

## A Heat and Mass Transfer Model of the Orion European Service Module Propulsion Sub-System

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Supported by the European Service Module Propellant Integration Team Project

# Orion European Service Module Thrusters

- Hypergolic, pressure fed, common supply
- 1x Space Shuttle Orbital Maneuvering System (OMS)
   AJ10-190

27 kN (6000 lbf) thrust with TVC

AM1 engine a spaceflight veteran: 19 missions, 89 burns.

8x Auxiliary thrusters (PlusX), European ATV heritage
 490 N (110 lbf), no TVC

Trajectory corrections

Backup to OMS

24x Reaction Control System thrusters, ATV heritage
 220 (50 lbf) thrust

12 nominal, 12 backup

6 clusters of 4 thrusters



### Propulsion Subsystem (PSS)

Two helium tanks

300 L, 0.41 meter radius

Up to 400 bar pressure

Cross-feed as backup (for AM2+)

Four propellant tanks

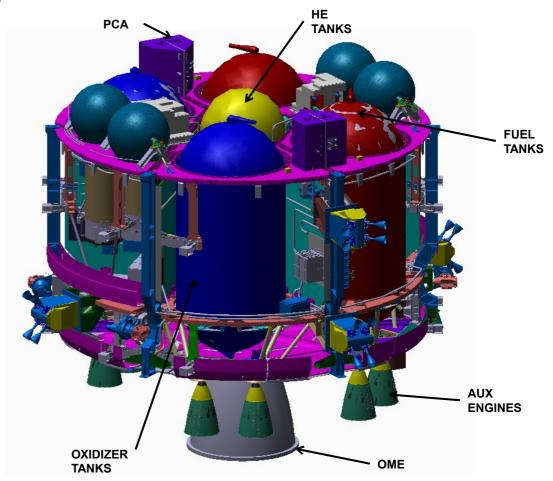
2 m<sup>3</sup> each, ~10 tons total propellant

Two tanks mixed oxides of nitrogen (MON)

Two tanks monomethyl hydrazine (MMH)

Serial configuration

Solenoid valves and electronic pressure regulation
 Programmable set-points, 17 bar nominal



#### **Prior Art**

Time stepping methods for analyzing spacecraft propulsion systems

 An Analysis of the Problem of Tank Pressurization During Outflow NASA TN D-2585 (1965)



- Modeling of the Intelsat VI bipropellant propulsion subsystem AIAA-1993-2518
- Development and Validation of Fluid Thermodynamic Models for Spacecraft Propulsion Systems (Journal of Propulsion and Power 2001)



AN ANALYSIS OF THE PROBLEM OF TANK PRESSURIZATION DURING OUTFLOW

by William H. Roudebush Lewis Research Center Cleveland, Ohio

ATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • JANUARY 1965

### NASA GRC Heat and Mass Transfer (HMT) Code

Energy and mass conservation

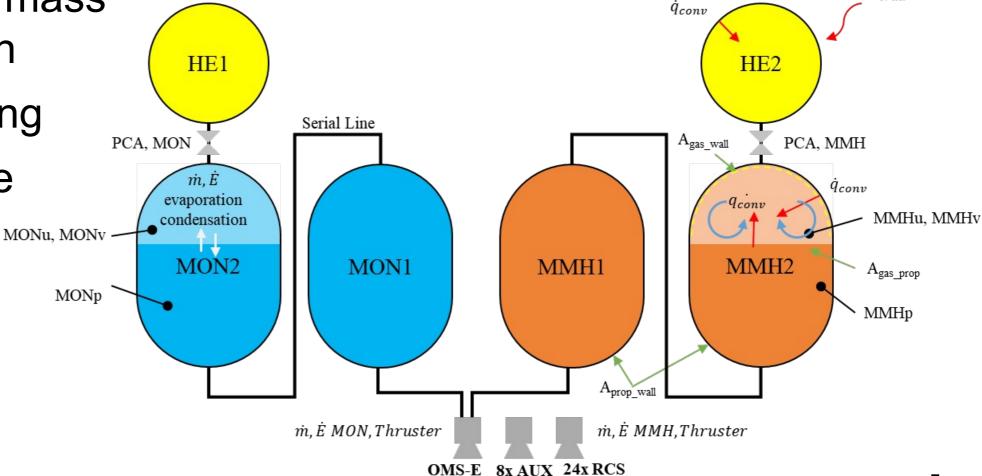
Time-stepping

Steady-state

• 1-D

MATLAB

~150 statevariables



 $\dot{q}_{rad}$ 

#### Propellant Vaporization and Heat Transfer

Propellant is a large mass in thin-walled titanium tanks

Heat transfer between liquid propellant and ullage gas
Heaters add energy to when propellant falls below 20°C
No other heat exchanged with environment currently

No other heat exchanged with environment currently modeled

Evaporation and condensation assumed instantaneous to maintain saturated vapor

Geometry changes affect heat transfer

During coast, ullage assumed to be a spherical bubble in center of tank

During thrusting, circular interface between ullage and liquid

Observations

Ullage cools as it expands during engine firing
Ullage warms as helium is added during pressurization
Thermal mass leads to slow changes in liquid temperature



Nitrogen Tetroxide Venting (from 1960s NASA Safety Video)

#### Helium and COPV Heat Transfer

 High pressure helium gas used to maintain pressure in propellant tanks

Conductive heat transfer between COPV and helium gas

Radiative heat transfer between environment and COPV

Observations

Large tank mass compared to mass of gas
Thermal mass of COPV significant
Helium cools as it expands



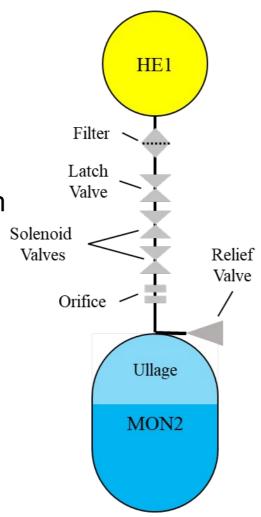
Example COPVs

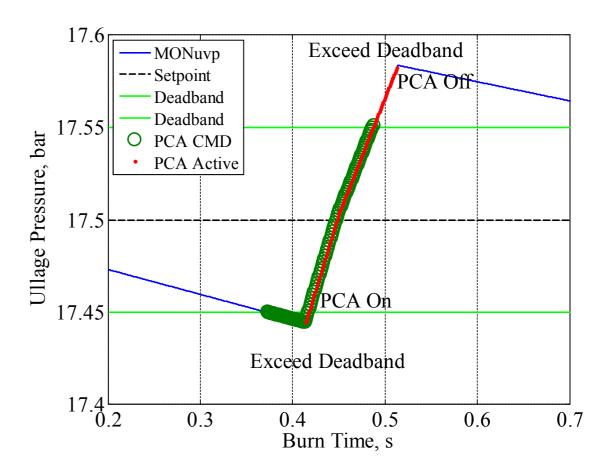
#### Electronic Pressure Regulator

- Pressure Control Assembly (hardware)
- Pressure Regulation Unit (avionics)
- Latch valve enables system
- High-pressure solenoid valves

Setpoint, deadband Timing, overshoot

Orifice throttles flow
 Choked and unchoked flow simulated, plus secondary losses





## Piping Flow Model

 Network of fluid resistance coefficients

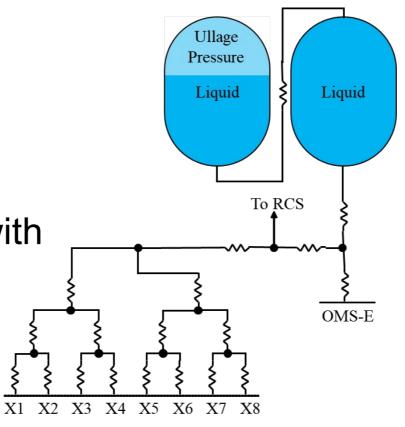
Solved at each time step

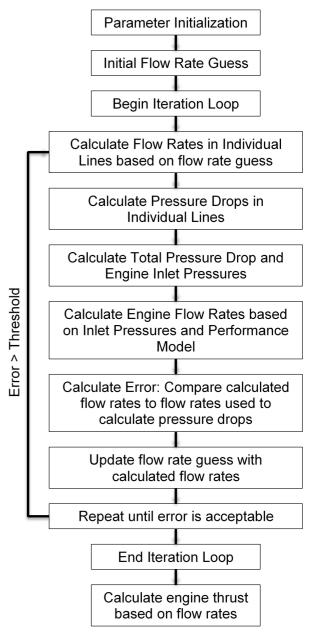
Accounts for changing ullage pressure

Fluid density changes with

temperature

Momentum neglected





## Workflo

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#### **Initial Conditions**

- Prop Load (mass)
- Helium Load (pressure)
- Initial Temperatures

#### **Global Variables**

- Material Properties
- Tank Volumes
- Vehicle Dry Mass
- Orifice Area

#### **Control Variables**

- Engine Valve State
- PCA Valve State
- Relief Valve State

# Calculate Primary State Variables

Mass and Energy of commodities

#### Secondary State Variables

- Heat and mass transfer rates
- Things needed to calculate heat and mass transfer rates

#### **Main Loop**

- 1) Update Mission Phase f(t)
- 2) Check logic for ending simulation *f*(*t*, *prop*, *helium*, *op-box*)
- 3) Set time step size *f(engines, pressurization)*
- 4) Update Control state *f(ullage, setpoint)*
- 5) Update Primary State Variables [m, e] = f(m, e, mdot, edot, dt)
- 6) Update Secondary State Variables
- 7) GOTO 1)

#### **Options**

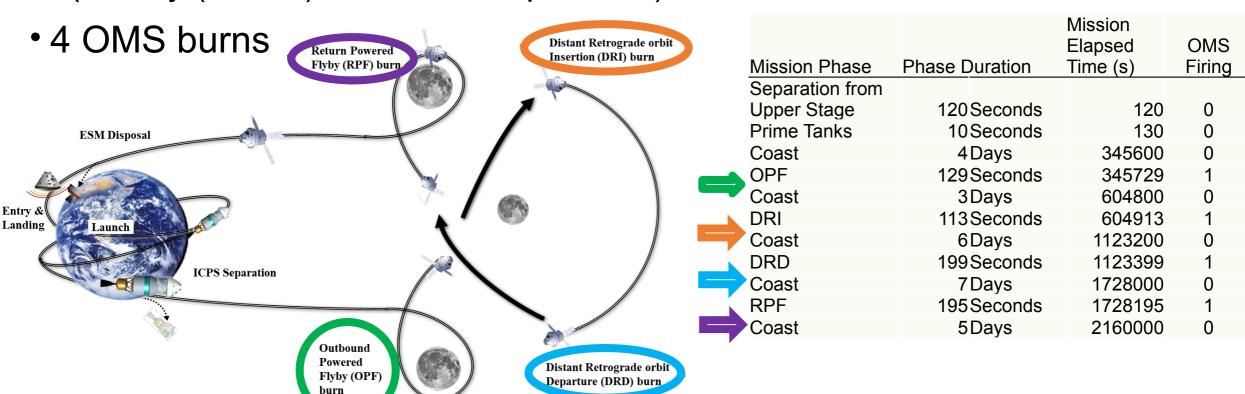
- Output choices
- Time step sizes
- Tank Priming
- Op-box options

#### **Mission Phases**

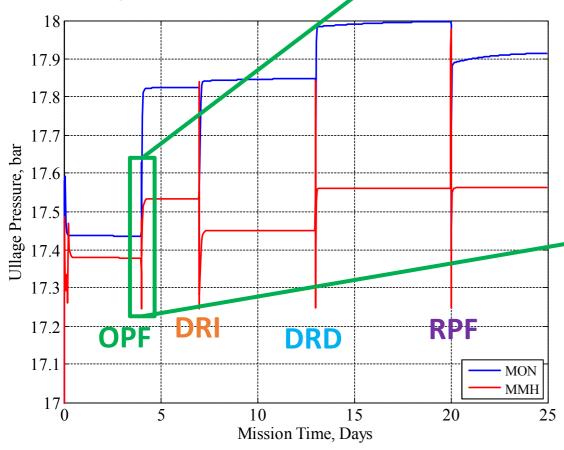
Time, Engine States

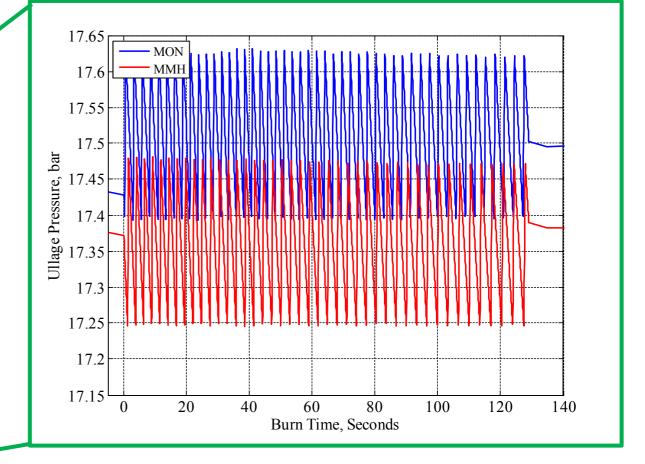
#### **Example Mission**

 25 day (1-orbit) Distant Retrograde Orbit (43 day (2-orbit) mission also possible)  $\Delta t$  OMS/PCA = 0.001 s  $\Delta t$  Aux/RCS/100 s after burn = 0.1 s  $\Delta t$  coast = 100 s O(10 m) Simulation Time

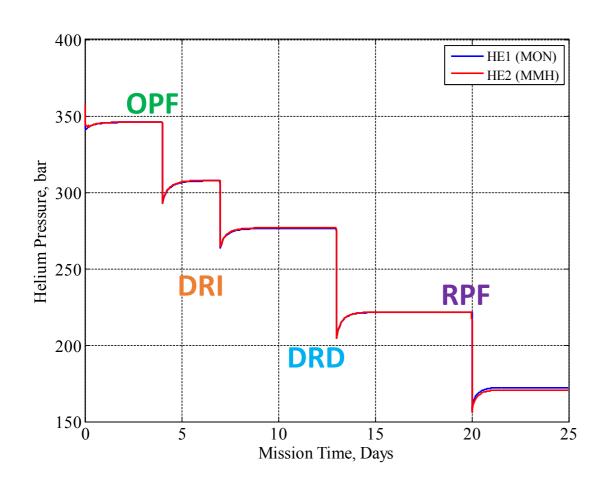


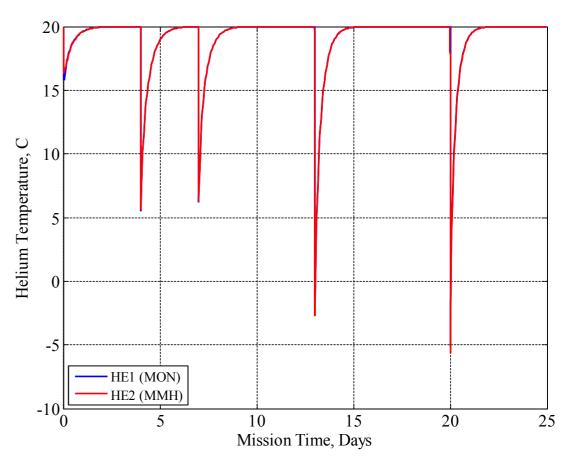
# Example Results: Ullage Pressure



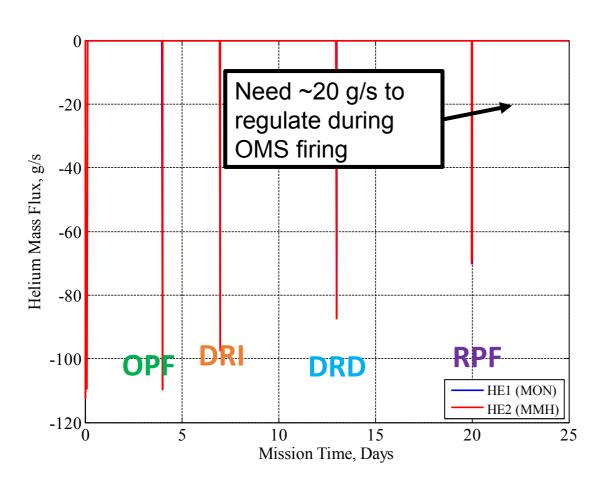


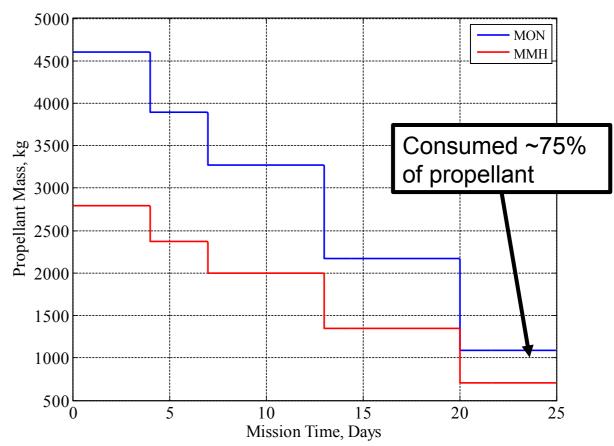
## Example Results: Helium Pressure and Temperature





## Example Results: Helium Mass Flux and Prop Mass





#### Summary

- A tool for modeling the thermodynamic state of the ESM PSS has been developed
- Code is fast, flexible and relatively easy to modify
- Multiple applications

Commodity consumption

Capabilities evaluation

Mass gauging

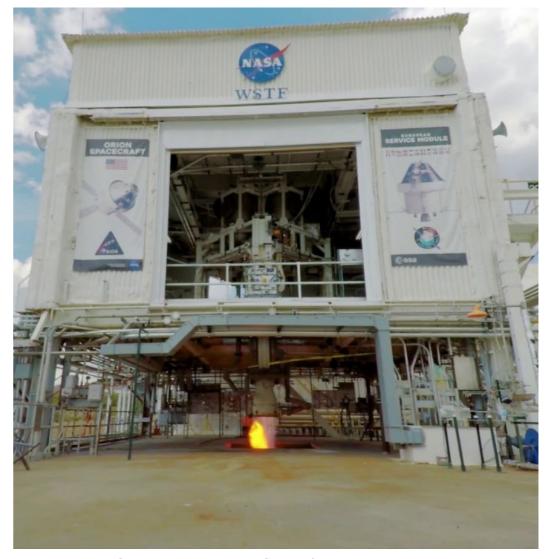
**Avionics simulation** 



AM1 Orion and SM at NASA GRC Plumbrook Station Vacuum Chamber

#### **Future Work**

- Helium solubility in propellants
- Timescales for vapor equilibrium
- Conductive/radiative heat transfer between components, sun exposure, mission, firing
- Individual propellant tanks



ESM Propulsion Qualification Module Test Firing at White Sands Test Facility

#### Acknowledgements

- Former NASA GRC engineer
   Aaron Schinder developed the initial version of the HMT code
- Technical Guidance by Jon Millard, Prop Integration Engineering Team Lead
- GRC Propulsion Division
   sponsored conference participation



NASA GRC Aircraft Hanger

## Questions?

