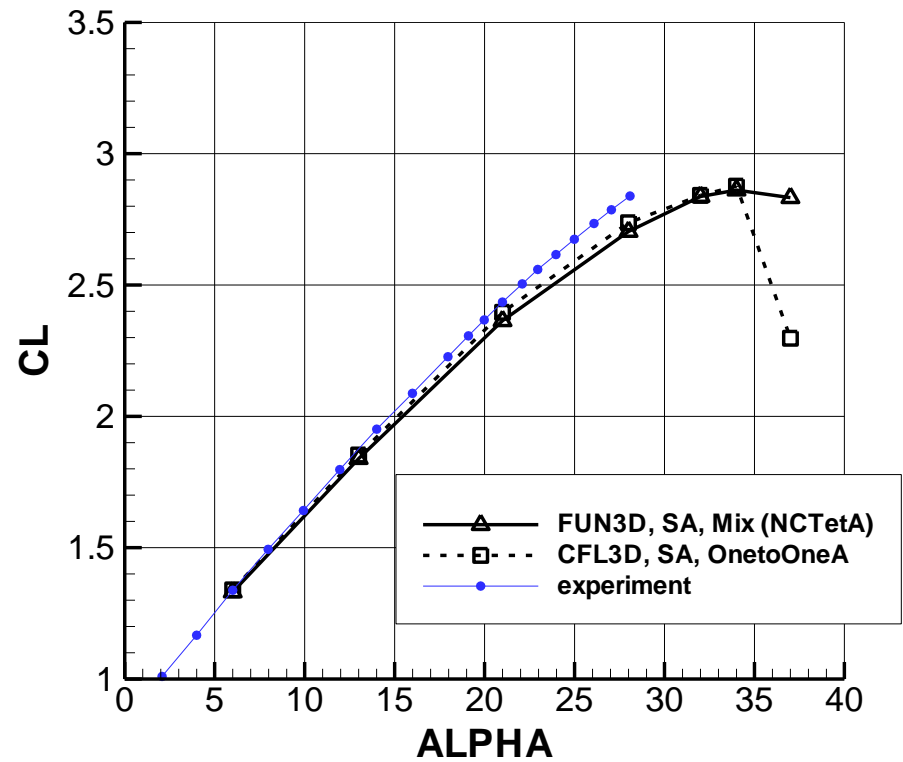
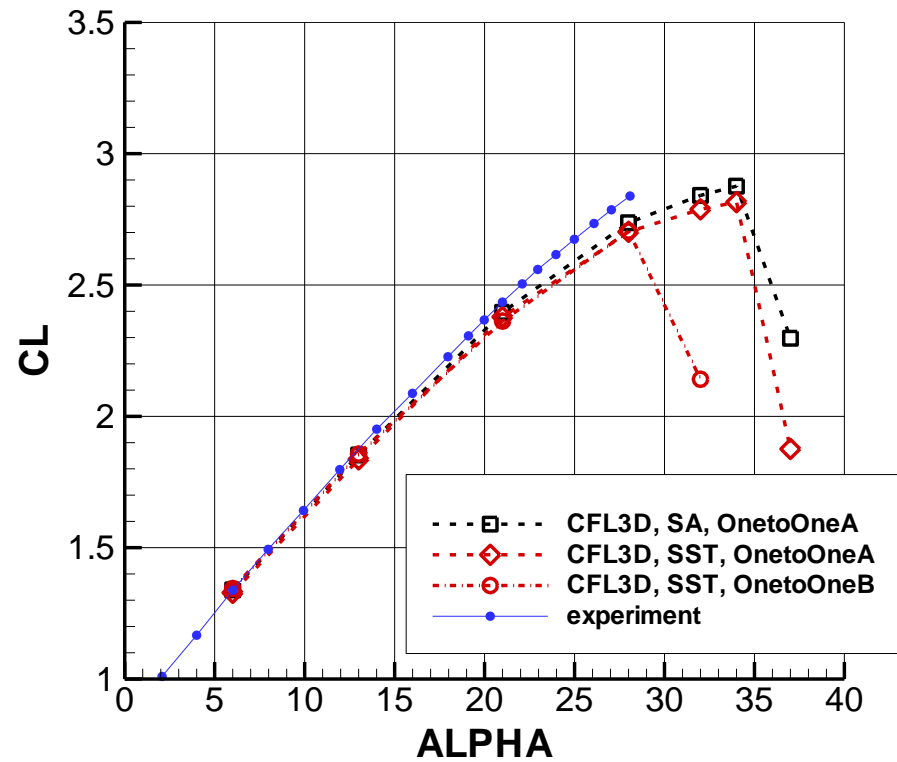


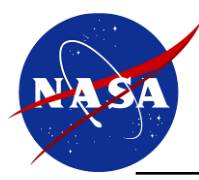
Config. 1 – Pitching Moment Polar



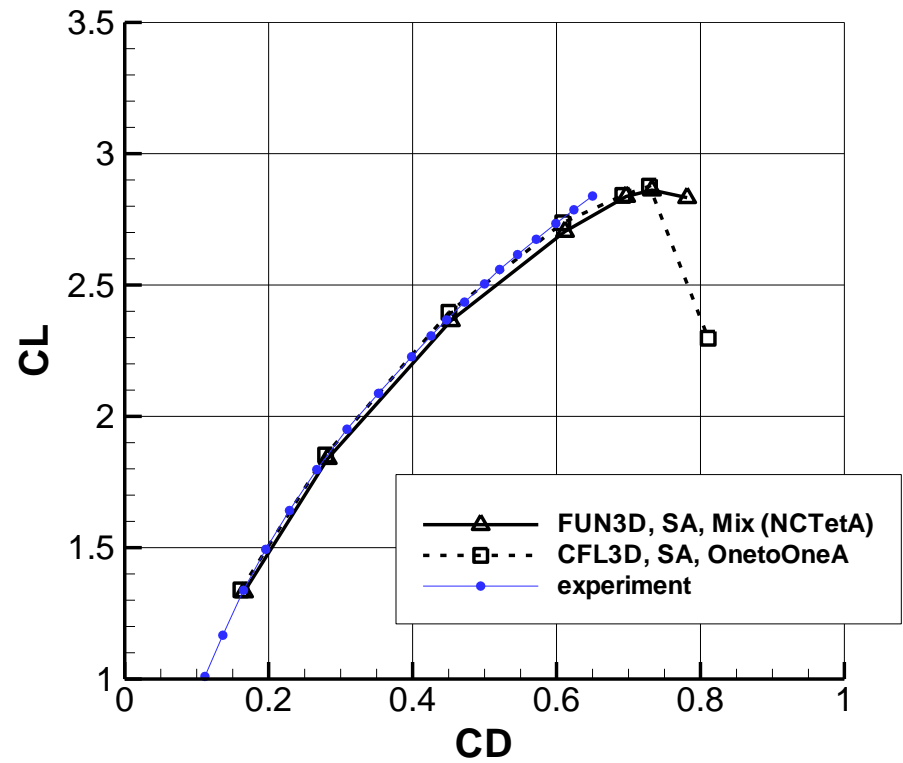
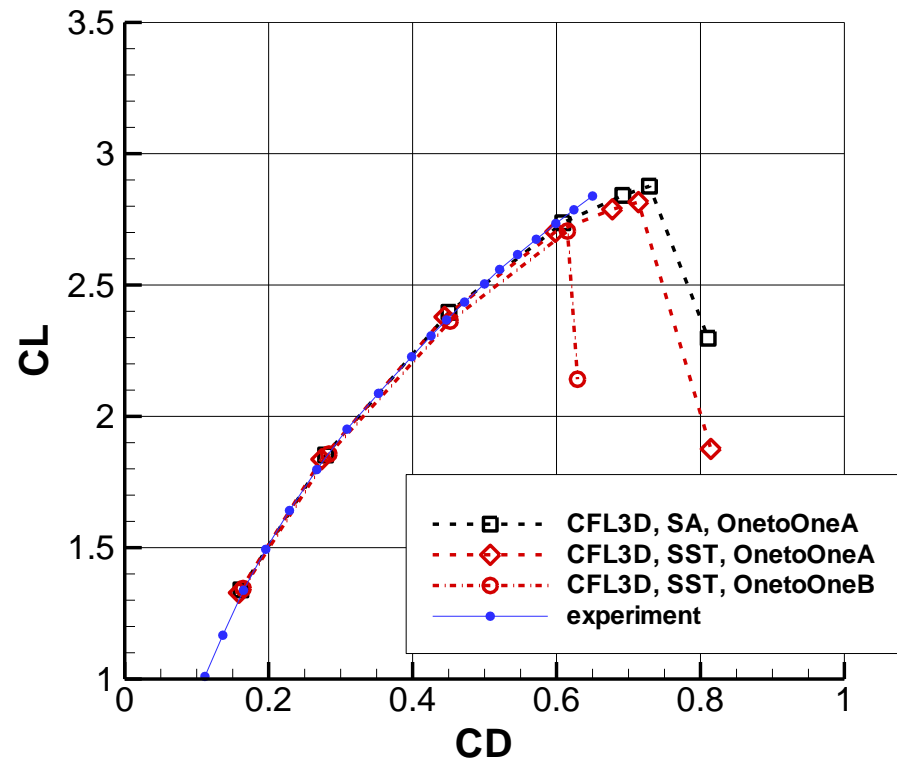


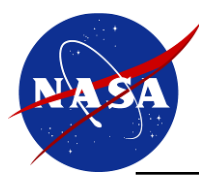
Configuration 8 – Lift Polar



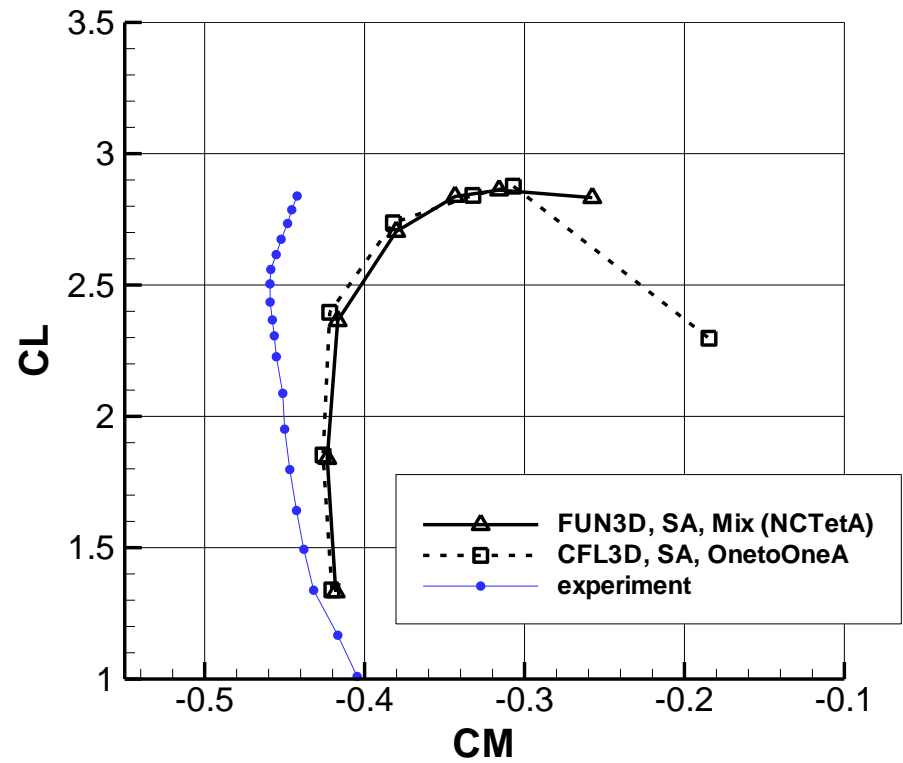
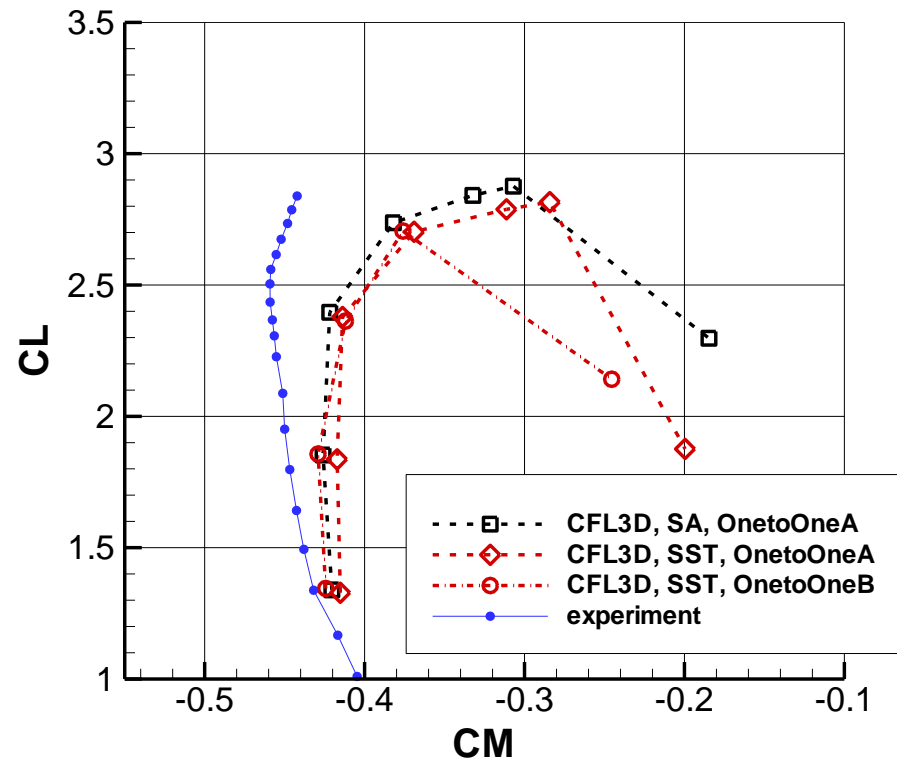


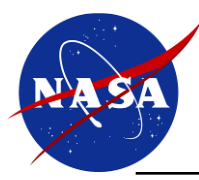
Configuration 8 – Drag Polar





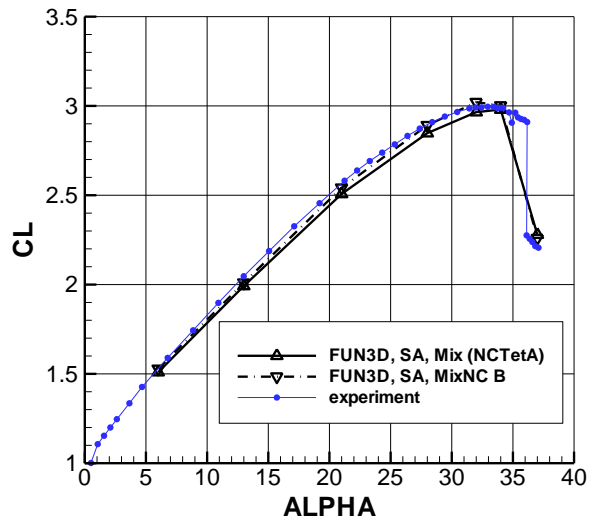
Config. 8 – Pitching Moment Polar



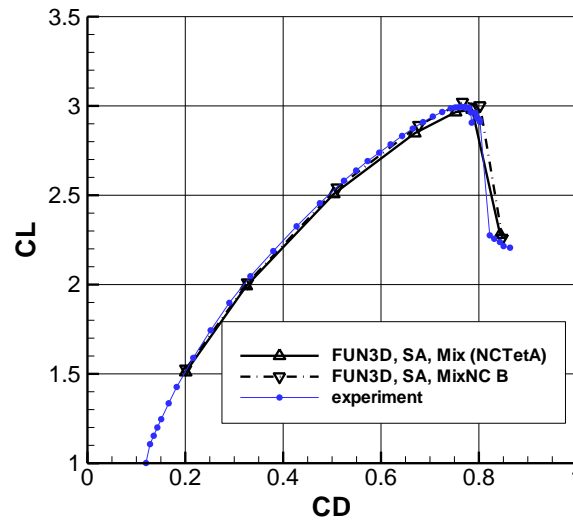


Configuration 1 – SOLAR Grids

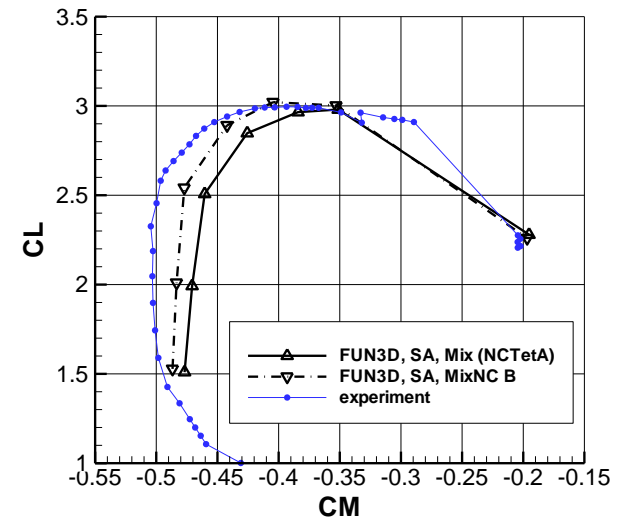
Lift

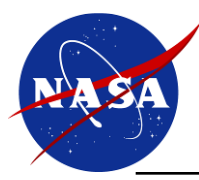


Drag



Pitching Moment



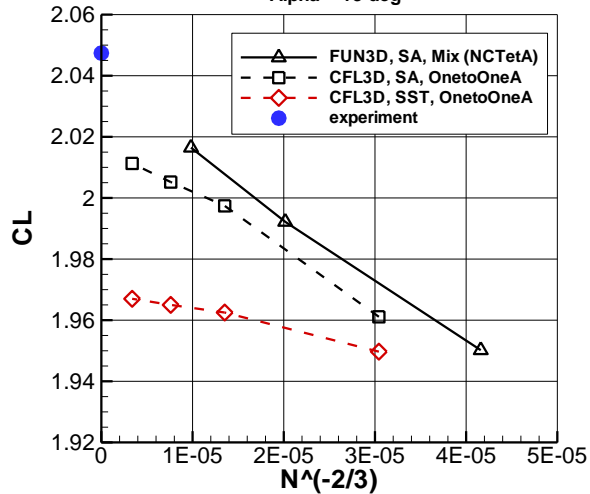


Grid Convergence – Config. 1

Angle of Attack 13 deg

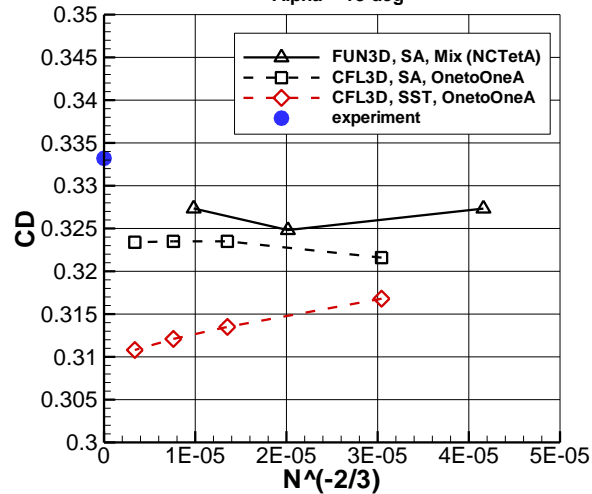
Lift

Alpha = 13 deg



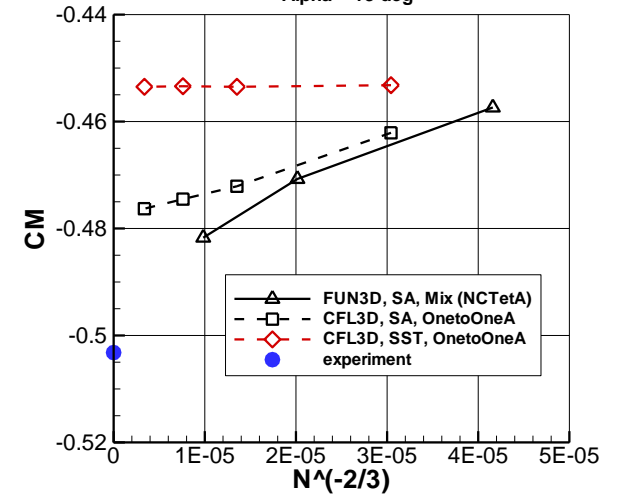
Drag

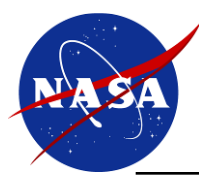
Alpha = 13 deg



Pitching Moment

Alpha = 13 deg



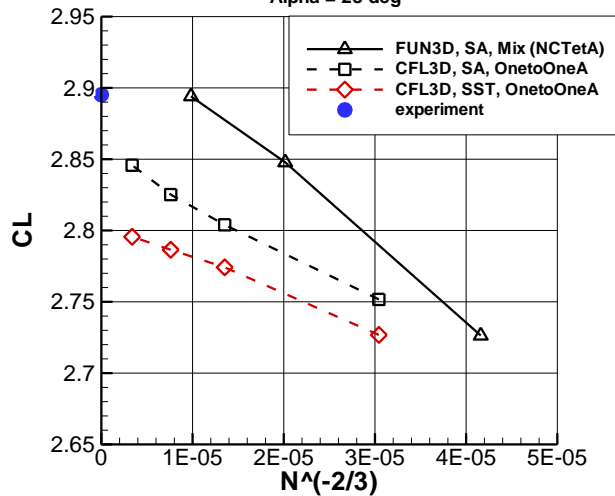


Grid Convergence – Config. 1

Angle of Attack 28 deg

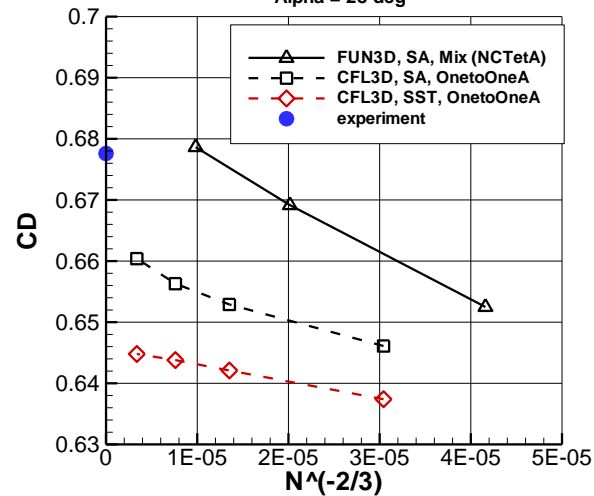
Lift

Alpha = 28 deg



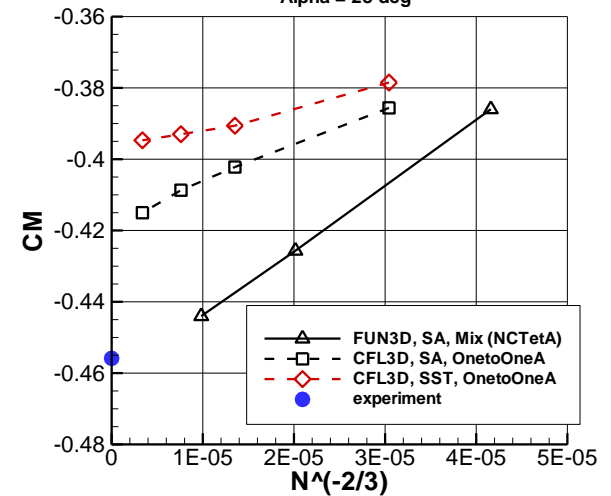
Drag

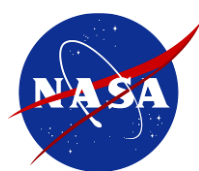
Alpha = 28 deg



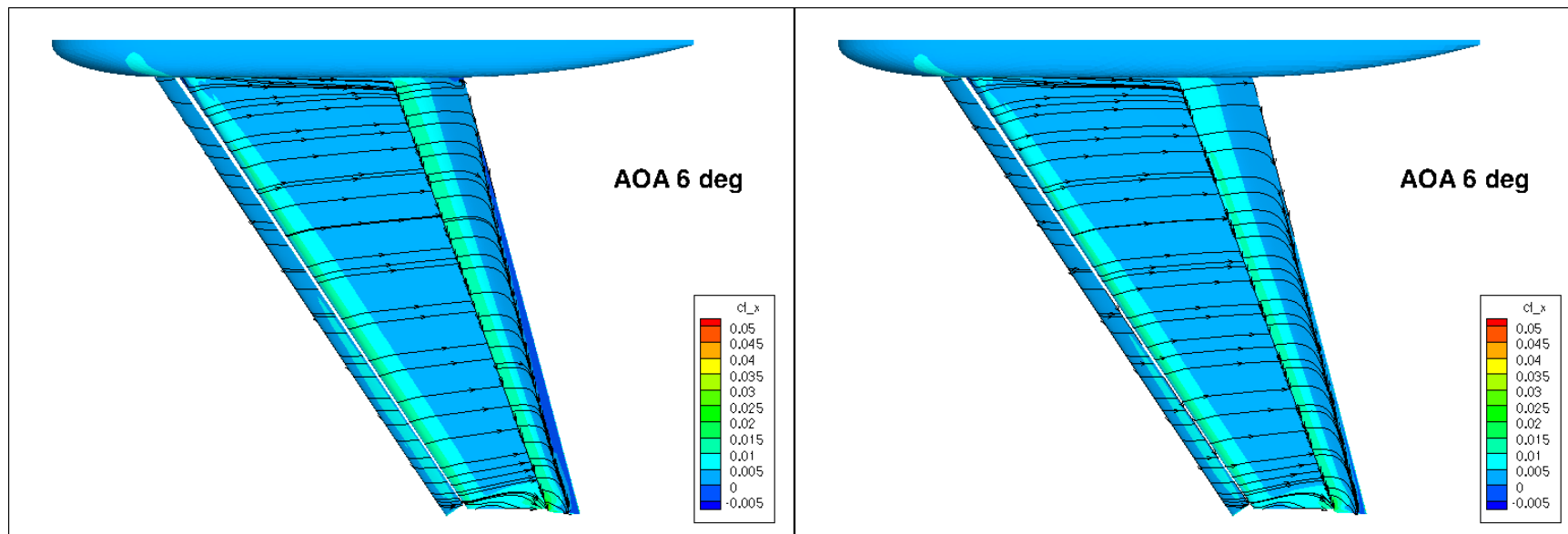
Pitching Moment

Alpha = 28 deg





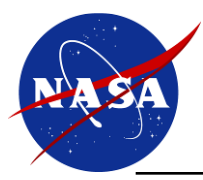
FUN3D Surface Restricted Streamlines



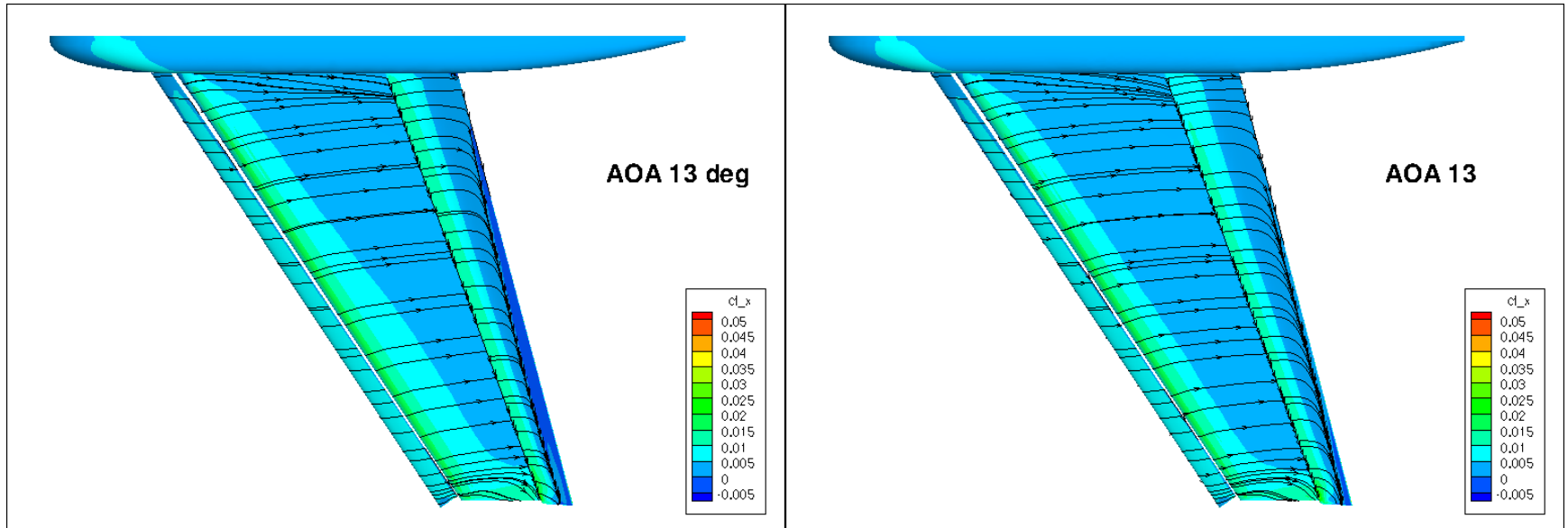
Config. 1

Config. 8

Medium Grid



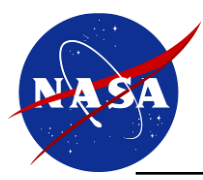
FUN3D Surface Restricted Streamlines



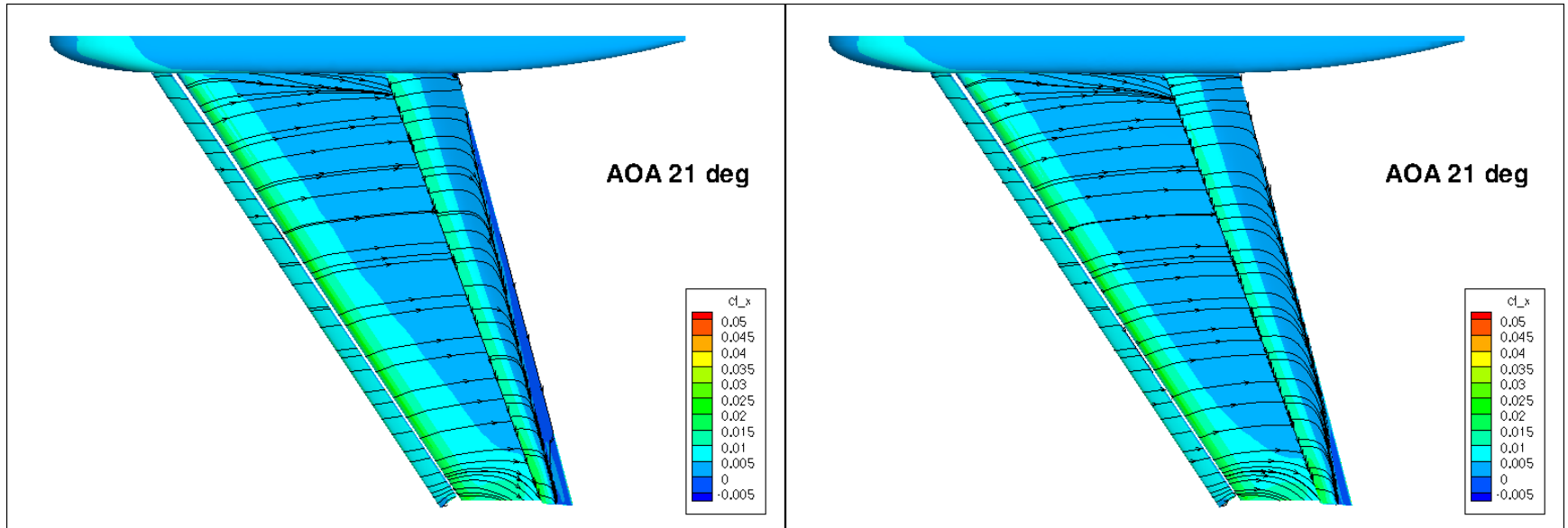
Config. 1

Config. 8

Medium Grid



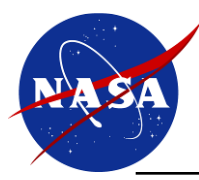
FUN3D Surface Restricted Streamlines



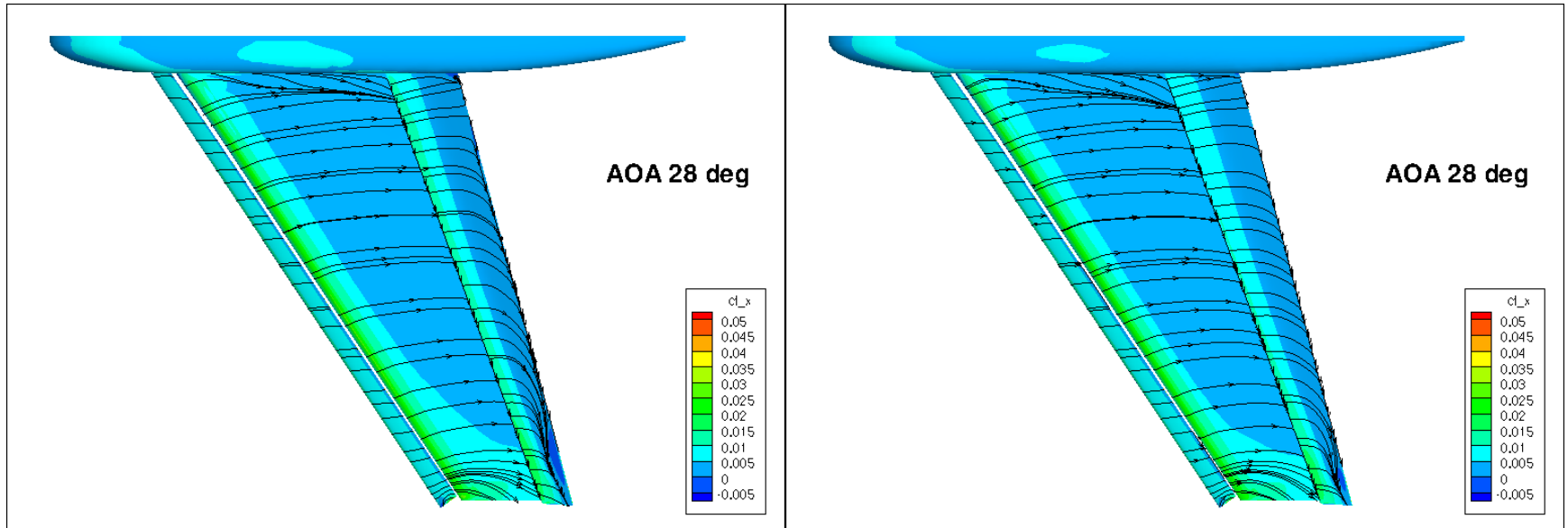
Config. 1

Config. 8

Medium Grid



FUN3D Surface Restricted Streamlines



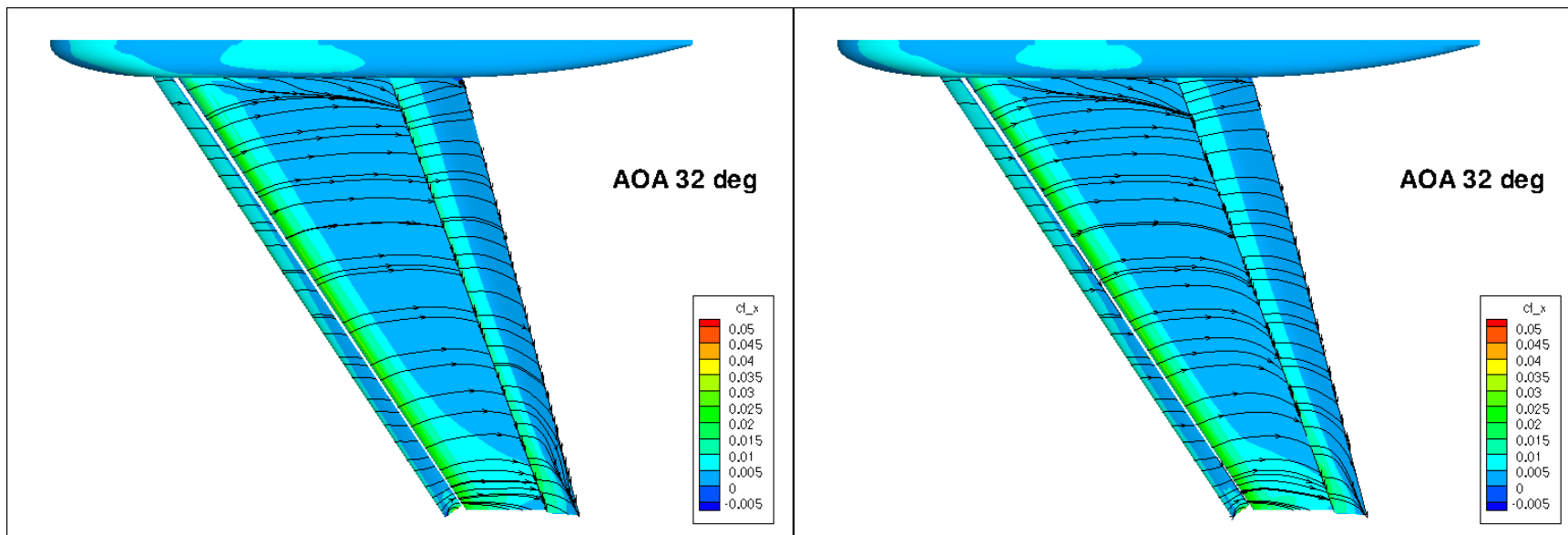
Config. 1

Config. 8

Medium Grid



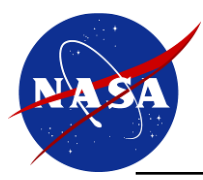
FUN3D Surface Restricted Streamlines



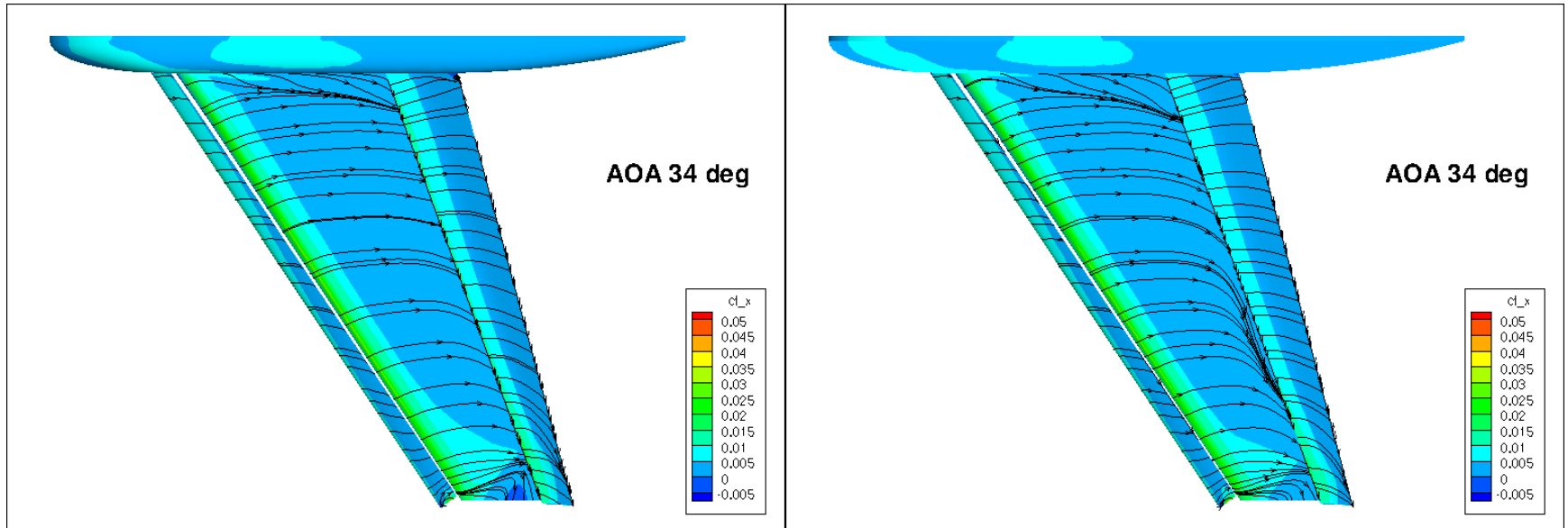
Config. 1

Config. 8

Medium Grid



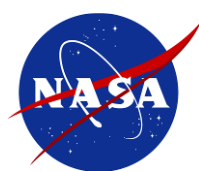
FUN3D Surface Restricted Streamlines



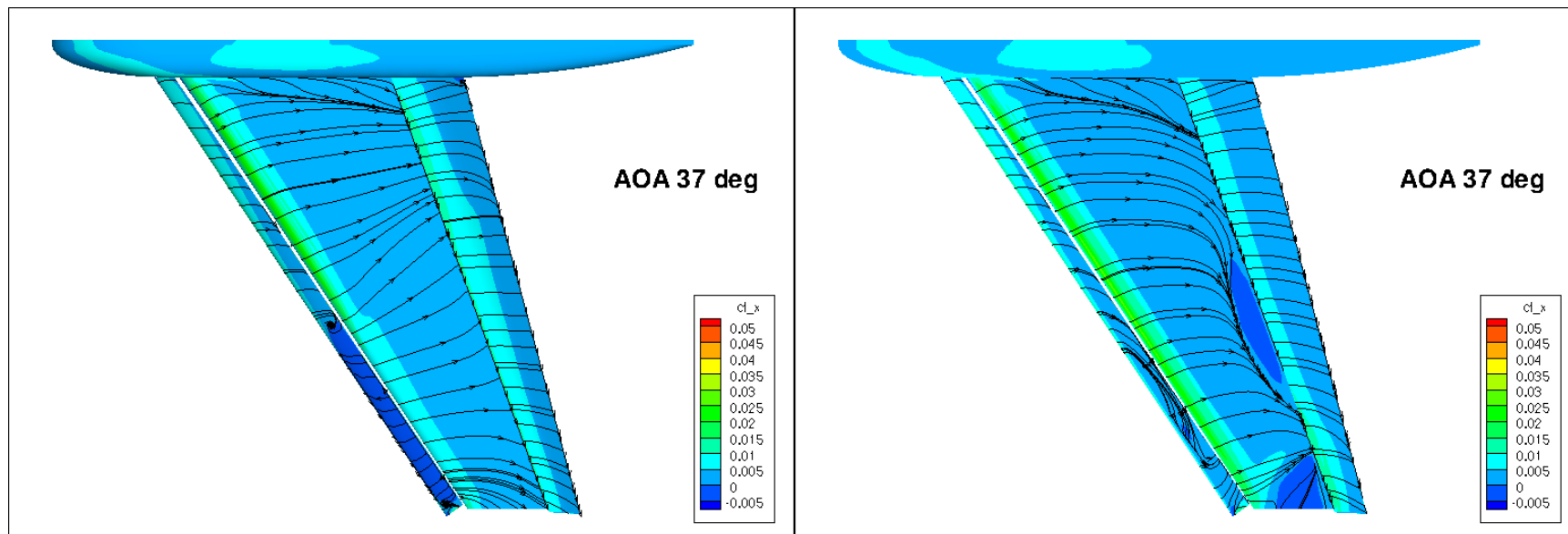
Config. 1

Config. 8

Medium Grid



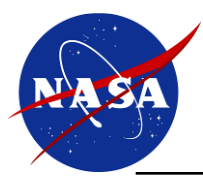
FUN3D Surface Restricted Streamlines



Config. 1

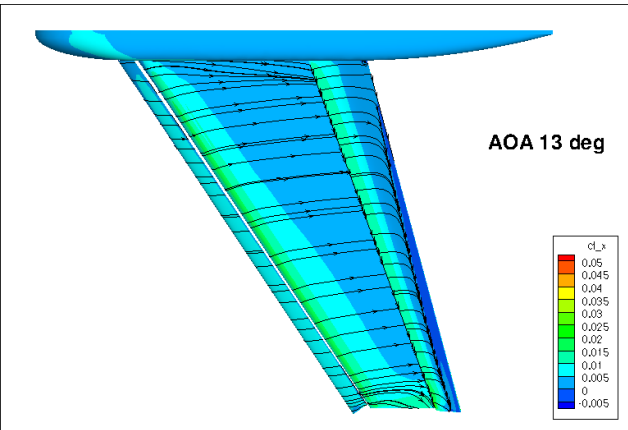
Config. 8

Medium Grid

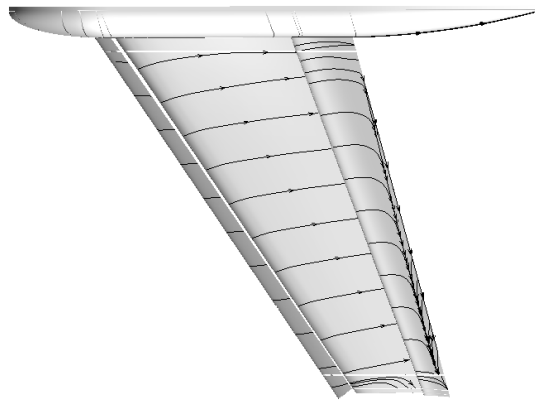


FUN3D vs CFL3D Surface Flows –Config. 1

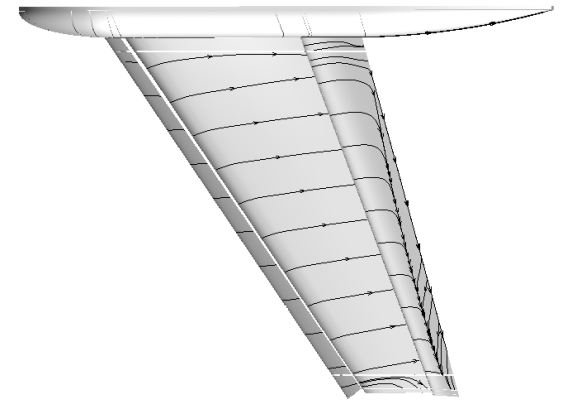
AOA 13 deg



FUN3D SA

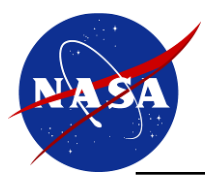


CFL3D SA



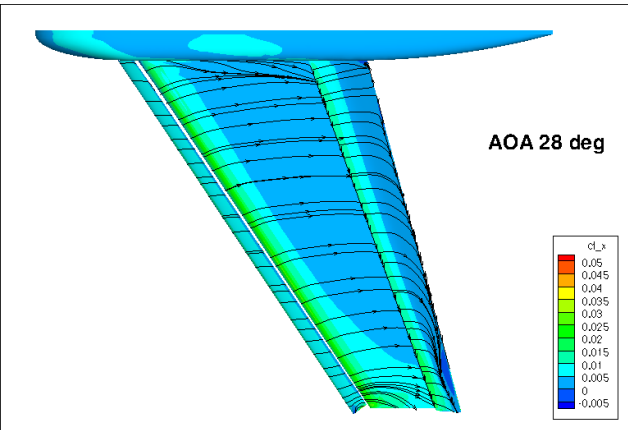
CFL3D SST

Medium Grid

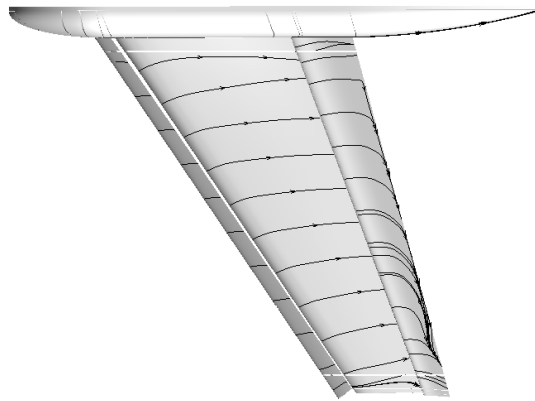


FUN3D vs CFL3D Surface Flows –Config. 1

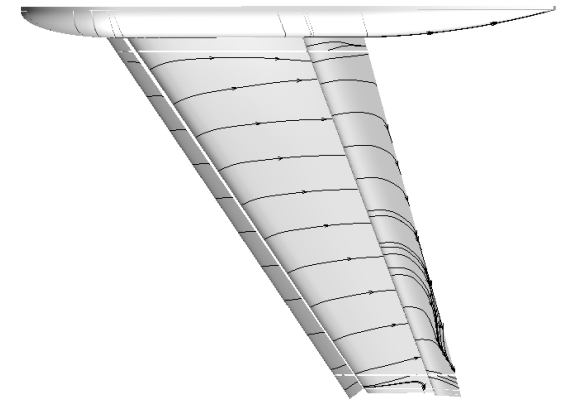
AOA 28 deg



FUN3D SA

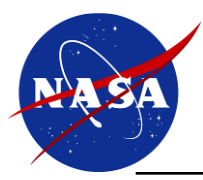


CFL3D SA

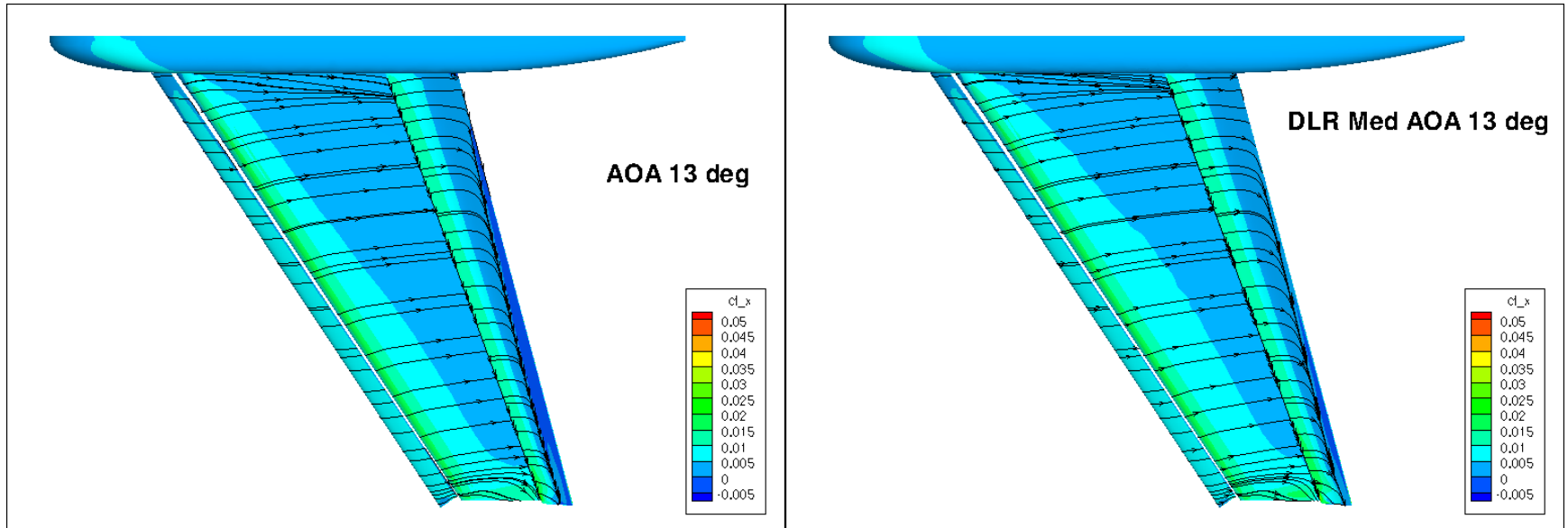


CFL3D SST

Medium Grid



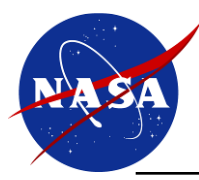
FUN3D Config. 1



Tet NC A
(Mixed)

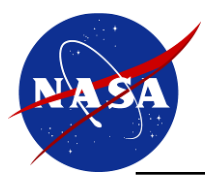
Mixed NC B

Medium Grid



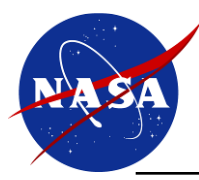
Summary

- **Grid convergence study**
 - SST lower lift than SA (likely flap separation)
 - Struct. Grid and unst. Grid results with same turbulence model compare well
 - At higher alpha more difference between codes and more variation with grid refinement
- **Flap study (medium grid)**
 - Grid density/topology matters at highest AOA
 - One-to-one structured grid B seems to predict early stall
 - SOLAR grid results improved correlation at high AOA
 - Config. 1 has more flap separation than Config. 8
 - SST predicts more flap separation than SA
 - FUN3D predicts wing separation at highest AOA for Config. 8 (not seen in CFL3D solutions)



Acknowledgements

- Dr. Eric Nielsen, NASA LaRC
- Dana Hammond, NASA LaRC



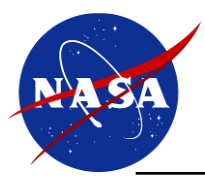
HiLiftPW-1 - Rehearsal Background

Objectives

- Assess the numerical prediction capability (mesh, numerics, turbulence modeling, high-performance computing requirements, etc.) of current-generation CFD technology/codes for swept, medium/high-aspect ratio wings in landing/take-off (high-lift) configurations.
- Develop practical modeling guidelines for CFD prediction of high-lift flowfields.
- Advance the understanding of high-lift flow physics to enable development of more accurate prediction methods and tools.
- Enhance CFD prediction capability for practical high-lift aerodynamic design and optimization.
- Provide an impartial forum for evaluating the effectiveness of existing computer codes and modeling techniques.
- Identify areas needing additional research and development.

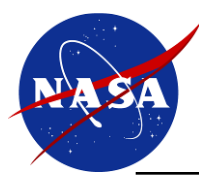
• Focus

- The focus of this workshop will be on multi-element high-lift swept wing force, moment, and surface pressure prediction accuracy; a priori experimental data will be available for comparison.
- The NASA "Trap Wing" model will be studied.
- A statistical framework will be used to assess the CFD results.



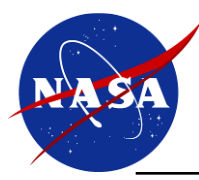
HiLiftPW-1 – Trap Wing Model





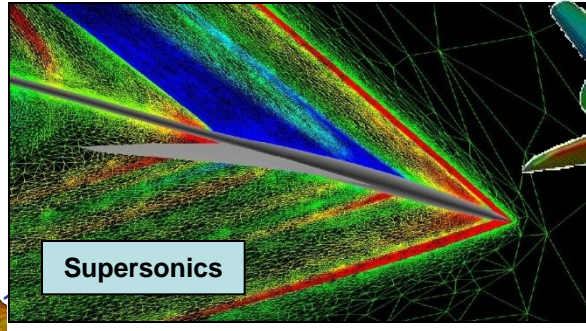
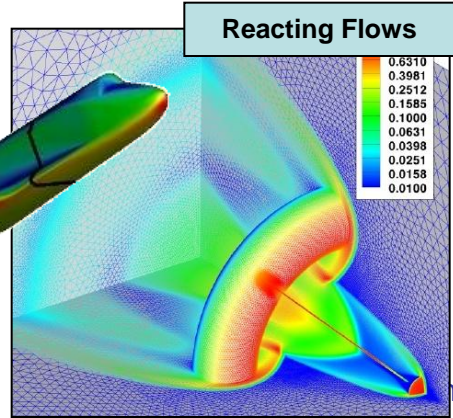
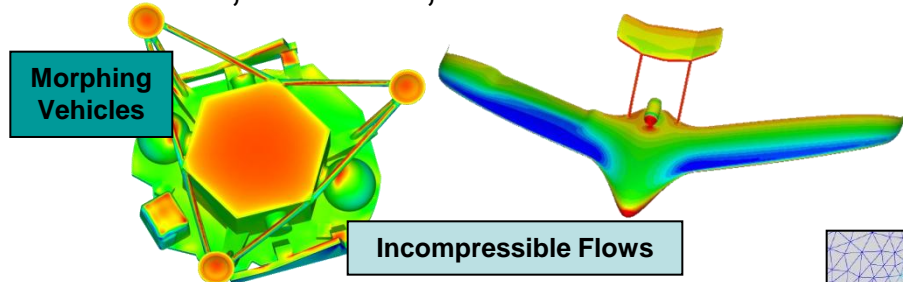
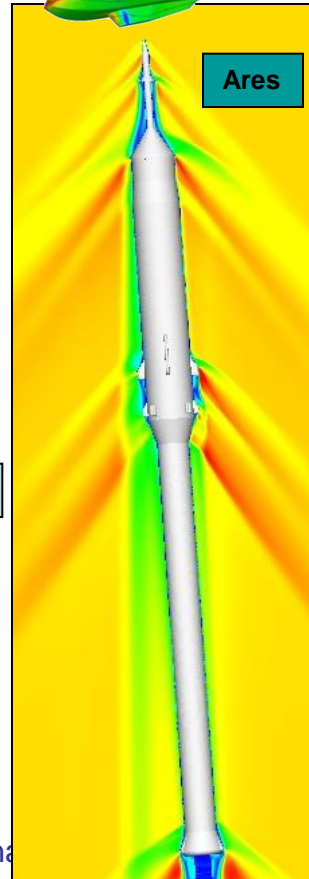
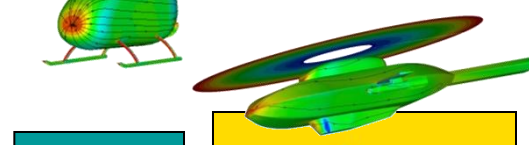
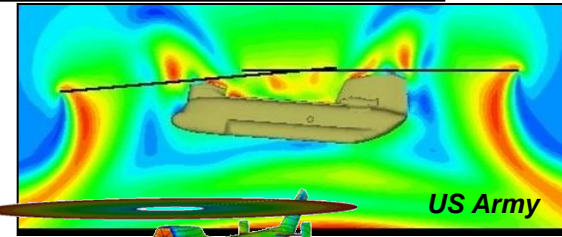
HiLiftPW-1 - Rehearsal Background

- Case 1 : Grid convergence study (required)
 - Mach = 0.2
 - Angles-of-attack to be computed (deg) = 13 and 28
 - Reynolds number = 4.3 million based on mean aerodynamic chord (MAC)
 - Reference Temperature = 520 R
 - Trap Wing "Config 1" - Slat 30, Flap 25
 - Coarse, medium, fine and extra-fine (optional)
- Case 2: Flap deflection prediction study (required)
 - Mach = 0.2
 - Angles-of-attack to be computed (deg) = 6, 13, 21, 28, 32, 34, and 37
 - Reynolds number = 4.3 million based on MAC
 - Reference Temperature = 520 R
 - Medium Mesh from Grid Convergence Study
 - Trap Wing "Config 1" - Slat 30, Flap 25
 - Trap Wing "Config 8" - Slat 30, Flap 20
- Case 3: Flap and slat support effects study (optional)
 - Medium Mesh from Grid Convergence Study
 - Trap Wing "Config 1" - Slat 30, Flap 25

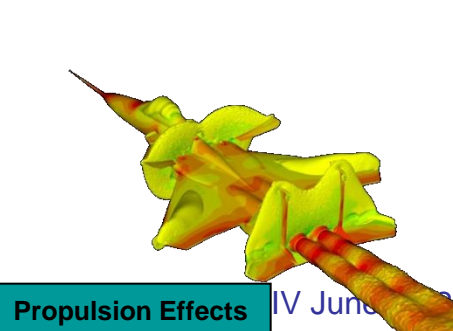


FUN3D Core Capabilities

- Solves 2D/3D steady and unsteady Euler and RANS equations on node-based mixed element grids for compressible and incompressible flows
- Used for numerous projects internal and external to NASA across the speed range
- General dynamic mesh capability: any combination of rigid/overset/morphing grids, including 6-DOF effects
- Aeroelastic modeling w/ mode shapes, full FEM, CC, etc
- Adjoint-based design optimization and mesh adaptation
- Linear scaling through 1000's of cores
- Capabilities fully integrated, large support team, online documentation, tutorials, etc



QuickTime™ and a decompressor are needed to see this picture.



IV Jun