

Some Applications of Computational Fluid Dynamics to Entry and Landing of the Mars Science Laboratory

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Outline

- Mars Science Laboratory (MSL) mission profile
- Computational Method
- Capsule flows*
 - Database calculations
 - Mass jettison
- Descent and landing
 - Parachute canister mortar launch
 - Rocket plumes with plume-plume interaction
 - Rocket plumes in proximity to the ground
- Conclusions

* Reference: M. Schoenenberger, A. Dyakonov, P. Buning, W. Scallion, and J. Van Norman, "Aerodynamic Challenges for the Mars Science Laboratory Entry, Descent and Landing," AIAA-2009-3914, June 2009.

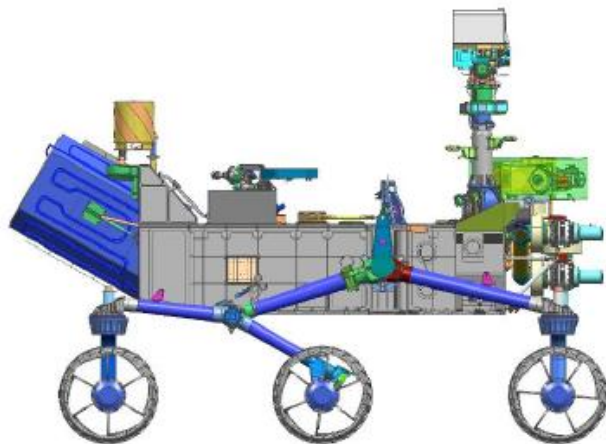
MSL Mission Profile

- Mission characteristics
 - Goal: “Explore and quantitatively assess a local region on Mars as a potential habitat for life, past or present”*
 - Cost: \$1.7B
- Curiosity rover characteristics
 - Mass: 900 kg (MER Spirit & Opportunity were 170 kg)
 - Range: 20 km+ (MER spec was 600 m)
 - Duration: 2 yr (MER spec was 3 mo)
- Mission dates
 - Launch: November 26, 2011
 - Landing: August 6, 2012

*Mission goal and following slides from “NASA's Next Rover: The 2009 Mars Science Laboratory,” a presentation by Dr. Alberto Behar (JPL), International Forum “SPACE: Science and the Challenges of the XXI Century,” Oct. 1-5, 2007, Moscow – St. Petersburg.
http://arc.iki.rssi.ru/oct4/2007/ppt/02_07_Alberto_Behar.pdf



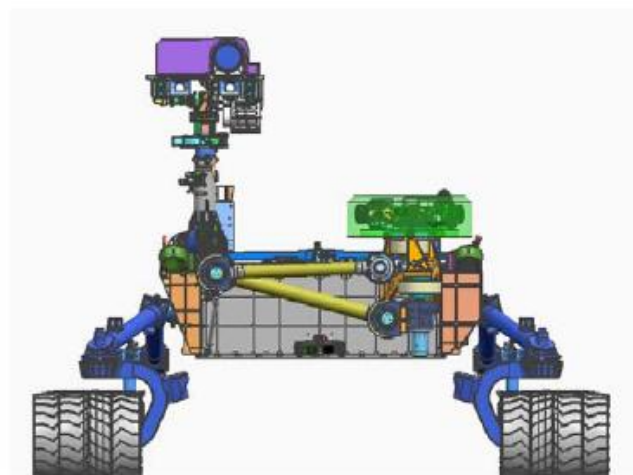
Size Comparison



JPL 2009 MSL Rover



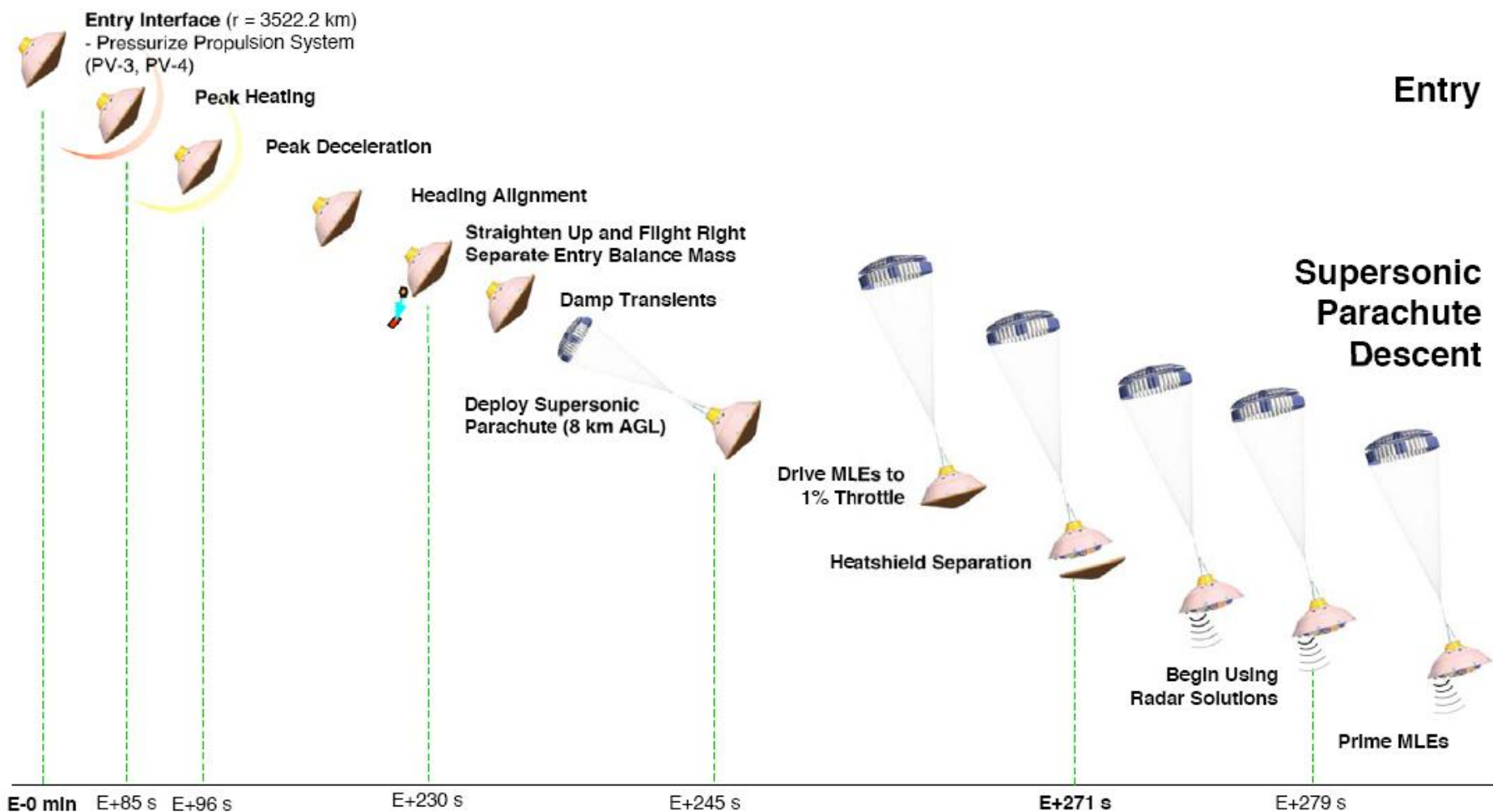
2005 MINI Cooper S



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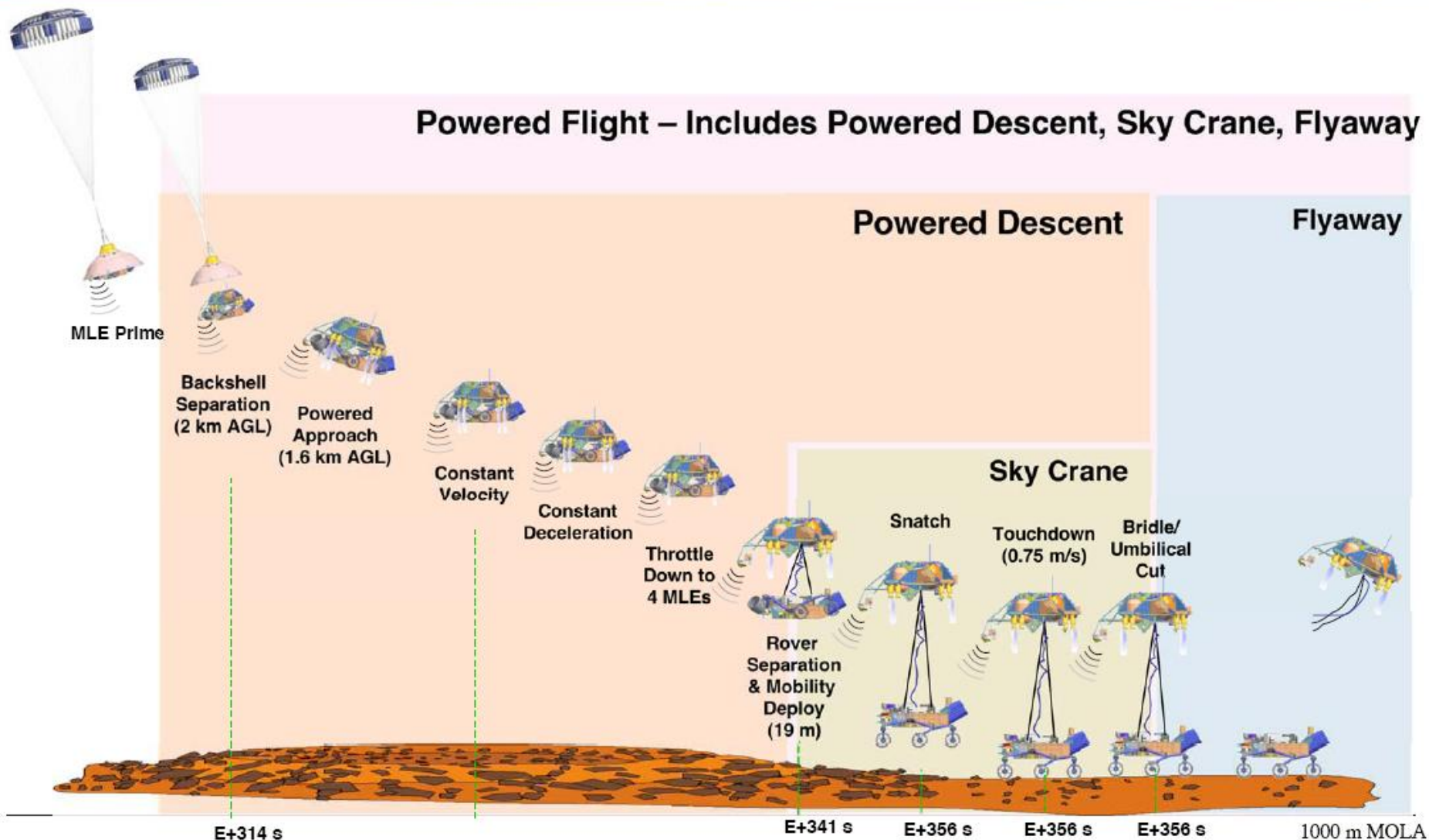


EDL Timeline (1 of 2)





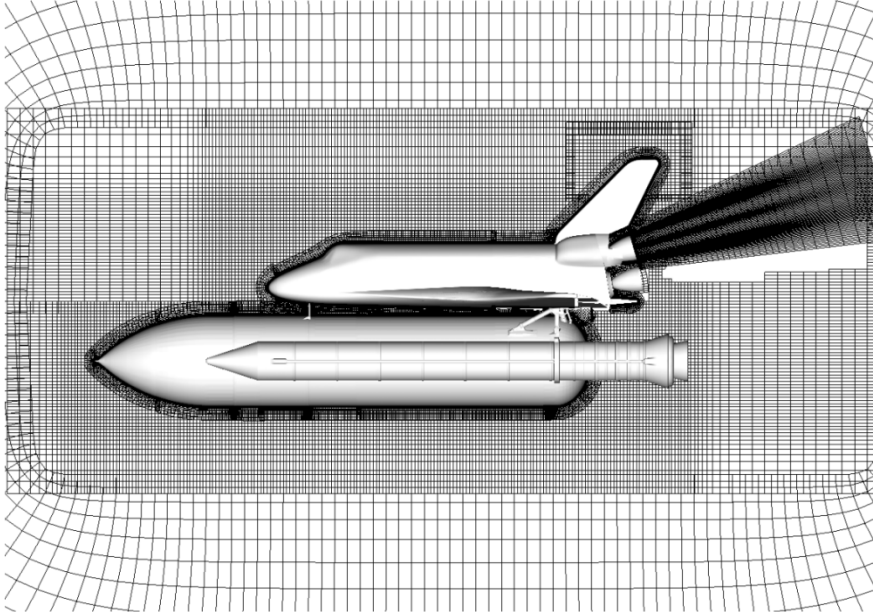
EDL Timeline (2 of 2)



Computational Method: OVERFLOW Code

- NASA-developed CFD code
 - Reynolds-averaged Navier-Stokes solver
 - Compressible flow (subsonic through supersonic)
- Overset, structured “Chimera” grids (Steger, Benek, Dougherty)
- Developed for multi-body and moving body simulations

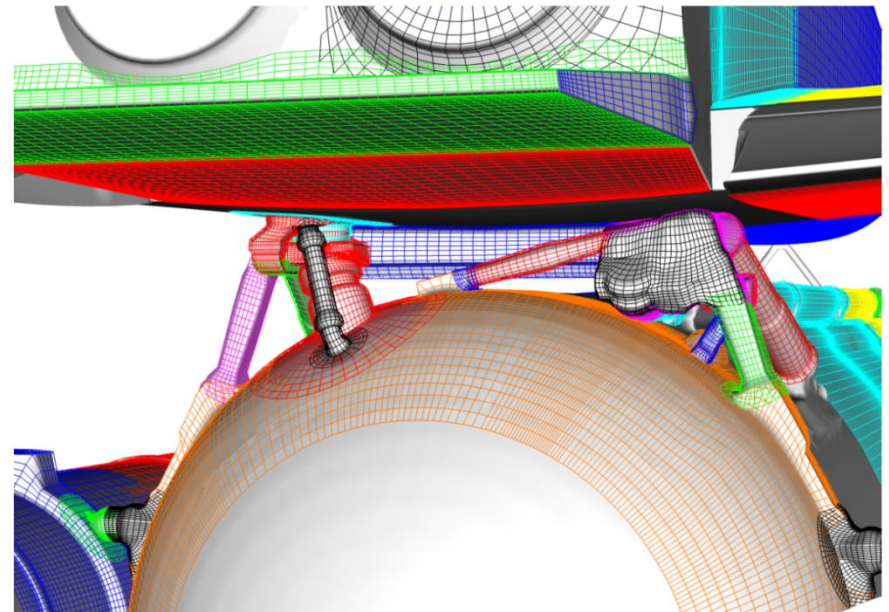
Domain Decomposition of Volume



The Grid Guys 1993

AIAA-93-0533

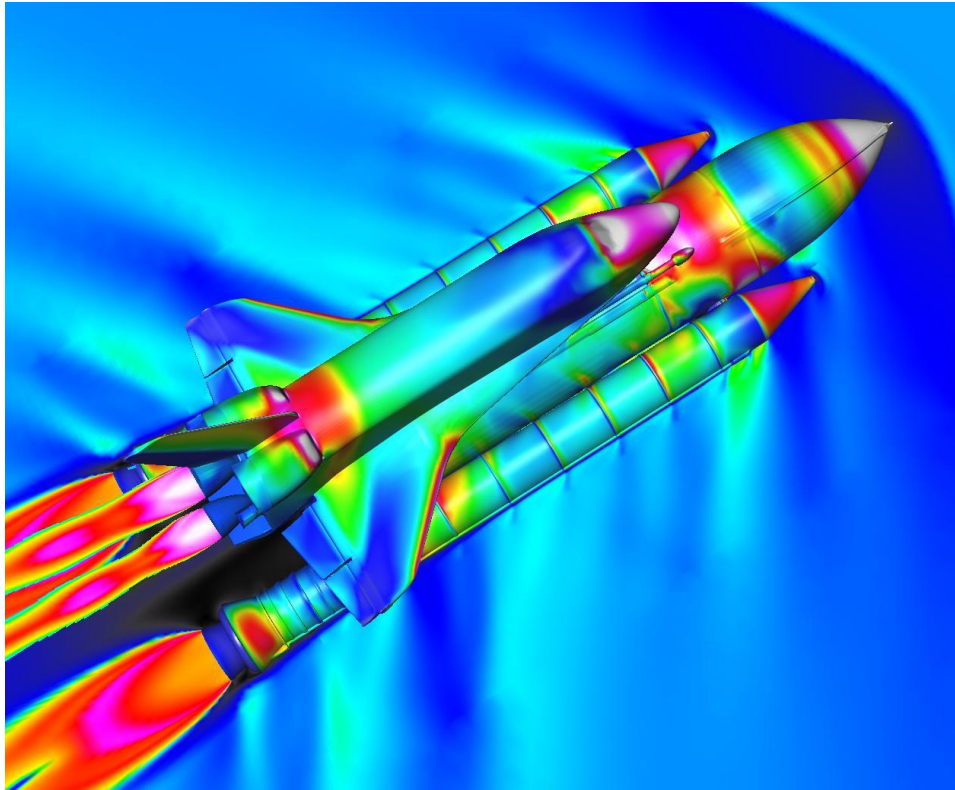
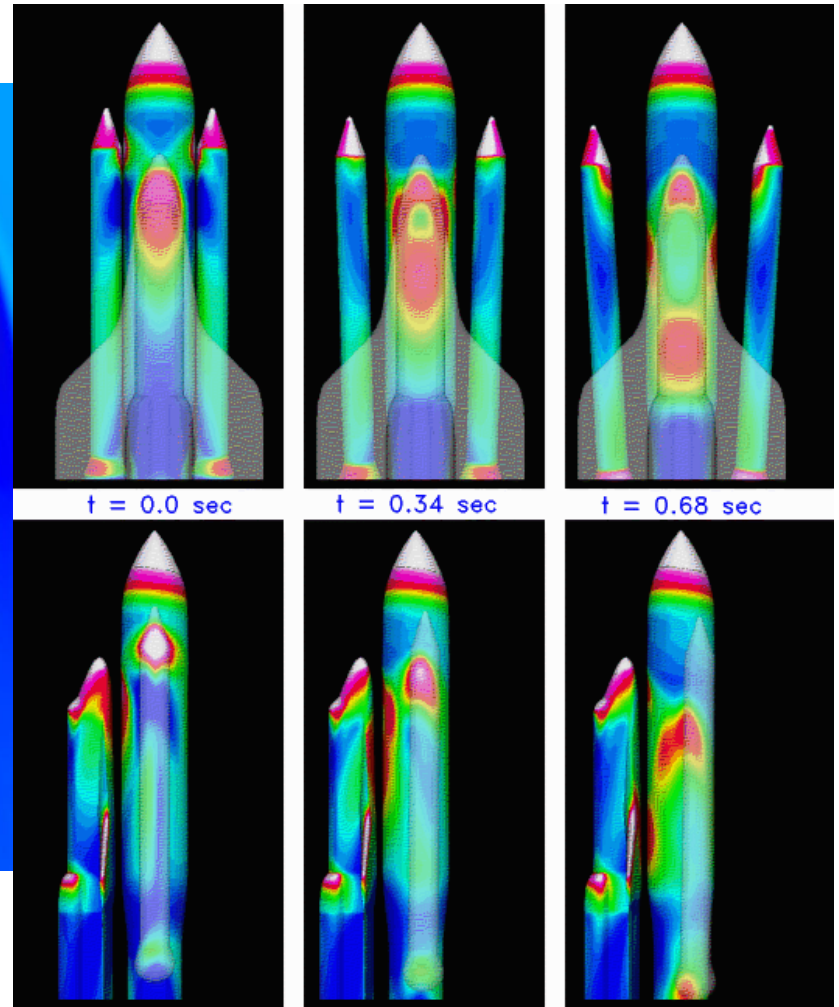
Surface Grid Topology of Aft Attach Region



The Grid Guys 1993

AIAA-93-0533

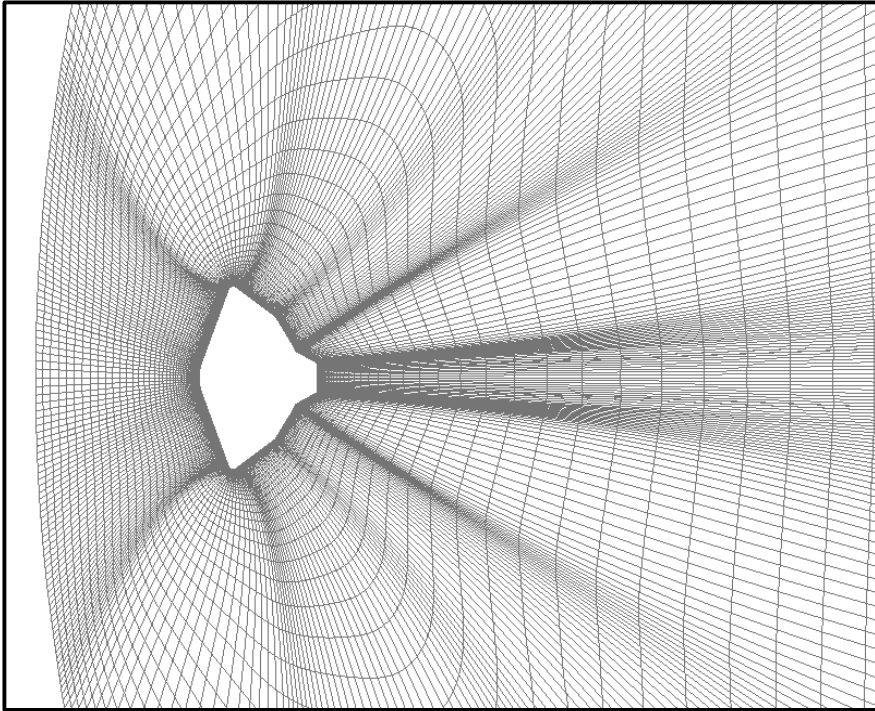
Computational Method: OVERFLOW Code



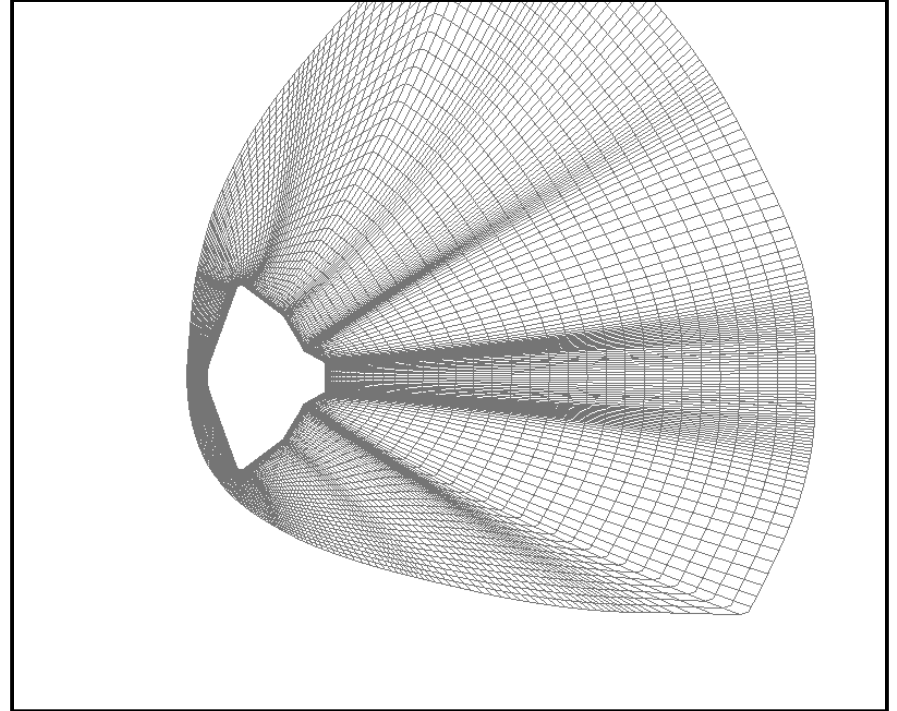
Supersonic Aero Database Calculations

- Database calculations
 - Mach 2-6, alpha 0-24 deg
 - LAURA grid (unadapted)
- Design issues:
 - Backshell pressure contribution to drag
 - Trim angle (pitching moment)
- Solver issues:
 - Effect of grid adaption on bow shock capturing
 - Grid adaption effect on convergence

LAURA Capsule Grids for MSL

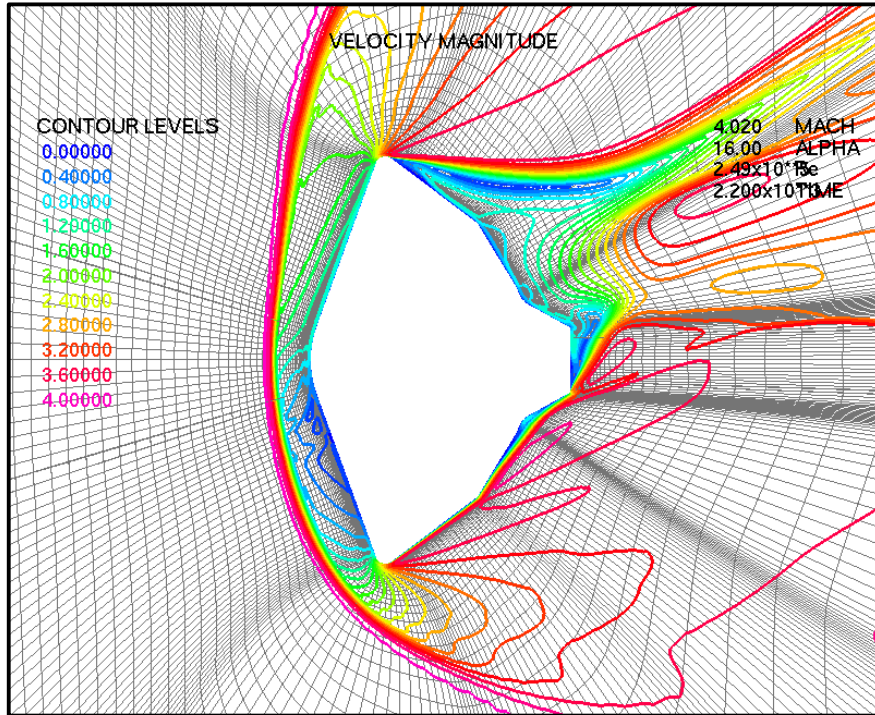


Unadapted

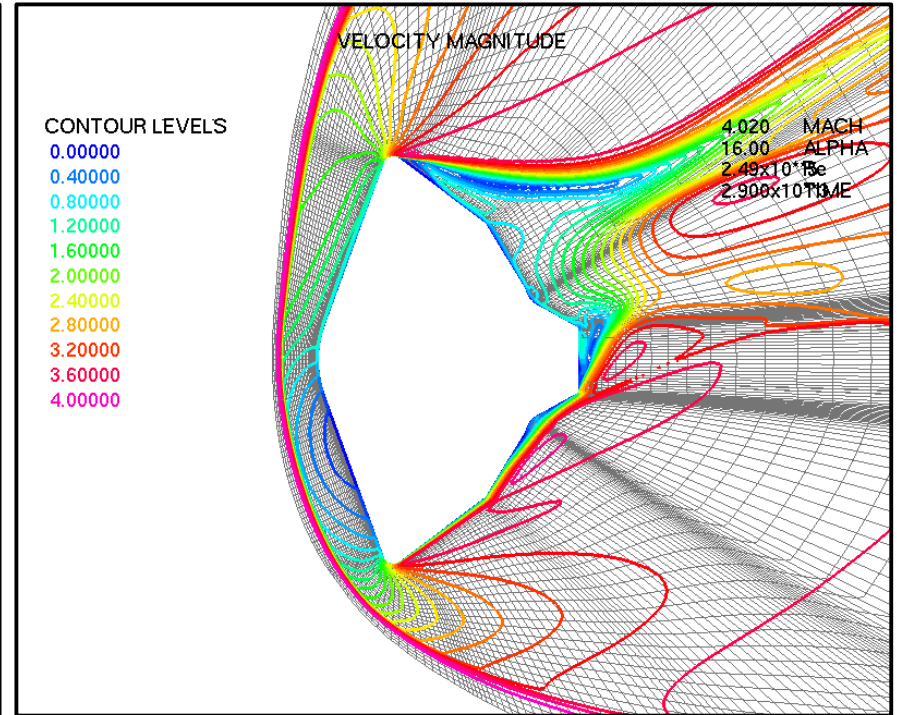


Adapted to bow shock
Mach 4, α 16 deg

Major flow-field features are identical, forces are close

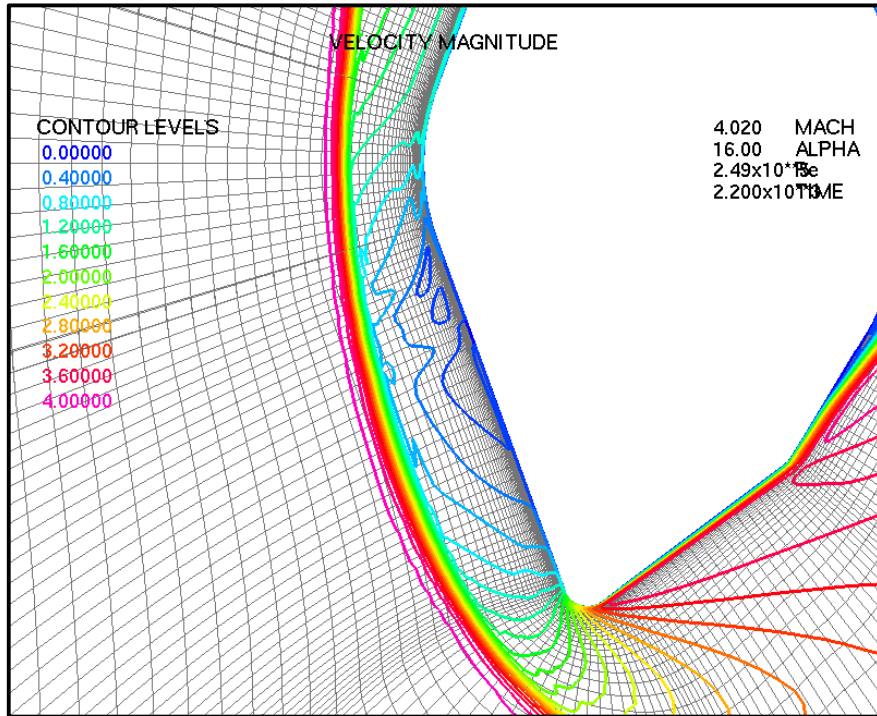


Unadapted

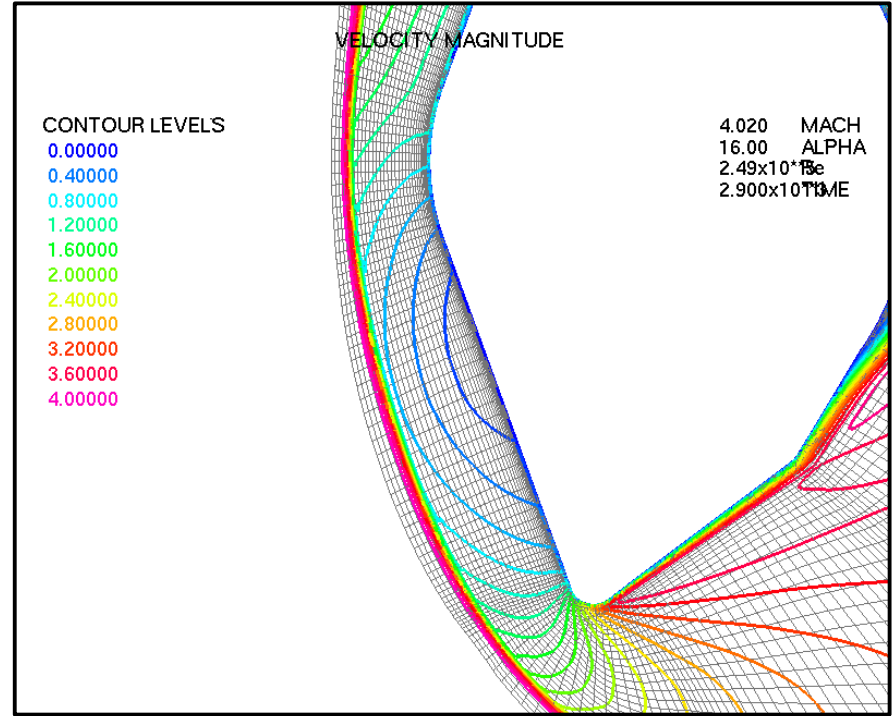


Adapted to bow shock
Mach 4, alpha 16 deg

Much better resolution of post-shock flow



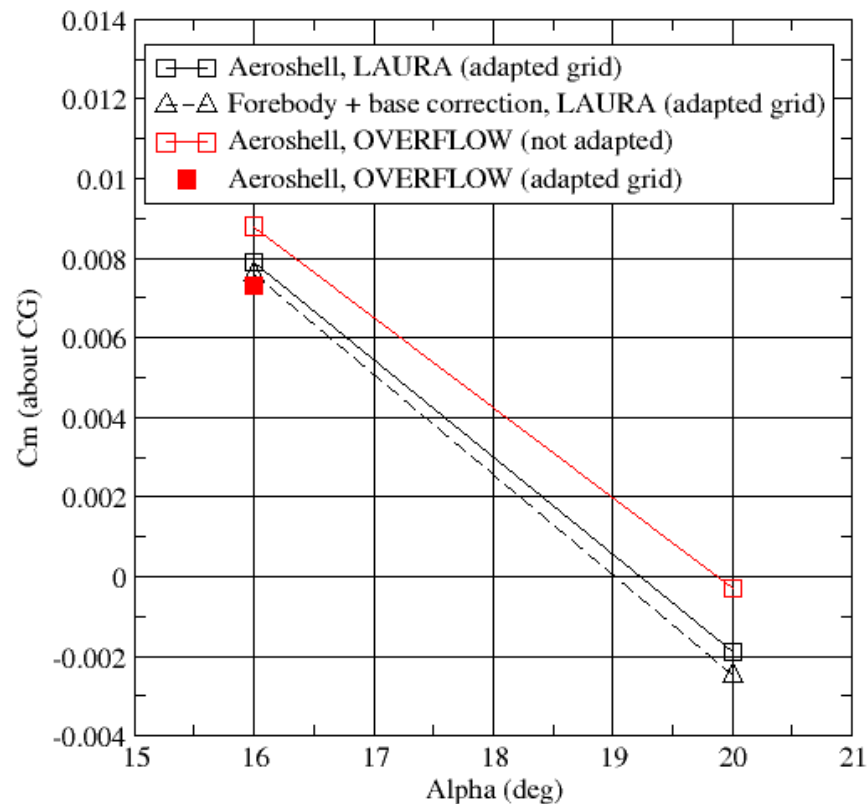
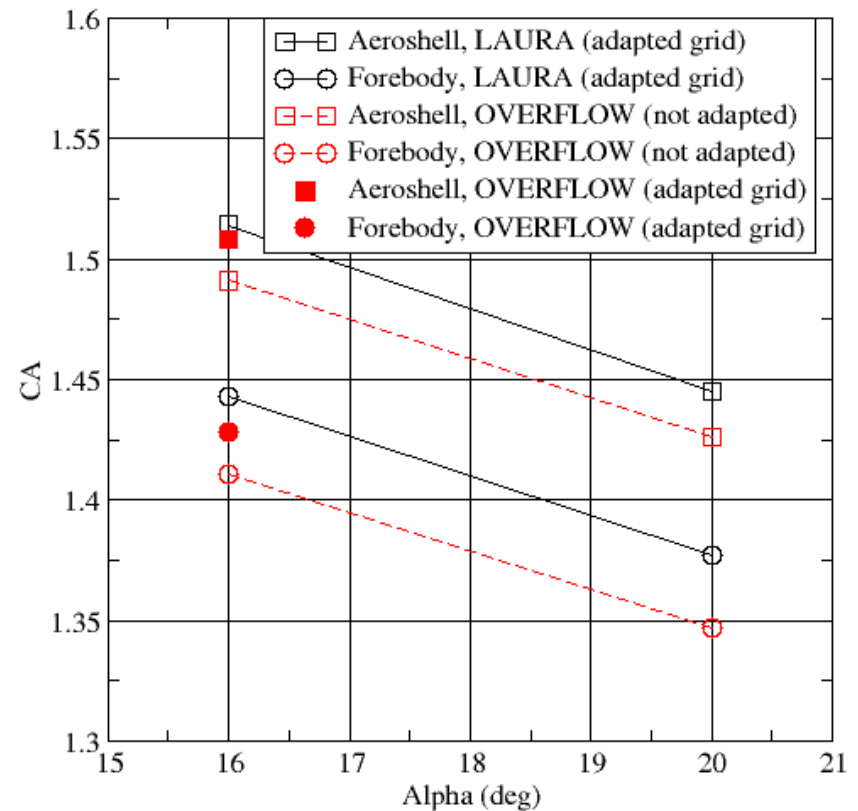
Unadapted



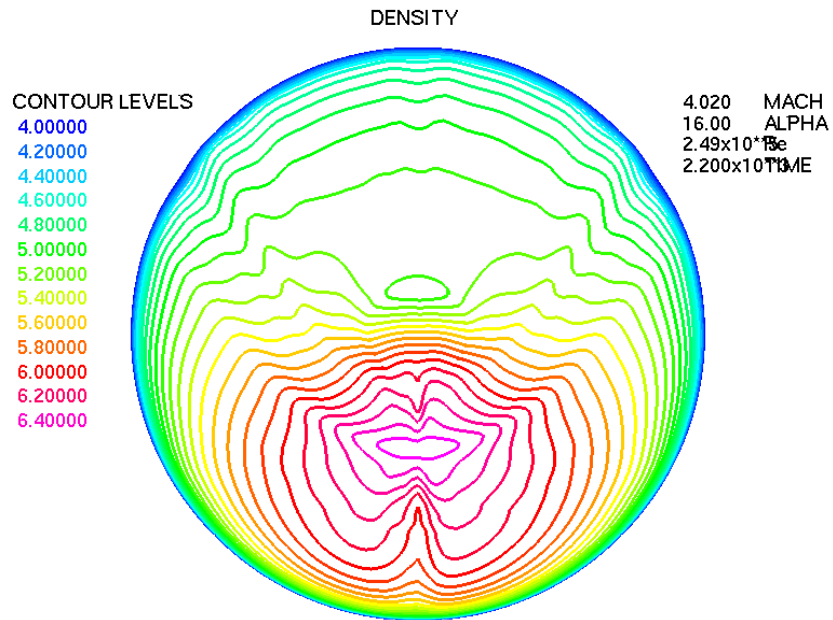
Adapted to bow shock
Mach 4, alpha 16 deg

Supersonic Aero Database Calculations

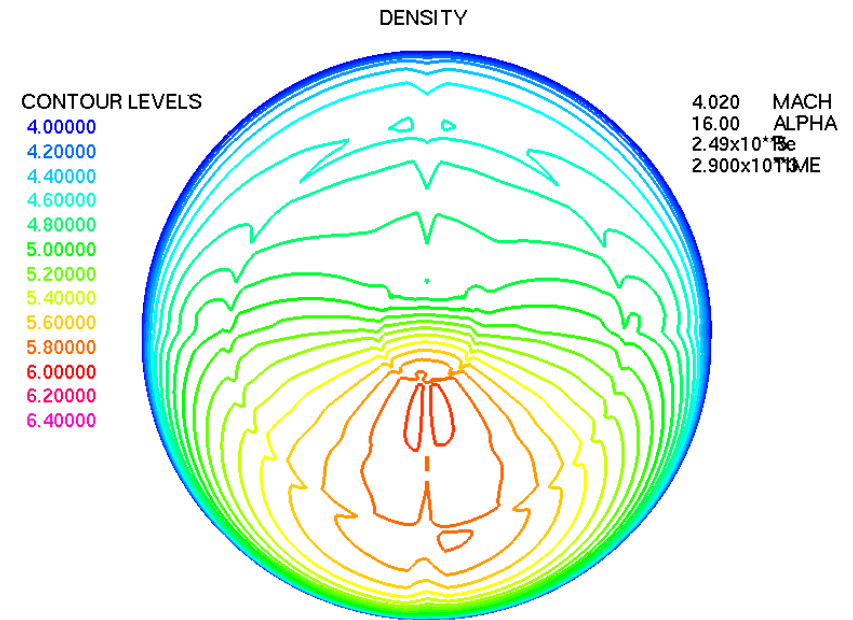
Mach 4, $\alpha=16$ and 20 deg



Unadapted grid shows anomalous
“feature” in surface density



Adapted grid shows grid-partitioning
artifacts due to poor convergence

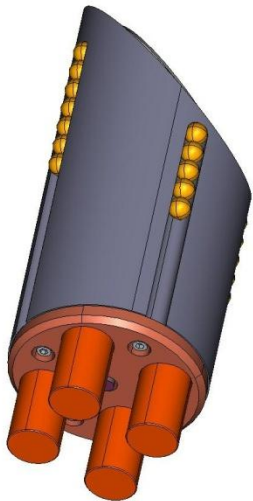


Entry Balance Mass Jettison

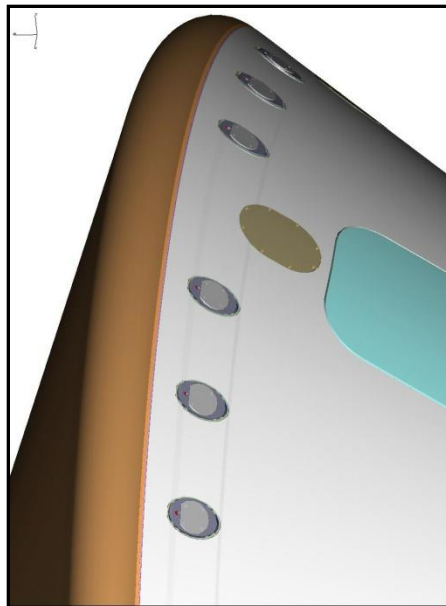
6 tungsten masses (29 kg each) jettisoned before parachute deploy, to shift center-of-gravity to capsule centerline

- Design issues:
 - Do masses separate cleanly?
 - Any aerodynamic effect on capsule?
- Solver issues:
 - Accept unresolved regions around mass-capsule intersection

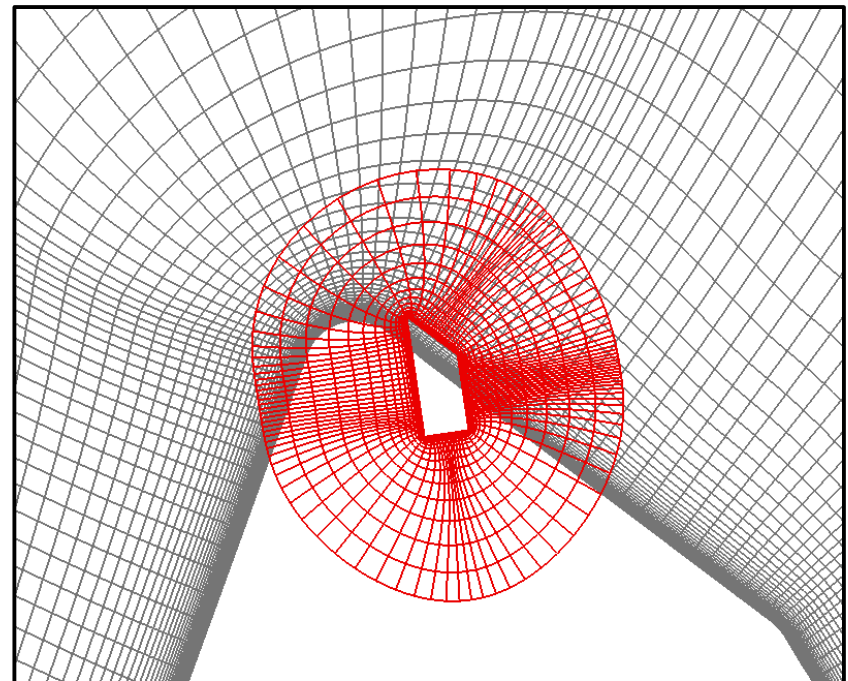
Drawing of EBMD mass



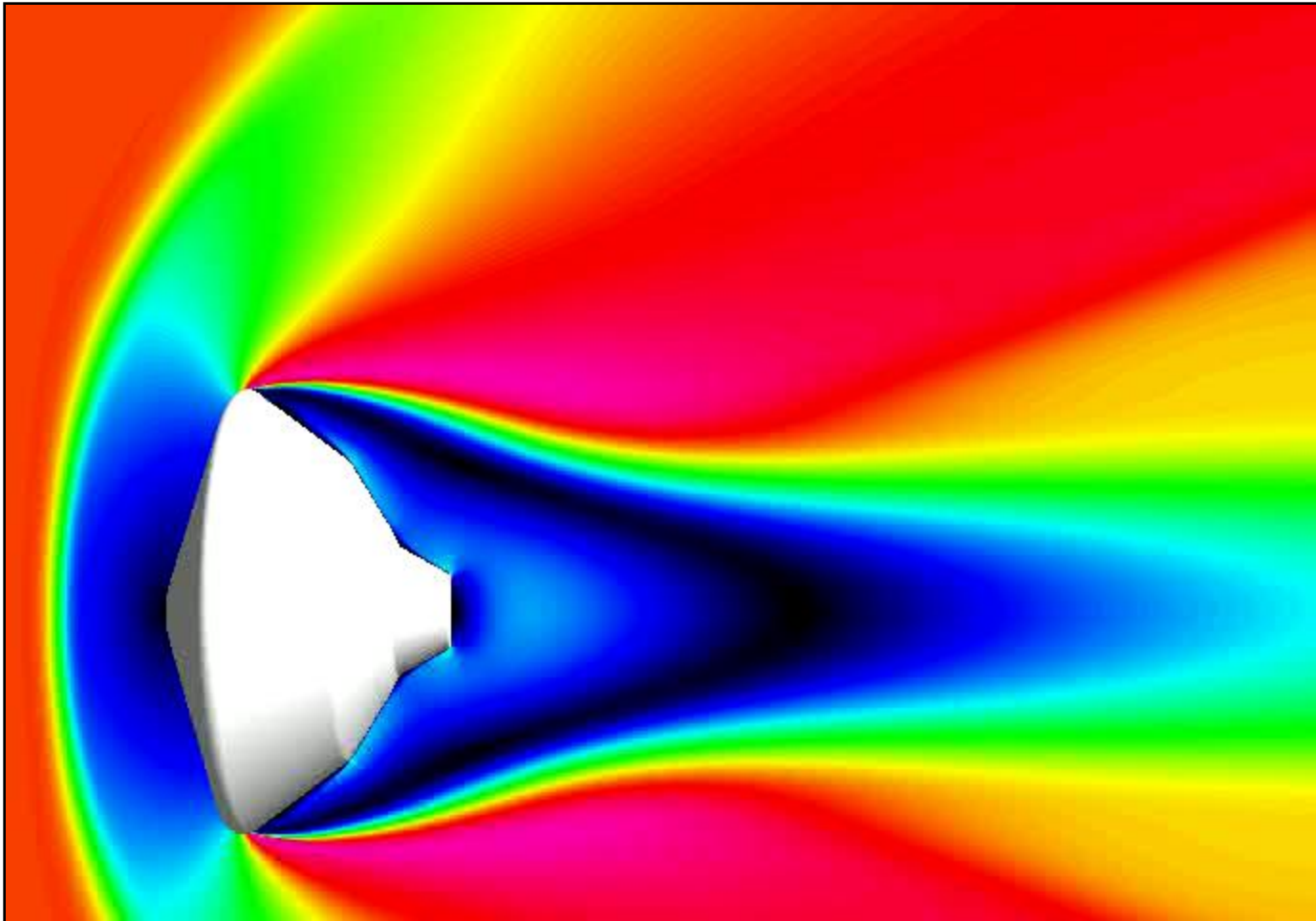
6 jettison locations on capsule



Coarse version of CFD grids



Entry Balance Mass Jettison



Capsule Flowfield Calculations

Lessons Learned

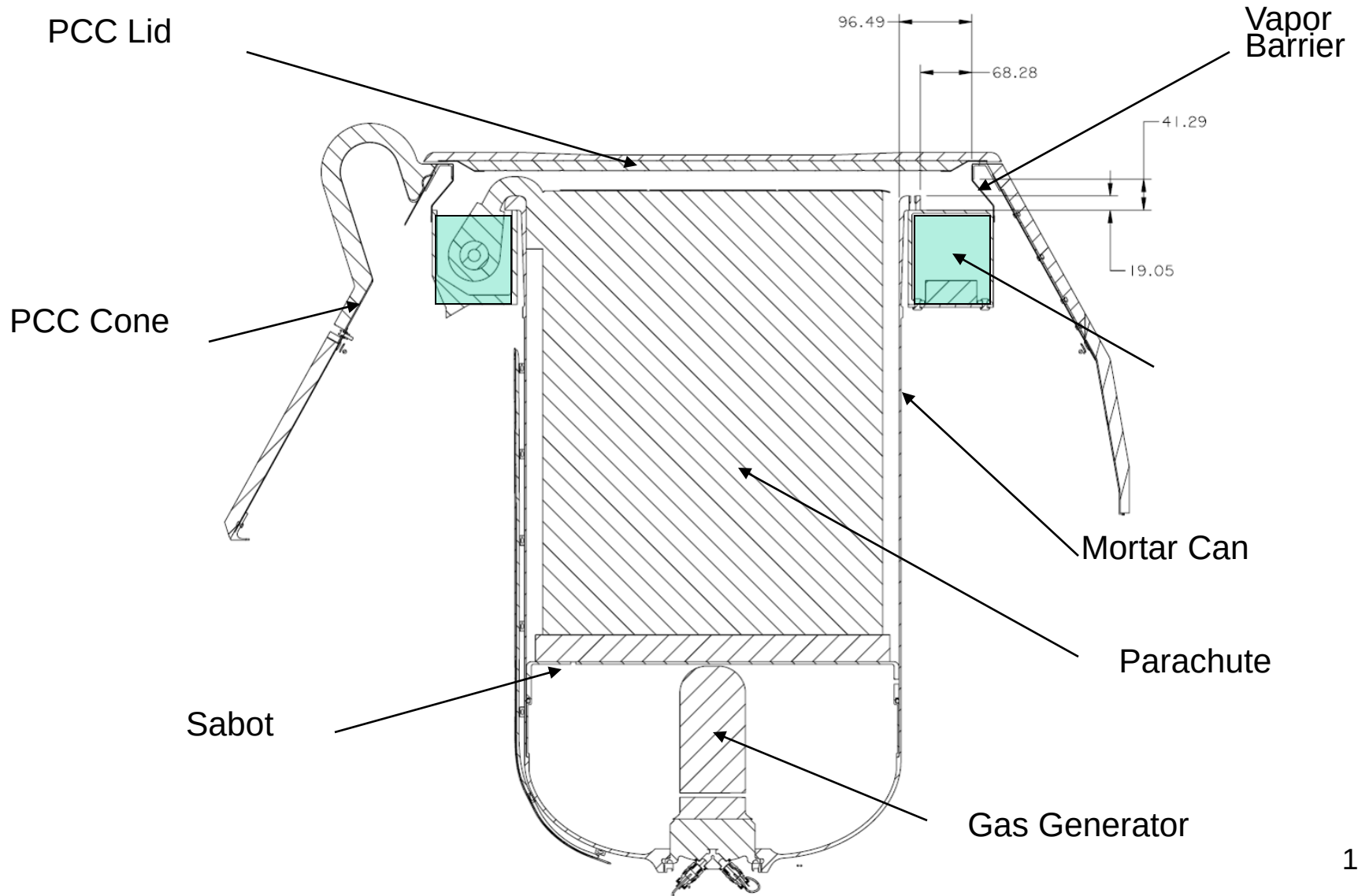
- Database calculations
 - For shocks above Mach 3(ish), watch for effects of non-aligned shocks on downstream flow properties
 - Can be mitigated by central differencing with scalar dissipation, at the expense of shock resolution
 - Be alert for grid boundary convergence issues, especially for
 - Extremely fine viscous clustering
 - Excessive grid splitting due to MPI load-balancing (OVERFLOW)
- Entry balance mass jettison
 - Ignoring resolution of capsule/mass intersection OK in this case
 - Simulation is good enough to answer engineering questions

Parachute Canister Mortar Launch

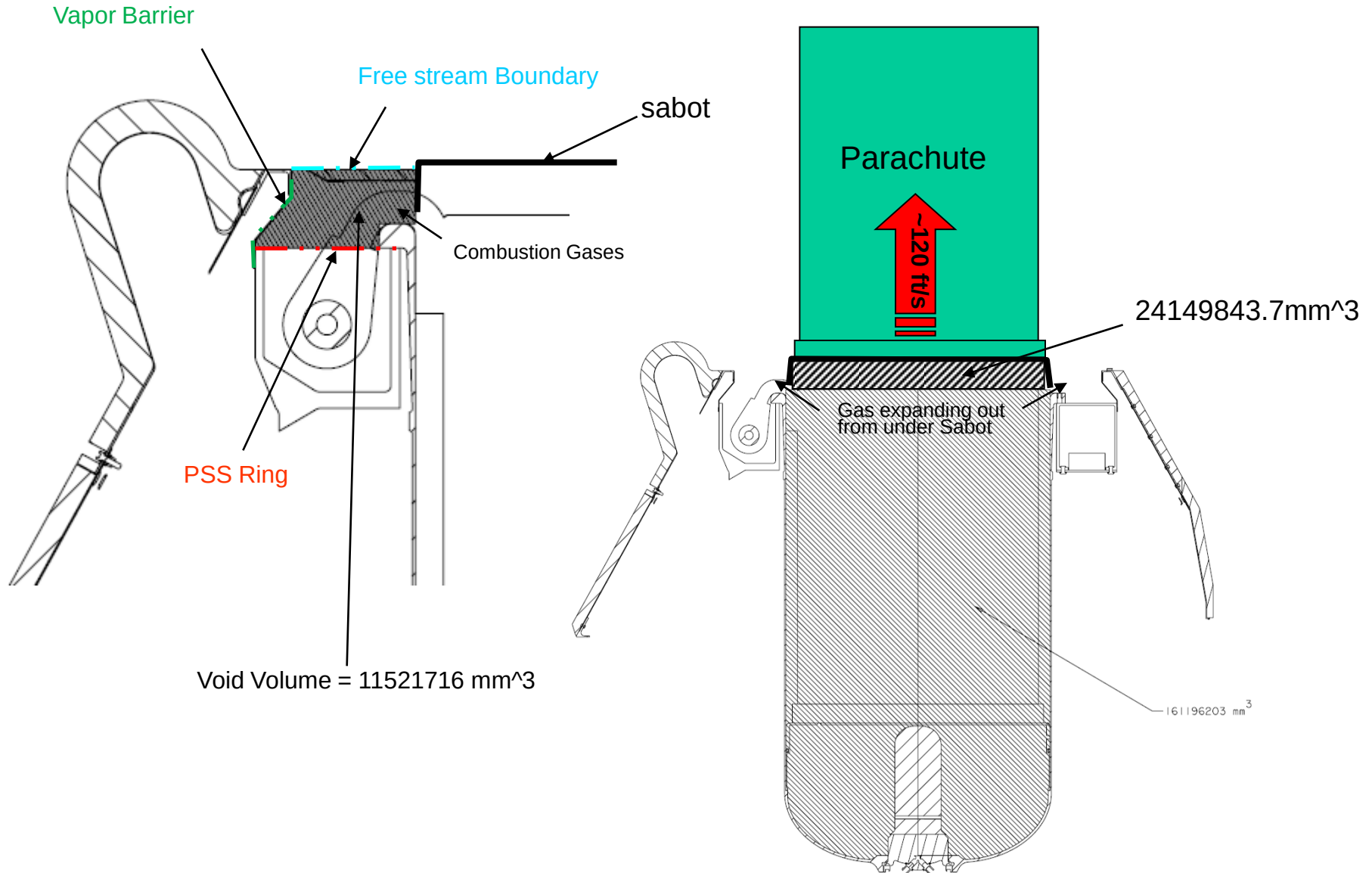
Parachute canister is expelled by mortar fire

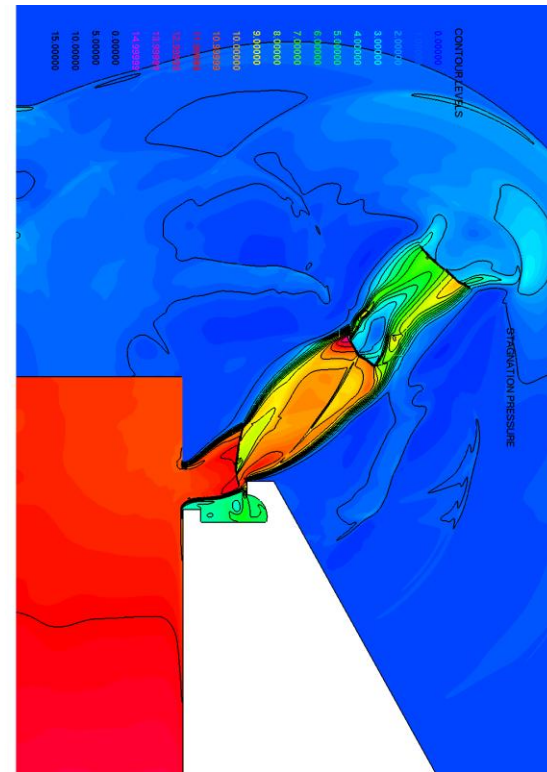
- Calculations with two gases
 - Mars atmosphere (molecular wt=43.5, $\gamma=1.29$)
 - Mortar gas (molecular wt=25.2, $\gamma=1.23$)
- Design issue:
 - What is worst-case pressure load on flexible vapor barrier?
- Solver/grid issues:
 - Sealing small gap
 - Shock capturing
 - Grid adaption

Mortar Launch (t = 0s)



Mortar Launch (t~1.15ms)

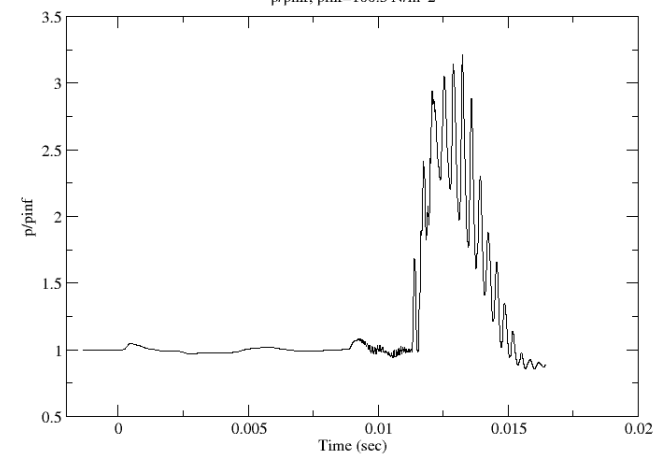




Stagnation
pressure
contours

Vapor Barrier External Pressure

p/p_{inf} , $p_{inf}=100.5 \text{ N/m}^2$



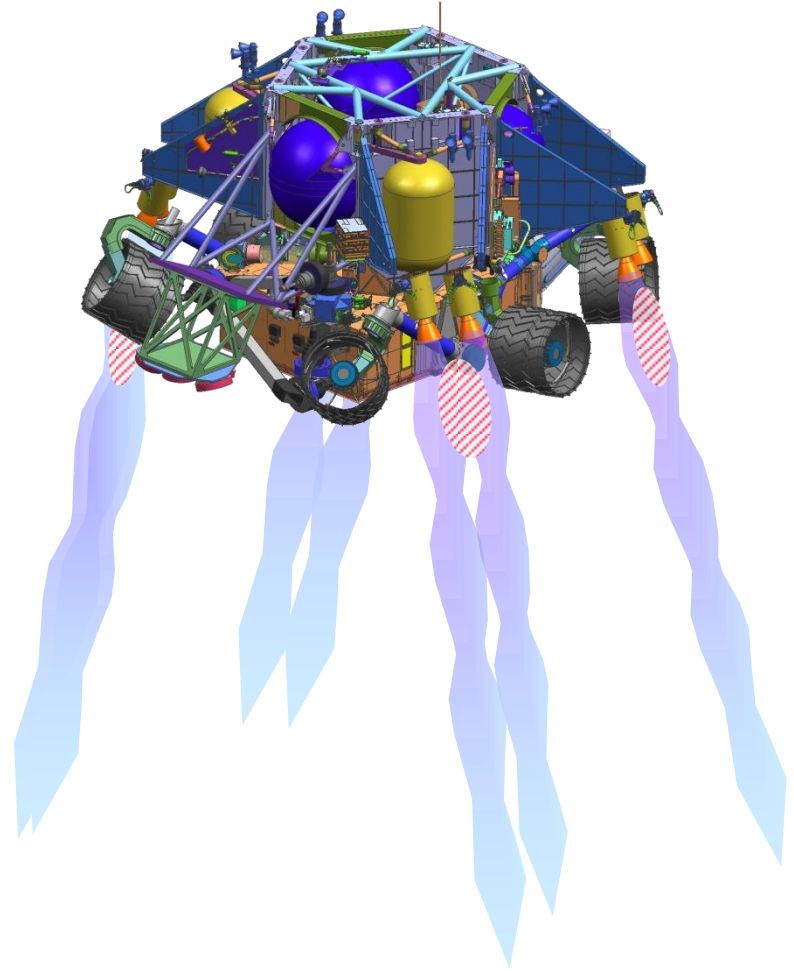
Powered Descent Plume Flowfields*

- Calculations with two gases
 - Mars atmosphere (molecular wt=43.5, $\gamma=1.33$)
 - Main Landing Engine (MLE) plume (molecular wt=13.4, $\gamma=1.38$)
- Design issues:
 - Highly under-expanded plumes (40:1)
 - Interaction of closely-paired plumes and proximity to stowed rover
- Solver issues:
 - Turbulence modeling
 - Shock capturing
 - Downstream boundary condition for oncoming flows

*Similar calculations were performed by Dr. Francisco Canabal (NASA MSFC), using the Loci-Chem CFD code. Information presented here reflects lessons learned from those calculations as well.

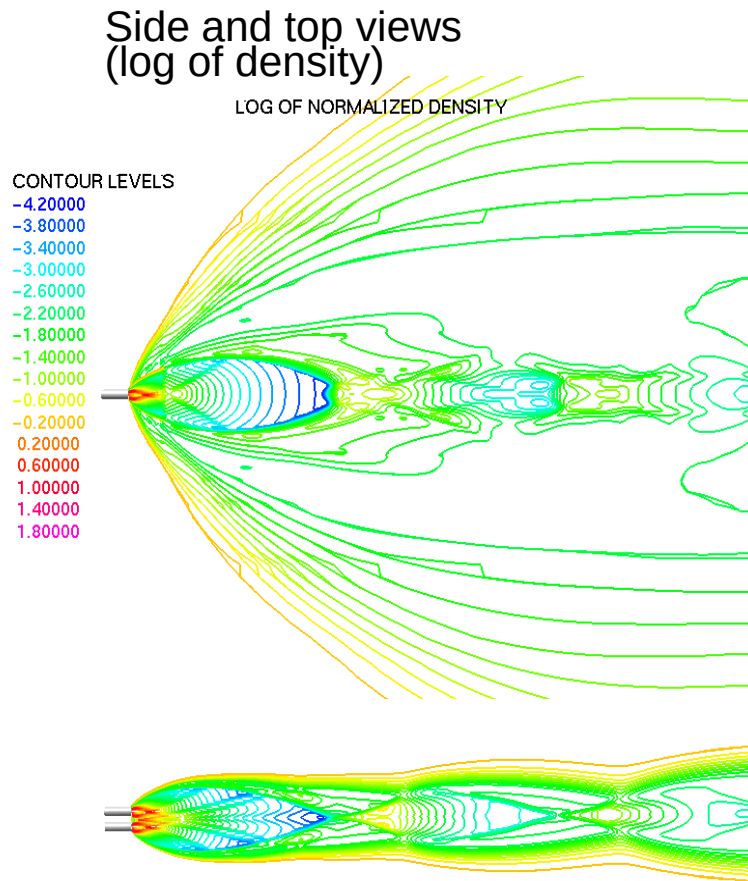
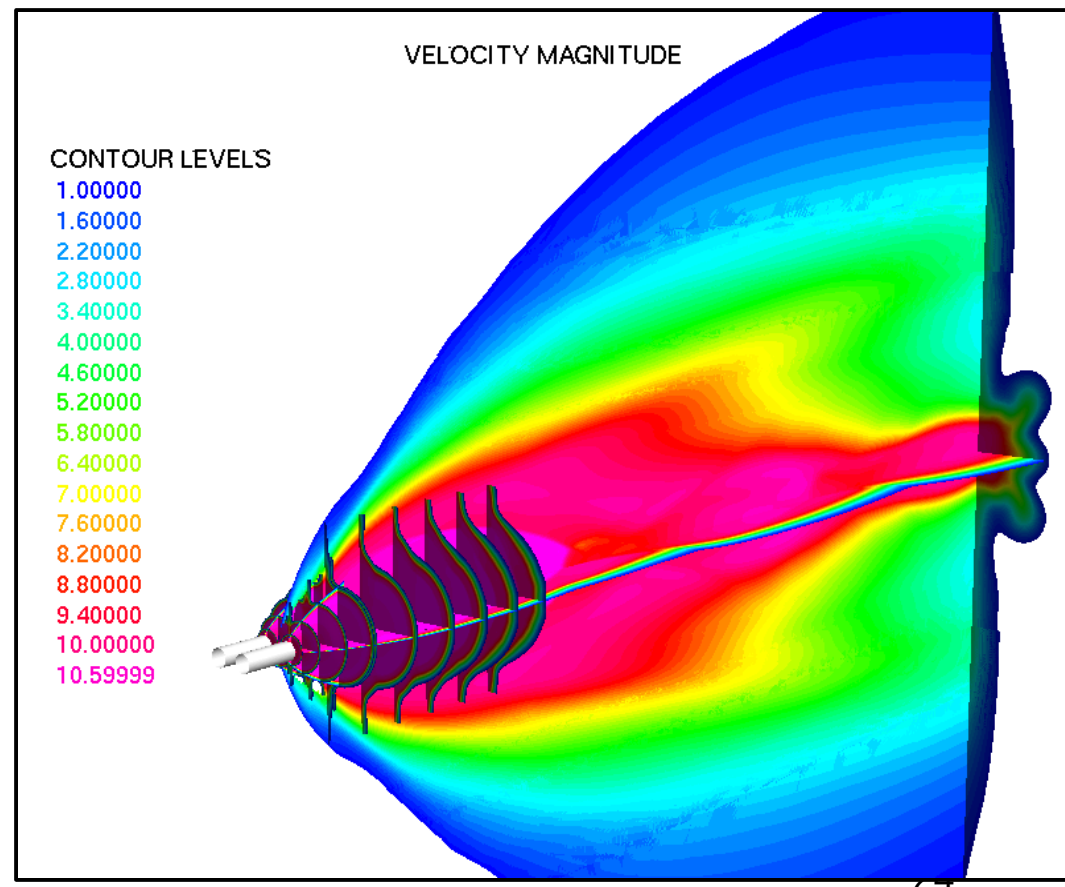
Powered Descent Plume Flowfields

- Rover heating due to plume radiation
- Direct plume impingement on rover



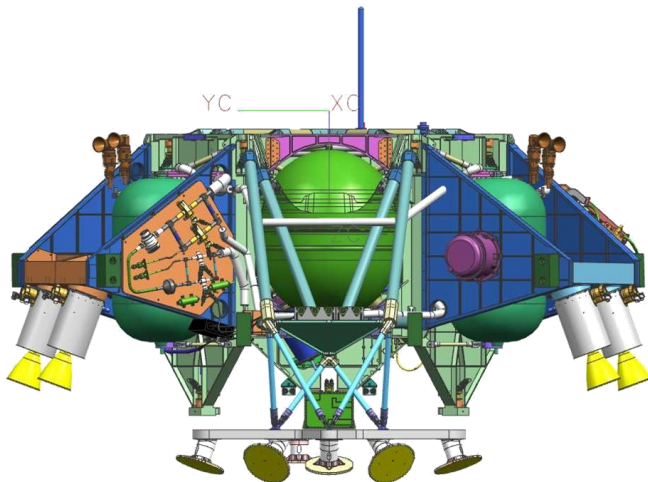
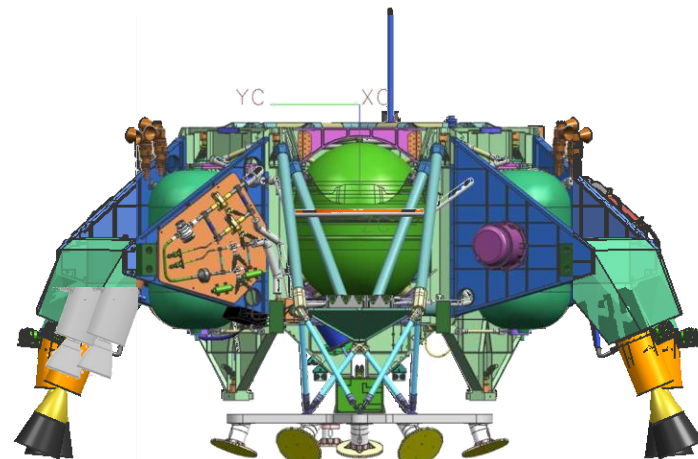
Powered Descent Plume Flowfields

- Plumes are highly underexpanded (40:1 pressure ratio)
- Two-plume simulation shows interaction sheet at intersection plane



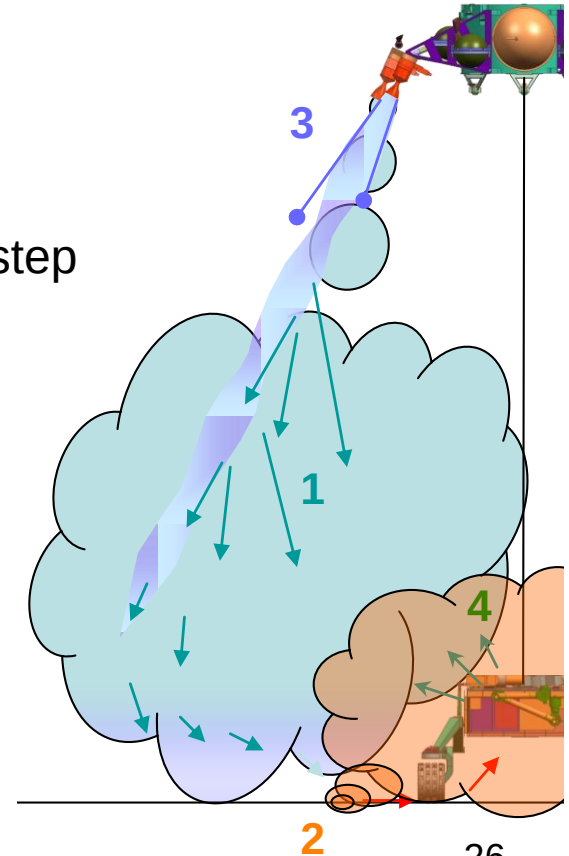
Powered Descent Plume Flowfields

- MLE's moved out and down
- MLE pairs changed from 20/20 deg cant angles to 22.5/5 deg
 - Reduces plume-plume interaction
- All 8 engines fire for initial slowing
- Outboard 4 (22.5 deg cant) fire for final descent and hover



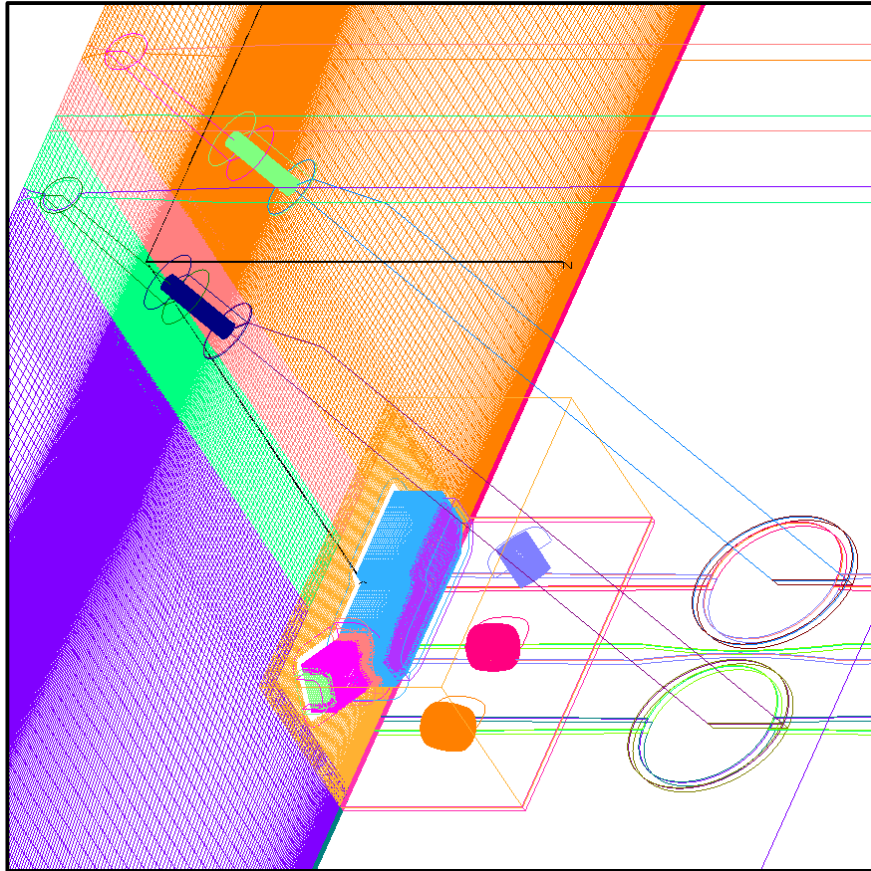
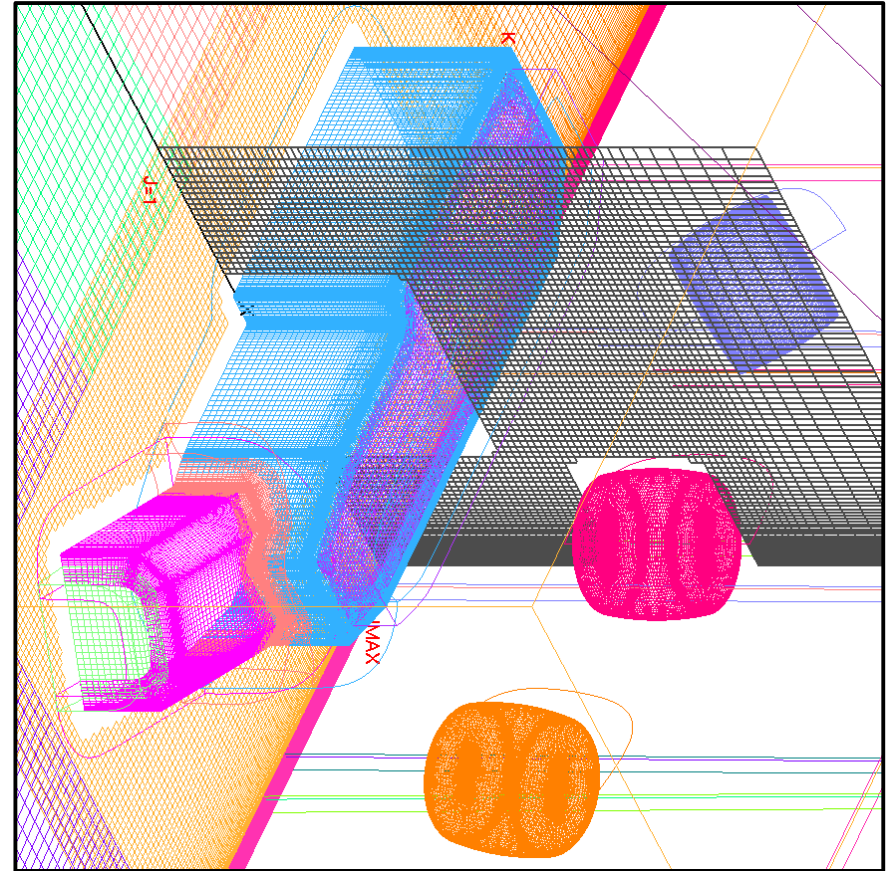
Plumes in Ground Proximity

- Design issues:
 - Flowfield in proximity to rover – dust, plume contaminants, heating effect on rover and its instruments
 - Effect of ground slope, shape
- Solver issues:
 - Robustness, time-accuracy and achievable time-step
 - Total physical time simulated, unsteadiness
 - Accuracy and uncertainty



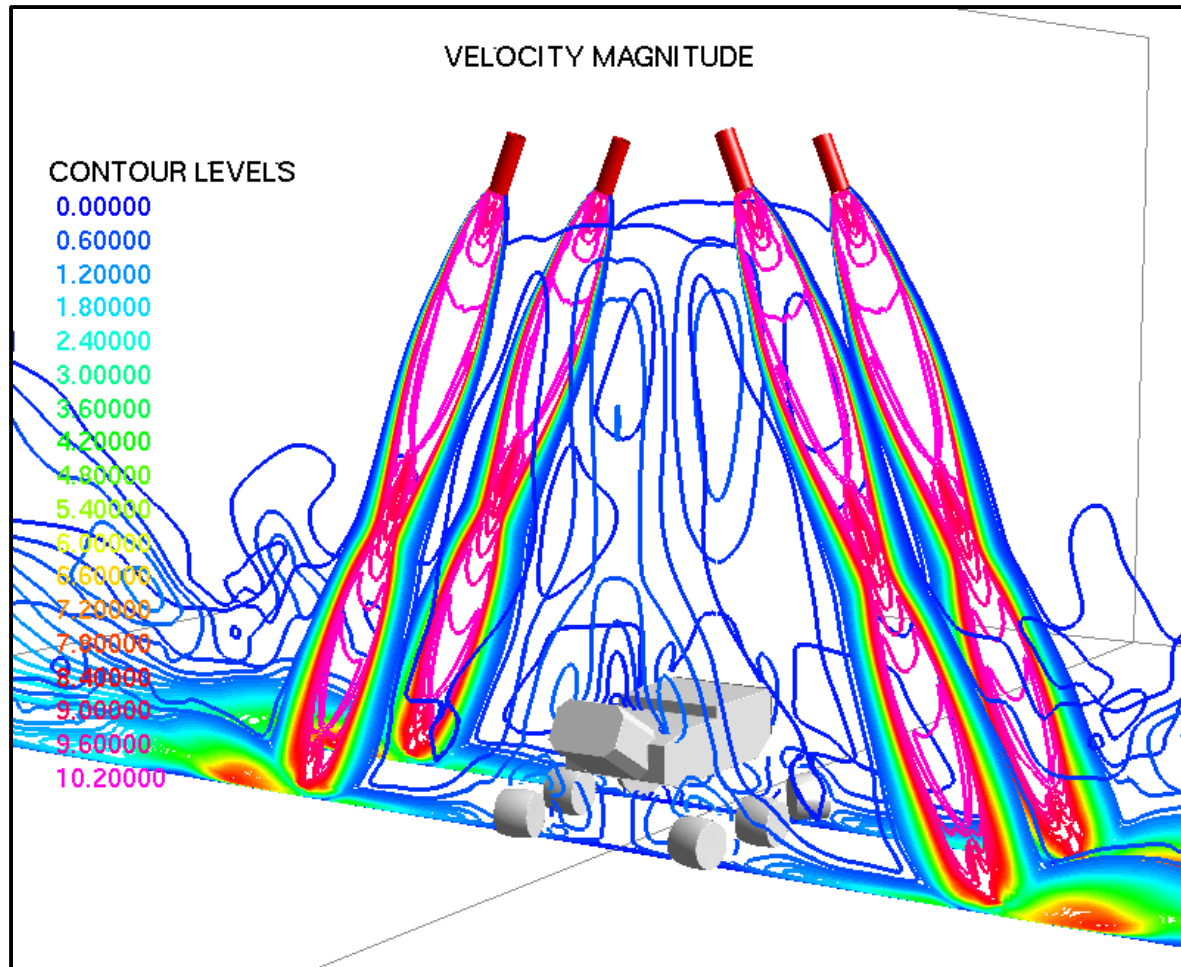
Plumes in Ground Proximity

32 million-point grid, $\frac{1}{2}$ symmetry

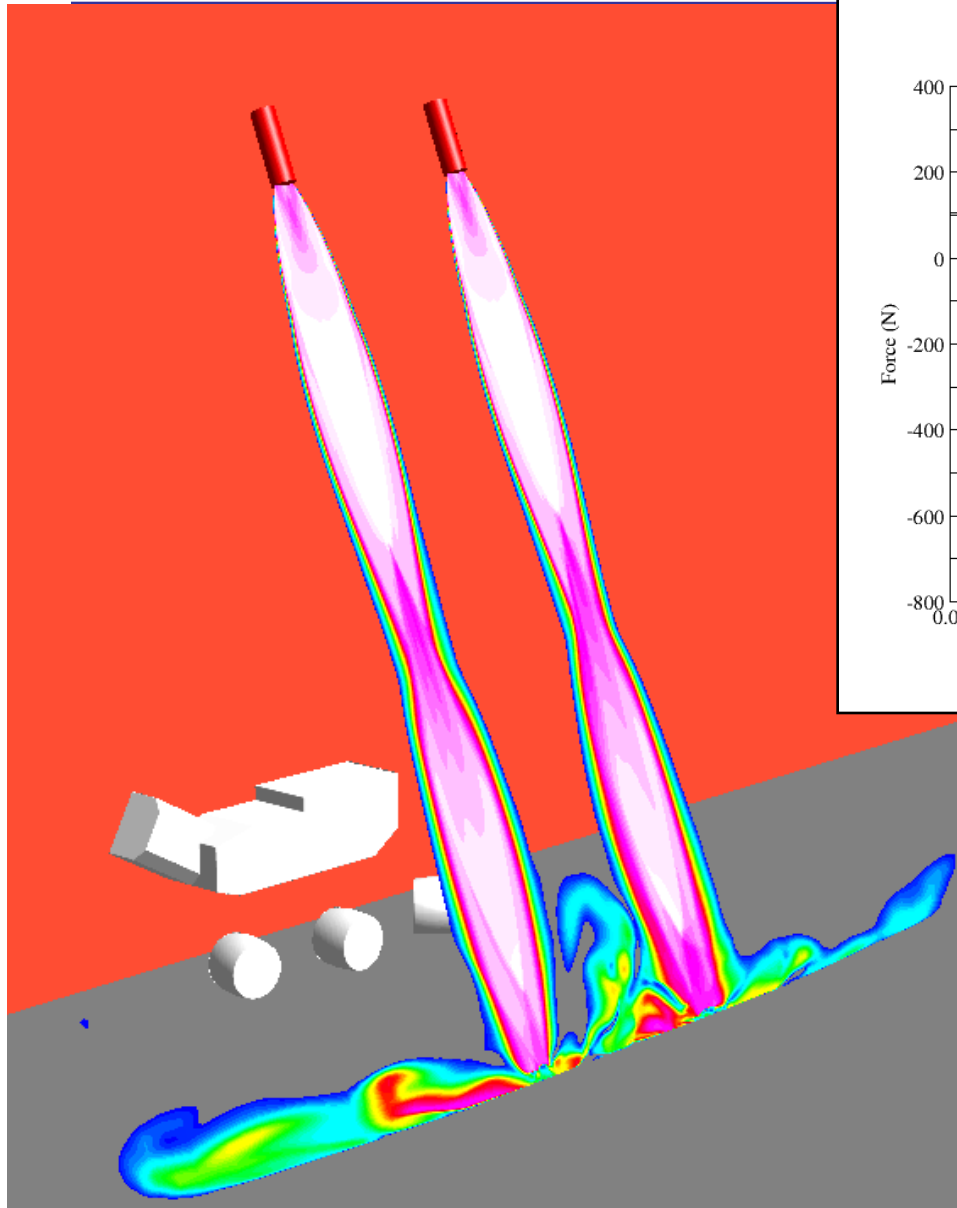
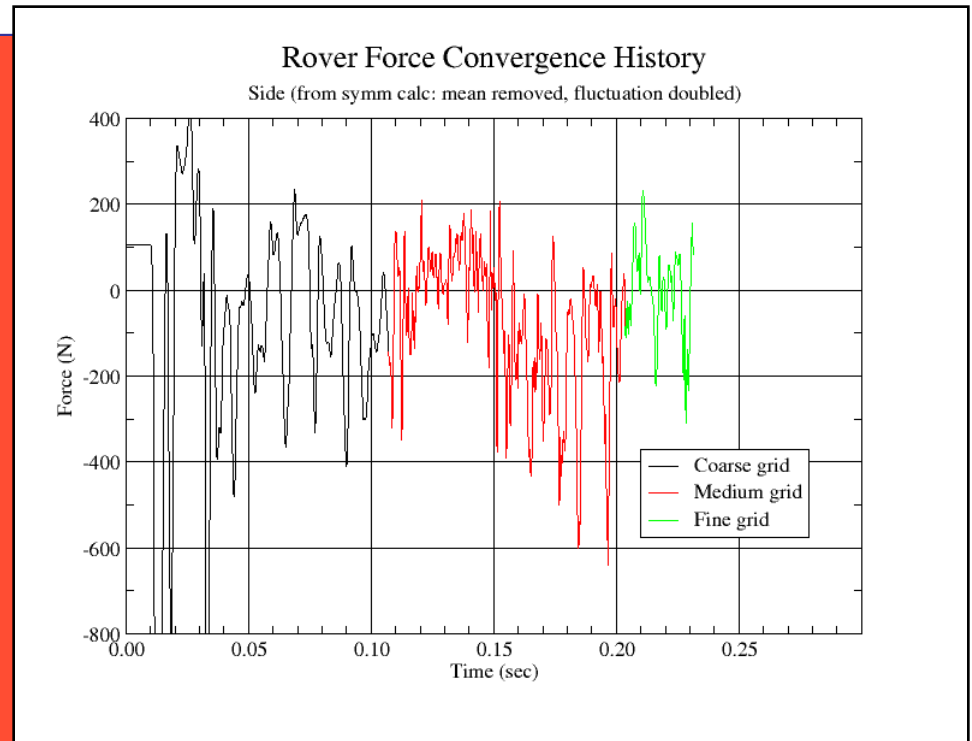


Plumes in Ground Proximity

- Dust velocity might be up to 600 m/s (1/3 micron, $CD=1$)

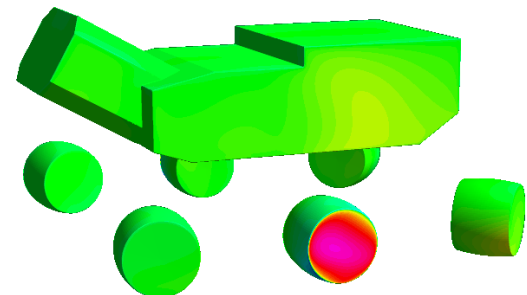


Plumes in Ground Proximity



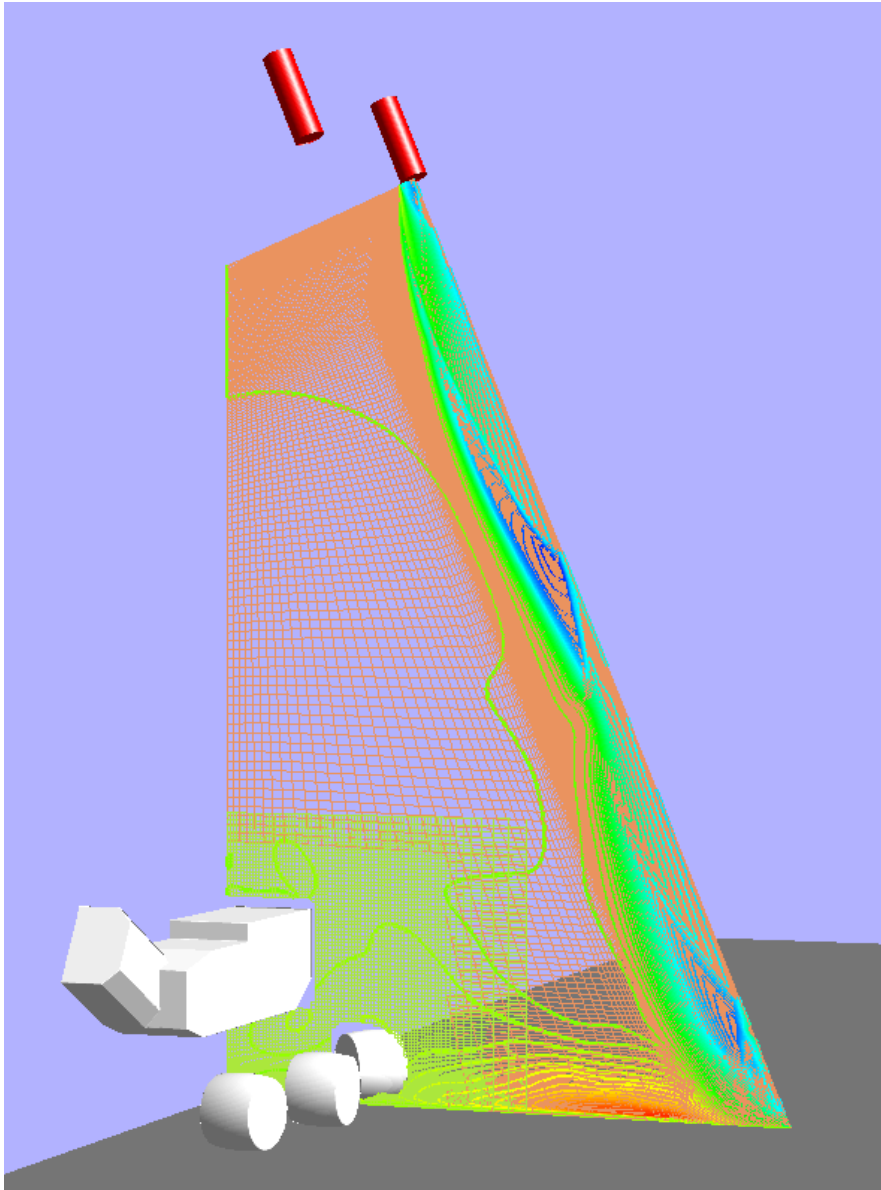
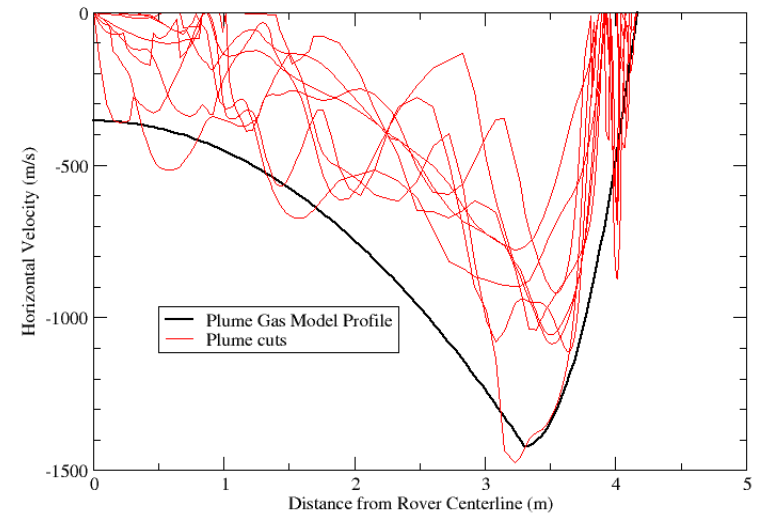
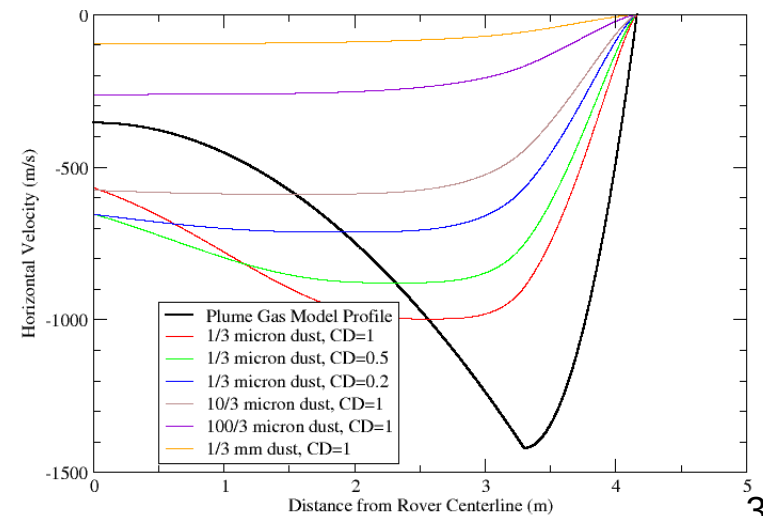
CONTOUR LEVELS

0.70000
0.76000
0.82000
0.88000
0.94000
1.00000
1.06000
1.12000
1.18000
1.24000
1.30000
1.36000
1.42000
1.48000



Rover surface pressure

Plumes in Ground Proximity



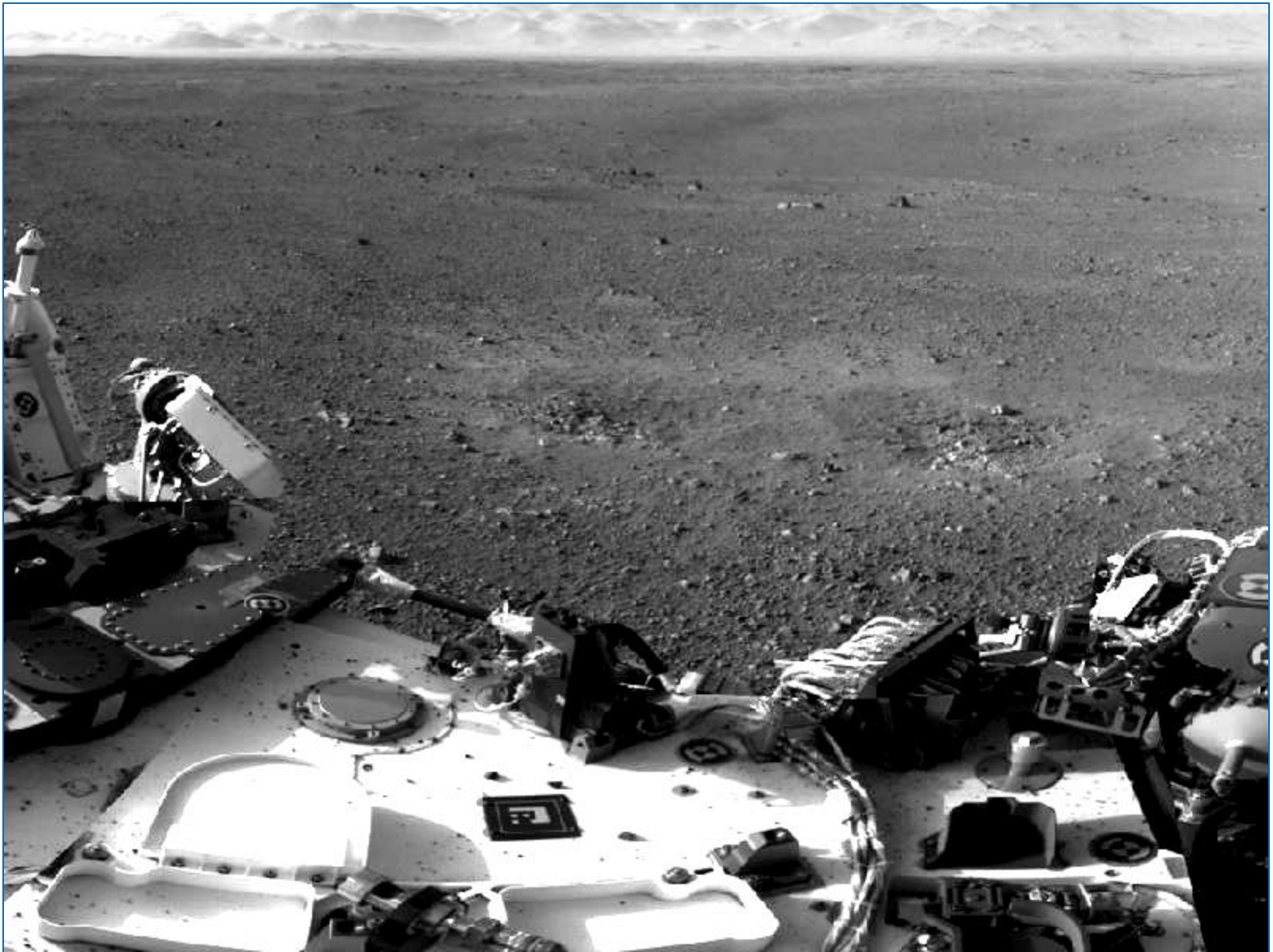


Image shows blast marks from descent rocket engines and debris on Rover deck. (Image credit: NASA/JPL-Caltech)

Descent and Landing Plumes

Lessons Learned

- For hover/ground proximity cases, never clearly achieved steady “average” flow-field
 - Plume termination shocks not steady (numerical?)
 - Expense of running fine-grid solution
 - 32Mpts, time-step=1.1.E-5 sec
 - 32 sec/step on 128 CPUs (NAS Columbia SGI Altix)
 - 1 sec real-time would take 33 days of computing
- ...and what was the accuracy again?
 - Grid, turbulence model sensitivity?
 - What engineering questions *can* we answer?

Conclusions

- Missions such as MSL have widely varying applications needing CFD analysis
- Both capsule and plume flowfield computations have unique requirements and concerns
 - Capsule flow simulations fairly routine
 - Plume flowfields still difficult due to stability limitations, unsteadiness, uncertainty
- CFD is still not as easy as we would like for addressing engineering questions!