

1 **Effect of ice sheet thickness on formation of the Hiawatha impact crater**

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25

26 **Abstract**

27 The discovery of a large putative impact crater buried beneath Hiawatha Glacier along the  
28 margin of the northwestern Greenland Ice Sheet has reinvigorated interest into the nature of large  
29 impacts into thick ice masses. This circular structure is relatively shallow and exhibits a small  
30 central uplift, whereas a peak-ring morphology is expected. This discrepancy may be due to past  
31 and ongoing subglacial erosion, but may also be explained by an impact through the Greenland  
32 Ice Sheet, which is expected to alter the final crater morphology. Here we model crater formation  
33 using hydrocode simulations, varying pre-impact ice thickness and impactor composition over  
34 crystalline target rock. We find that an ice-sheet thickness of 1.5 or 2 km results in a crater  
35 morphology that is consistent with the present morphology of this structure. Further, an ice sheet  
36 that thick substantially inhibits ejection of rocky material, which might explain the absence of  
37 rocky ejecta in existing Greenland deep ice cores if the impact occurred during the late  
38 Pleistocene. We conclude that the present morphology of the putative Hiawatha impact crater is  
39 plausibly explained by formation through locally thick ice after the Pleistocene inception of the  
40 Greenland Ice Sheet.

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46 **Keywords:** impacts, craters, ice sheets

47 **1. Introduction**

48 Recently, a putative impact crater with the diameter of  $31.1 \pm 0.3$  km was discovered beneath the  
49 Hiawatha Glacier in northwestern Greenland (Fig. 1) (Kjær et al., 2018). The analysis of the  
50 glaciofluvial sediment samples collected from the river draining the structure shows the presence  
51 of shocked quartz, a marker indicative of meteoritic impact. Further, elevated concentrations of  
52 platinum-group elements (PGE) were found in the samples containing shocked quartz, and Kjær  
53 et al. (2018) further asserted that the putative impact crater may have been formed by a fairly  
54 rare iron asteroid. The size of the crater suggests that its formation likely caused significant  
55 regional – and perhaps even global – environmental perturbations (Toon et al., 1997; Erickson et  
56 al., 2020). As per scaling laws (Johnson et al., 2016b), to form a 31 km in diameter impact  
57 structure, an iron asteroid impacting at  $17 \text{ km s}^{-1}$  at an incidence angle of  $45^\circ$  would have to be  
58 nearly 2 km wide (Collins et al., 2004). The probability of an asteroid of that size hitting Earth is  
59 low but non-negligible, occurring once every  $\sim 2$  million years (Silber et al., 2018).

60

61 One of the major questions concerning the Hiawatha structure is its age. Although material  
62 suitable for radiometric dating has not yet been found and analyzed, radiostratigraphic and  
63 geomorphologic evidence suggest that the structure is unlikely to have formed prior to the  
64 Pleistocene inception of the Greenland Ice Sheet (Kjær et al., 2018). This tentative conclusion  
65 was further supported by identification of impact-heated Early Pleistocene conifer wood  
66 fragments from Hiawatha glaciofluvial outwash (Garde et al., 2020). So, while the sum of  
67 available evidence is suggestive of a geologically young age, no firm evidence of its age yet  
68 exists.

69

70 Confirmed impact craters generally contain shock-diagnostic materials, such as extensive  
71 fracturing and brecciation, high-pressure minerals, and planar deformation features (PDFs) in  
72 quartz. Younger craters generally exhibit well-defined morphologic features and are less  
73 degraded than older impact structures (French and Koeberl, 2010; Melosh, 1989). For example,  
74 fresh craters feature relatively sharp and raised rims with overturned stratigraphy, and the lack of  
75 disrupted features (French and Koeberl, 2010; Melosh, 1989). Based on these identifiers, the  
76 putative Hiawatha impact structure might be relatively fresh. It has a rim-to-floor depth of  $320 \pm$   
77  $70$  m, and a dissected central uplift that is up to 50 m high and whose peaks are up to  $\sim 8$  km  
78 apart (Kjær et al., 2018). For a subaerial impact (no ice present), simple modeling suggests that a  
79 fresh, 31-km-diameter subaerial crater would display a peak ring (Pike, 1985) and have a rim-to-  
80 floor depth of  $\sim 830$  m (Collins et al., 2005). So, Hiawatha's morphology is muted compared to  
81 that expected for a subaerial impact, and yet it retains fundamental elements of a crater  
82 morphology (Fig. 1). One would also expect an impact of this size would blanket Greenland in  
83 rocky ejecta. If the impact occurred in the late Pleistocene, such ejecta should be easily  
84 identifiable within the six existing deep ice cores that typically record most of Last Glacial  
85 Period (115–11.7 ka) to the present day, including the Bølling-Allerød and the Younger Dryas  
86 (YD) transitions (Kjær et al., 2018). The YD is the millennium-long cold period that followed  
87 the Bølling-Allerød interstadial near the end of the last ice age at  $\sim 12.8$  ka. Although there is a Pt  
88 anomaly of cosmic origin at the Bølling-Allerød/YD boundary in the Greenland Ice Sheet  
89 Project 2 (GISP2) ice core (Petaev et al., 2013), there is no other evidence of rocky ejecta in any  
90 ice cores (Seo et al., 2019) and substantial evidence challenging an impact that time (e.g., Sun et  
91 al., 2020). The presence of ice, however, would affect the morphology and depth of the final  
92 crater, as well as the distribution of rocky ejecta (Senft and Stewart, 2008).

93

94 Here we model several possible scenarios for the formation of the putative Hiawatha impact  
95 crater using the iSALE-2D shock physics code (Collins et al., 2004; Wünnemann et al., 2006).

96 To understand the effect of a pre-impact ice sheet, we investigate how the presence of thick ice  
97 affects the crater morphology and the dynamics and placement of the distal ejecta blanket.

98

## 99 **2. Methods**

100

101 We model the formation of the putative Hiawatha impact crater using the iSALE-2D Eulerian  
102 shock physics code (Collins et al., 2004; Ivanov et al., 1997; Melosh et al., 1992; Wünnemann et  
103 al., 2006), which is based on the SALE (Simplified Arbitrary Lagrangian Eulerian) hydrocode  
104 solution algorithm (Amsden et al., 1980). This hydrocode has been used previously to model  
105 impacts on Earth and other planetary bodies, and its outputs compare well against laboratory  
106 experiments (e.g., Bray et al., 2014; Collins et al., 2002; Rae et al., 2019; Silber and Johnson,  
107 2017).

108

109 Due to the model's axial symmetry, all impacts are assumed to be vertical, with the projectile  
110 striking surface at a velocity ( $v$ ) of  $12 \text{ km s}^{-1}$  (Collins et al., 2004). Because the most probable  
111 impact angle is  $45^\circ$ , the impact velocity we use represents the vertical component of the mean  
112 asteroidal impact velocity of  $17 \text{ km s}^{-1}$  for Earth (Collins et al., 2004). The projectile diameter  
113 needed for an iron impactor to produce a 31-km-wide crater is approximately 1.8 km, which we  
114 adopt in this study (Johnson et al., 2016b).

115

116 The rocky target is assumed to be composed of granite (Pirajno et al., 2003), represented by the  
117 ANEOS-derived equation of state (EOS) for granite (Pierazzo et al., 1997). Terrestrial ice sheets  
118 are composed of ice Ih, represented by the Tillotson EOS (Ivanov et al., 2002; Tillotson, 1962).  
119 This approximation is consistent with earlier modeling studies of impacts on icy bodies (Bray et  
120 al., 2014; Cox and Bauer, 2015; Silber and Johnson, 2017). Following Kjær et al. (2018), the  
121 projectile is assumed to be metallic, represented by the ANEOS for iron (Thompson, 1990). The  
122 target surface temperature ( $T$ ) was set to 250 K, and gravity ( $g$ ) to  $9.81 \text{ m s}^{-2}$ . The thermal  
123 gradient ( $dT/dz$ ) of the Earth's crust was set to  $10 \text{ K km}^{-1}$ . The temperature in the ice sheet is  
124 expected to be relatively uniform through much of the ice sheet and increase near the base of the  
125 ice sheet (e.g., Dahl-Jensen et al., 1998). For simplicity, here we assume a spatially uniform ice  
126 sheet temperature ( $T = 250 \text{ K}$ ), which is a sufficient approximation for the purpose of the  
127 problem investigated here. We also tested different uniform englacial temperatures of 240 and  
128 260 K and these changes did not significantly affect our results.

129  
130 Table 1 lists the strength and damage model parameters for the target (ice sheet, rock) and the  
131 projectile (iron). In our models, we included the effect of acoustic fluidization, a mechanism  
132 responsible for controlling the degree to which the target is weakened during the cratering  
133 process. The two model parameters describing the Block Model of acoustic fluidization are the  
134 decay time ( $\gamma_\beta$ ) and the limiting viscosity ( $\gamma_\eta$ ) of the fluidized target (Melosh, 1979), for which  
135 we used  $\gamma_\beta = 300$  and  $\gamma_\eta = 0.015$  (Table 1; Collins, 2014; Rae et al., 2019). We also implemented  
136 the dilatancy model in iSALE-2D using the parameters given by Collins (2014). Finally, the code  
137 also includes the implementation of viscoelastic-plastic ice rheology to account for any viscous  
138 contribution to material deformation (Johnson et al., 2016a).

139

140 We modeled impact scenarios with and without an ice sheet, aiming to evaluate the most likely  
141 conditions that existed at the time the putative Hiawatha impact crater formed. We varied the  
142 pre-impact thickness of the ice sheet ( $t_{ice}$ ) from 0.5 km to 2 km, in increments of 0.5 km. The  
143 reasoning for implementing these scenarios is two-fold. First, we are interested in the degree to  
144 which the final crater morphology, such as the development of the central uplift, is affected by  
145 ice-sheet thickness, or by excluding the ice sheet altogether. Second, we assume that the  
146 presence of an ice sheet could inhibit the ejection of rocky material, and thus we investigate the  
147 placement of distal ejecta to obtain the thickness of this layer. In all our models, we used the  
148 parameters as described earlier in this section and given in Table 1. However, our two modeling  
149 targets (morphology and distal ejecta thickness) require a slightly different setup in terms of grid  
150 size, resolution and simulation period.

151

152 In Section 3.1, we focus on crater morphology using a grid resolution of 18 cells per projectile  
153 radius (CPPR), which corresponds to the cell size of 50 m. This resolution provides sufficient  
154 detail to resolve the final crater morphology while minimizing computational expense. For the  
155 sake of completeness, we also ran a suite of test simulations using a rocky asteroid to investigate  
156 the effect on crater morphology. Assuming the impactor to be of the same composition as the  
157 target rock and applying the scaling laws (Johnson et al., 2016b), the projectile diameter needed  
158 to obtain a 31 km wide crater is 2.4 km. To maintain the same cell size throughout all models,  
159 the CPPR in these simulations was set to 24.

160

161 In Section 3.2, we evaluate distal ejecta emplacement, because we can make a direct comparison  
162 with observations to constrain the conditions that may have existed when this impact structure  
163 formed. These simulations were performed at 200 CPPR, to optimize tracking of the material  
164 being ejected (e.g., Johnson and Melosh, 2014). Our simulations included the implementation of  
165 Lagrangian tracer particles allocated to track the location of a parcel of material. Using the  
166 velocity of ballistically ejected tracers, we calculate the tracer's ballistic trajectory and assume  
167 emplacement where the trajectory intersects the pre-impact surface. The thickness of ejecta is  
168 estimated by dividing the volume of ejecta in each 10-km-wide (radial) bin by the area of that  
169 bin. Moreover, we ran a suite of simulations, also at 200 CPPR, to evaluate the ejecta  
170 emplacement in the case of a rocky asteroid impacting the surface.

171

172 In Section 3.3, we investigate the production of impact-induced melt. We ran the simulations at  
173 50 CPPR for the iron impactor and 60 CPPR for the rocky impactor. To optimize the  
174 computation time, the simulations were ended after several seconds, as that is the sufficient  
175 length of time for the shock to propagate through the target and cause melting. Taking advantage  
176 of Lagrangian tracer particles, we track ice and rock separately and record the highest shock  
177 pressure ( $P_{\text{shock}}$ ) these materials experience during the impact (Pierazzo et al., 1997). That  
178 information is then used to obtain the total volume of material shocked above the certain  
179 pressure threshold that is required to either partially or fully melt the given material. Following  
180 the work by Pierazzo et al. (1997), the peak pressures required to partially and fully melt and  
181 vaporize ice are as follows: 0.4 GPa (incipient melt), 3 GPa (total melt), 4.5 GPa (incipient  
182 vaporization), and 43 GPa (total vaporization). The peak shock pressures of 46 GPa and 56 GPa,  
183 respectively, are needed to partially and fully melt rock (granite) (Pierazzo et al., 1997). Finally,



184 we also evaluate the volume of target rock that will be subjected to pressures between 10 GPa  
185 and 25 GPa, as PDFs form in this range (French and Koeberl, 2010).

186

### 187 **3. Results and discussion**

188

189 In this section, we describe the effect of ice thickness on crater morphology and distal rocky  
190 ejecta. The final crater diameter produced in all simulations is approximately 31 km, consistent  
191 with the putative Hiawatha impact structure.

192

#### 193 **3.1 Effect of ice thickness on crater morphology**

194 Fig. 2 shows time series of the formation of an impact crater as a result of an iron projectile  
195 striking a 1.5-km-thick ice sheet overlying the rocky target. The time steps shown are  $t = 5, 30,$   
196  $75, 140$  and  $340$  s. Upon impact, a tremendous amount of energy is released by the projectile into  
197 the target, sending a shockwave away from the point of origin. The expanding shockwave and  
198 following rarefaction wave set up an excavation flow, which opens a transient cavity (Fig. 2a,b).  
199 The earliest, fastest ejecta is always composed of near-surface material, in this case ice (Fig. 2a).  
200 The transient crater (Fig. 2b) subsequently collapses due to gravity. Note that at 250 K, ice is  
201 much weaker and deforms more readily than rock. As the crater collapses, a central uplift is  
202 produced and weak ice covered by rocky ejecta collapses into the crater (Fig. 2c). As the central  
203 uplift collapses, it pushes rocky material outward, which would normally produce a peak ring  
204 (Morgan et al., 2016). The outward collapsing rock material is met by inward collapsing weak  
205 ice (Fig. 2d) producing a complex ice–rock mixture where we would normally expect to find a  
206 peak ring (Fig. 2e). The inward collapse of weak ice pushes some rocky material towards the

207 crater center, resulting in the formation of a rocky central peak and a final crater filled with ice  
208 (Fig. 2e). We note that iSALE hydrocode tracks the cratering process only until the final crater is  
209 formed (order of minutes), and it does not address either subsequent subglacial erosion or the  
210 longer-term thermal evolution of the impacted region after the crater is formed.

211

212 Fig. 3 shows the cross-sections of the final impact crater for all five scenarios modeled in this  
213 study: impact into the purely rocky material without the presence of ice (Fig. 3a), and impact into  
214 an ice sheet with thicknesses of 0.5, 1, 1.5, and 2 km (Fig. 3b-e, respectively). Our results show  
215 unambiguously that the morphology of the rocky portion of the resulting final crater is  
216 modulated by the presence and thickness of an ice sheet, a finding also consistent with previous  
217 studies (e.g., Senft and Stewart, 2008). While the final crater diameter in all models is the same,  
218 the overall appearance of the crater rim, the crater wall and the crater floor varies according to  
219 ice-sheet thickness (Fig. 3). The crater rim is most prominent if formed by an impact into rock;  
220 as ice thickness increases, the crater rim becomes less pronounced. This pattern is expected,  
221 because there is less rocky material available to form the rim, and more of the impact energy is  
222 expended into displacing ice. Modeled crater depth is measured from the rim to the deepest part  
223 of the crater interior to the disrupted peak ring. Without an ice sheet, the modeled crater depth is  
224 1050 m. As ice thickness increases (0.5, 1, 1.5 and 2 km), crater depth generally decreases to  
225 850, 550, 300 and 400 m, respectively. Our simulations with 1.5 or 2 km of pre-impact ice are  
226 roughly consistent with the present observed rim-to-floor depth of the putative Hiawatha ( $320 \pm$   
227 70 m; Kjær et al., 2018).

228

229 In addition to their resulting crater depths, our simulations with 1.5 or 2 km of pre-impact ice  
230 thickness result in disrupted peak rings and central uplifts that are qualitatively consistent with  
231 the observed morphology of the putative Hiawatha impact crater. However, in simulations  
232 without ice and with an ice sheet up to 1 km thick, a peak-ring basin is still produced. Thus, the  
233 presence of a thicker ice sheet promotes the formation of central uplift and subdues the peak-ring  
234 that is otherwise expected at this size (e.g., Pike, 1985). In models with an ice sheet 1.5 to 2 km  
235 thick, the rocky portion of the final crater exhibits a central uplift, buried under ice (Fig. 3d,e). A  
236 disrupted peak ring may be more easily eroded than other parts of the crater. In the thinnest ice-  
237 sheet scenario (0.5 km), no ice overlies the final crater (Fig. 3b), and in the 1-km-thick ice-sheet  
238 scenario, the impact structure is only partially covered by ice that moved inward during crater  
239 collapse (Fig. 3c). Note that these models ignore any ice flow into the crater after the model  
240 period (minutes), but which is expected to occur from outside the impact-affected area. Lastly, if  
241 the impactor was composed of rocky material instead of iron, there is no substantial difference in  
242 the final crater morphology across all scenarios. This analysis indicates that the thickness of the  
243 ice sheet significantly influences the morphological expression of the resulting impact structure.

244

245 We note the recent discovery of a possible second – and slightly larger – impact crater beneath  
246 the northwestern Greenland Ice Sheet (MacGregor et al., 2019). This second structure’s diameter  
247 and depth are estimated at 36.5 km and  $160 \pm 100$  m, respectively, so it is more degraded and  
248 likely older than the putative Hiawatha impact crater. However, it appears to possess a more  
249 dispersed and degraded central uplift than the putative Hiawatha impact crater, making it closer  
250 to a nascent peak-ring morphology. Our simulations suggest tentatively that the potential peak-

251 ring morphology of this putative crater is more consistent with formation before the inception of  
252 the Greenland Ice Sheet.

253

### 254 **3.2 Effect of ice thickness on distal rocky ejecta**

255 Early in the cratering process, near-surface material is ejected at high velocity and the earliest  
256 ejecta has the highest velocities (Melosh, 1989, Johnson and Melosh, 2014). The behavior of the  
257 ejecta curtain when the ice sheet is present is best illustrated in Fig. 2a at  $t = 5$  s. At this time, the  
258 earliest fastest ejecta are composed only of ice. Another factor limiting ejection of rocky material  
259 is the large contrast in target properties, with ice and rock responding to shock loading in a  
260 different manner. This assertion is consistent with previous studies that examined the dynamics  
261 of ejecta for impacts into icy layers (Senft and Stewart, 2008). Therefore, we should not expect  
262 to find rock-dominated ejecta far from the impact point.

263

264 The thicknesses of distal ( $>200$  km) rocky ejecta as a function of radial distance from the crater  
265 center for an iron asteroid are shown in Fig. 4a and a rocky asteroid in Fig. 4b, with a particular  
266 focus on the thickness of ejecta at existing deep ice-core sites in Greenland. In Fig. 5, we include  
267 the map of modern Greenland with each panel showing modeled thickness of rocky ejecta  
268 produced by an iron impactor for all five scenarios (no ice, and ice thickness of 0.5, 1, 1.5 and 2  
269 km).

270

271 As radial distance from the crater center increases, ejecta thickness decreases. In addition to  
272 reducing the thickness of rocky ejecta, the ice sheet limits the distance that rocky ejecta travel  
273 (Fig. 4). For an iron asteroid, the maximum distance that any significant quantity of rocky ejecta

274 ( $\geq 0.01$  mm) travel are 691, 636, 479, and 245 km for pre-impact ice-sheet thicknesses of 0.5, 1,  
275 1.5, and 2 km, respectively. For a rocky asteroid, these distances are 690, 440, 420, and 320 km  
276 for pre-impact ice-sheet thicknesses of 0.5, 1, 1.5, and 2 km, respectively. Note that the larger  
277 rocky impactor produces more distal rocky ejecta than the smaller iron impactor. Beyond the  
278 above distances, all ejecta are composed of ice only. In terms of the projectile, there will be  
279 exactly zero impactor material in the fast ejecta for a vertical impact. As we discuss later, this is  
280 not the case in oblique impacts.

281

282 The deep ice core sites are located at distances ranging from 210 to 1030 km away from  
283 Hiawatha Glacier, and reach depths from just over 1 km to as approximately 3 km, recording ice  
284 as old as the Eemian period (130-115 ka; Dahl-Jensen et al., 2013). The ice-core distances and  
285 core thicknesses are: Camp Century (210 km,  $\sim 1.2$  km) NEEM (378 km,  $\sim 2.5$  km), NorthGRIP  
286 (721 km,  $\sim 3.1$  km), GISP2 (1011 km,  $\sim 2.8$  km), and GRIP (1030 km,  $\sim 1.8$  km). Note that DYE-  
287 3 is not included in this analysis due to its greater distance (1673 km) from Hiawatha Glacier. In  
288 all scenarios with pre-impact ice cover, between 0.1 and 10 mm of rocky ejecta is expected at the  
289 closest deep ice core, Camp Century. However, that ice core is also the oldest of the six ice cores  
290 and less intensely studied than the later, more distal ice cores (Dansgaard et al., 1969; Johnsen et  
291 al., 1972; Kjær et al., 2018). At NEEM, the most recent ice core and 378 km away, less than 0.1  
292 mm of rocky ejecta is expected for pre-impact ice-cover scenarios of 1.5 or 2 km. For all other  
293 ice cores, only 1 km of pre-impact ice cover is needed to result in no or negligible rocky ejecta  
294 being deposited at those sites. Note that this assessment ignores the effect of horizontal ice flow,  
295 which leads to the sourcing of each ice core's present ice column from up to tens of kilometers  
296 farther upstream, closer to the central ice sheet (e.g., Dahl-Jensen et al., 2003).

297

298 We also generated a rough estimate on the proximal (<200 km) rocky ejecta blanket thickness  
299 (Fig. 4c,d). Because it is computationally prohibitive to run simulations at a very high resolution  
300 (200 CPPR), we used the ‘normal’ resolution outputs to generate these results. The inward flow  
301 of ice after ejecta emplacement makes a thickness estimate within 100 km of the crater less  
302 useful.

303

304 For several reasons, our model estimates of the thickness of rocky ejecta from the target should  
305 be considered as upper limits. First, oblique impacts into ice sheets are expected to further limit  
306 ejection of rocky material (Stickle and Schultz, 2012). Additionally, a continuous ejecta blanket  
307 is not expected to occur at distances greater than about one crater diameter from the crater rim  
308 (Melosh, 1989). Beyond that distance, ejecta are expected to be thinner and patchier. A related  
309 effect of oblique impacts is the wedge of avoidance, i.e., a wedge-shaped region uprange of the  
310 impact where ejecta is generally absent (Ekholm and Melosh, 2001). The arc of the wedge of  
311 avoidance is related to the impact angle, i.e., as the impact angle decreases, the wedge of  
312 avoidance increases. For example, a projectile entering the obliquely at 20° and 40° produces the  
313 wedge of avoidance with the angular size of 45° and 115°, respectively (Ekholm and Melosh,  
314 2001). Therefore, depending on the angle and direction of impact, the wedge of avoidance could  
315 be so large that the ejecta would be absent at the ice-core sites for a yet-thinner ice sheet than  
316 that implied by our vertical-impact modeling.

317

318 Another possible source of rocky ejecta is the impactor, depending on its composition. During an  
319 oblique impact much of the impactor material will be deposited downrange of the impact (e.g.,

320 Pierazzo and Melosh, 2000a). Even for a vertical impact, an impact vapor plume may produce  
321 distal ejecta layers (e.g., Johnson and Melosh, 2012). Accurate models of the distribution of  
322 impactor material would require full 3D simulation with updated EOS that more accurately  
323 account for silicate vaporization (Kraus et al., 2012; Kurosawa et al., 2012). Without knowledge  
324 of the impact direction and full 3D simulation of the impact we cannot estimate the possible  
325 contribution of impactor material. However, to obtain an order-of-magnitude upper limit on how  
326 thick the impactor-originating ejecta could be, we assume that the entire rocky impactor was  
327 distributed as a uniform thickness layer with radial extent equal to the location of the various  
328 drill cores. Under this assumption this layer could be 25.5, 8, 2.2, 1.1, and 1.1 mm for core  
329 distances of 210, 378, 721, 1011, and 1030 km, respectively.

330

331 Considering that ice dominates the fast – and therefore distally emplaced – ejecta, the apparent  
332 absence of rocky ejecta in existing ice cores does not in and of itself rule out the possibility that  
333 the putative Hiawatha impact crater formed during the time period spanned by the ice cores, i.e.,  
334 most of the Last Glacial Period. In other words, based on our modeling, a possible Late  
335 Pleistocene timing for the putative Hiawatha impact crater formation cannot be discounted if it  
336 occurred through a sufficiently thick ice sheet. This result is consistent with the preliminary age  
337 constraints presented by Kjær et al. (2018). The lack of ejecta in ice cores does not necessarily  
338 rule out a Last Glacial Period age, including the YD period, for the impact if the ice sheet was at  
339 least 1.5 km thick there at the time of the impact. However, we note that the ICE-6G model does  
340 not predict ice thicker than ~1 km at Hiawatha Glacier for the past 26 kyr (Stuhne and Peltier,  
341 2015). Our modeling suggests that further investigation of the Camp Century ice core for ejecta

342 or impactor signatures could more robustly rule out a late Pleistocene age for the putative  
343 Hiawatha impact crater.

344

### 345 **3.3 Impact-induced melting**

346 In Table 2, we summarize our results by outlining the peak shock pressures and the impact-  
347 induced melt volumes for both an iron asteroid and a rocky asteroid, separated out by the target  
348 material (ice or rock). Fig. 6 shows the provenance plot of peak shock pressures reached within  
349 the material upon the impact by a 1.8 km wide iron asteroid (Fig. 6a-c), and a 2.4 km wide rocky  
350 asteroid (Fig. 6d-f). The iron asteroid produces greater shock pressures overall compared to its  
351 rocky counterpart, which is expected because of its higher density. In both cases, the peak shock  
352 pressures are more than sufficient to melt or vaporize ice and melt rock, but a sufficiently thick  
353 ice sheet also dissipates shock propagation.

354

355 Unless the impact is very shallow ( $<30^\circ$ ), axisymmetric models can still provide good estimates  
356 for melt production in oblique impacts (Pierazzo and Melosh, 2000b). If the ice sheet was 1.5–2  
357 km thick at the time the putative Hiawatha crater formed, the impact by an iron asteroid would  
358 have melted 106–164 km<sup>3</sup> of ice, comparable to the amount of water in Lake Tahoe, USA. A  
359 rocky extraterrestrial body would produce an even greater volume of melted ice, 141–217 km<sup>3</sup>  
360 (Fig. 7a). Moreover, about 4 km<sup>3</sup> of ice would completely vaporize (Table 2). It should be noted  
361 that our simulations account for impact-induced melting only (i.e., immediately upon the  
362 impact), which means that any post-impact ice melting or water retention due to the presence of  
363 the melt sheet in the rocky target is not accounted for. Therefore, our ice melt estimates represent



364 a lower limit. Future studies should consider the effect of melt sheet on post-impact evolution of  
365 the region, melting of the inflowing ice sheet, and the resulting hydrothermal activity.

366  
367 In terms of rocky target material within a melt sheet produced with an iron impactor, ~32–36  
368 km<sup>3</sup> of rock would be fully melted, regardless of ice thickness (Fig. 7b). In the case of a rocky  
369 asteroid, the rocky melt volume would be lower, but still substantial (~19–28 km<sup>3</sup>; Fig. 7b).  
370 Finally, we determined the volume of rocky target material experiencing peak shock pressures  
371 conducive to the formation of PDFs (Fig. 7c). Up to 990 km<sup>3</sup> (iron asteroid) and 750 km<sup>3</sup> (rocky  
372 asteroid) of target rock could potentially be exposed to  $P_{\text{shock}} > 10$  GPa.

373

#### 374 **4. Conclusions**

375

376 The recent discovery of the putative 31-km-wide Hiawatha impact crater beneath the Greenland  
377 Ice Sheet reinvigorated interest in ice-affected impact processes (Kjær et al., 2018). We used  
378 iSALE-2D shock physics code to model possible formation scenarios for this putative impact  
379 crater and investigate the resulting morphology and the emplacement of distal rocky ejecta to  
380 infer possible conditions at the time of crater formation. The morphology of the simulated crater  
381 is qualitatively consistent with present observations if the ice sheet is 1.5–2 km thick, implying  
382 that the crater could have formed geologically recently if thick ice were present there at the time  
383 of impact (e.g., during a Pleistocene stadial). We also find that the presence of an ice sheet  
384 inhibits ejection of rocky material and that no rocky ejecta should be expected at distances  
385 exceeding 245 km for a 2-km-thick ice sheet. Thus, ignoring subsequent erosion, our results are  
386 consistent with the existing hypothesis that the putative Hiawatha impact crater formed after

387 inception of the Greenland Ice Sheet around 2.6 Ma (Bierman et al., 2016). Further, its possible  
388 formation during the Last Glacial Period or at the onset of YD cannot yet clearly be ruled out  
389 based on the lack of rocky ejecta in existing ice cores alone. While future radiometric dating of  
390 this putative crater remains a priority for understanding when and how it formed, our study  
391 directly demonstrates the value of numerical modeling for contextualizing the history of impacts  
392 into ice sheets on Earth and elsewhere in the Solar System.

393

### 394 **Acknowledgements**

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396 code used in this work, including Gareth Collins, Kai Wünnemann, Dirk Elbeshausen, Boris  
397 Ivanov and Jay Melosh. Some plots in this work were created with the pySALEPlot tool written  
398 by Tom Davison. All data associated with this study are listed in tables in the supporting  
399 information and shown in figures. The simulations were performed using iSALE-2D, version  
400 Dellen r-2114. The simulation inputs and model outputs are available on Harvard Dataverse (doi:  
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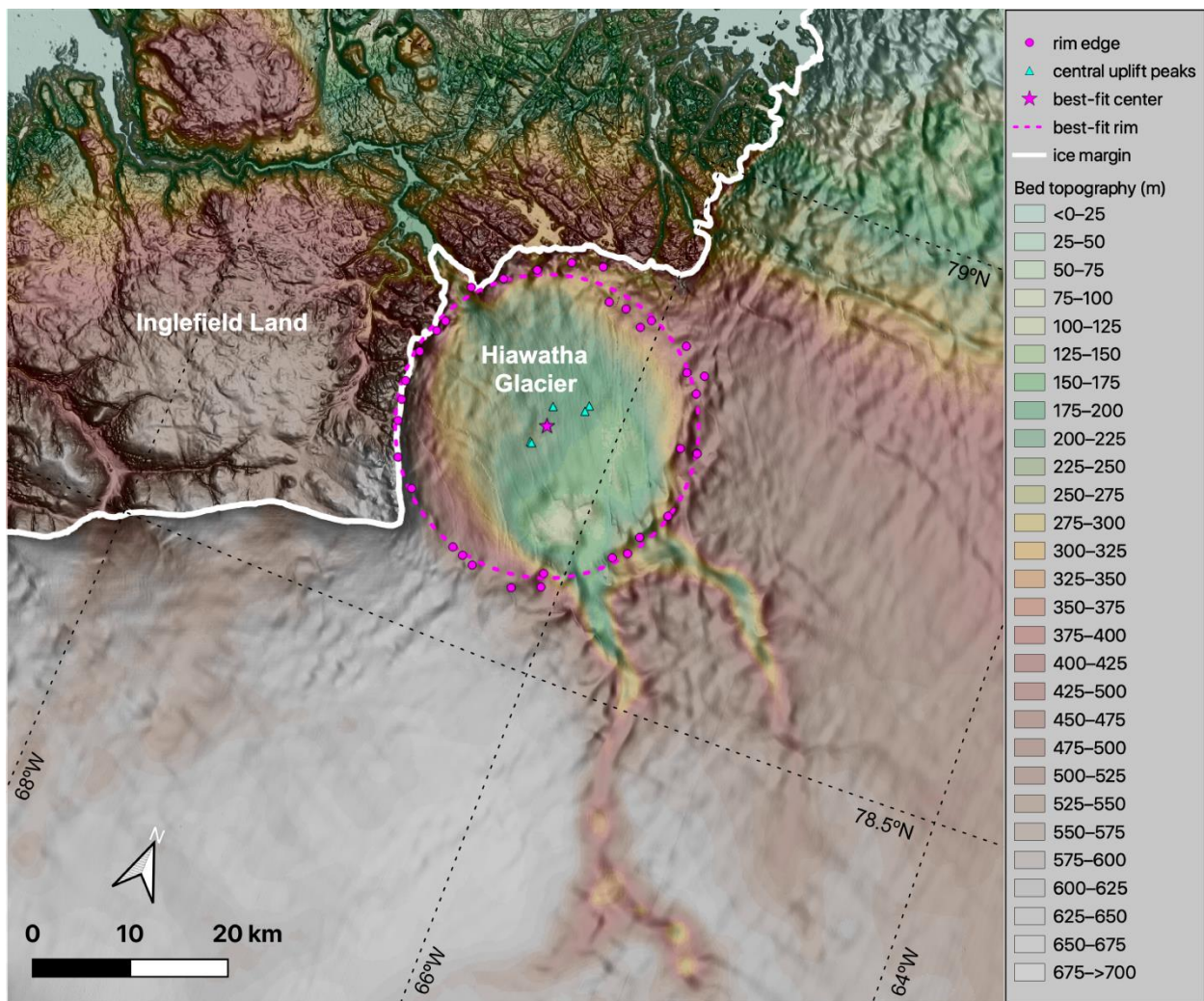
409 *Note, we will archive model results on Harvard Dataverse and provide a doi in the final*  
410 *publication once the manuscript has been accepted for publication.*

411

412 **Competing interests:** The authors declare no competing interests.

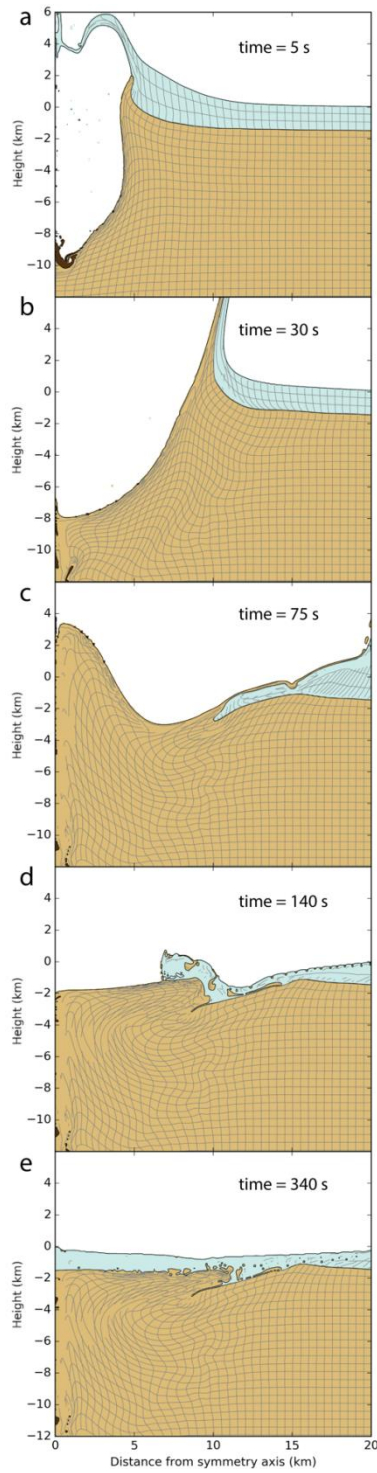
413 **List of Figures**

414 **Figure 1:** Bed topography beneath and in the vicinity of Hiawatha Glacier, northwestern  
415 Greenland (Kjær et al., 2018) overlain on hillshaded surface elevation (10-m ArcticDEM (Digital  
416 Elevation Model) mosaic; Porter et al., 2018). Symbology follows radar-identified features  
417 described by Kjær et al. (2018). Ice margin is from the Greenland Ice Mapping Project (Howat et  
418 al., 2014).



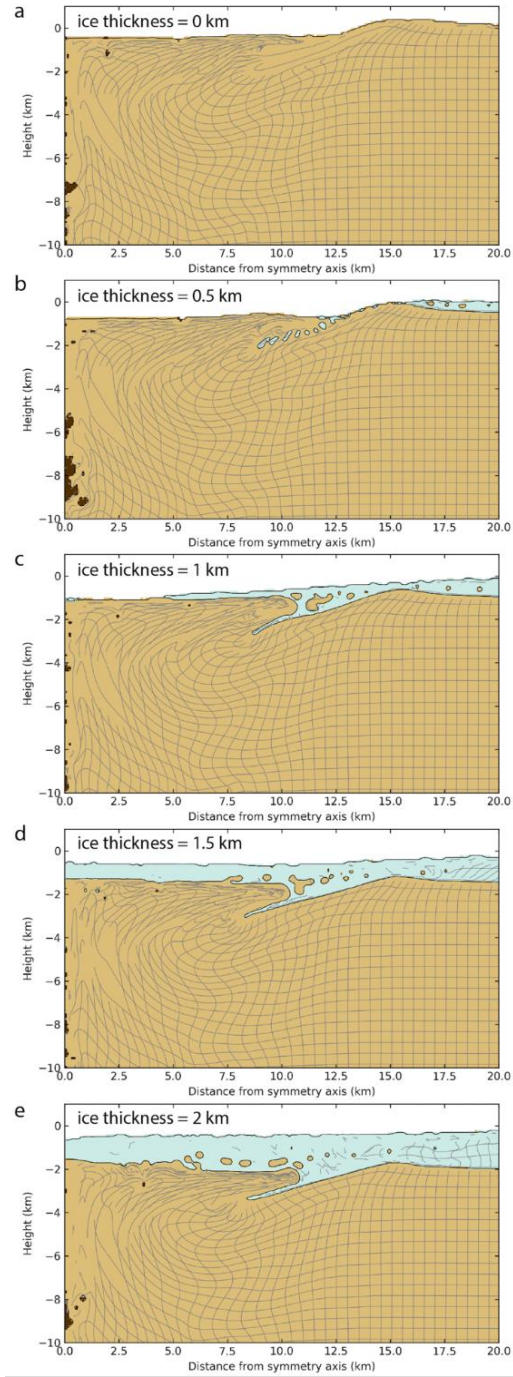
419

420 **Figure 2:** Time series of a modeled impact into a 1.5-km-thick ice sheet. Material is colored  
421 according to material type; dark brown, light brown and blue represent the iron impactor, granitic  
422 crust and ice, respectively. Axis origin marks the point of impact. Originally vertical and  
423 horizontal gray lines connect Lagrangian tracers and track deformation as the impact progresses.



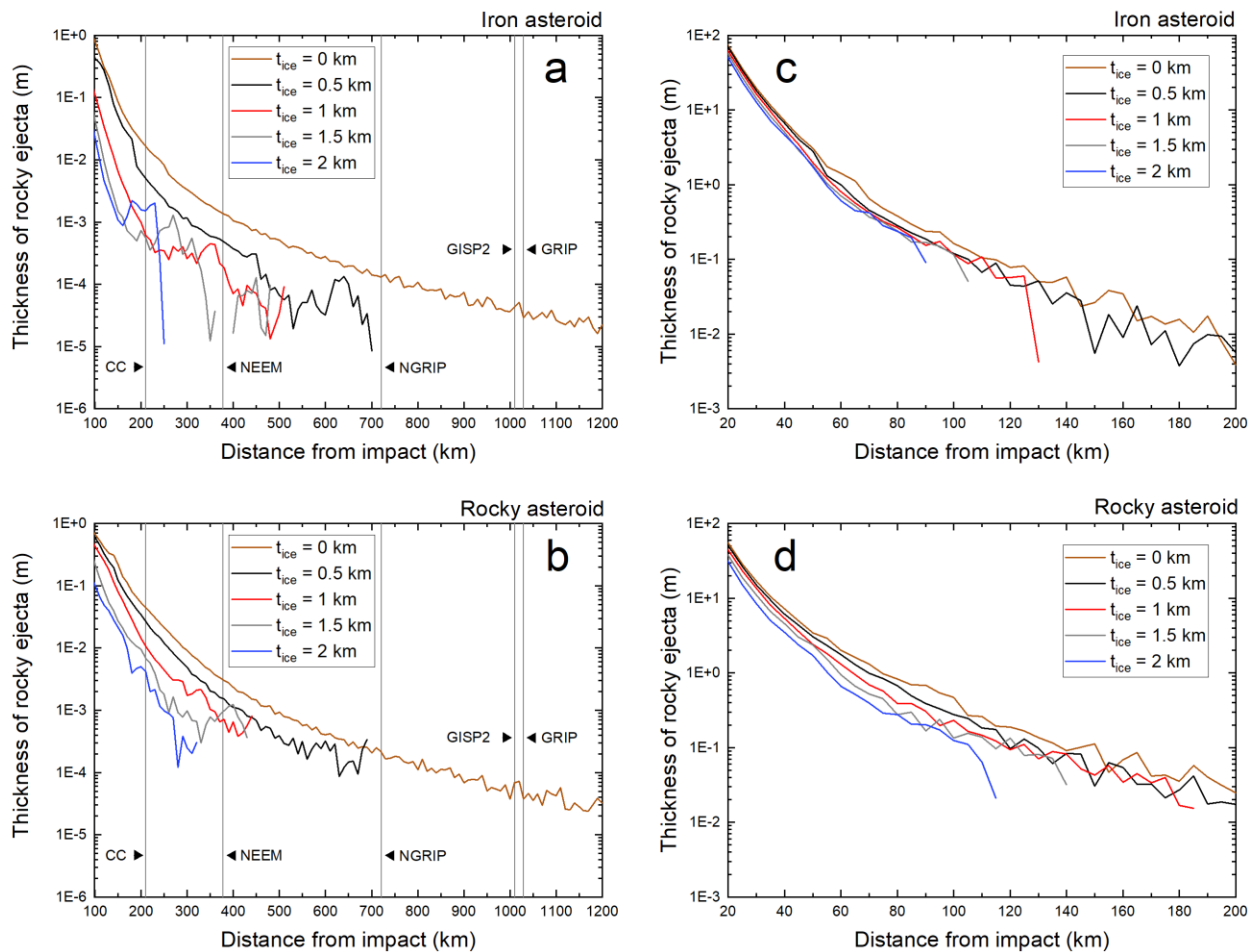
424

425 **Figure 3:** The cross-section of the final crater formed as a result of an impact into (a) a purely  
 426 rocky target (no ice) and (b-e) an ice sheet with varying thickness. In the panels (b-e), top to  
 427 bottom, the ice sheet thicknesses are 0.5, 1, 1.5 and 2 km. Colors and grid scheme follow Fig. 2.





429 **Figure 4:** Thickness of distal rocky ejecta as a function of radial distance from the point of  
 430 impact for (a) an iron and (b) a rocky asteroid. Runs are at 4.5-m resolution (200 CPPR) with  
 431 pre-impact ice thickness indicated in the legend. Vertical lines mark the distance of ice cores  
 432 (DYE-3 is 1673 km away and not included here). The maximum distance that any rocky ejecta  
 433 travel are 691, 636, 479, and 245 km (iron asteroid) and 518, 384, 241, and 276 km (rocky  
 434 asteroid) for pre-impact ice thickness of 0.5, 1, 1.5, and 2 km, respectively. Also is shown  
 435 thickness of proximal ejecta extending up to 200 km for (c) and iron and (d) a rocky asteroid.  
 436 Note that these runs are at 50-m resolution; while these do not capture ejecta in as great detail as  
 437 high resolution runs, they offer a reasonable approximation.

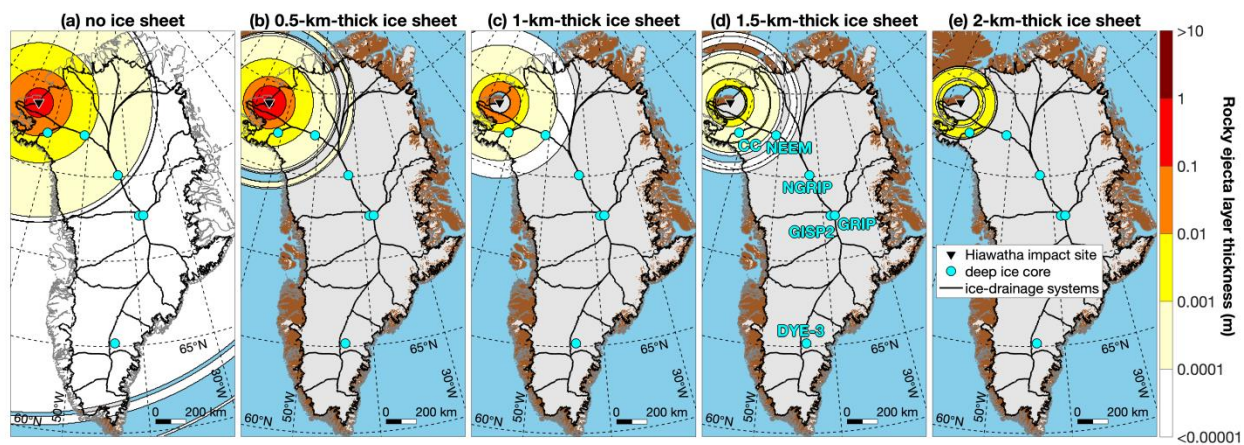


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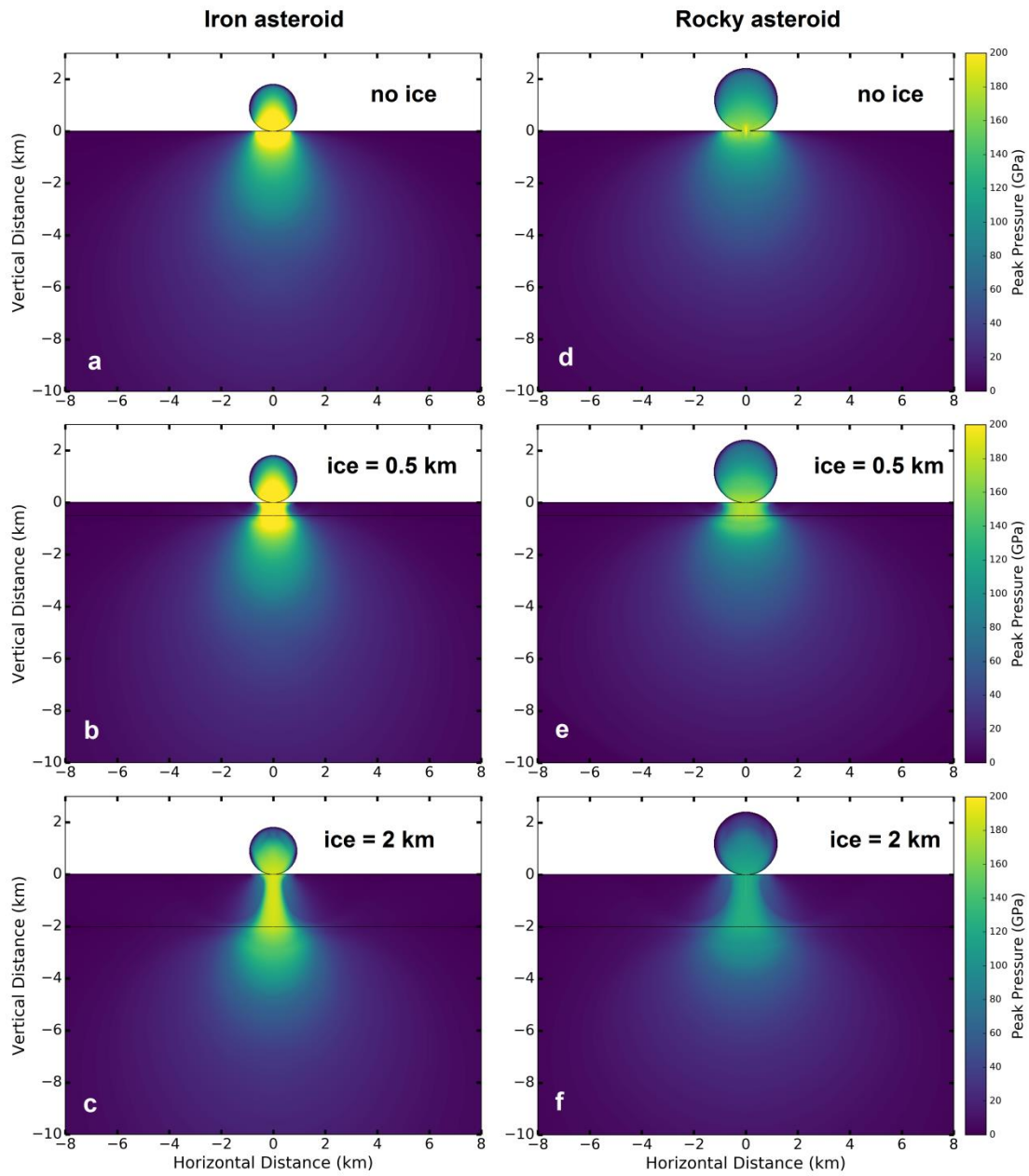


440 **Figure 5:** Map of modern Greenland with each panel showing modeled thickness of rocky ejecta  
441 due to impact of an iron asteroid, assuming no ice present (“no ice sheet”) and then for all four  
442 considered Hiawatha ice-target scenarios (0.5, 1, 1.5 and 2 km, respectively).



443

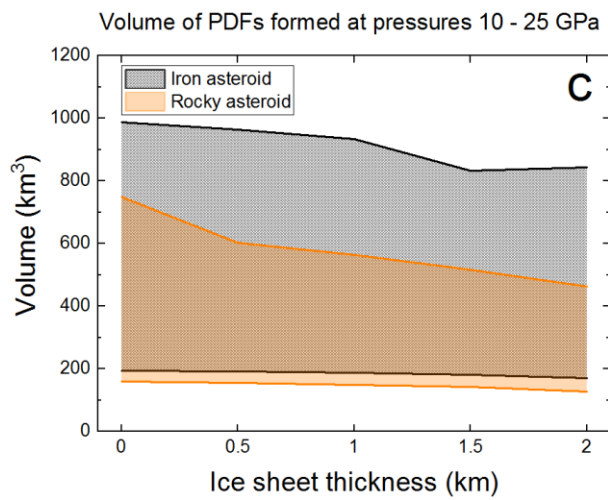
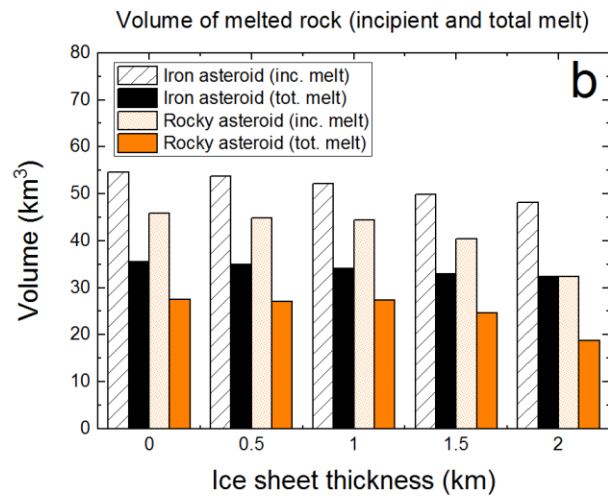
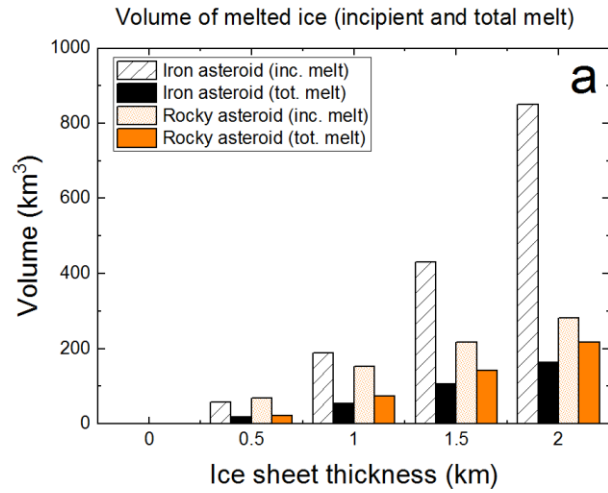
444 **Figure 6:** Provenance plot of peak shock pressures reached within the material 0.5 s and 0.7 s  
445 after impact by a 1.8 km wide iron asteroid (a-c), and a 2.4 km wide rocky asteroid (d-f),  
446 respectively. For easier visualization, the color bars represent the same scale across all panels (0–  
447 200 GPa). While the iron asteroid produces overall greater shock pressures than its rocky  
448 counterpart, in both cases the shock pressures are sufficiently high to readily melt ice and rock,  
449 while the ice sheet somewhat dissipates shock propagation.



450

451

452 **Figure 7:** (a) Volumes of partially and fully melted ice; (b) volumes of partially and fully melted  
453 rock; (c) the volume of rock subjected to pressure range conducive to PDF formation (10–25  
454 GPa).



456 **List of Tables**

457 **Table 1:** Summary of model parameters for ice sheet, rock (Earth’s crust) and iron (impactor).  
 458 The parameters for ice correspond to Bray et al. (2014), with the exception of the friction  
 459 coefficient for damaged material, which comes from Bray (2009) fits to laboratory data (Beeman  
 460 et al., 1988). The parameters for rock are consistent with those listed in Rae et al. (2019). The  
 461 parameters for the Block Model of acoustic fluidization (Melosh, 1979) correspond to the  
 462 previous studies (e.g., Collins, 2014; Rae et al., 2019).

463

Parameter Description, variable, units	Variable	Units	Ice sheet	Rock	Impactor
Surface temperature	$T_s$	K	250	250	250
Poisson's ratio	$\nu$	-	0.33	0.30	0.29
Melt temperature at zero pressure	$T_m$	-	273	1673	1811
Thermal softening coefficient	$\zeta$	-	1.2	1.2	1.2
Material constant, Simon $a$	$a$	GPa	1.253	6.0	6.0
Material constant, Simon $c$	$c$	-	3	3	3
Cohesion, intact	$Y_{i0}$	GPa	0.01	0.01	0.01
Coefficient of internal friction, intact	$\mu_i$	-	2	2	-
Limiting strength at high pressure, intact	$Y_{lim}$	GPa	0.11	2.5	-
Cohesion, damaged	$Y_{d0}$	MPa	0.01	0.01	-
Coefficient of internal friction, damaged	$\mu_d$	-	0.6	0.6	-
Limiting strength at high pressure, damaged	$Y_{dlim}$	GPa	0.11	2.5	-
Acoustic fluidization viscosity constant	$\gamma_\eta$	-	0.015	0.015	-
Acoustic fluidization time decay constant	$\gamma_\beta$	-	300	300	-
Equation of state (EOS)			ice Tillotson	granit2 ANEOS	iron ANEOS

464

465

466 **Table 2:** Summary of the results outlining the peak pressures and the impact-induced melt  
 467 volumes for an iron asteroid and a rocky asteroid. The columns are as follows: [1] ice sheet  
 468 thickness; shock pressure required for [2] incipient and [3] total melting of ice, and [4] incipient  
 469 and [5] total vaporization of ice (Pierazzo et al., 1997); [6-7] shock pressure range at which PDFs  
 470 form (French and Koeberl, 2010); shock pressure required for [8] incipient and [9] total melting  
 471 of rock (Pierazzo et al., 1997); [10] maximum shock pressure reached within the target rock  
 472 layer.

473

		Ice sheet				Rocky target					
		[1]	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]
		Ice sheet thickness [km]	V [km <sup>3</sup> ], P > 0.4 GPa	V [km <sup>3</sup> ], P > 3 GPa	V [km <sup>3</sup> ], P > 4.5 GPa	V [km <sup>3</sup> ], P > 43 GPa	V [km <sup>3</sup> ], P > 10 GPa	V [km <sup>3</sup> ], P > 25 GPa	V [km <sup>3</sup> ], P > 46 GPa	V [km <sup>3</sup> ], P > 56 GPa	Max P [GPa]
Iron Asteroid	0	n/a	n/a	n/a	n/a	n/a	986.8	194.3	54.6	35.5	302
	0.5	58.3	17.5	13.4	1.3	1.3	964.6	191.7	53.7	35.0	251
	1	189.2	53.9	31.6	2.2	2.2	933.6	188.1	52.1	34.1	224
	1.5	431.0	106.9	57.5	3.4	3.4	832.1	181.8	49.8	33.0	204
	2	850.7	163.8	85.4	4.7	4.7	843.2	170.6	48.1	32.3	189
Rocky Asteroid	0	n/a	n/a	n/a	n/a	n/a	749.5	159.6	45.9	27.5	222
	0.5	68.4	22.5	14.6	0.6	0.6	603.3	154.7	44.8	27.0	176
	1	153.2	74.1	43.0	1.0	1.0	563.5	149.5	44.5	27.4	157
	1.5	218.0	141.4	77.8	3.9	3.9	516.6	142.0	40.4	24.7	140
	2	282.7	217.4	119.7	9.6	9.6	462.2	127.9	32.3	18.8	126

474



475 **References**

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