



# Aftbody Shape Effects on Dynamic Stability using Free-Flight CFD



Zachary Johnston

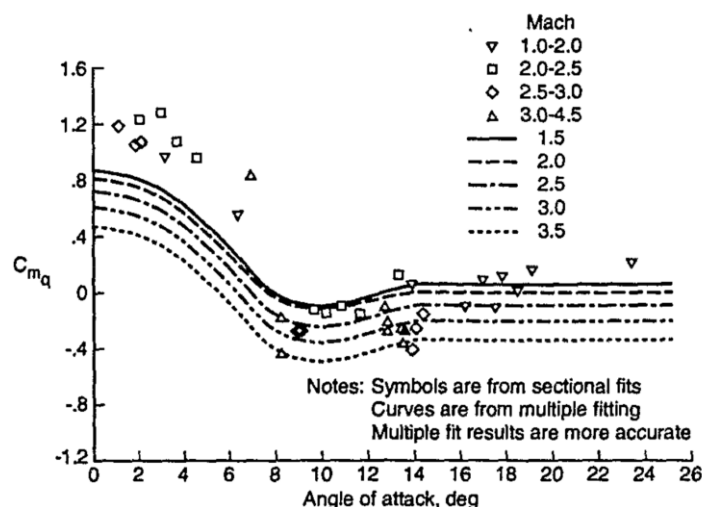
Mentors: Joseph Brock & Dirk Ekelschot

August 28<sup>th</sup>, 2020

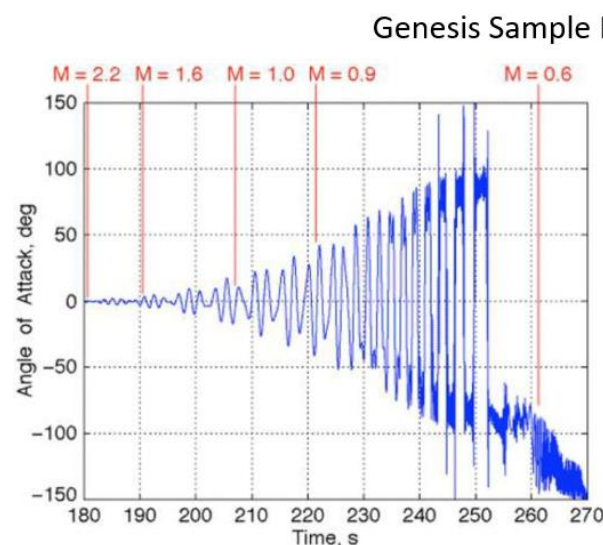
# Genesis Sample Return Mission



- Dynamic stability is typically characterized by experiments
  - Forced-Oscillation Testing, Free-Oscillation Testing, Free-Flight Wind-Tunnel Testing, and **Ballistic Range Testing**
  - Flight parameters are not always completely represented
- Dynamic stability of the Genesis capsule were characterized by BR campaign in 1999
  - Experiment suggested capsule stability above Mach 2.0 for all angles
  - Due to a failure of drogue parachute deployment, capsule decelerated through dynamic unstable regime and saw unbounded growth in total angle of attack

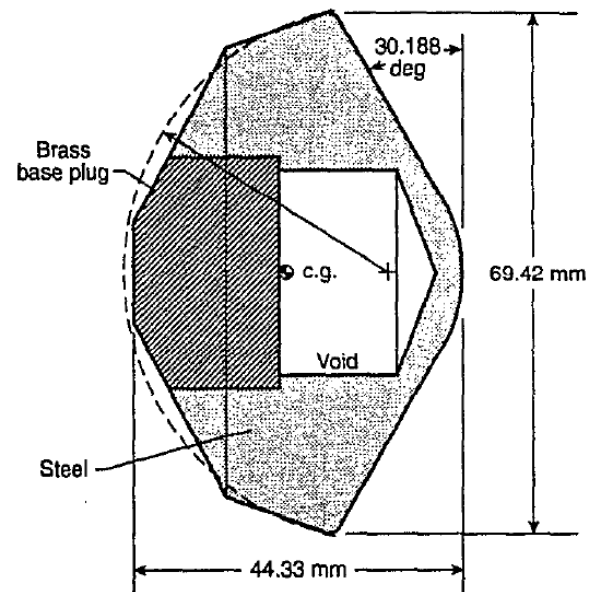


**Figure 10. Pitch Damping Moment Coefficient vs. Mach Number.**

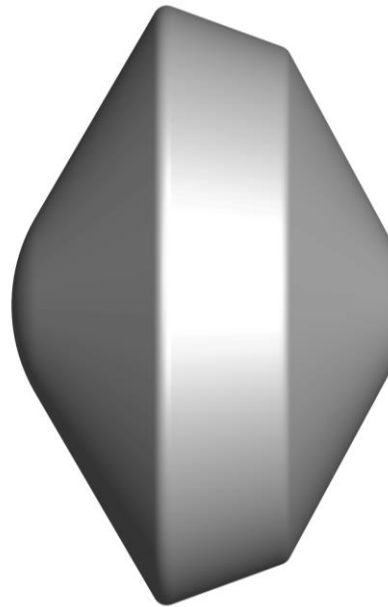


# Free-Flight Modeling Motivation

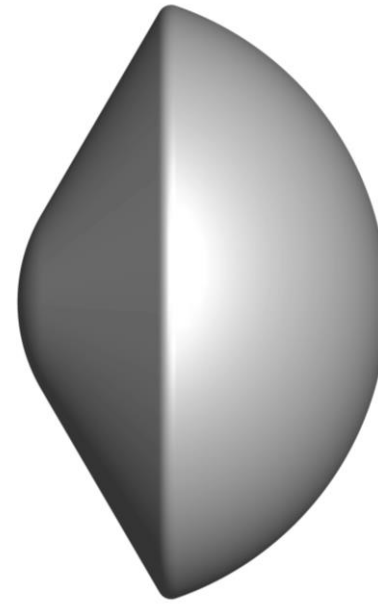
- Unsteady wake flow is believed to be a key contributor to vehicle dynamic instability
- Leveraging the Free-Flight CFD (FFCFD) capability within US3D, the goal is to perform 1 Degree of Freedom (DoF) simulations of the Genesis geometry for;
  - Mach and initial pitch amplitudes
  - Several aftbody outer mold line (OML) shapes



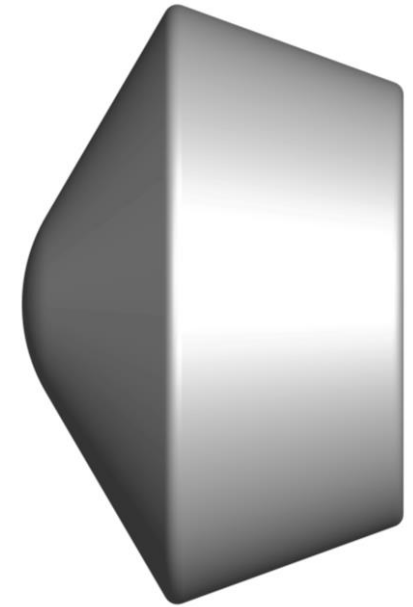
<sup>2</sup>Cheatwood et al. 2000



BS1



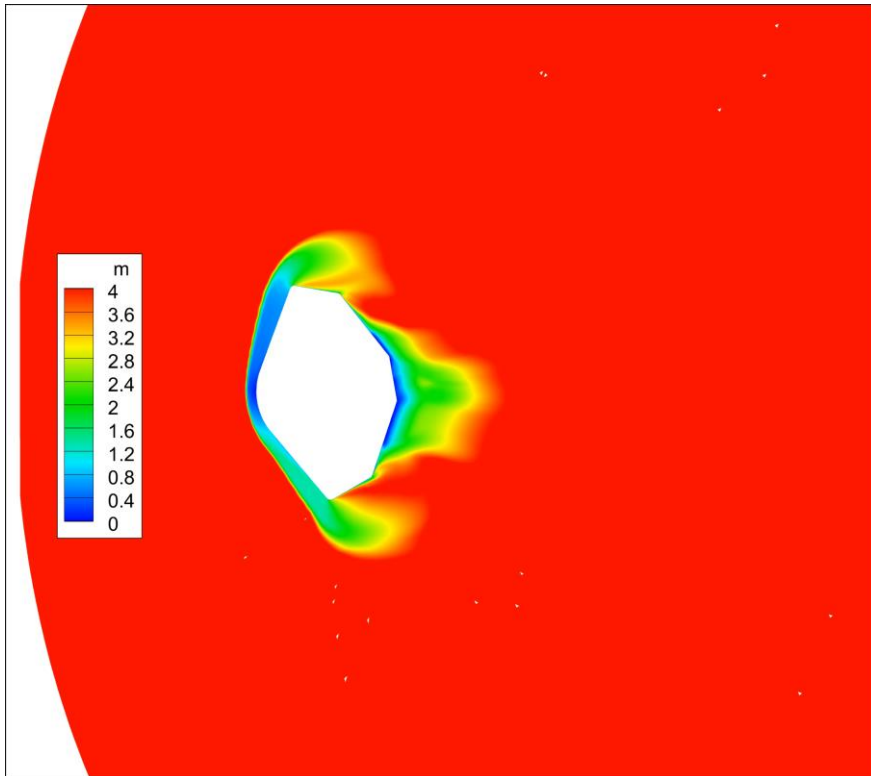
BS2



BS3

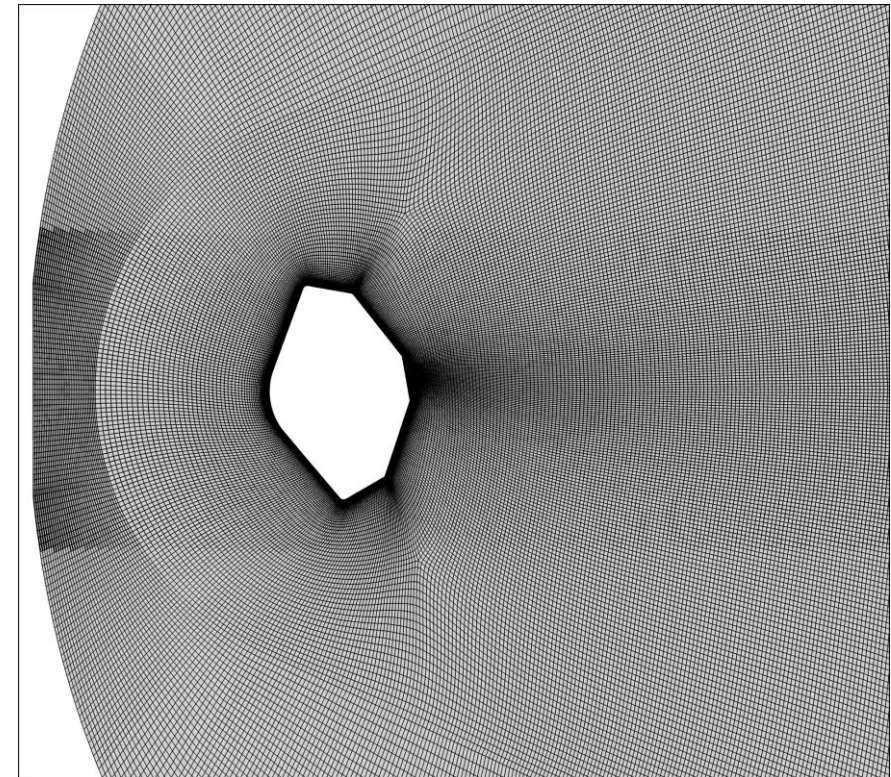
## Free-flight Solver Loop:

- US3D computes the forces and moments
- Moments are integrated to obtain rigid body rotation
- Rigid body dynamics determine the grid deformation
- Lift and drag are integrated to determine frame velocity



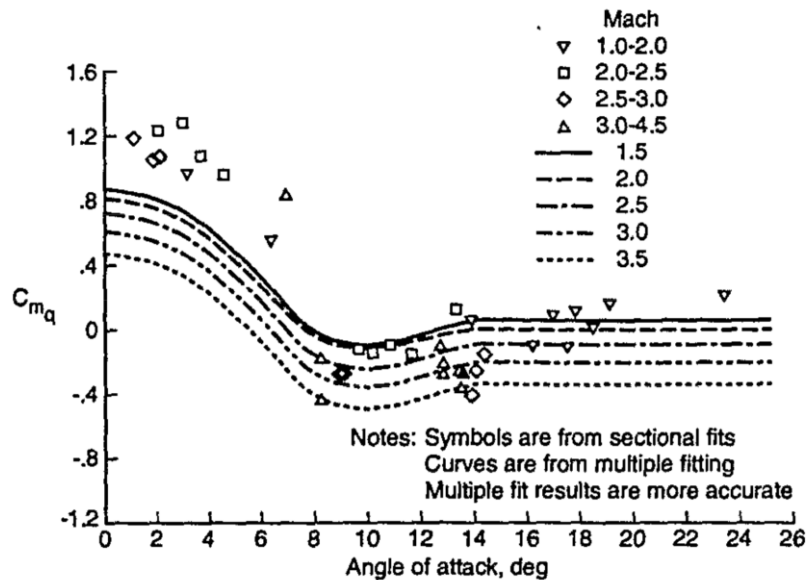
## Mesh Deformation:

- Inner region rotates in response to moments imparted to the aftbody
- Intermediate region linearly interpolates node displacements between the inner and outer regions
- Outer region remains static

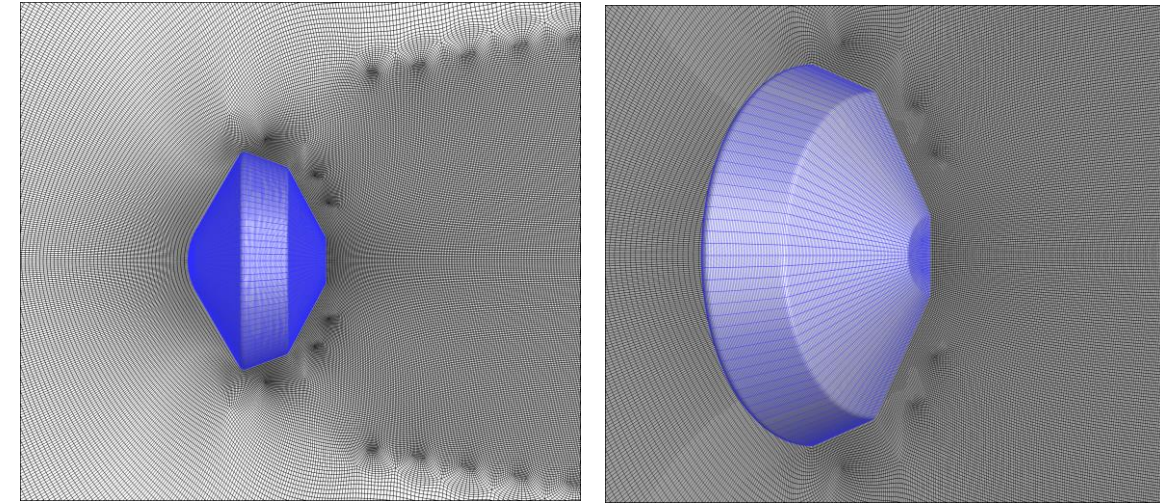


# Simulation Parameters

- Reduce the number of effective parameters on free-flight dynamics
  - Initial position, velocity, and rotation rates set to zero
  - 1 DoF – rotation about z-axis
- **4 cases for each configuration:**
  - Initial attitudes of 2° and 15°
  - Freestream Mach number of 1.5 and 2.5
  - Simulation at least 5 periods in pitch oscillations
    - To provide a large enough data set to observe dynamic stability behavior



<sup>2</sup>Cheatwood et al. 2000



7.1 million elements (clustering not shown)

## Flow Conditions (subscale)

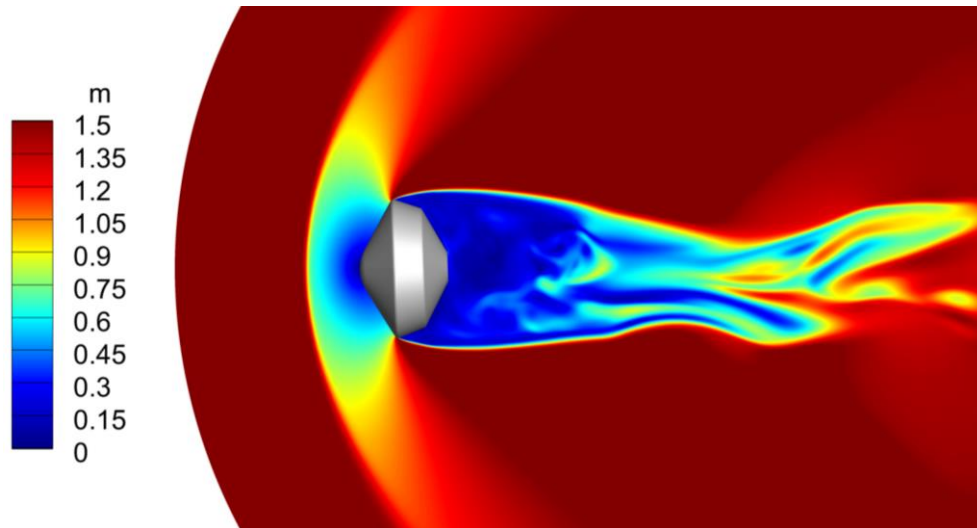
| $M_\infty$ | $U_\infty$ (m/s) | $\rho_{\infty}$ (kg/m <sup>3</sup> ) | $T_\infty$ (K) |
|------------|------------------|--------------------------------------|----------------|
| 1.5        | 514.6            | 1.2149                               | 292.94         |
| 2.5        | 857.6            | 1.2149                               | 292.94         |

- Modified Steger-Warming flux evaluation scheme
- Time integration uses 2<sup>nd</sup> Order Implicit Euler
- Detached eddy simulation
  - Subscale grid modeled using the Spalart-Allmaras<sup>3</sup> turbulence model
- 1000 cores, Walltime ~41.3 hrs, physical time ~0.3 sec

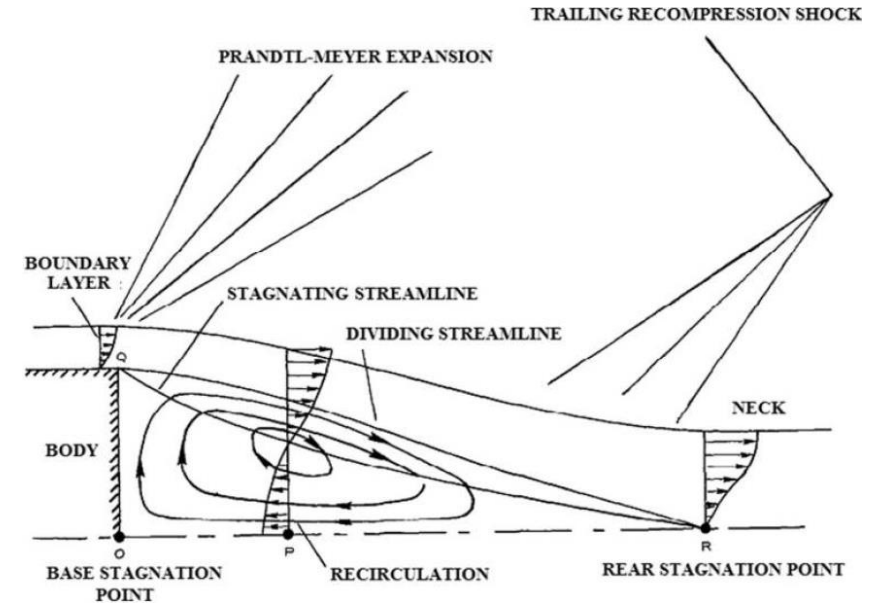
<sup>3</sup>Spalart & Allmaras 1992

8/28/2020

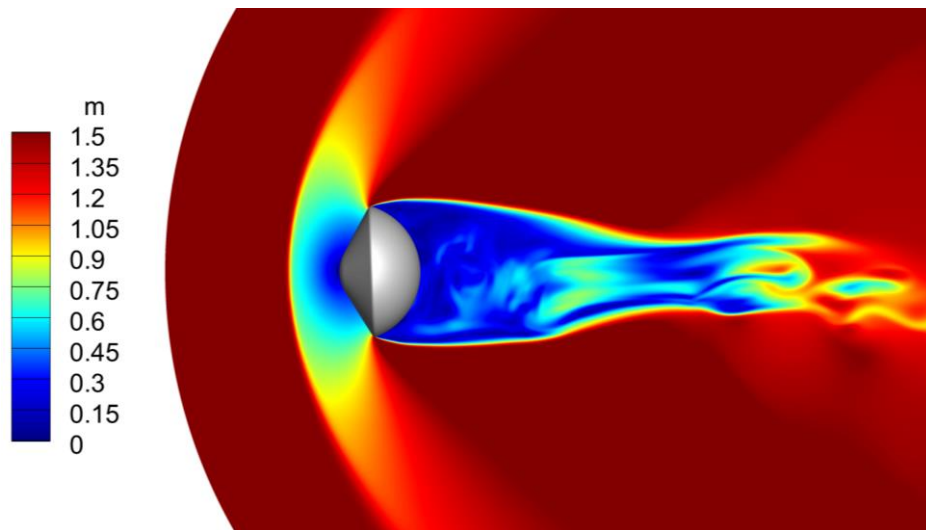
# Wake Structures



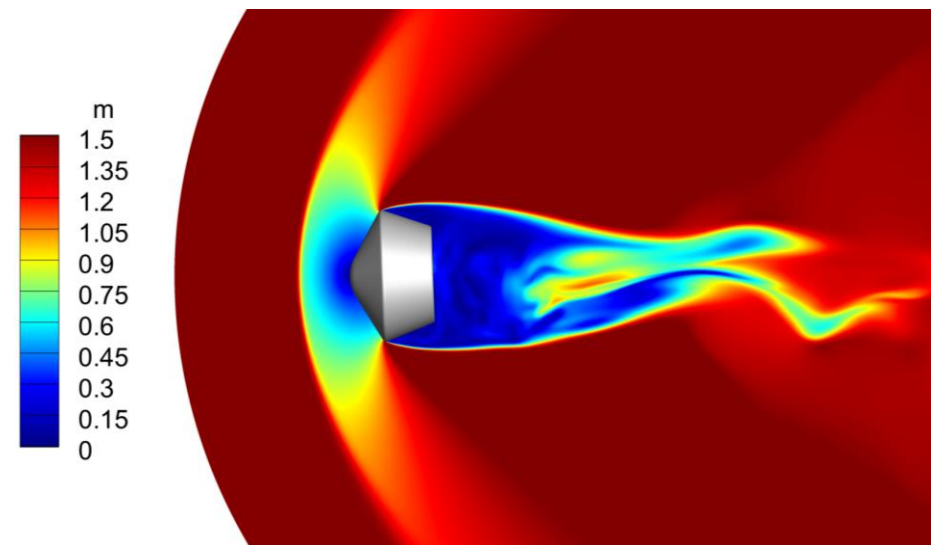
BS1:  $M=1.5$ ,  $\theta=2^\circ$



<sup>4</sup>Jaremenko et al. 1967



BS2:  $M=1.5$ ,  $\theta=2^\circ$

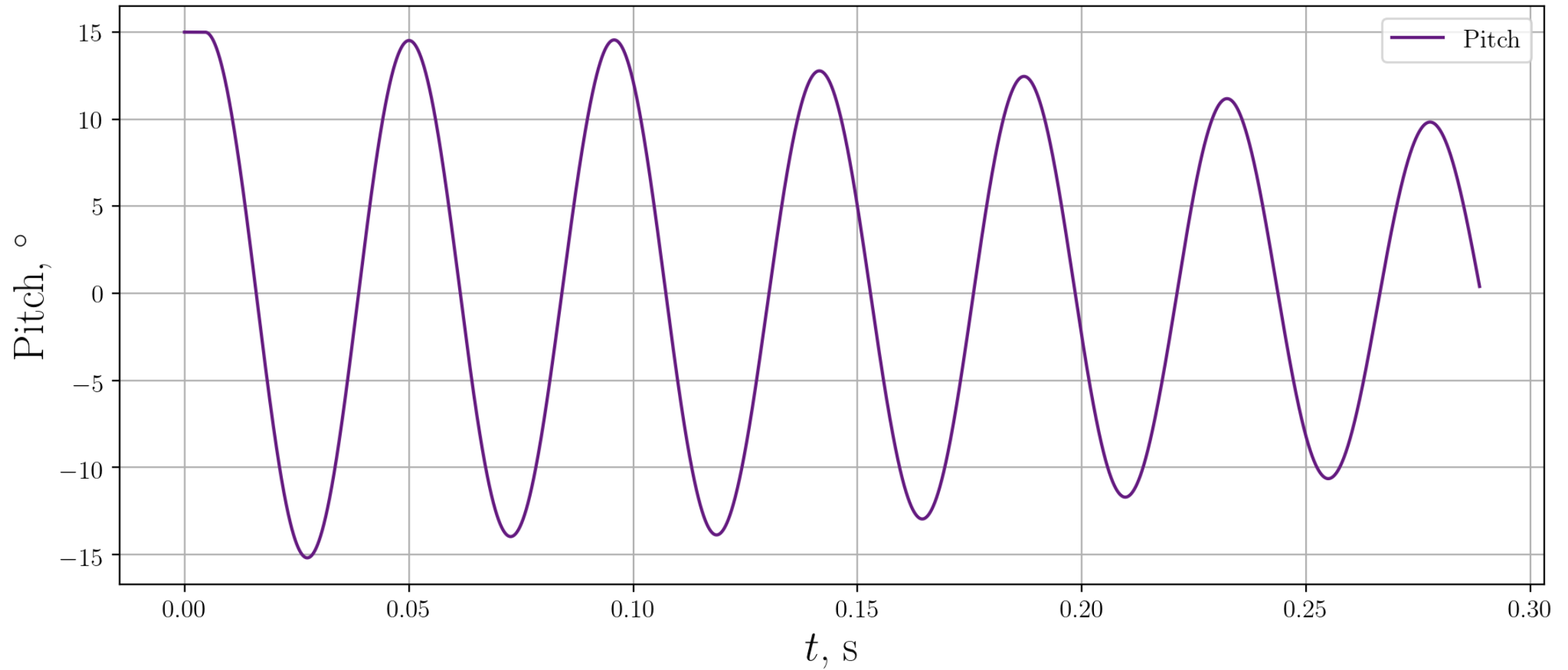


BS3:  $M=1.5$ ,  $\theta=2^\circ$

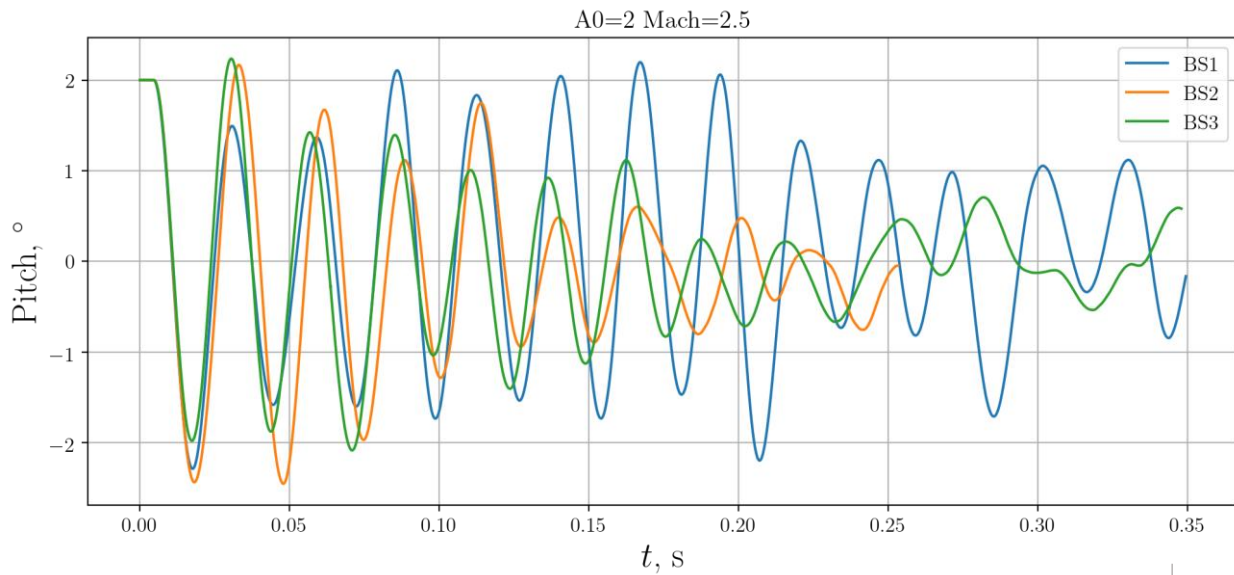
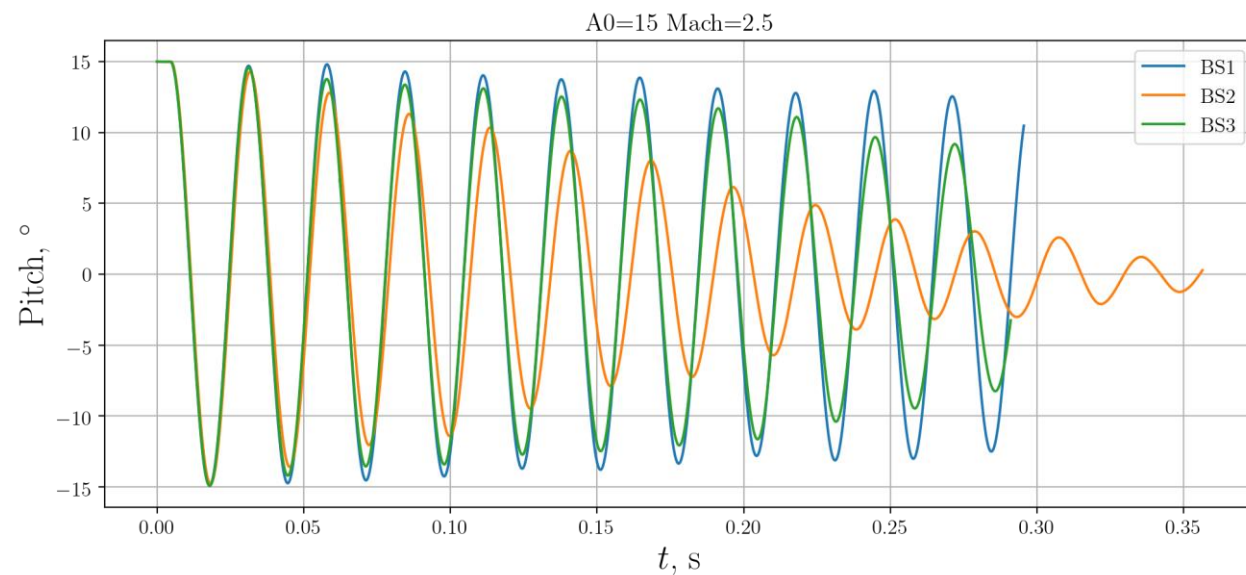
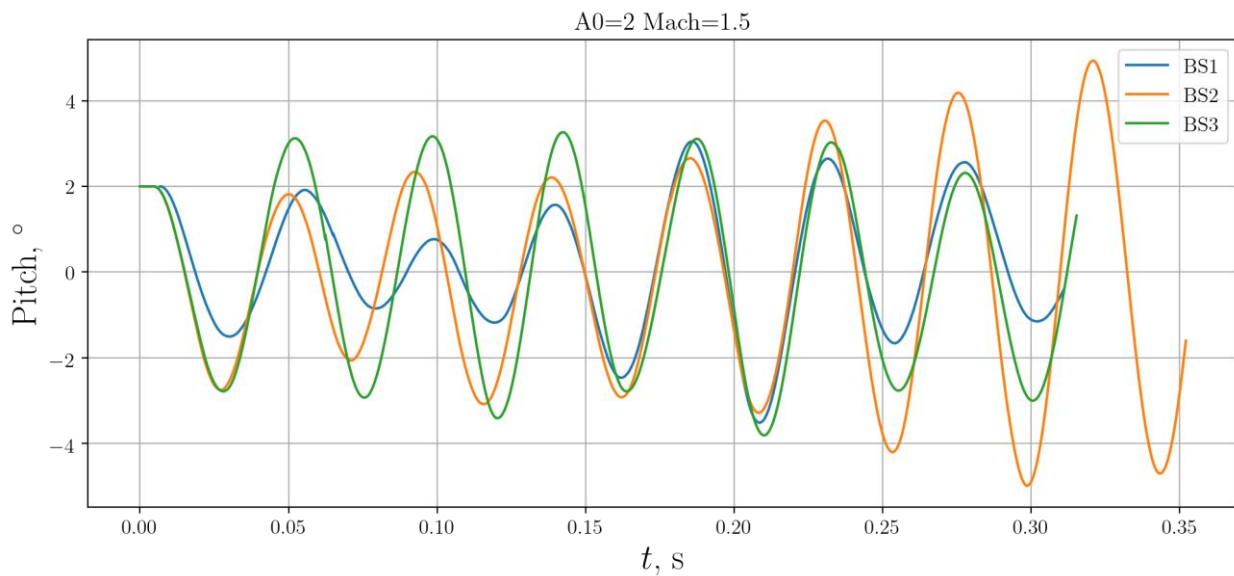
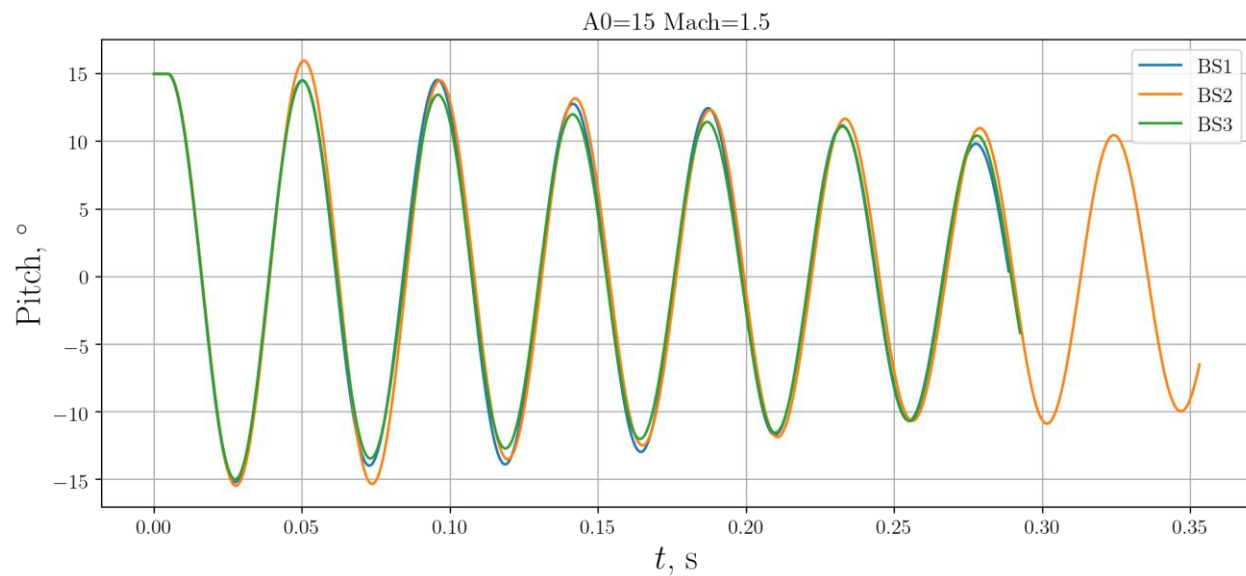
# FFCFD Dynamic Data



BS1 A0=15 Mach=1.5



# Pitch vs. Time



# Pitch Damping Coefficient ( $C_{mq} + C_{m\dot{\alpha}}$ )

- Simplified relevant EOM based off Schoenenberger & Queen<sup>5</sup> 2008
  - Assuming constant velocity, free-to-Oscillate, no-heave:

$$\ddot{\alpha} - \frac{\rho V_{\infty} S d^2}{4I} (C_{mq} + C_{m\dot{\alpha}}) \dot{\alpha} - \frac{\rho V_{\infty}^2 S d}{2I} C_{m\alpha} \alpha = 0$$

- Constant coefficients gives solution for simple harmonic oscillator with damping:

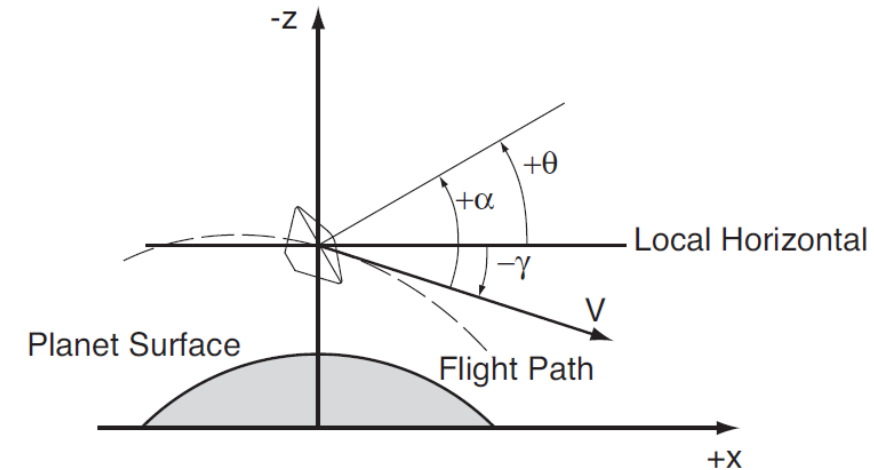
$$\alpha = A e^{\xi_1 t} \cos(\omega t + \delta) \quad \text{where,} \quad \xi_1 = \frac{\rho V S d^2}{8I} (C_{mq} + C_{m\dot{\alpha}})$$

Initial pitch amplitude

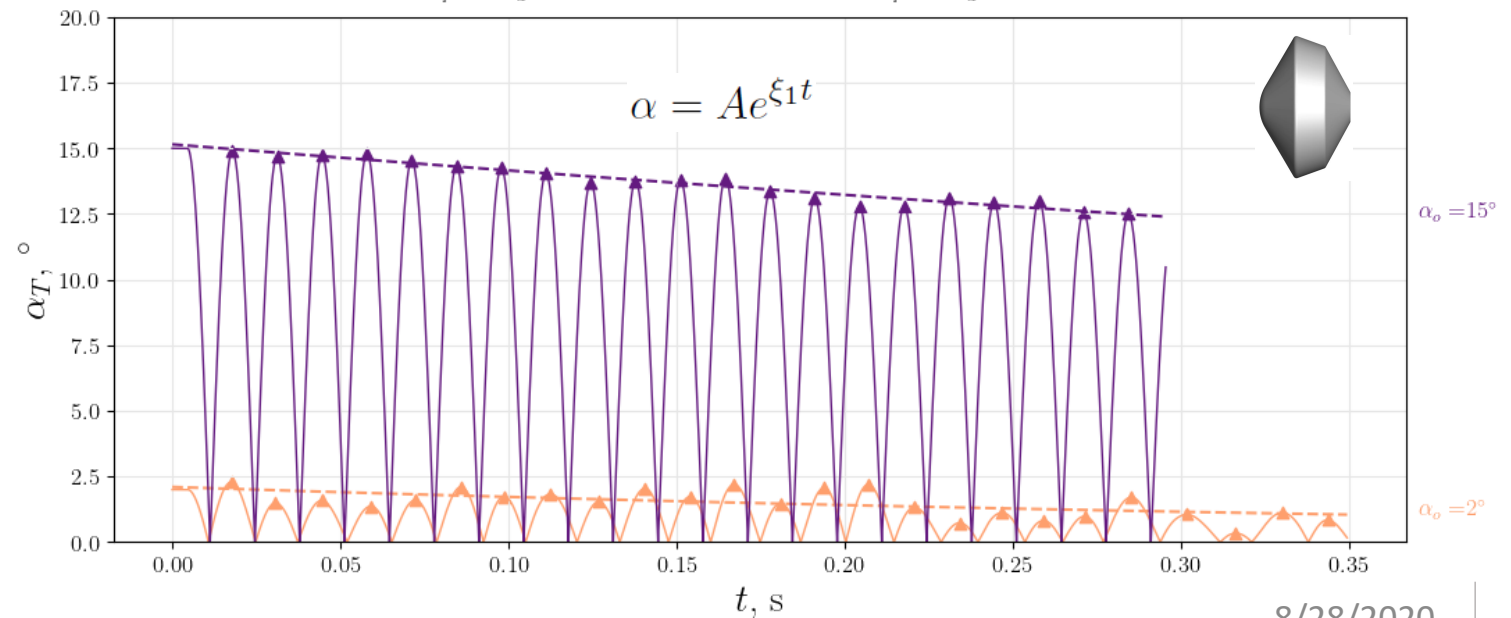
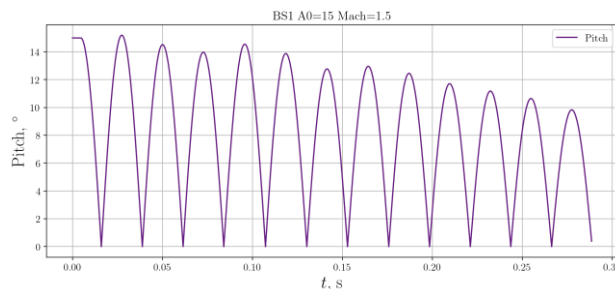
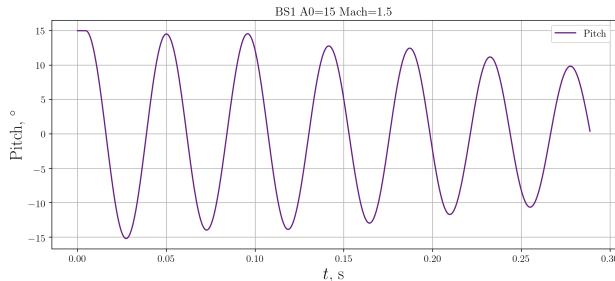
Oscillation frequency

Phase shift constant

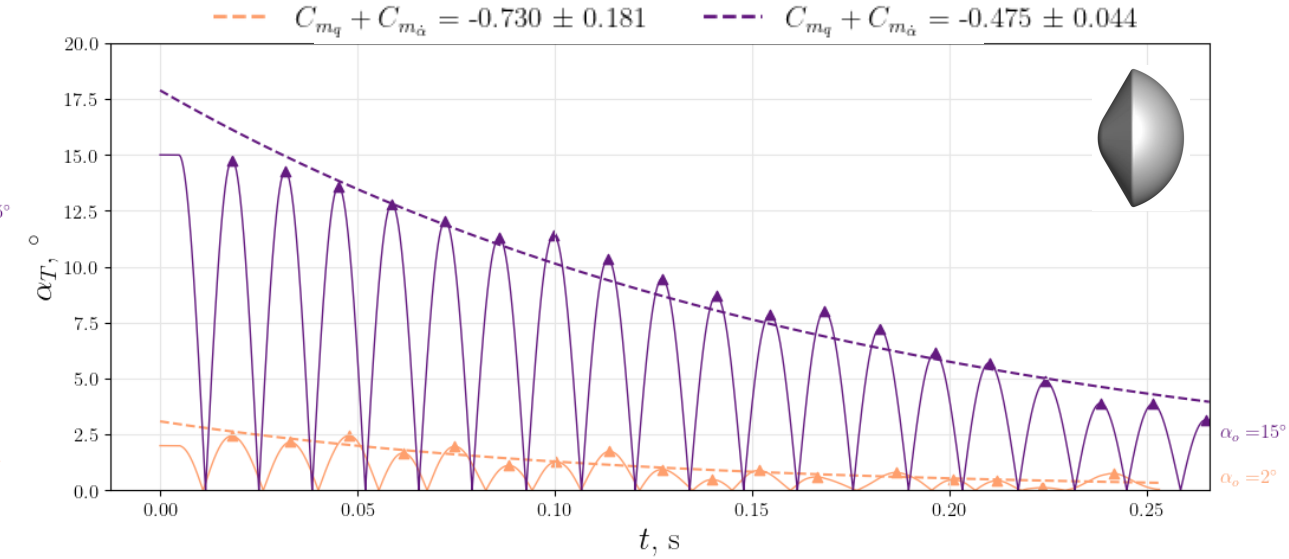
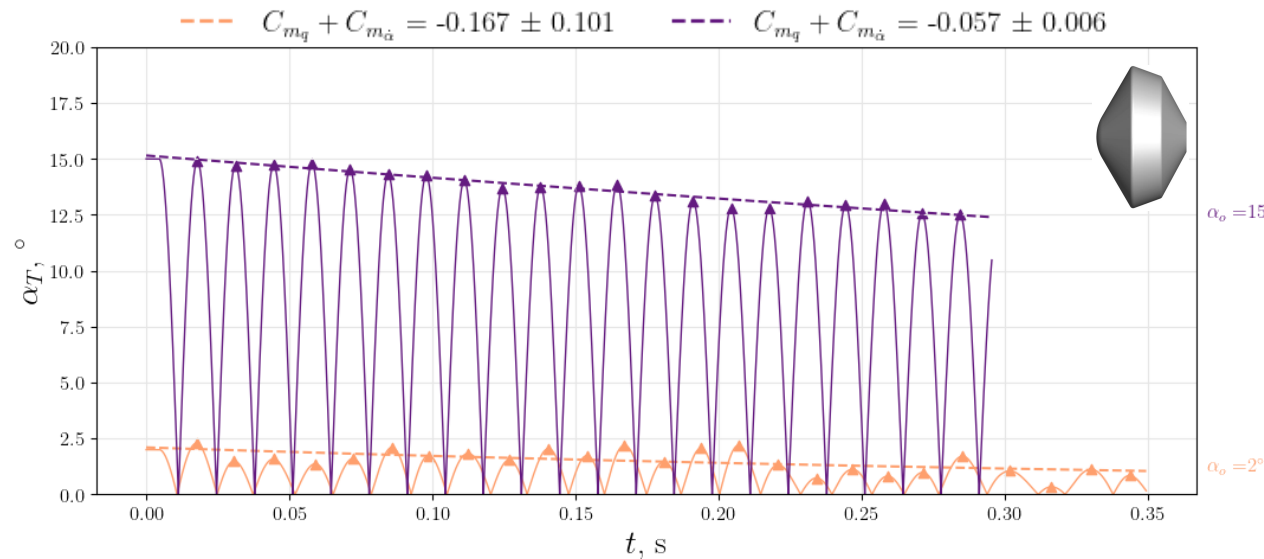
Constant velocity damping coefficient



$$C_{mq} + C_{m\dot{\alpha}} = -0.167 \pm 0.101 \quad C_{mq} + C_{m\dot{\alpha}} = -0.057 \pm 0.006$$

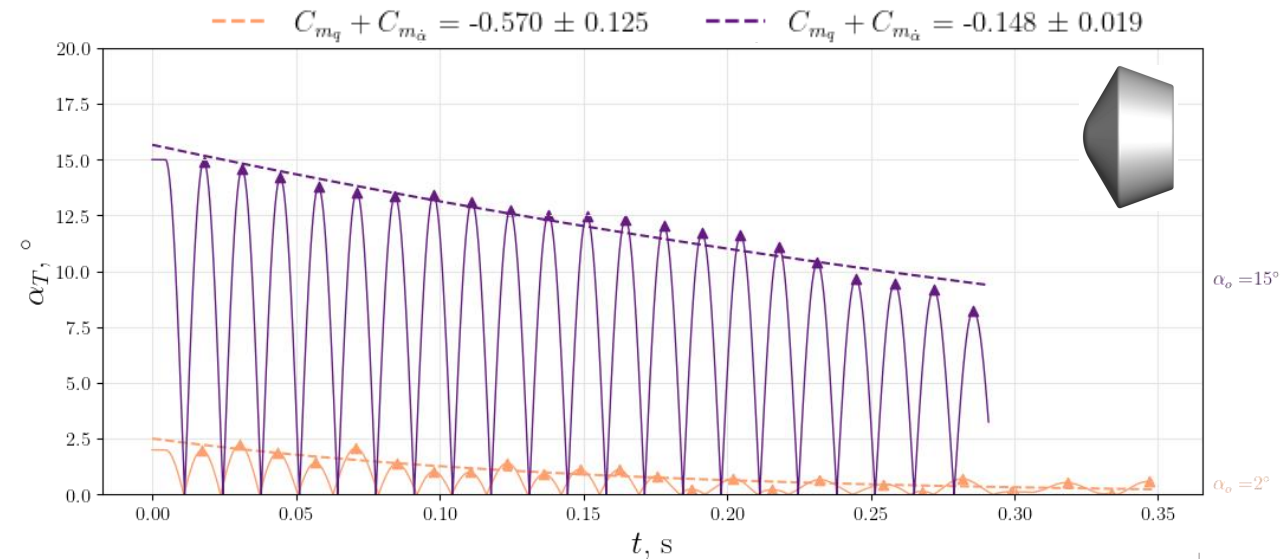


# Pitch Damping Coefficient Mach 2.5

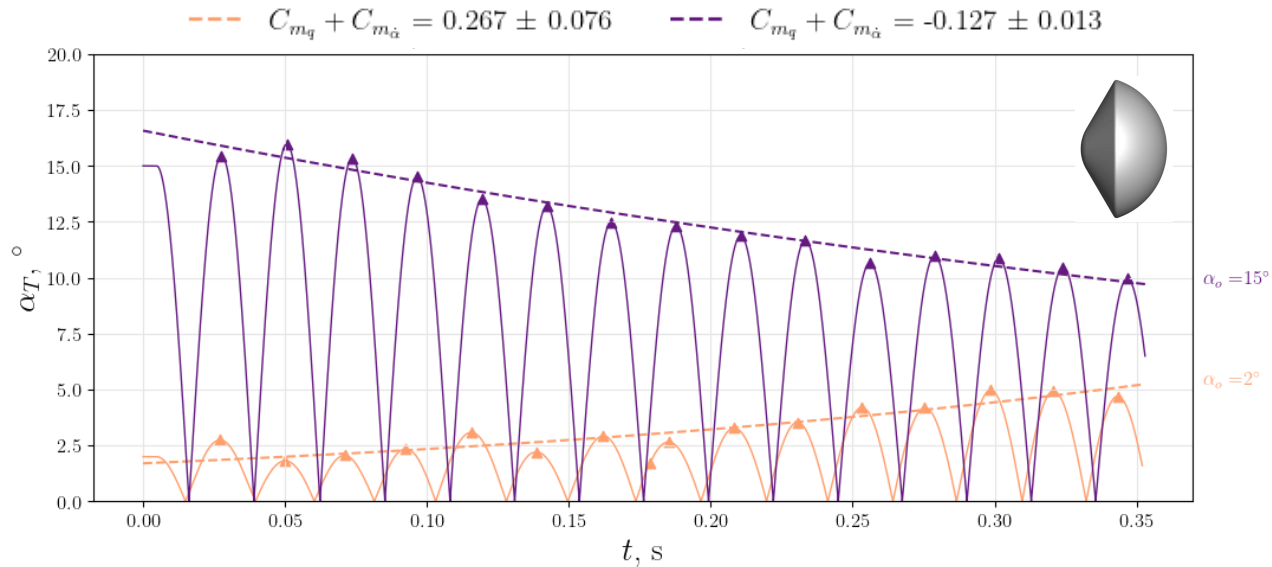
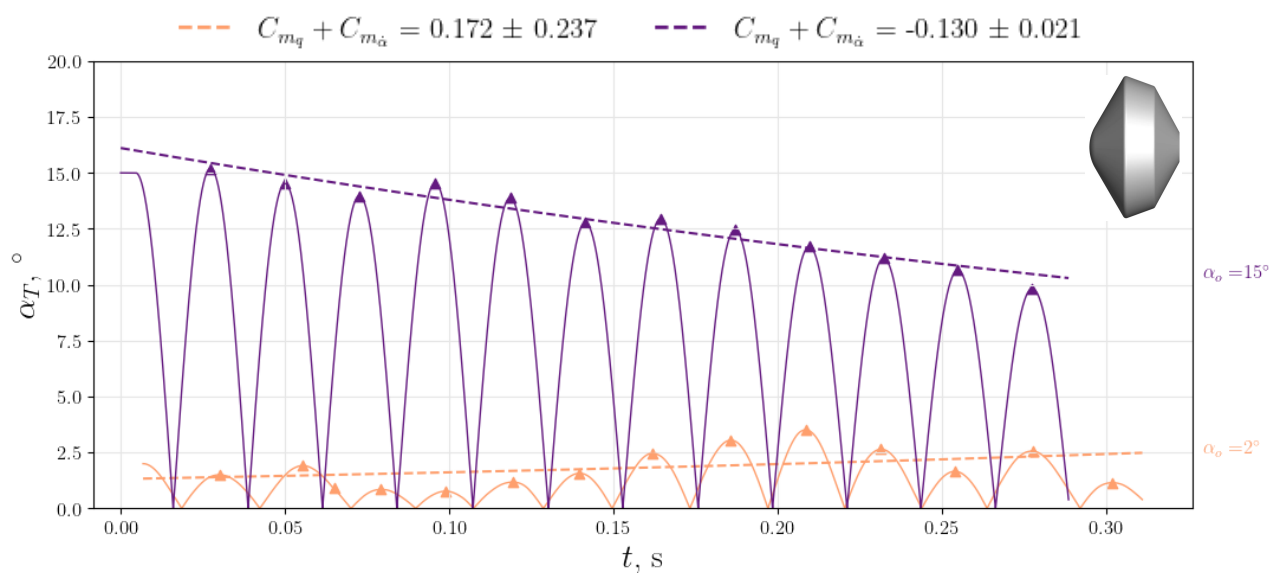
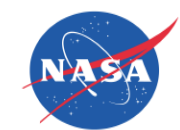


## Dynamic stability summary:

- Pitch oscillations decay for all cases
- Pitch damping (in descending order)
- $15^\circ$  cases – BS2, BS3, BS1
  - $2^\circ$  cases – BS2, BS3, BS1



# Pitch Damping Coefficient Mach 1.5



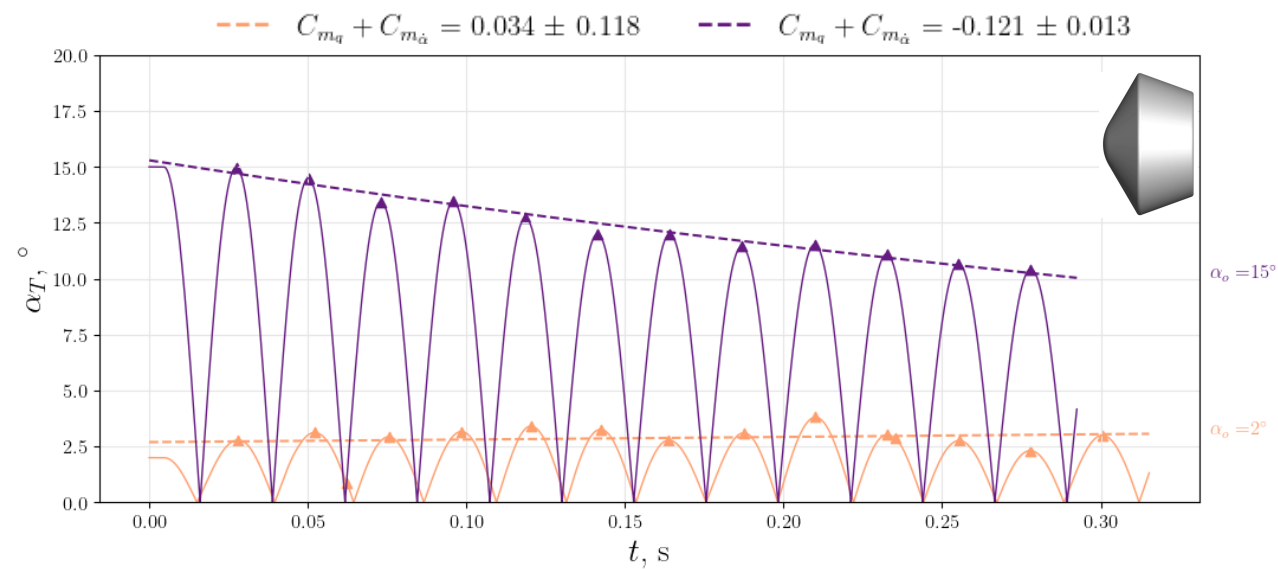
## Dynamic stability summary

Pitch oscillation damping (BS1 more damping)

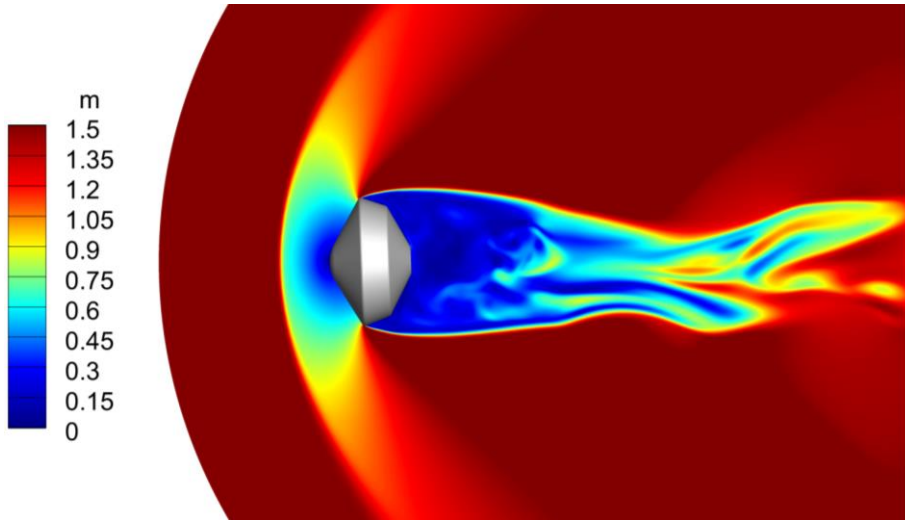
- $15^\circ$  cases – BS1, BS2, BS3

Pitch oscillation growth (BS2 more growth)

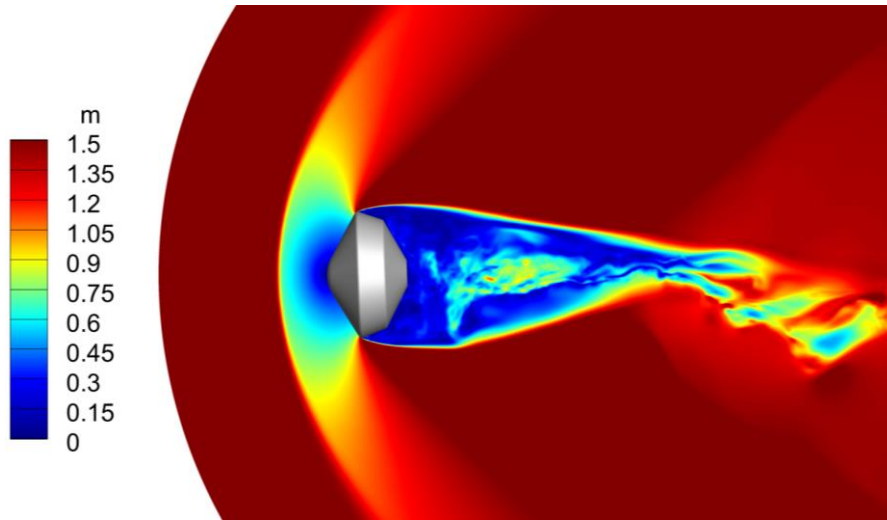
- $2^\circ$  cases – BS2, BS1, BS3



# Low dissipation flux evaluation

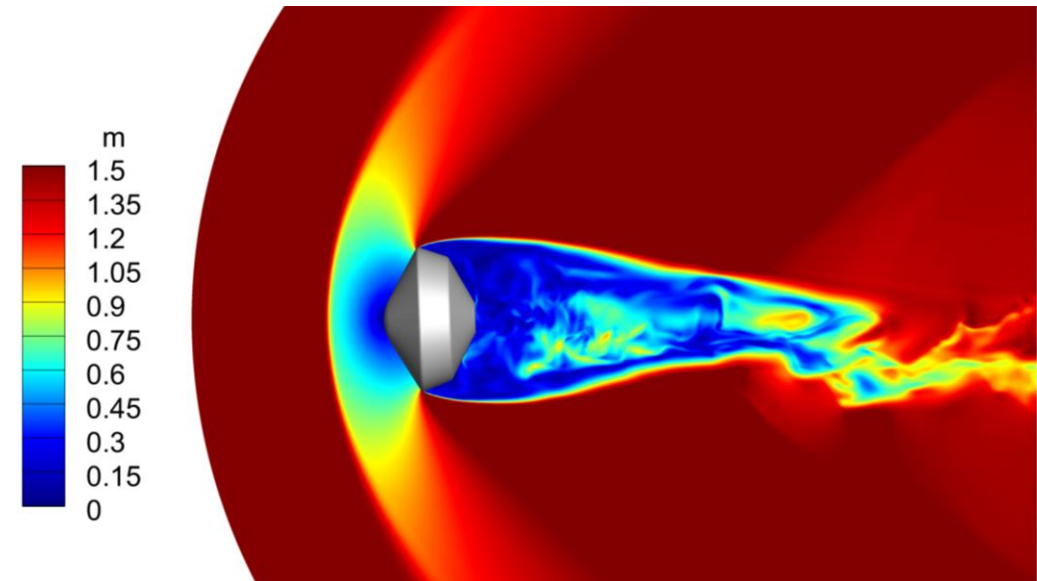


BS1(MSW):  $M=1.5$ ,  $\theta=2^\circ$



BS1(2<sup>nd</sup> Order KEC, Ducros Sensor):  $M=1.5$ ,  $\theta=2^\circ$

- 2<sup>nd</sup> Order gradient-based reconstruction<sup>6</sup> (KEC)
  - Larsson<sup>7</sup> sensor vs. modified Ducros<sup>8</sup> sensor
  - Computational cost comparison using 1000 cores:
    - MSW - 6710 cpu hours
    - KEC - 7550 cpu hours
    - Results in an 12.5% increase in computational cost

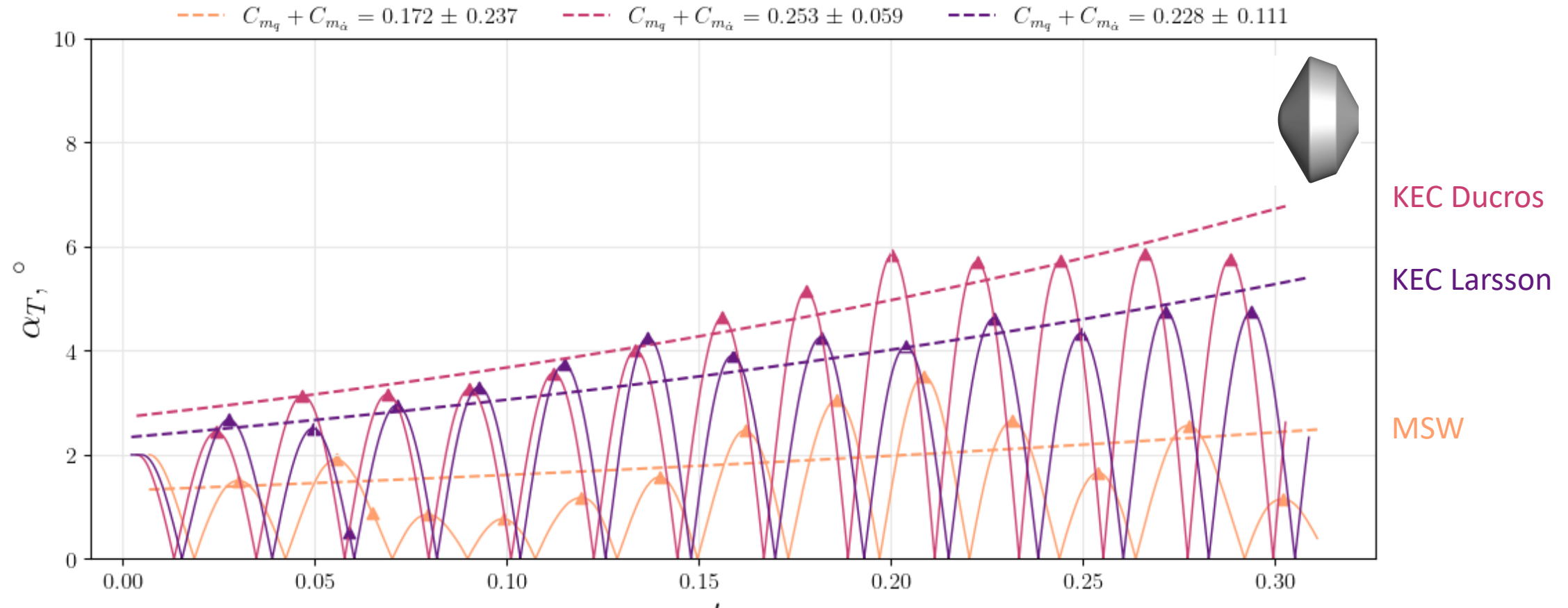


BS1(2<sup>nd</sup> Order KEC, Larsson Sensor):  $M=1.5$ ,  $\theta=2^\circ$

<sup>6</sup>Subbareddy et al. 2014, <sup>7</sup>Larsson et al. 2012, <sup>8</sup>Hendrickson et al. 2018

# Pitch Damping Comparison: MSW vs. KEC

Mach 1.5,  $A_0=2^\circ$  for BS1:



Suggestions for future work:

- Quantify resolved frequencies over a variety of test cases
- Vary timestep and grid resolution
- Make direct comparisons to experiments if possible

- Generated a Mach-Alpha database for 3 different backshell geometries
  - Observed dynamic instability for low initial pitch angles
  - Dynamic behavior remained stable for high pitch angles
  - Mach number saw similar trends but less sensitive than pitch angle
- Analyzed pitch damping for each configuration for 1 DoF
  - Pitch damping for Mach 2.5 at initial pitch of  $2^\circ$  and  $15^\circ$  (BS2 most damped)
  - $M=1.5$ ,  $15^\circ$  - nearly identical dynamic behavior
  - $M=1.5$ ,  $2^\circ$  - unstable regime, pitch oscillation growth for all cases
- Investigated effects of numerical flux schemes on individual results for BS1 at unstable conditions
  - Dynamic behavior is sensitive to the numerics
  - Numerical method becomes increasingly more important than the backshell shape when modeling small-scale features



## Acknowledgements:

Joseph Brock, Dirk Ekelschot, Eric Stern, Jeff Hill, and Brett Cruden

# Questions?