



Impact of Thermochromic Coatings on Thermal Management for Human Spacecraft Applications

Joseph Peoples*, Sydney Taylor**, Christopher Massina**, and Xiulin Ruan*

*Purdue University

**Johnson Space Center

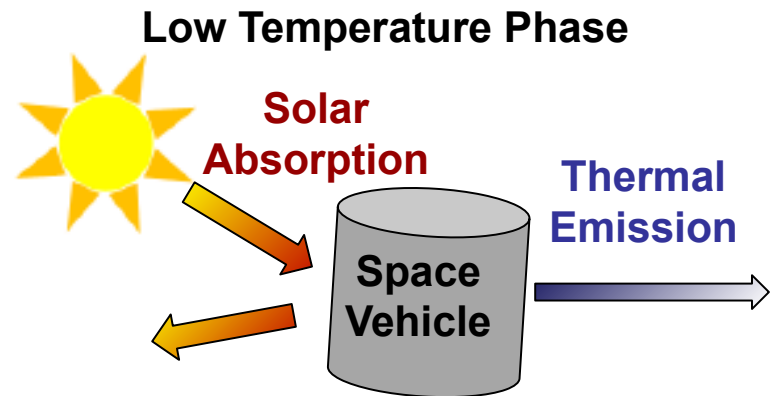
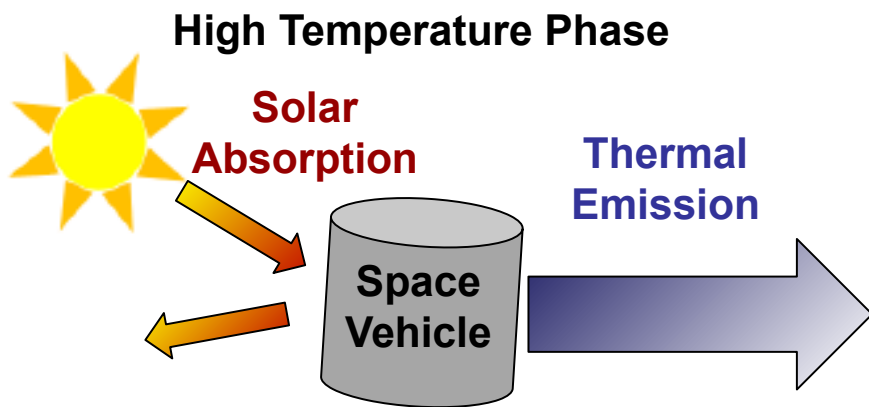
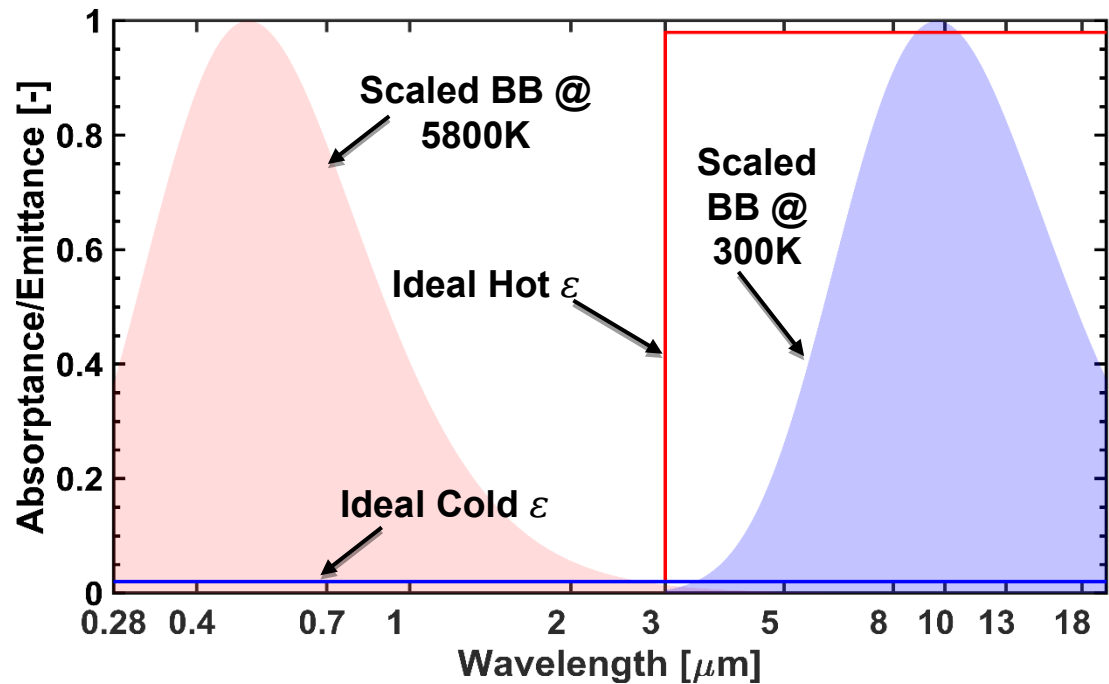


Presented By
Joseph Peoples

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- Motivation and Background
 - Ideal Variable Emitter
 - Thermochromic Material: Lanthanum Strontium Manganite
 - Solar Reflective Material: Barium Sulfate
 - Micropatterned Thermochromic Coatings
- Design Parameters for Micropatterned Coatings
 - Dopant Dependent Transition Temperature
 - Coupled Solar Absorptance and Variable Emittance
- Thermal Desktop Modeling
 - Representative Radiator Design and Setup
 - Transition Temperature Study
 - Absorptance vs Emittance Study
- Conclusions and Future Work

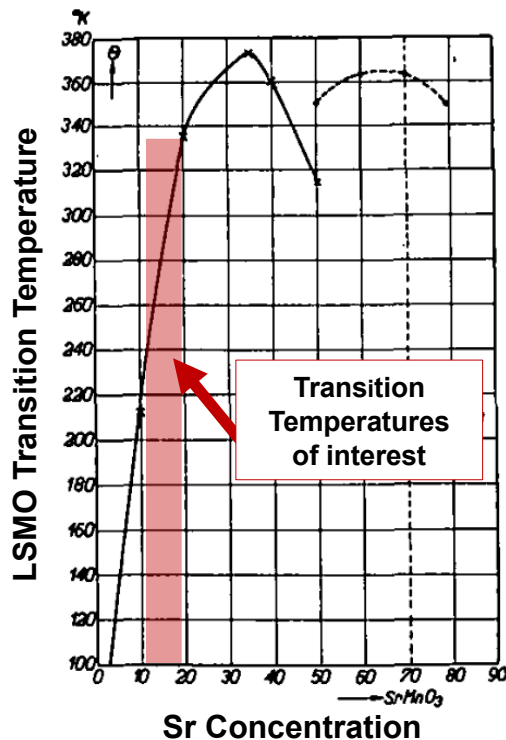
- Thermochromic Coatings have temperature dependent emissivity
- Deep Space is considered an infinite heat sink at ~ 3 K
- Extraterrestrial Solar Irradiation is ~ 1400 W/m²
- Ideal: $\epsilon_{\text{cold}} = 0$, $\epsilon_{\text{hot}} = 1$



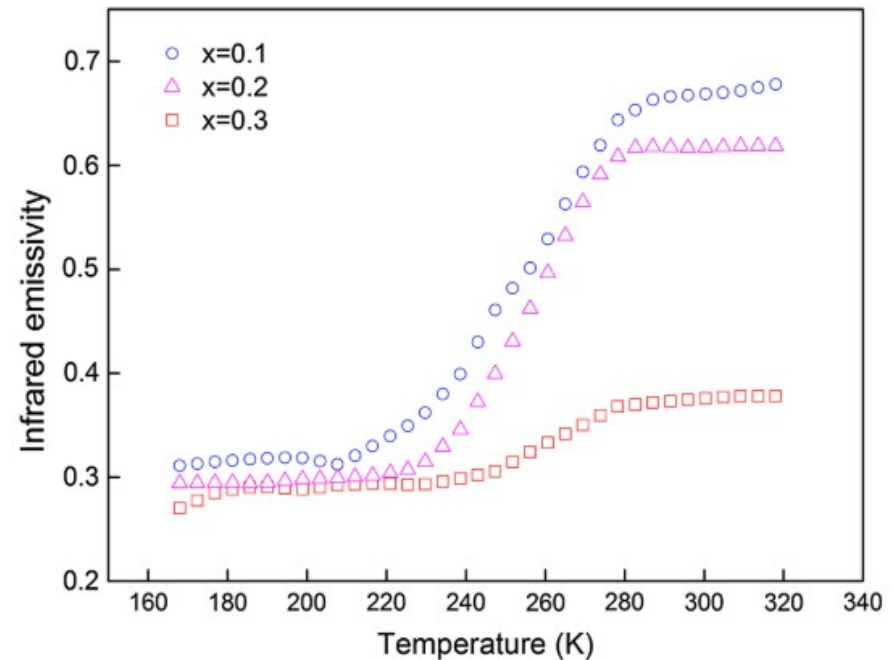
- Lanthanum Strontium Manganite (LSMO)
 - Temperature Dependent Variable Emittance
 - $\text{La}_{1-x}\text{Sr}_x\text{MnO}_3$
 - Sr is a dopant in the LaMnO_3 which can change the transition temperature as well as the emittance
 - $\alpha = 0.7$ in bulk phase



Source: <https://bit.ly/31ca7Zn>



Jonker, G. H., & Van Santen, J. H., *Physica*, (1950).

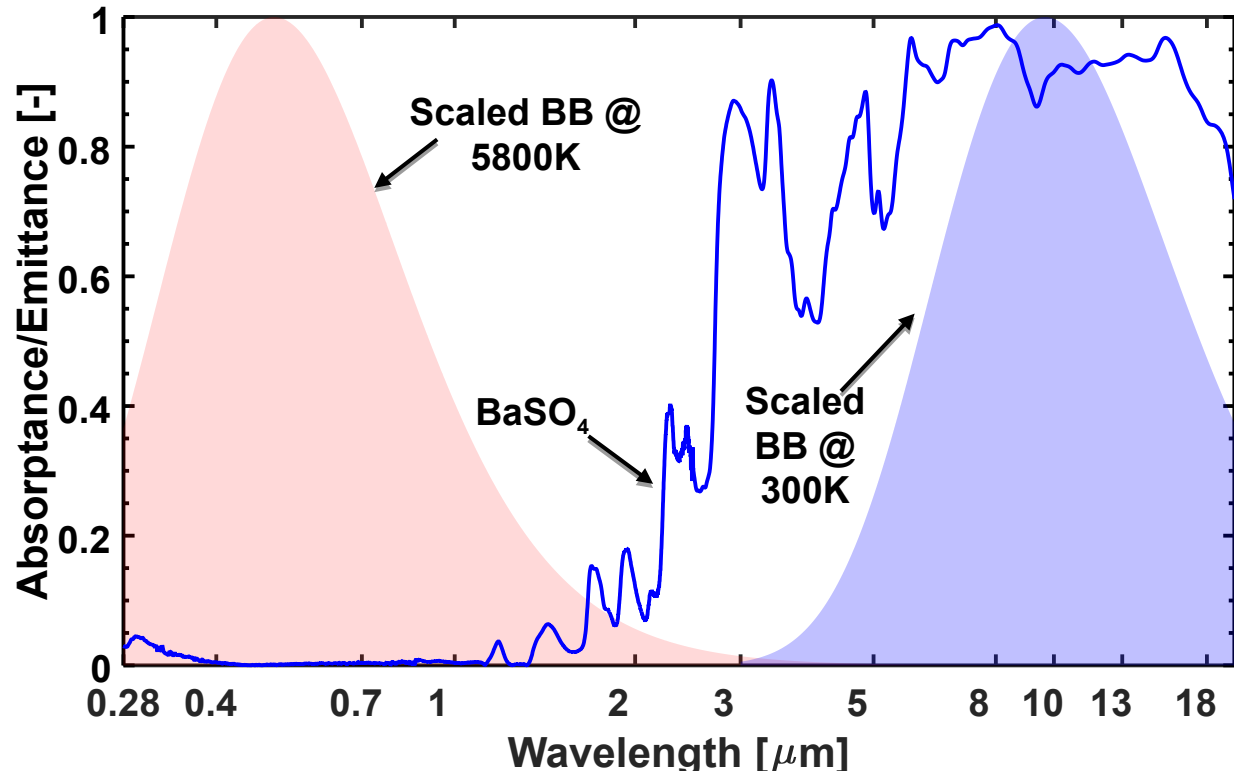


Wang, C. B., et al., *Journal of Materials Science*, (2015).

- Barium Sulfate (BaSO₄) highly solar reflective
 - White paint form
 - $\alpha = 0.03$, $\varepsilon = 0.92$
 - Other typical white paints
 - $\alpha \sim 0.15-0.2$
 - $\varepsilon \sim 0.8-0.9$



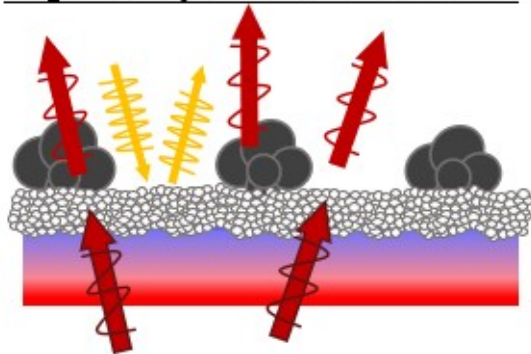
Source: <https://tinyurl.com/yu68pakp>



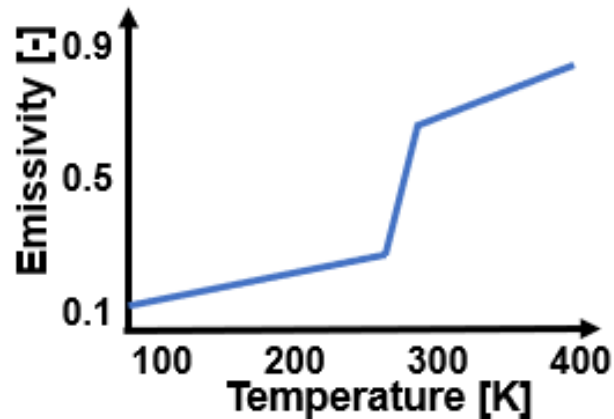
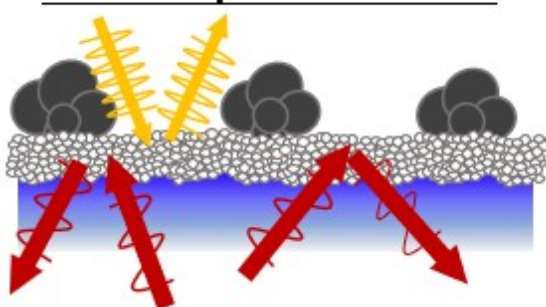
X. Li, J. Peoples, et. al., ACS Applied Materials and Interfaces (2021)

- Objective: Create a coating with a low ε at low temperatures and high ε at high temperatures while maintaining a low α
- Approach: Develop a computational model to study effects of micropatterned thermochromic coatings on radiator turndown and pertinent temperatures
- Objective: Define design targets for the transition temperature, cold state emittance, and solar absorptance

High Temp: Insulator Phase

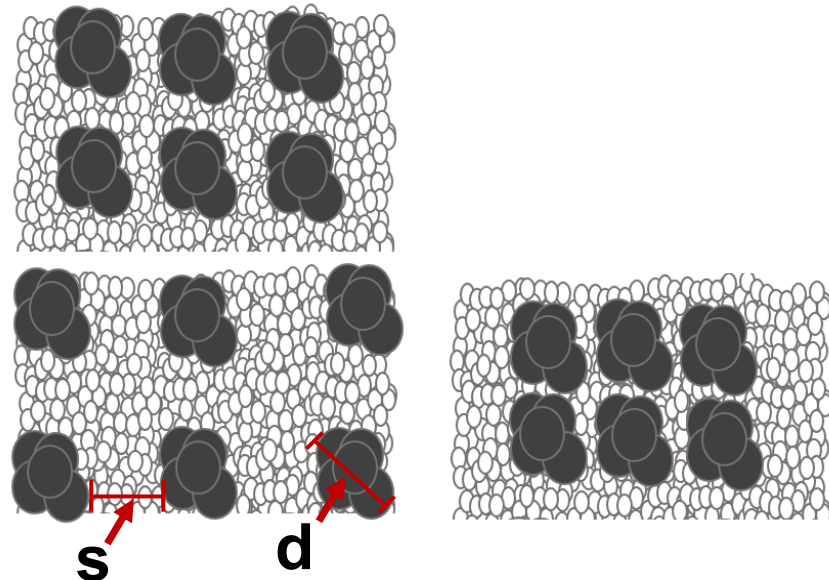
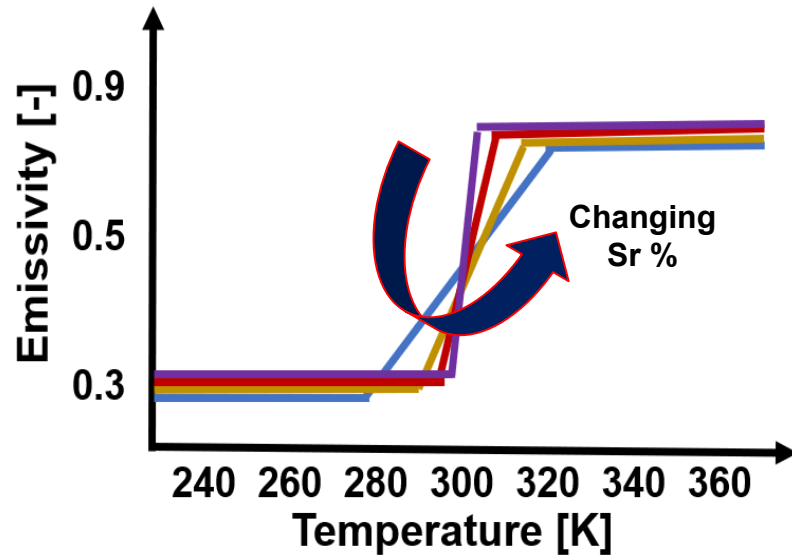
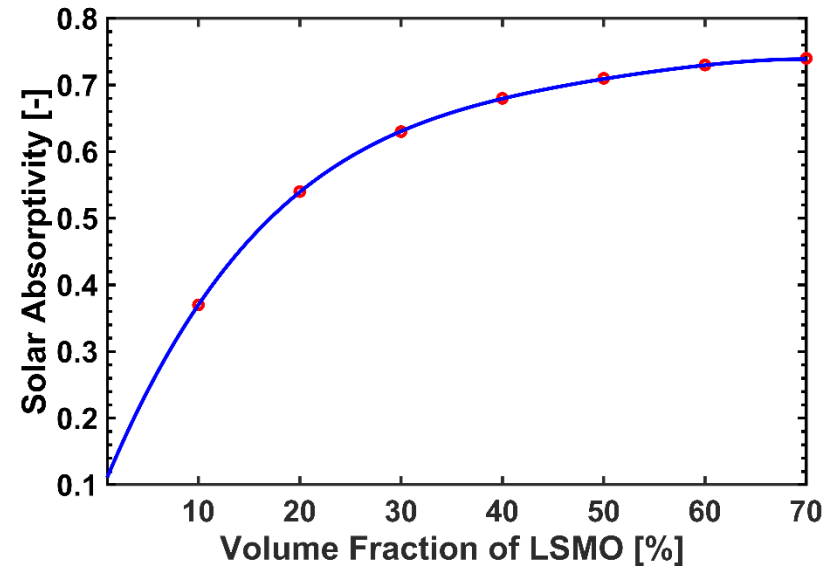


Low Temp: Metal Phase

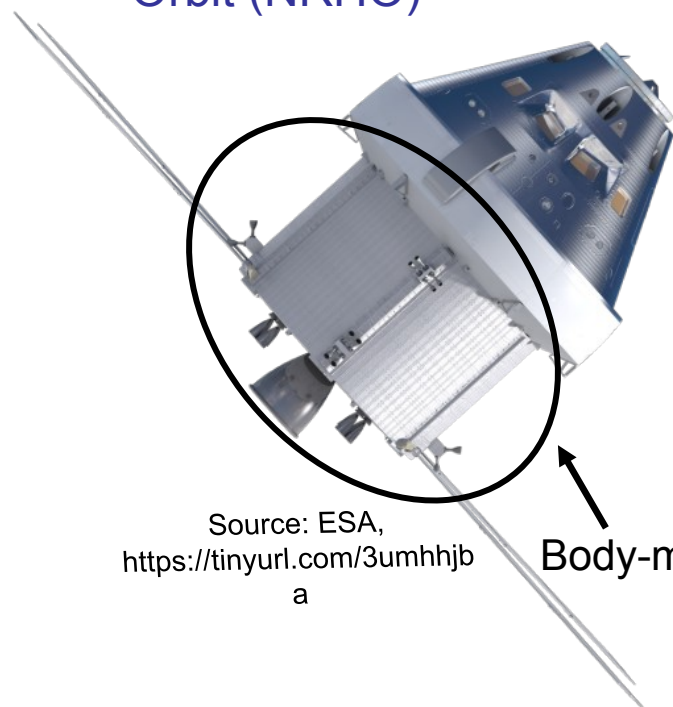


= 0~3 μm Wavelength
 = 3~25 μm Wavelength
 ○ = BaSO₄ ● = LMS

- Three variable sets to examine
 - Transition Temperatures: T_{start} and T_{stop}
 - Solar Absorptance (α)
 - Emittance: cold ε and hot ε

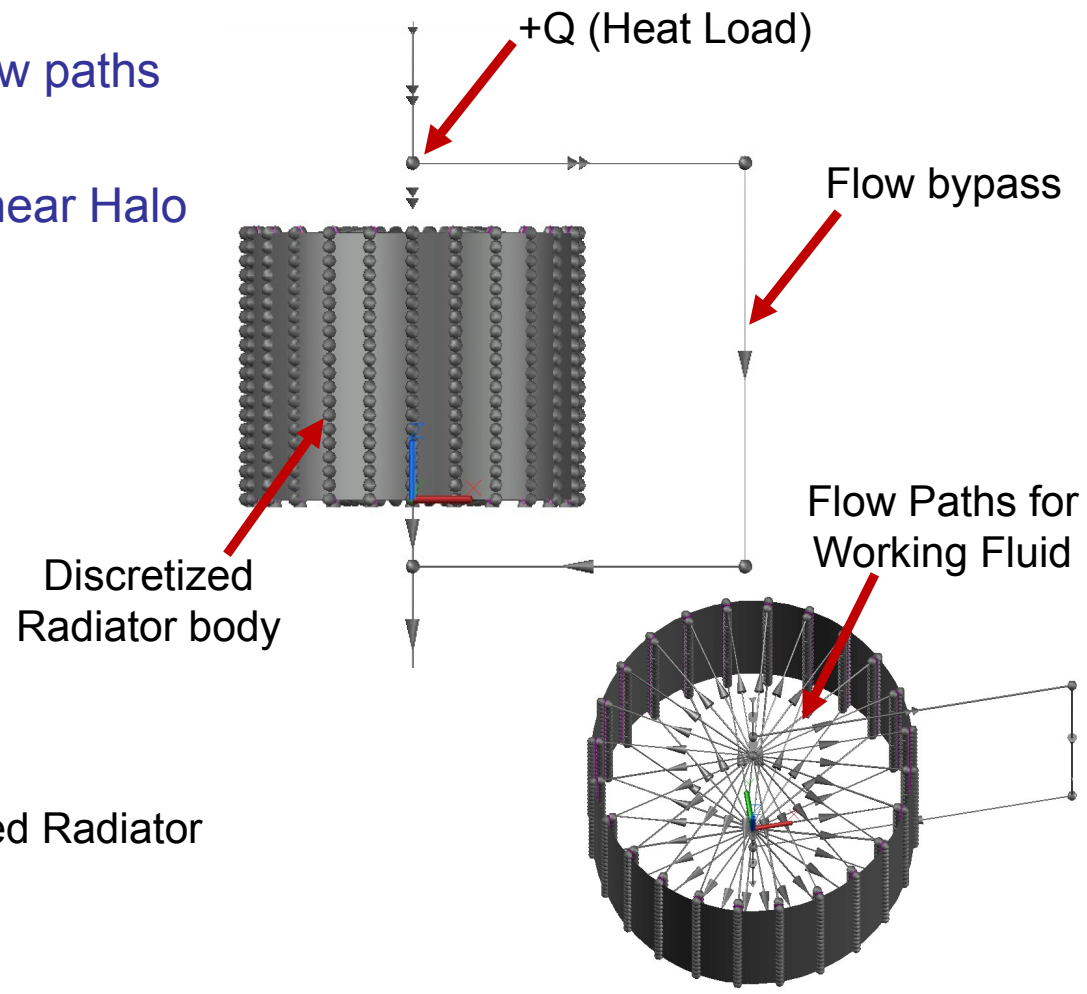


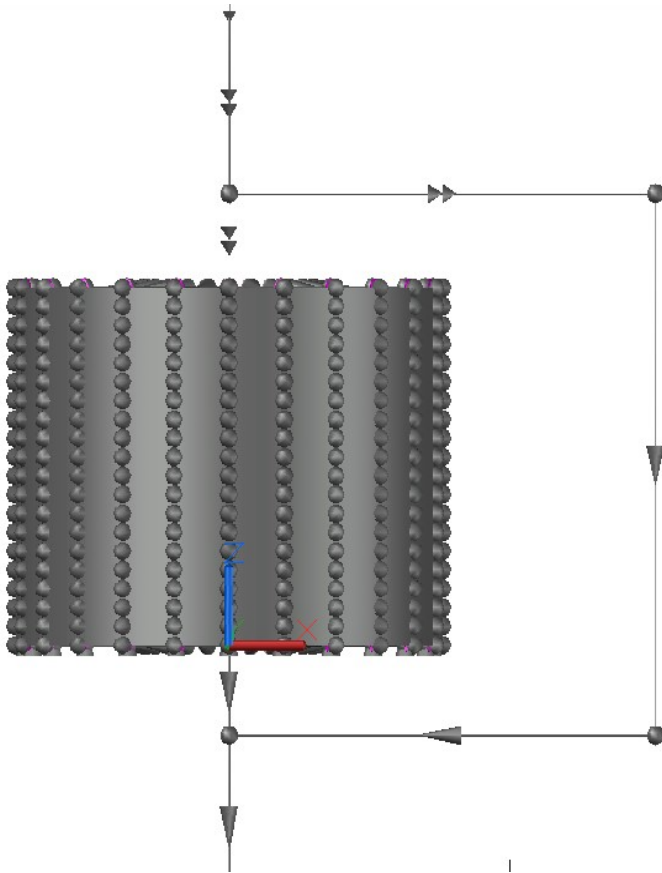
- Body-mounted radiator design based on Orion Space Craft
- 25 angular body section, 25 flow paths
- 20 axial nodes
- Orbit Considered: Near Rectilinear Halo Orbit (NRHO)



Source: ESA,
<https://tinyurl.com/3umhhjb>
 a

Body-mounted Radiator

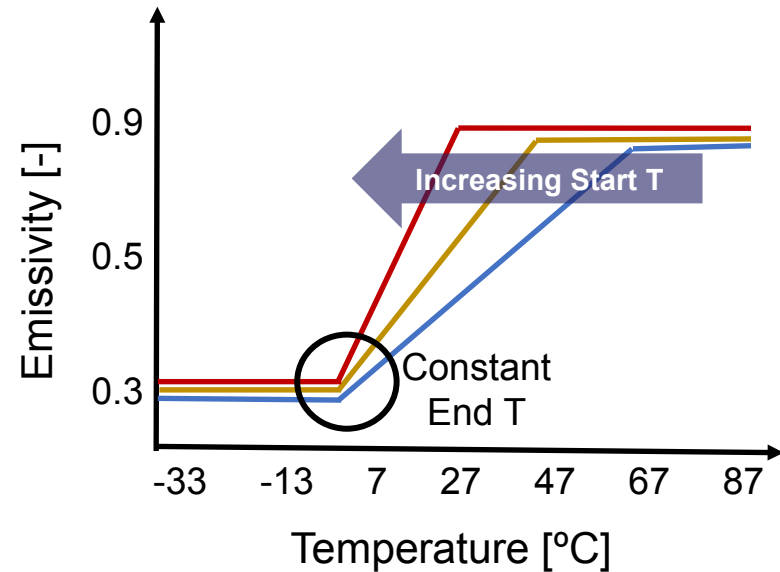
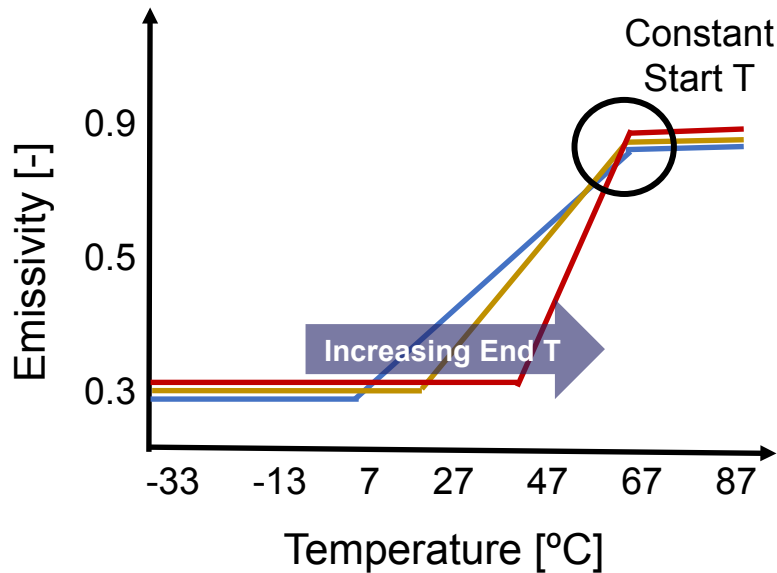




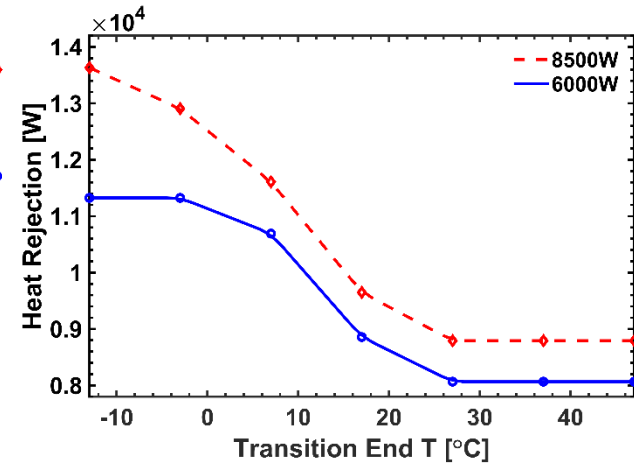
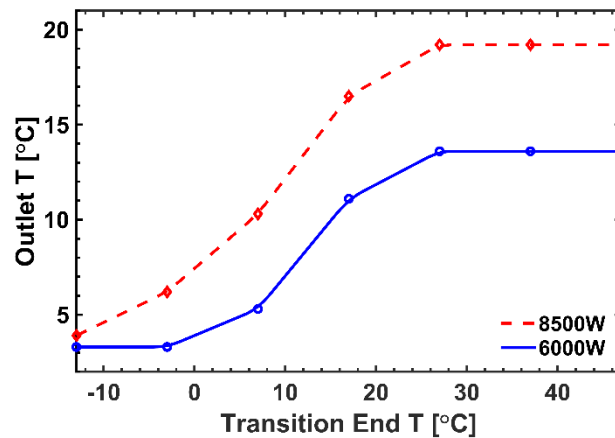
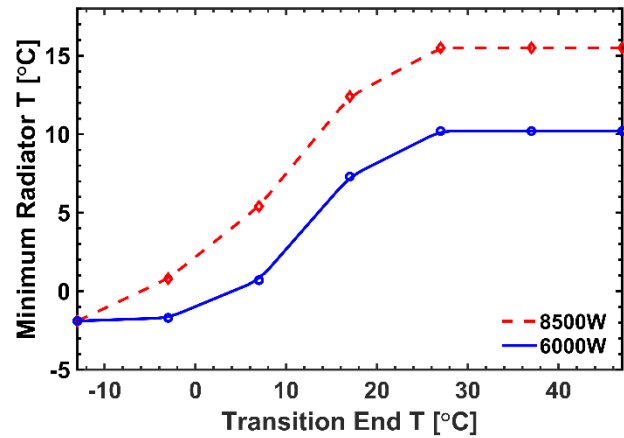
Parameter	Value
Diameter of Radiator [m]	5
Length of Radiator [m]	3.96
Crewed heat load [W]	8500
Un-crewed heat load [W]	6000
Mass flow rate [lb/hr]	600
Radiator Wall UA [W/mK]	100
Working Fluid	Water
Freezing Point [°C]	0
Flow Bypass Ratio [%]	8
Axial Radiator Sections	20
Angular Radiator Sections	25

- Bypass Ratio set by sizing to static emissivity case and achieving a 4 °C outlet temperature based on avionics requirements

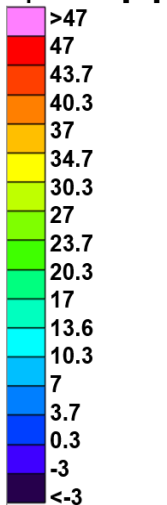
- First, we will investigate how the transition temperature effects the heat flux turndown and minimum body temperature
- Varying the transition start and end temperatures to under the impact of heat rejection
- $\epsilon_{\text{cold}} = 0.3$
- $\epsilon_{\text{hot}} = 0.9$



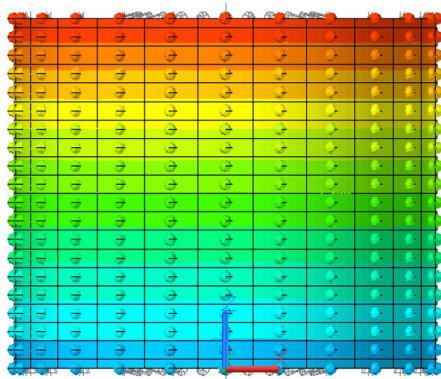
- Transition Start $T = 67\text{ }^{\circ}\text{C}$, $\epsilon_{\text{cold}} = 0.3$, $\epsilon_{\text{hot}} = 0.9$



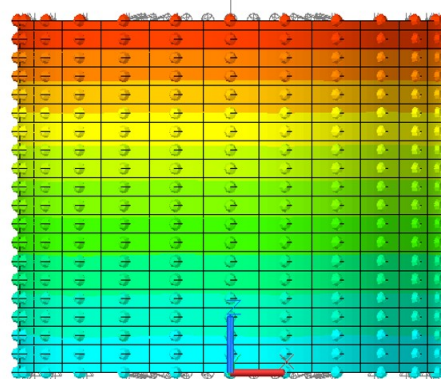
Temperature [$^{\circ}\text{C}$]



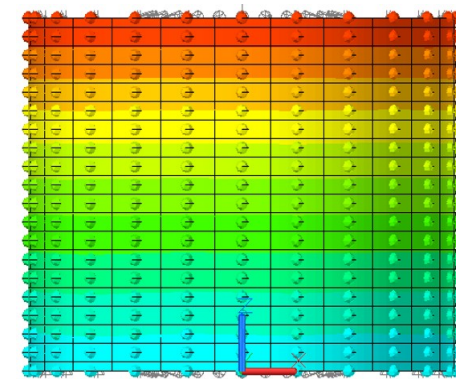
Transition End: 17 $^{\circ}\text{C}$



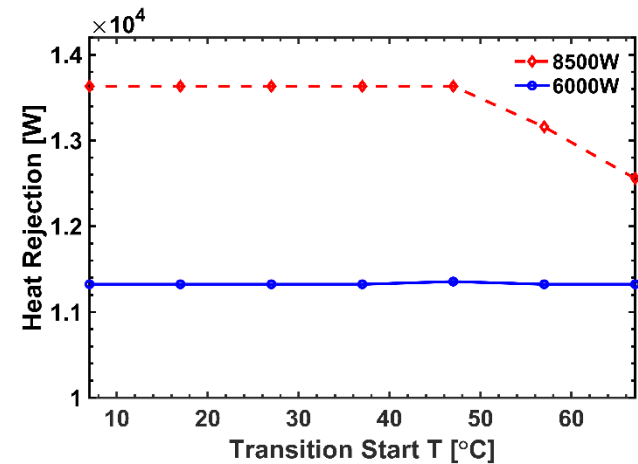
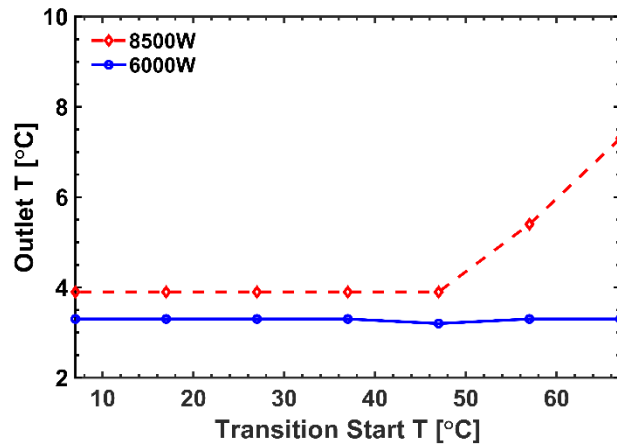
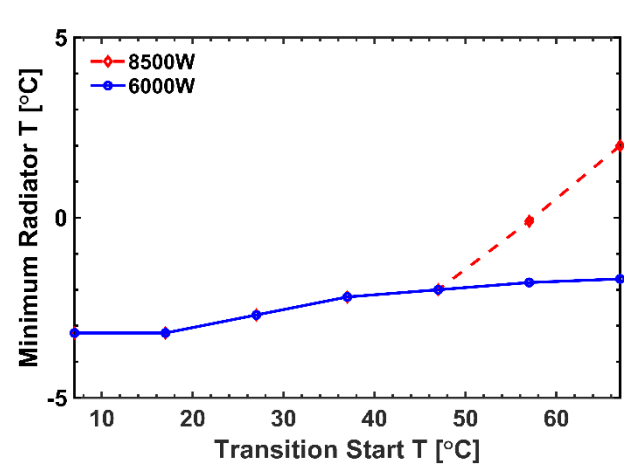
Transition End: 27 $^{\circ}\text{C}$



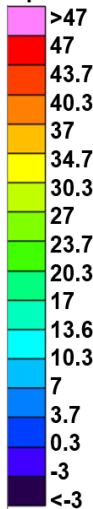
Transition End: 37 $^{\circ}\text{C}$



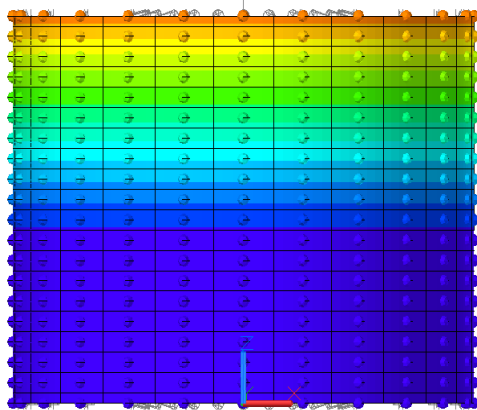
- Transition End T = 0 °C, $\epsilon_{\text{cold}} = 0.3$, $\epsilon_{\text{hot}} = 0.9$



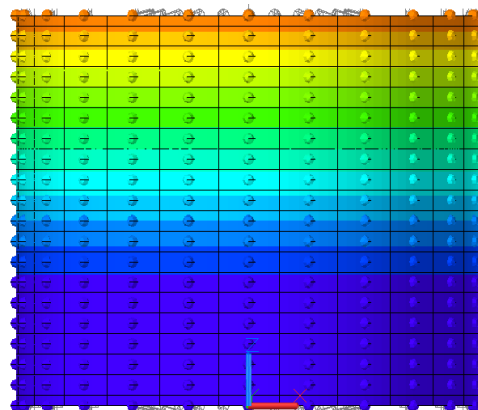
Temperature [°C]



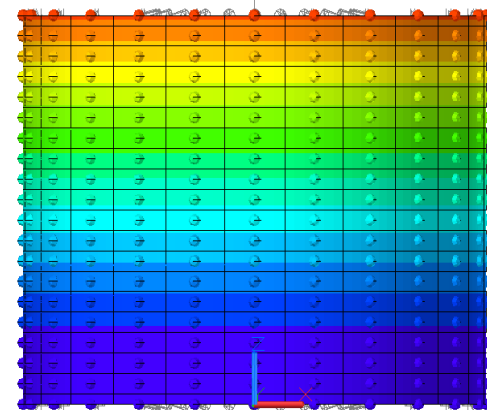
Transition Start: 17 °C



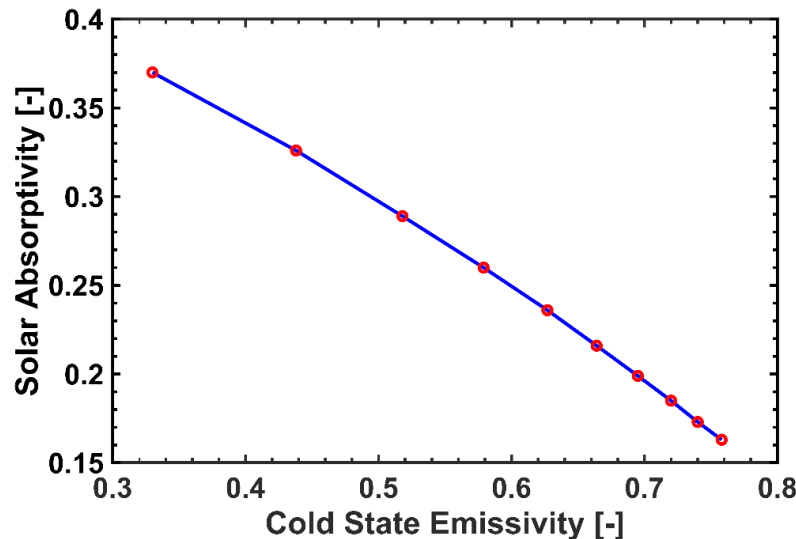
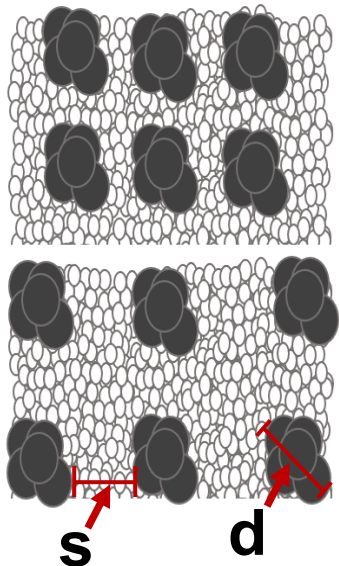
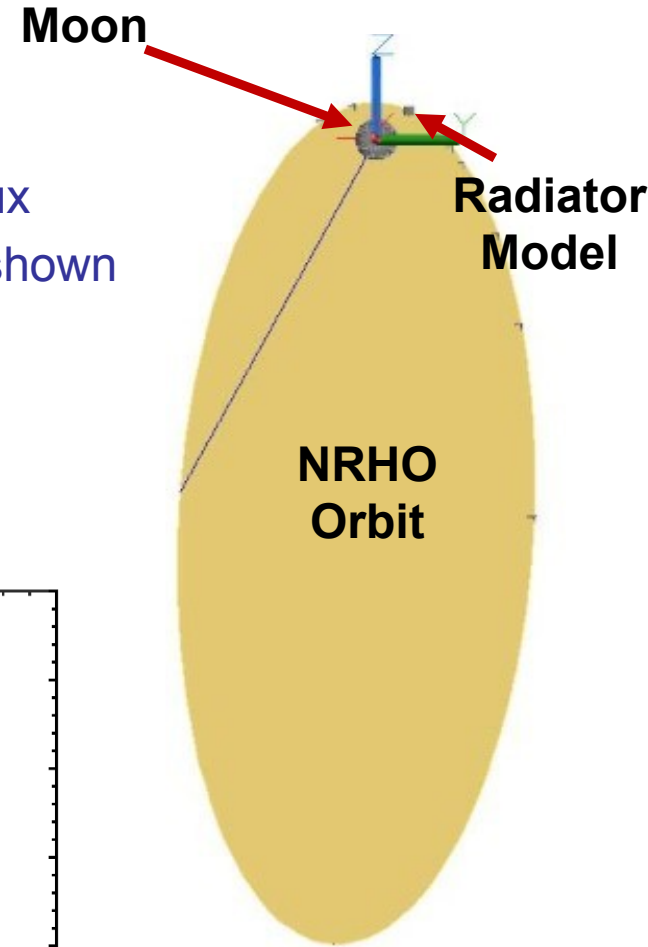
Transition Start: 27 °C



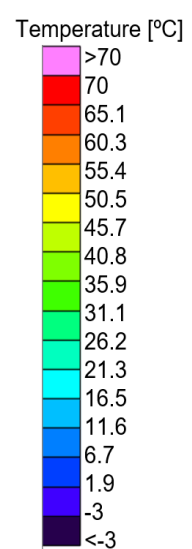
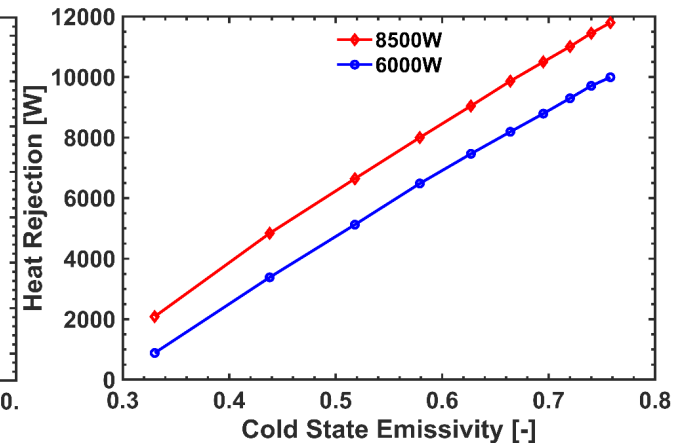
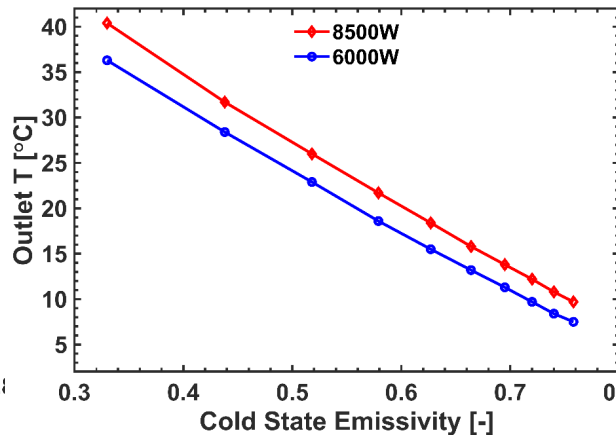
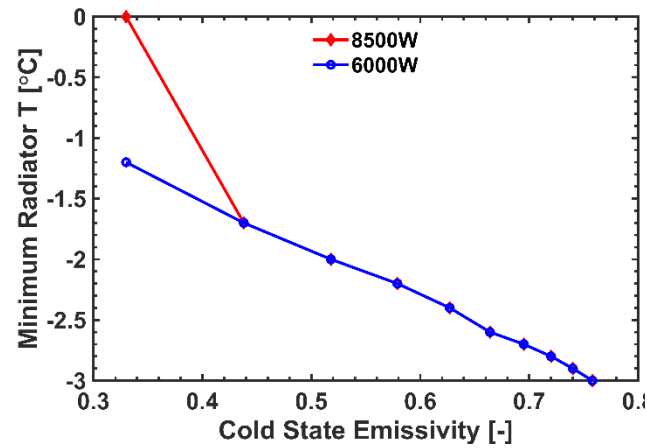
Transition Start: 37 °C



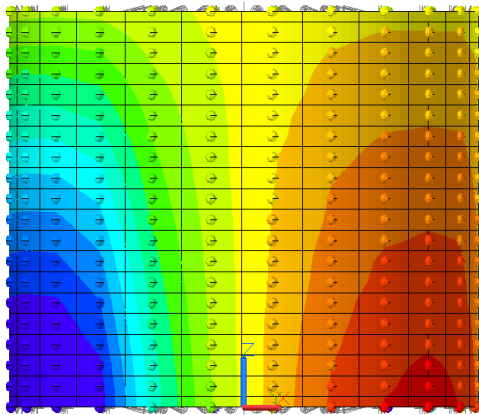
- Next, we will investigate how the coupling of the solar absorptance and cold state emittance
- We consider an NRHO Orbit to study the solar heat flux
- Varying the absorptance and cold state emittance as shown below
- Hot Emittance is constant at 0.9
- Transition Temperatures are constant at:
 - Start T = 67 °C
 - End T = 27 °C



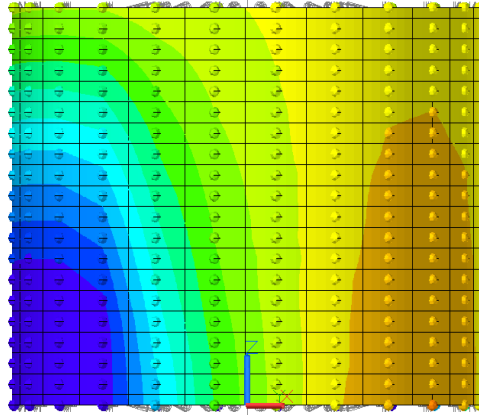
- Transition Start $T = 67\text{ }^{\circ}\text{C}$, Transition End $T = 27\text{ }^{\circ}\text{C}$, $\epsilon_{\text{hot}} = 0.9$



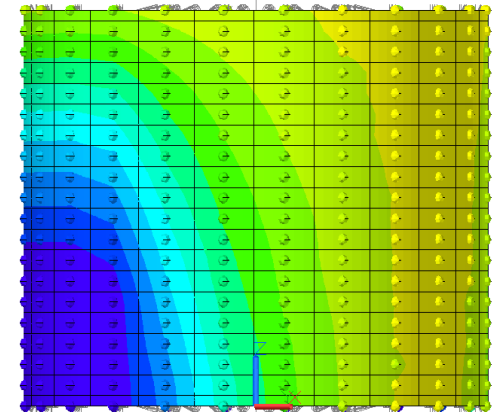
$\alpha = 0.33, \epsilon_{\text{cold}} = 0.44$



$\alpha = 0.29, \epsilon_{\text{cold}} = 0.52$



$\alpha = 0.26, \epsilon_{\text{cold}} = 0.58$





Conclusion and Future Work



- We have discussed the design parameters for our micropatterned variable emissivity coatings
- We found that the transition temperature saturates after **27 °C** for the transition End Temperature
- We presented a relation between the absorptivity and emissivity of the micropatterns
- We found that solar absorptance in an NRHO orbit does have significant impact on the fluid outlet temperature which will in turn affect the heat rejection of down stream avionics
- For future work, we would like to add dynamic bypass to the fluid loop to further understand the turndown potential
- We would also like to study the transient behavior of these coatings and the transition state.



Acknowledgements



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 - Dr. Sydney Taylor, Dr. Christopher Massina, Jonah Smith, Lisa Erickson, Abigail Zinecker, and Brittany Spivey
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