

Flow Boiling & Condensation Experiment (FBCE): From Initial Concept to Full Implementation on the ISS

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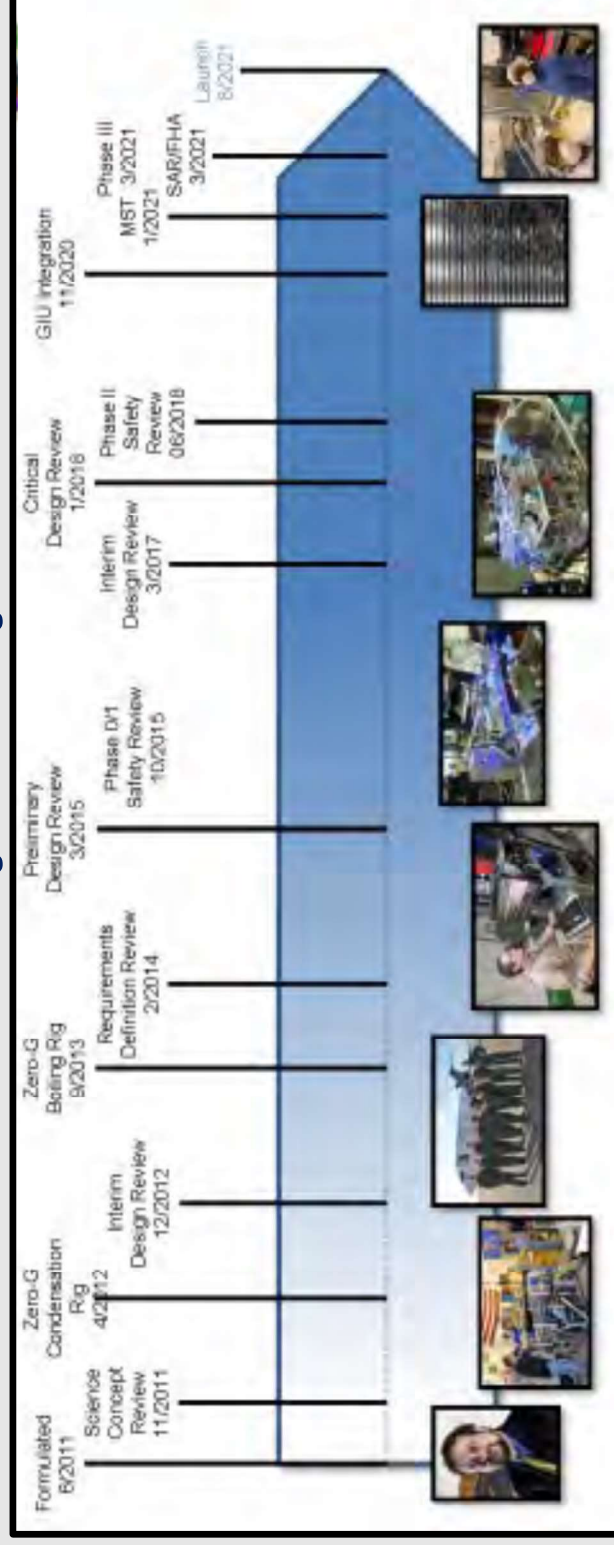
Jeffrey Mackey

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3000 Aerospace Parkway, Brook Park,
Cleveland, OH 44142*



Culmination of efforts started in the mid-1990s!!

- **1994 – 1999:** two unsuccessful proposals to NASA; difficulty promoting a shift in microgravity efforts from pool boiling to flow boiling
- **2000 - 2006:** first NASA grant addressing flow boiling in reduced gravity
- **2011:** initial FBCE concept
- **2013:** provided detailed designs to Glenn for:
 - **Flow Boiling Module (FBM)**
 - **Condensation Module for Heat Transfer Measurements (CM-HT)**
 - **Condensation Module for Flow Visualization (CM-HT)**
- **2013:** validated soundness of designs of three modules based on parabolic flight experiments
- **2014-2017:** developed detailed predictions in the form of
 - **Empirical correlations for flow boiling and flow condensation in reduced gravity**
 - **Theoretical models for flow boiling and flow condensation in reduced gravity**
- **2017-2021:** Purdue's initiated CFD modeling of flow boiling and flow condensation





Long Term

The proposed research aims to develop an integrated two-phase flow boiling/condensation facility for the International Space Station (ISS) to serve as primary platform for entire fluid physics community to obtain two-phase flow and heat transfer data in microgravity.

Overriding objectives are to investigate *the two most fundamental mechanisms* for phase change in microgravity: **FLOW BOILING** and **FLOW CONDENSATION**. This includes obtaining *long-duration* (1) *heat transfer data* and (2) *video records of interfacial flow structure* for both.

Applications

- Nuclear fission/Rankine power cycle for future space missions to the Moon, and Mars and deep space missions
- Vapor compression heat pump for planetary bases (Moon, Mars)
- Thermal control systems and advanced life support systems in spacecraft
- Cryogenic systems: nuclear thermal propulsion, fuel depots, tank chilldown



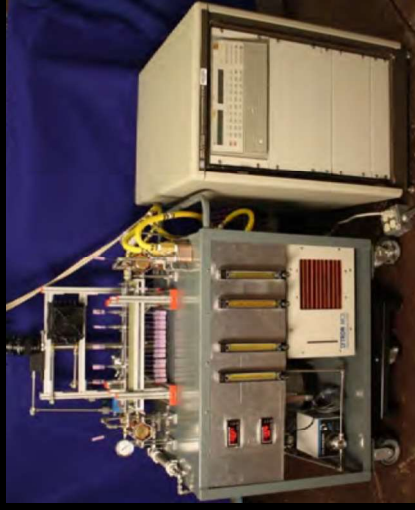
For both Flow Boiling and Flow Condensation

- Conduct one- g_e experiments at different flow orientations
- Conduct microgravity experiments in parabolic flight aircraft
- Develop empirical correlations applicable to different gravities
- Develop theoretical models applicable to different gravities
- Develop CFD models applicable to different gravities (**in progress**)
- Refine empirical correlations, theoretical models, and CFD models using ISS data (**future**)

ISS will enable obtaining large duration steady state wall temperature measurements and video records of interfacial structure; both are essential for validation purposes!!



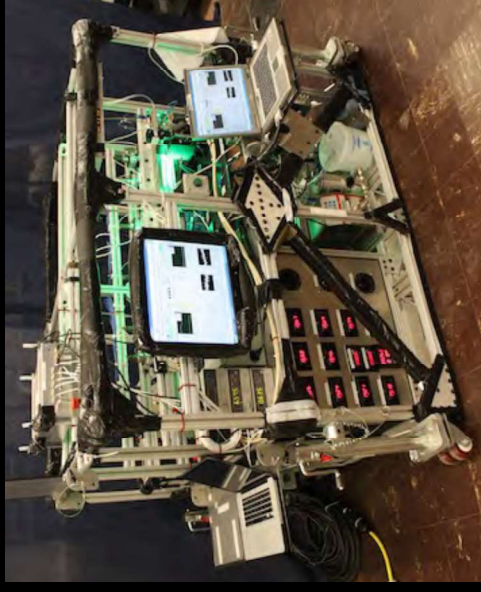
**High-Capacity
Condensation Facility**



**Mini/micro-channel
Condensation Facility**



**Falling-Film
Heating/Evaporation
Facility**



**Parabolic Flight
Condensation Facility**



**One-G Flow
Boiling Facility**



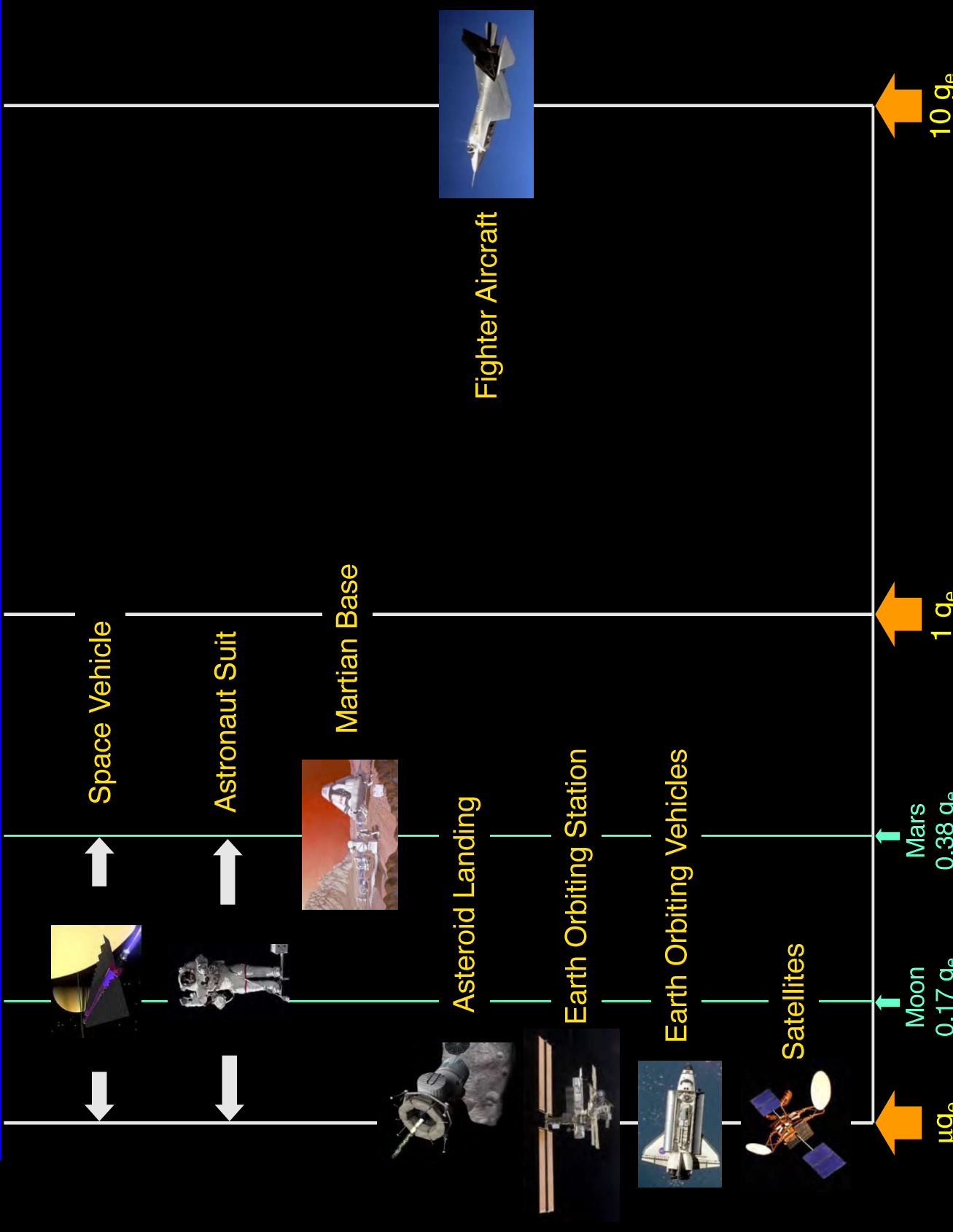
**Hybrid Thermal Control
System (H-TCS)**



**Parabolic Flight Flow
Boiling Facility**



Examples of Systems Demanding Predictive Models of Effects of Gravity on Two-Phase Flow and Heat Transfer



Fighter Aircraft

Space Vehicle

Astronaut Suit

Martian Base

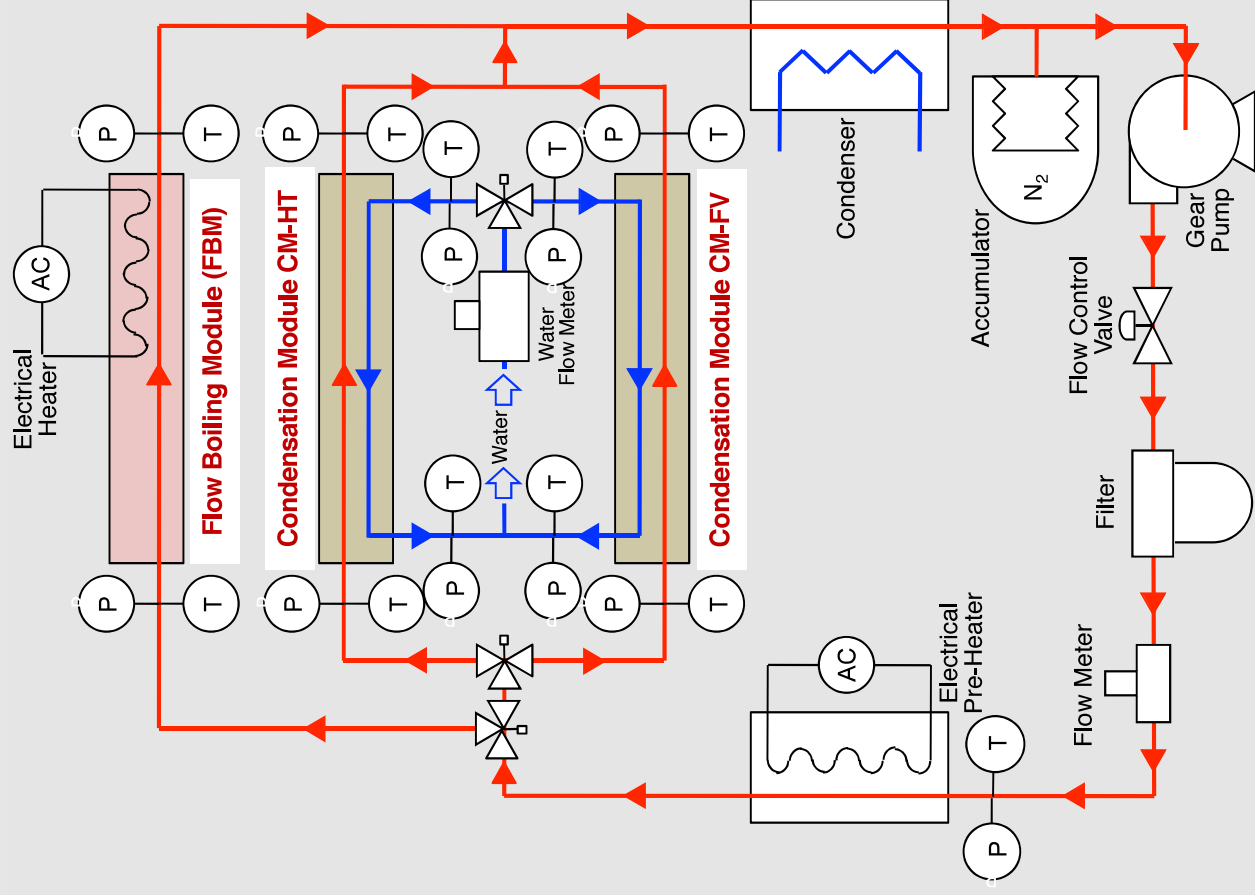
Asteroid Landing

Earth Orbiting Station

Earth Orbiting Vehicles

Satellites





Consists of:

- **nPFH (normal perfluorohexane, C₆H₁₄) sub-loop**
- **Water sub-loop**

Three interchangeable test modules:

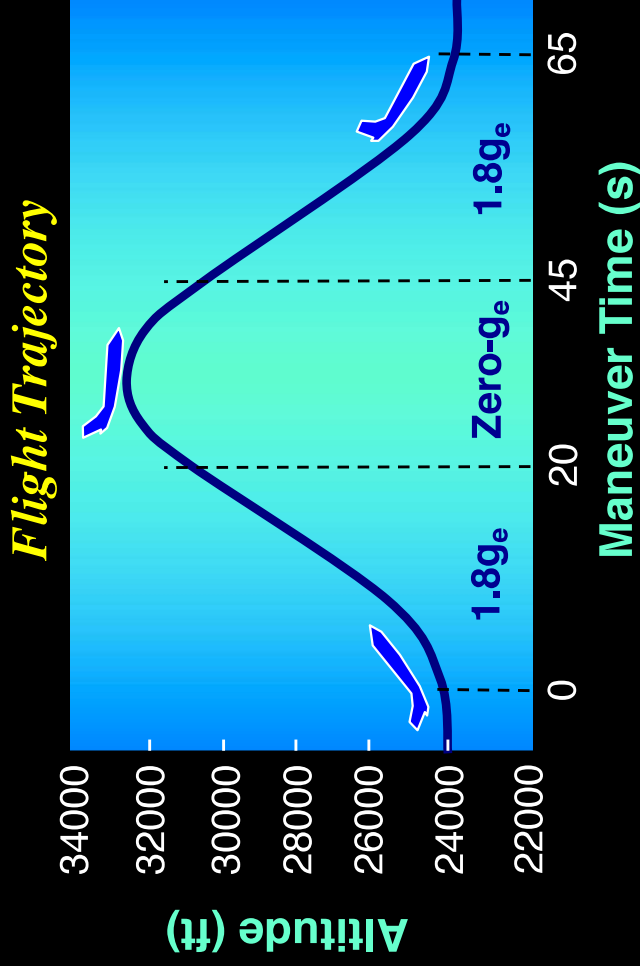
- **Flow Boiling Module (FBM)**
- **Condensation Module for Heat Transfer Measurements (CM-HT)**
- **Condensation Module for Flow Visualization (CM-FV)**



Flow Boiling Module (FBM)

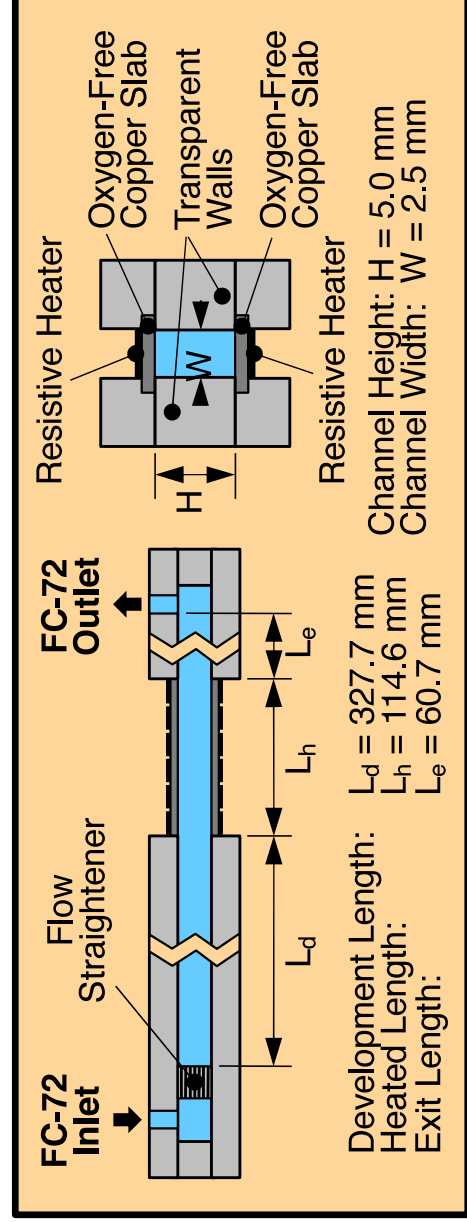
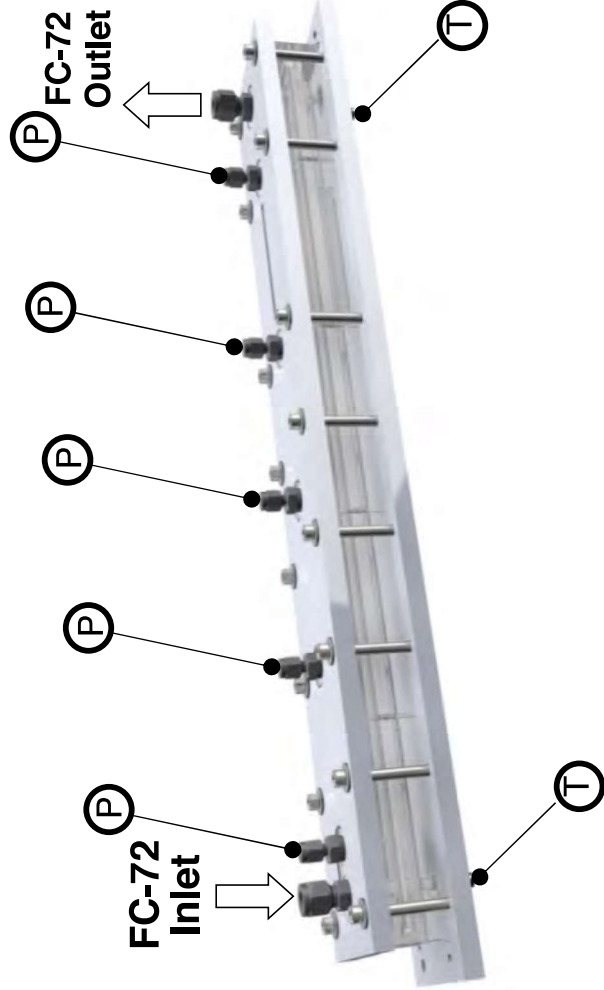
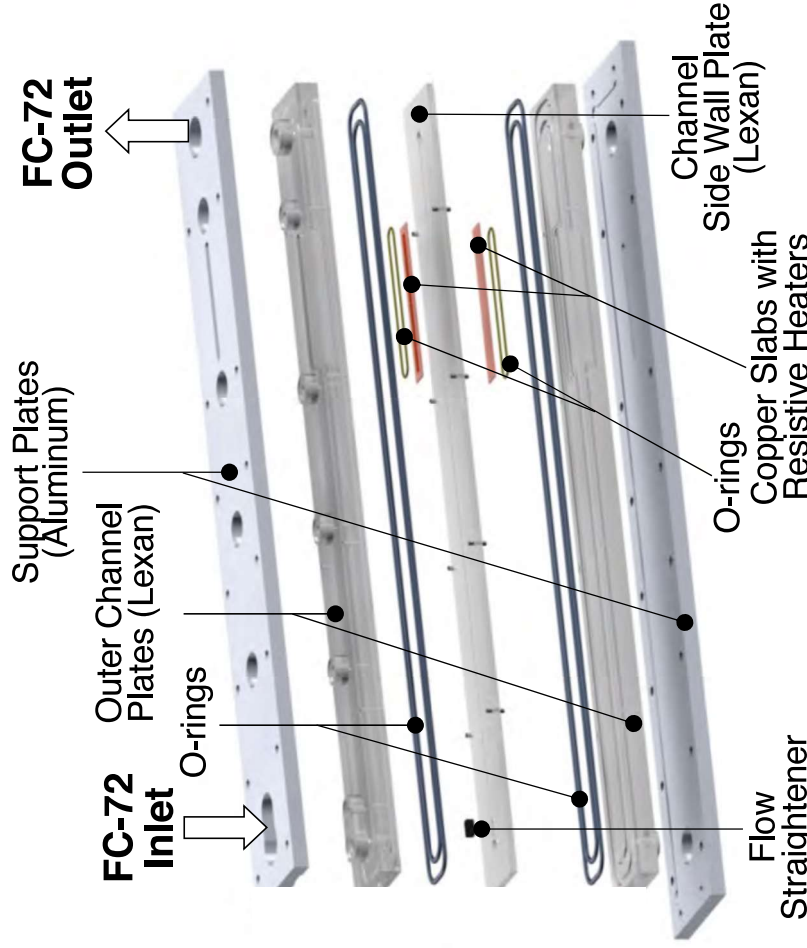


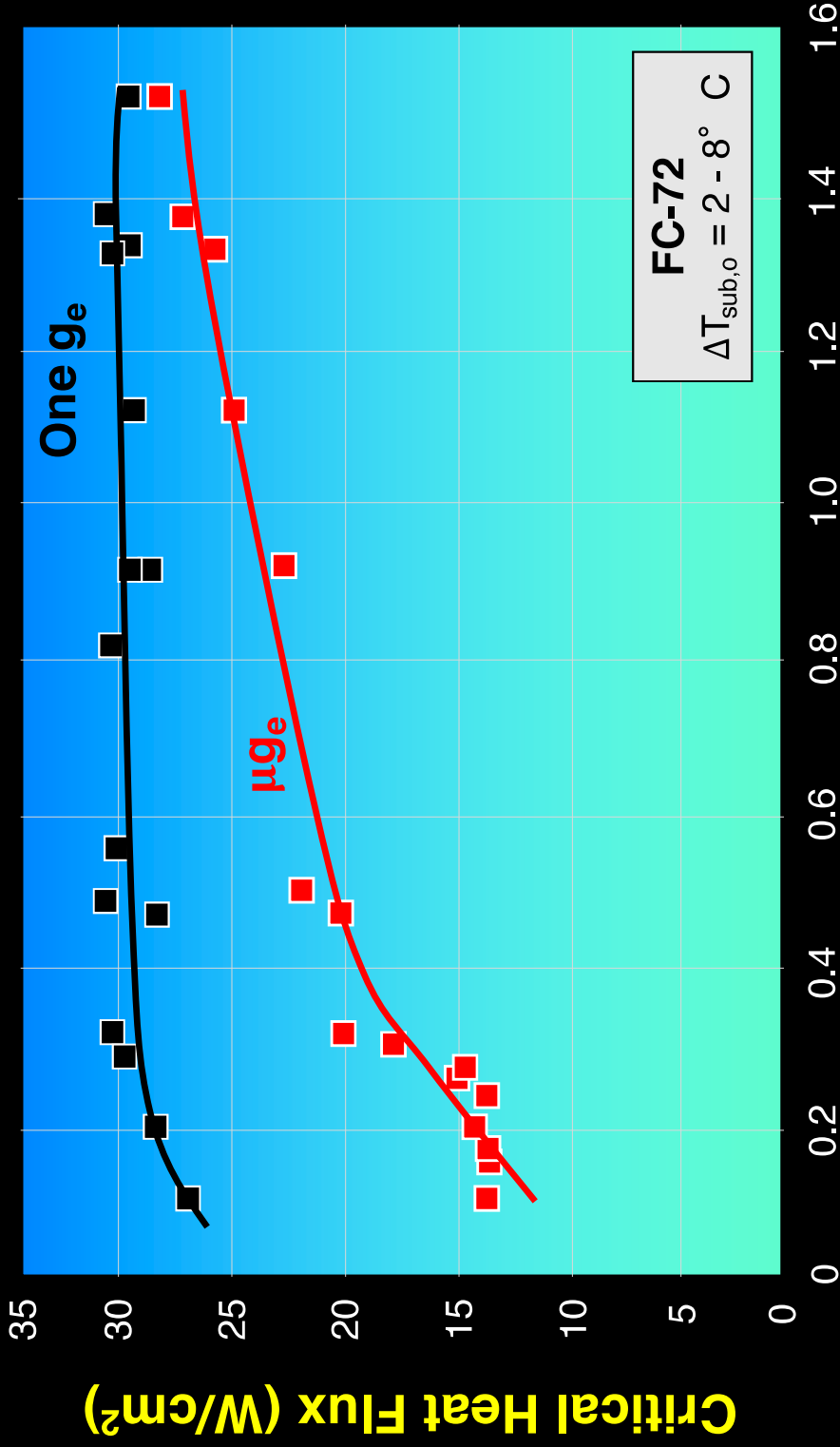
KC-135 Tests performed at NASA Glenn Research Center



Phase Change Photo Library (Mudawar, 1984 - 2016)







Inlet Flow Velocity (m/s)

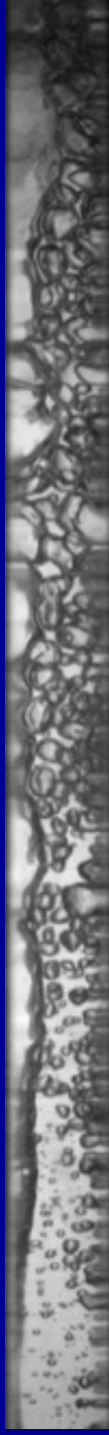
- Critical heat flux (CHF) is the most important design parameter for flow boiling systems, exceeding which can lead to surface overheating or burnout
- Compared to one- g_e CHF data, parabolic flight data show appreciable degradation at low velocities but convergence at high velocities





**CHF for Double-sided
Heating: Low U
(~ 0.1 m/s)**

Horizontal one g_e



Microgravity



**CHF for Double-sided
Heating: High U
(~ 2 m/s)**

Horizontal one g_e



Microgravity



Low U:

1. CHF in horizontal one g_e flow is associated with appreciable stratification resulting from strong buoyancy and weak inertia
2. CHF in microgravity at drastically different in interfacial structure compared to one g_e

High U:

1. CHF in horizontal one g_e flow is no longer stratified as strong inertia dwarfs buoyancy
2. Similar CHF interfacial behavior observed in both microgravity and one g_e



Use separated flow model to determine axial variations of:

- U_{gl}, U_{g2} Near-wall vapor layer velocities
- U_f Liquid layer velocity
- δ_1, δ_2 Near-wall vapor layer thicknesses

Critical interfacial wavelength

$$k_c = \frac{2\pi}{\lambda_c} = \frac{\rho_f'' \rho_g'' (U_g - U_f)^2}{2\sigma(\rho_f'' + \rho_g'')} + \sqrt{\left[\frac{\rho_f'' \rho_g'' (U_g - U_f)^2}{2\sigma(\rho_f'' + \rho_g'')} \right]^2 + \frac{(\rho_f - \rho_g) g_n}{\sigma}}$$

where $\rho_f'' = \rho_f \coth(2\pi H_f / \lambda_c)$ and $\rho_g'' = \rho_g \coth(2\pi H_g / \lambda_c)$

Earth Gravity: $g_{n,1} = g_e \cos\theta$ and $g_{n,2} = g_e \cos(\theta + \pi) = -g_e \cos\theta$

Microgravity: $g_{n,1} = g_{n,2} = \mu g_e \approx 0$ ➔ $\lambda_c = \frac{2\pi\sigma(\rho_f'' + \rho_g'')}{\rho_f'' \rho_g'' (U_g - U_f)^2}$

Mean pressure difference across wetting front

$$\overline{P_f - P_g} = \frac{4\pi\sigma\delta}{b\lambda_c^2} \sin(b\pi)$$

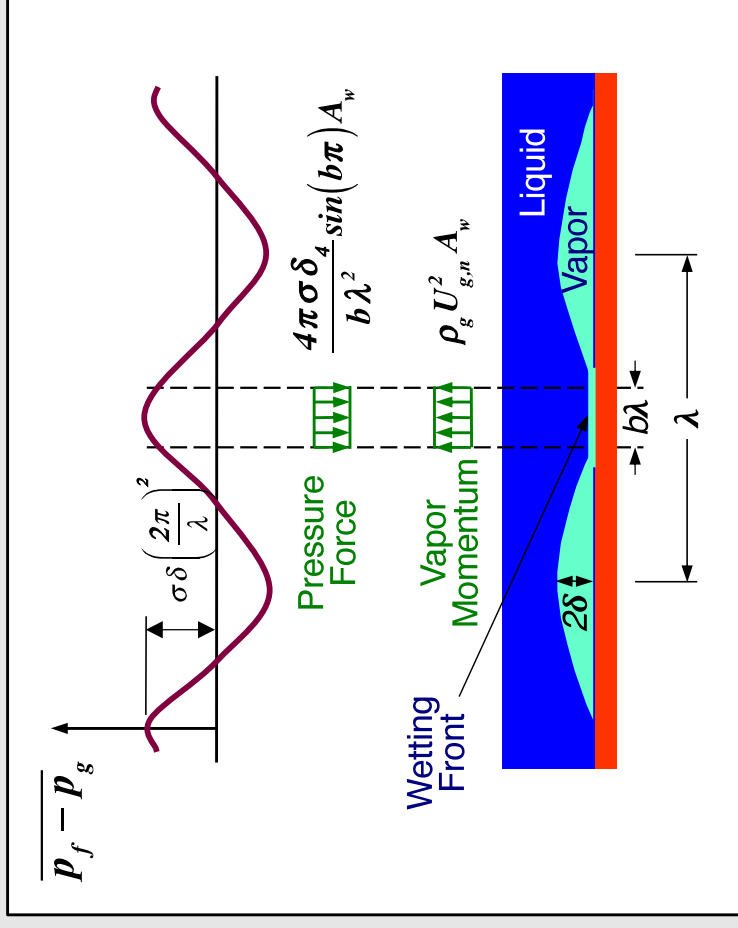
where $b = 0.20$ is ratio of wetting front length to wavelength

Interfacial lift-off criterion

$$\overline{P_f - P_g} = \rho_g \left[\frac{q_w''}{\rho_g h_{fg}} \right]^2$$

Surface energy balance

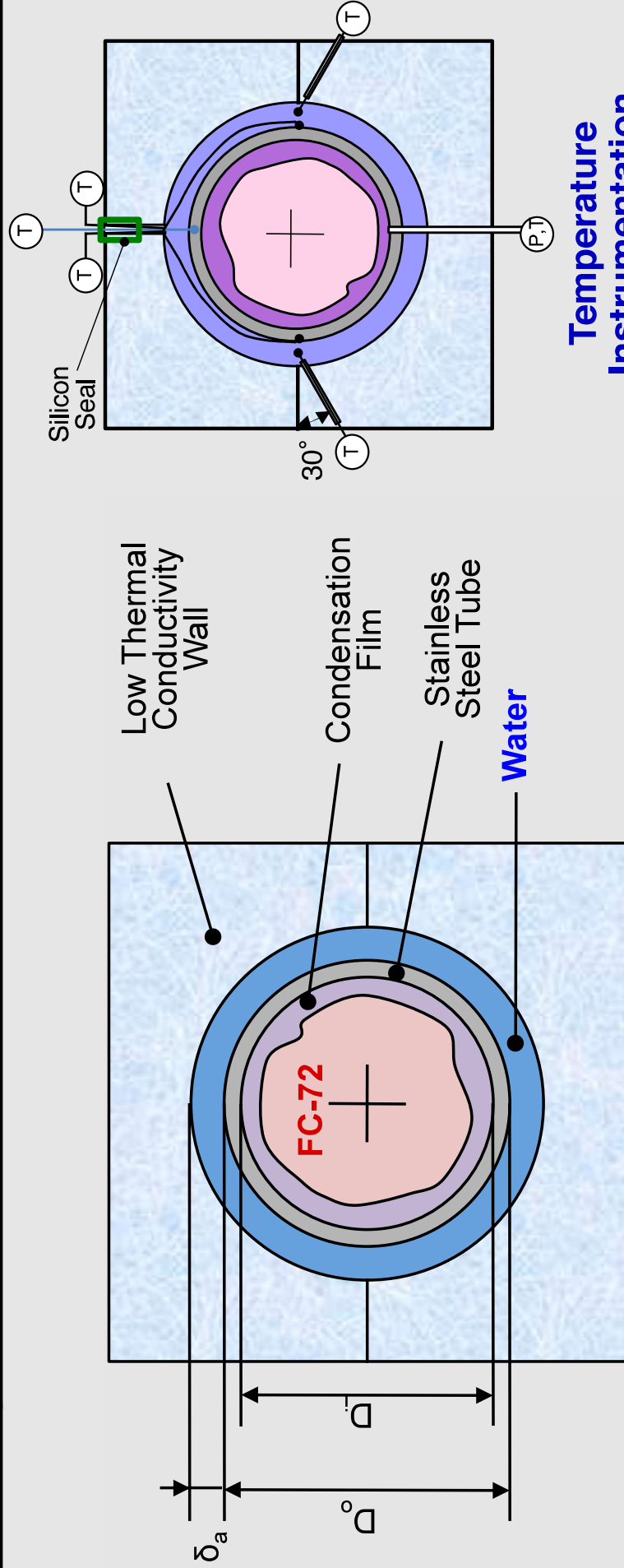
$$q_m'' = b q_w''$$



Critical heat flux

$$q_m'' = \rho_g \left(c_{p,f} \Delta T_{sub,in} + h_{fg} \right)^{1/2} \left[\frac{4\pi\sigma b \sin(b\pi)}{\rho_g} \right]^{1/2} \frac{\delta^{1/2}}{\lambda_c |z^*|}$$

***Condensation Module for
Heat Transfer Measurements (CM-HT)
&
Condensation Module for
Flow Visualization (CM-FV)***



Temperature Instrumentation

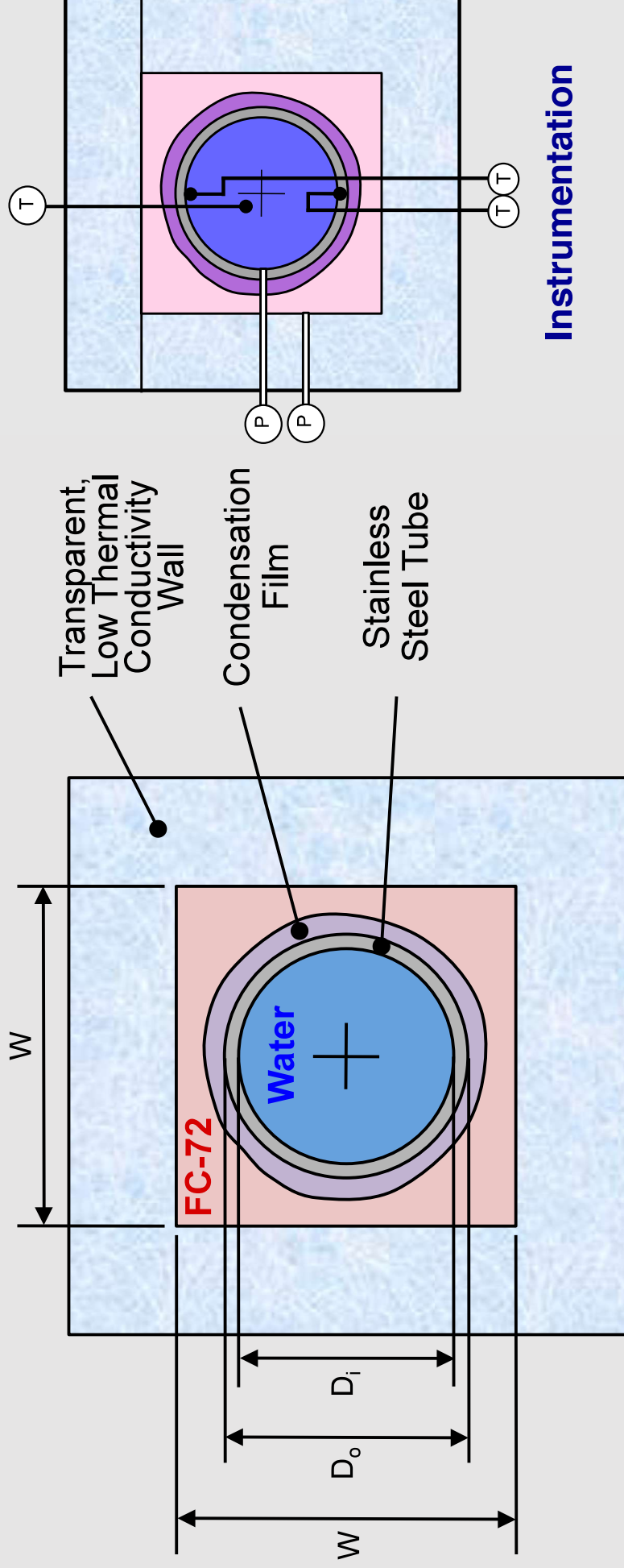
- CM-HT is designed to simulate flow condensation occurring naturally within actual condensation tubes
- FC-72 vapor supplied at inlet rejects heat to external water flow and condenses into gradually thickening annular liquid film
- Wall temperature measurements available externally on water side to avoid disrupting liquid film motion; this allows installing large number of thermocouples spanning entire condensation length
- Metal condensation tube precludes video access to interfacial structure of condensation film.

FC-72 side: **Water side:**

$D_i = 7.12 \text{ mm}$ $\delta_a = 2.38 \text{ mm}$

$t_{\text{wall}} = 0.41 \text{ mm}$

$L = 574.6 \text{ mm}$

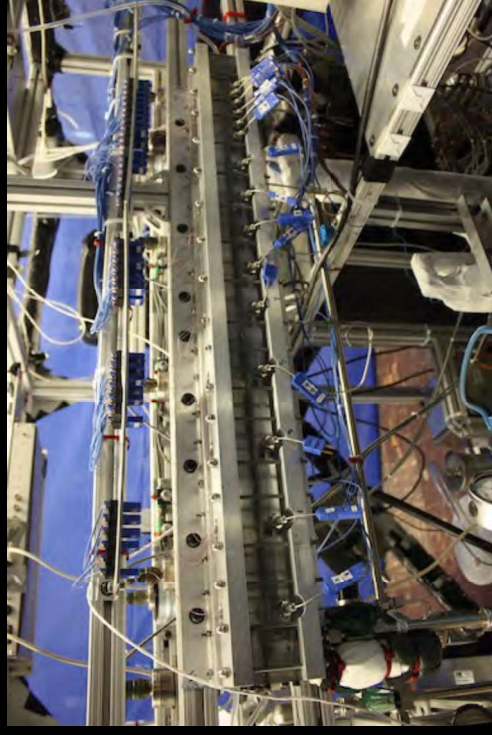
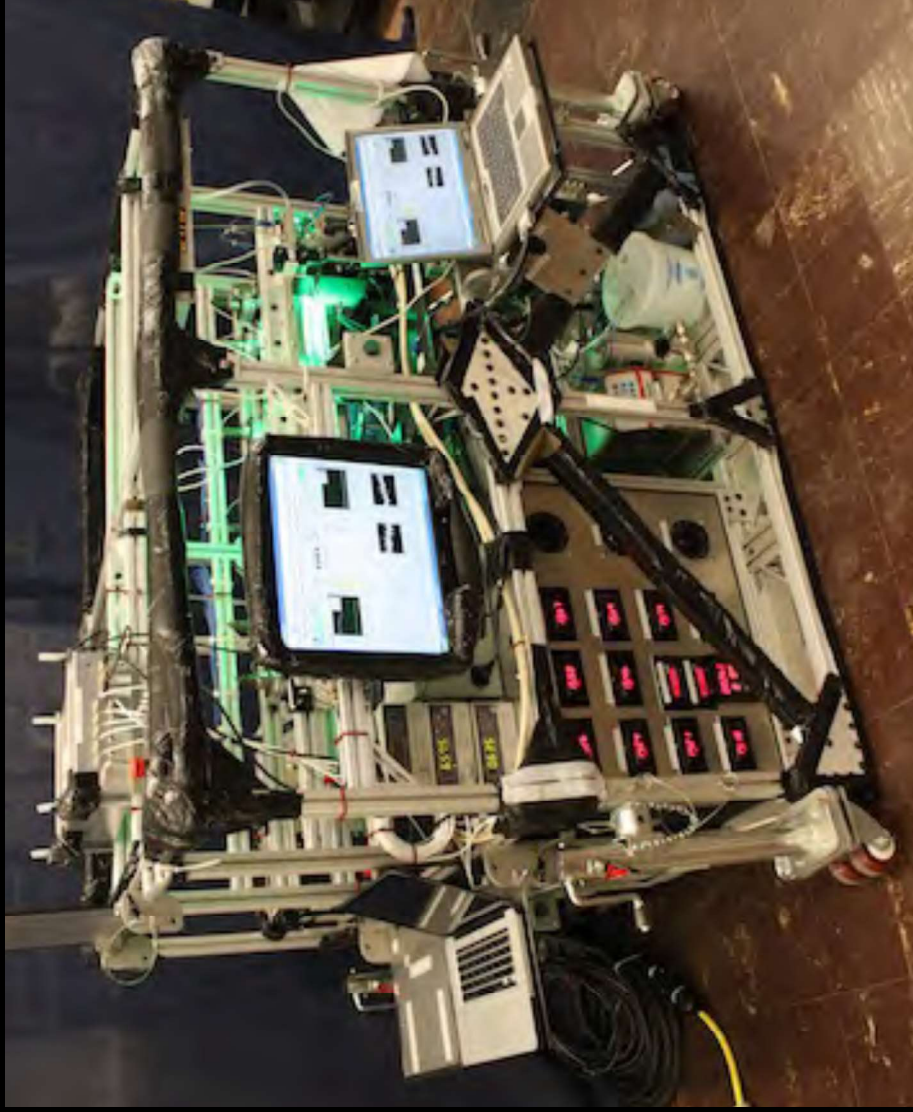


Instrumentation

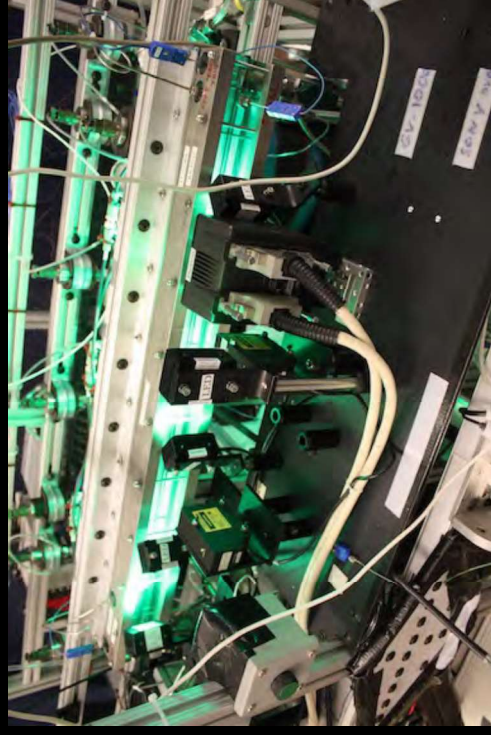
- CM-FV is designed to facilitate video access to interfacial flow structure of condensation film
- Dimensions are based on equivalency of condensation length between CM-FV and CM-HT, with nPFH vapor superficial velocity ratio in CM-FV to that in CM-HT of 0.48
- Condensation occurs on tube outside as FC-72 vapor condenses into gradually thickening liquid film
- Wall temperature measurements available internally on water side to avoid disrupting liquid film motion
- Small inner diameter limits number of thermocouples for wall temperature measurements
- Primary function of CM-FV is to capture interfacial flow structure rather than detailed wall temperature measurements

FC-72 side: **Water side:**
 $W = 11.13 \text{ m}$ $D_i = 7.14 \text{ mm}$
 $L = 587 \text{ mm}$ $t_{\text{wall}} = 0.406 \text{ mm}$

Condensation Rig

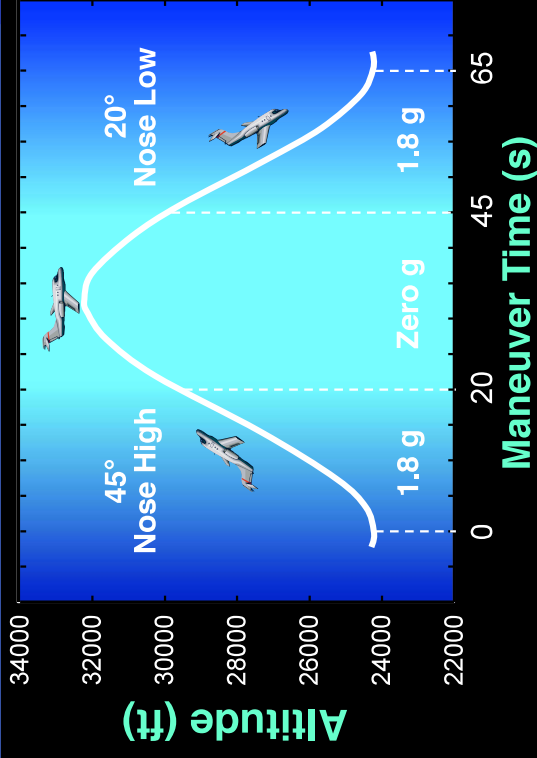


**CM-HT: Condensation
Module for Heat Transfer
Measurements**



**CM-FV: Condensation
Module for Flow
Visualization**

**CM-HT and CM-FV were successfully tested
in parabolic flight**



Microgravity
 CM-FV interfacial flow structure video

G = 90.2 kg/m²s

($X_{e,in} = 0.73$, $G_w = 678$ kg/m²s)

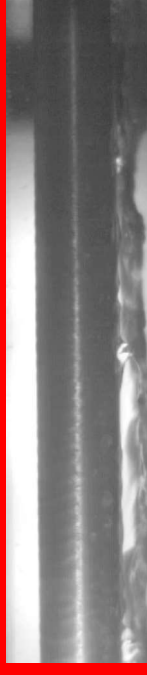


z = 58 mm, 4000 fps

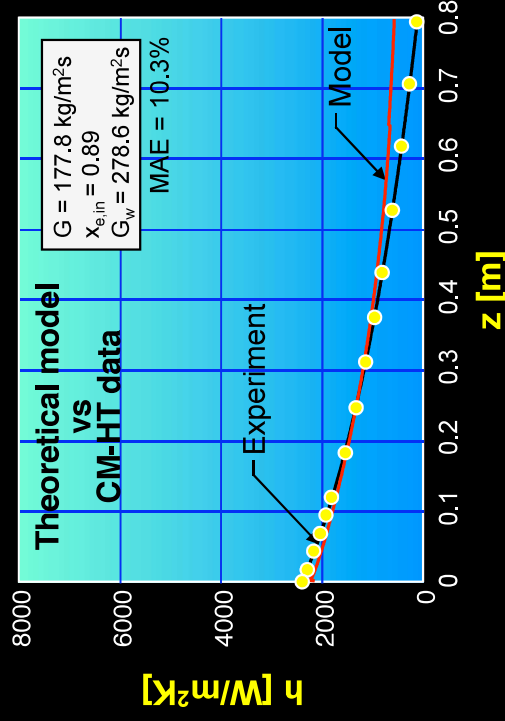
Hyper-G

G = 68.0 kg/m²s

($X_{e,in} = 0.4$, $G_w = 601$ kg/m²s)

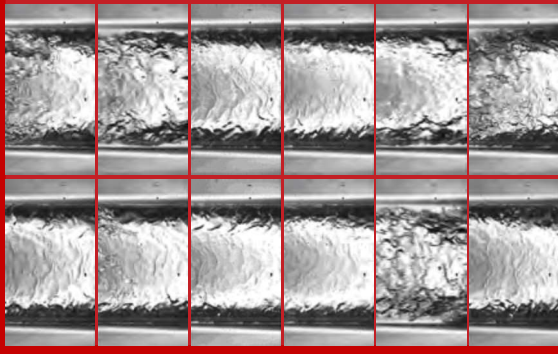


z = 351 mm, 4000 fps

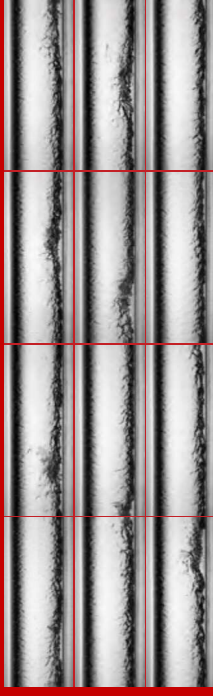
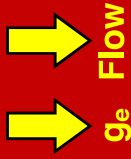


Key limitation of both condensation modules is difficulty achieving steady state during parabolas

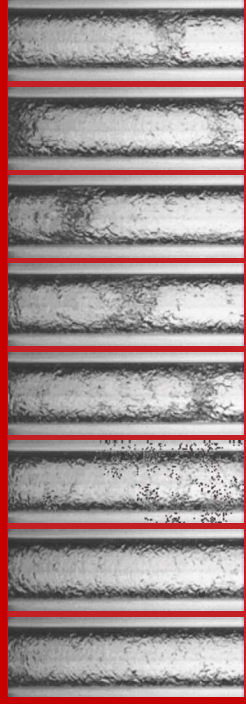
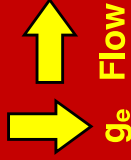
Heat Transfer in Annular Condensation at One-G



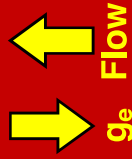
Vertical Downflow



Horizontal Flow



Vertical Upflow



Ultimate Goal:

Develop experimentally validated correlations, theoretical models, and CFD models for both flow boiling and flow condensation

Computational Models used:

- ❑ **Volume-of-fluid (VOF) model**
Tracks interface between liquid and vapor, involves interface shape reconstruction
- ❑ **Shear-stress transport (SST) k- ω model**
Accounts for turbulent effects including interfacial damping
- ❑ **Lee model**
Predicts interfacial mass and heat transfer resulting from phase change, evaporation and condensation
- ❑ **Continuum surface force (CSF) model**
Incorporates surface tension in VOF calculation, considering the pressure jump across the surface

Forces Acting Bubble:

Forces parallel to surface

$$\sum F_z = F_{s,z} + F_{du,z} + F_{gs} + F_b = \rho_g V_b \frac{du_z}{dt}$$

Forces normal to surface

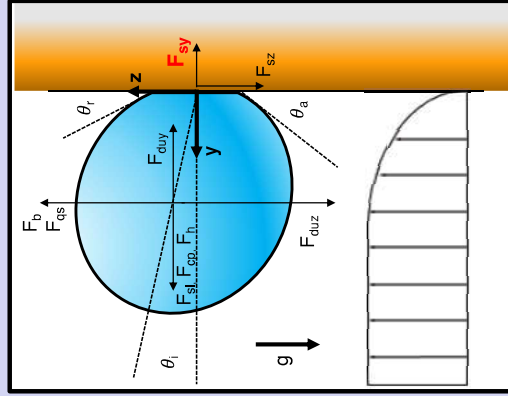
$$\sum F_y = F_{s,y} + F_{du,y} + F_{sl} + F_h + F_{cp} = \rho_g V_b \frac{du_y}{dt}$$

Shear-lift coefficient

$$C_L = \frac{F_{sl}}{\frac{1}{2} \rho_f U_r^2 \pi a^2} = 3.877 G_s^{1/2} \times \left[\text{Re}_b^{-m/2} + (0.344 G_s^{1/2})^{m-1} \right]$$

Dimensionless shear rate

$$G_s = \left| \frac{dU_x}{dy} \right| \frac{a}{U_r}, \quad a = d_b/2$$



Governing Equations:

- ❑ **Continuity of volume fraction**

$$\frac{\partial \alpha_f}{\partial t} + \nabla \cdot (\alpha_f \vec{u}_f) = \frac{1}{\rho_f} \sum (\dot{m}_{gf} - \dot{m}_{fg})$$

$$\frac{\partial \alpha_g}{\partial t} + \nabla \cdot (\alpha_g \vec{u}_g) = \frac{1}{\rho_g} \sum (\dot{m}_{fg} - \dot{m}_{gf})$$

- ❑ **Momentum**

$$\frac{\partial}{\partial t} (\rho \vec{u}) + \nabla \cdot (\rho \vec{u} \vec{u}) = -\nabla P + \nabla \cdot \left[\mu (\nabla \vec{u} + \nabla \vec{u}^T) \right] + \vec{F}$$

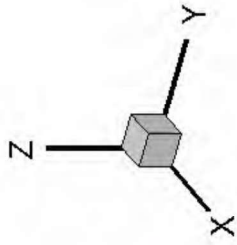
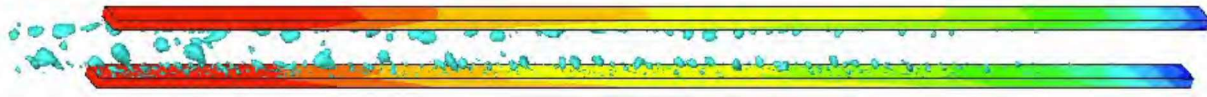
- ❑ **Energy**

$$\frac{\partial}{\partial t} (\rho E) + \nabla \cdot (\vec{u} (\rho E + P)) = \nabla \cdot (k_{eff} \nabla T) + S_h$$

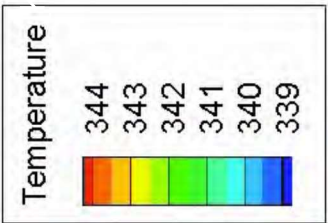
- ❑ **Turbulent kinetic energy and dissipation transport**

$$\frac{\partial}{\partial t} (\rho k) + \nabla \cdot (\rho k \vec{u}) = \nabla \cdot (\Gamma_k \nabla k) + \widetilde{G}_k - Y_k + S_k$$

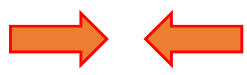
$$\frac{\partial}{\partial t} (\rho \omega) + \nabla \cdot (\rho \omega \vec{u}) = \nabla \cdot (\Gamma_\omega \nabla \omega) + G_\omega - Y_\omega + D_\omega + S_\omega$$



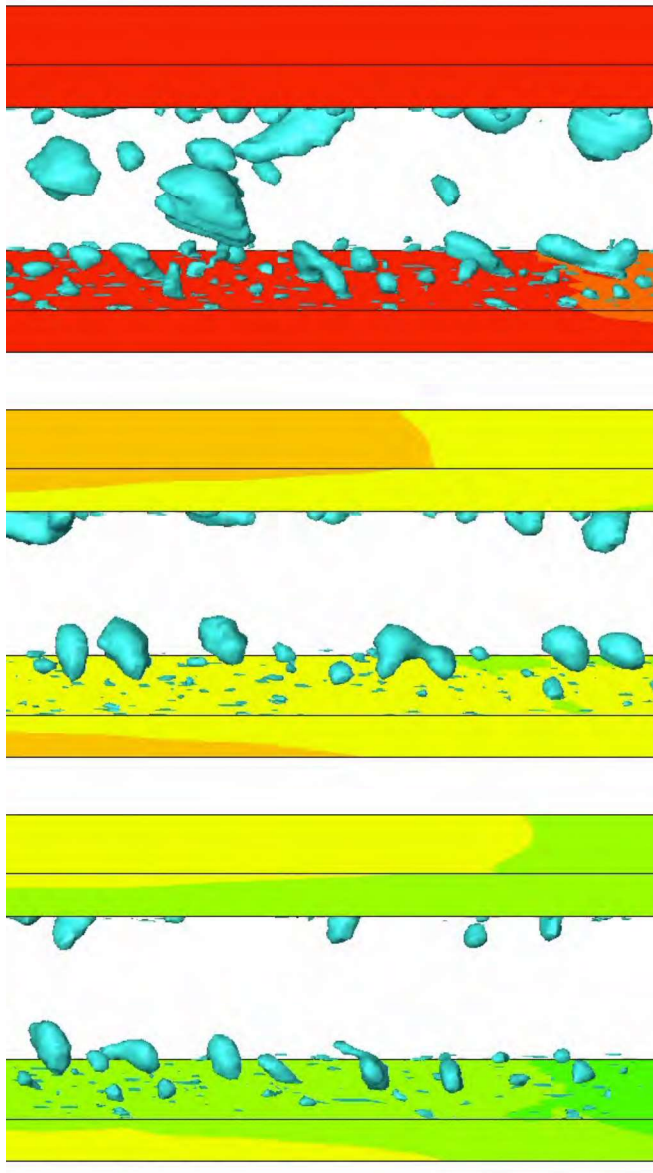
$G = 445.75 \text{ kg/m}^2\text{s}$
 $q'' = 143 \text{ kW/m}^2$
 $\Delta T_{\text{sub}} = 30.81 \text{ }^\circ\text{C}$
 Vertical upflow
 One-G



Gravity

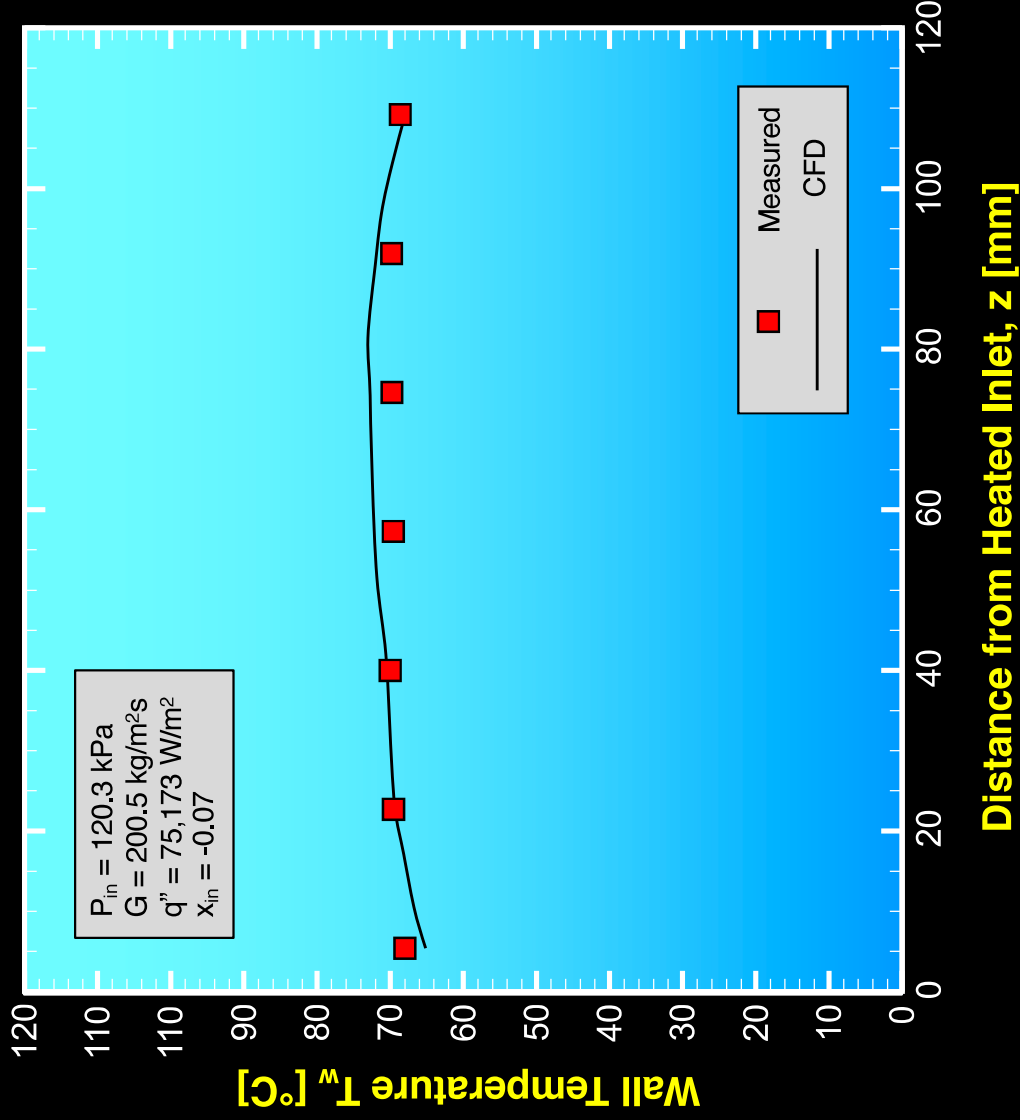


FC-72
Flow



Upstream Middle Downstream

Video frame rate is 5 fps
Individual images in sequence separated by 1 ms

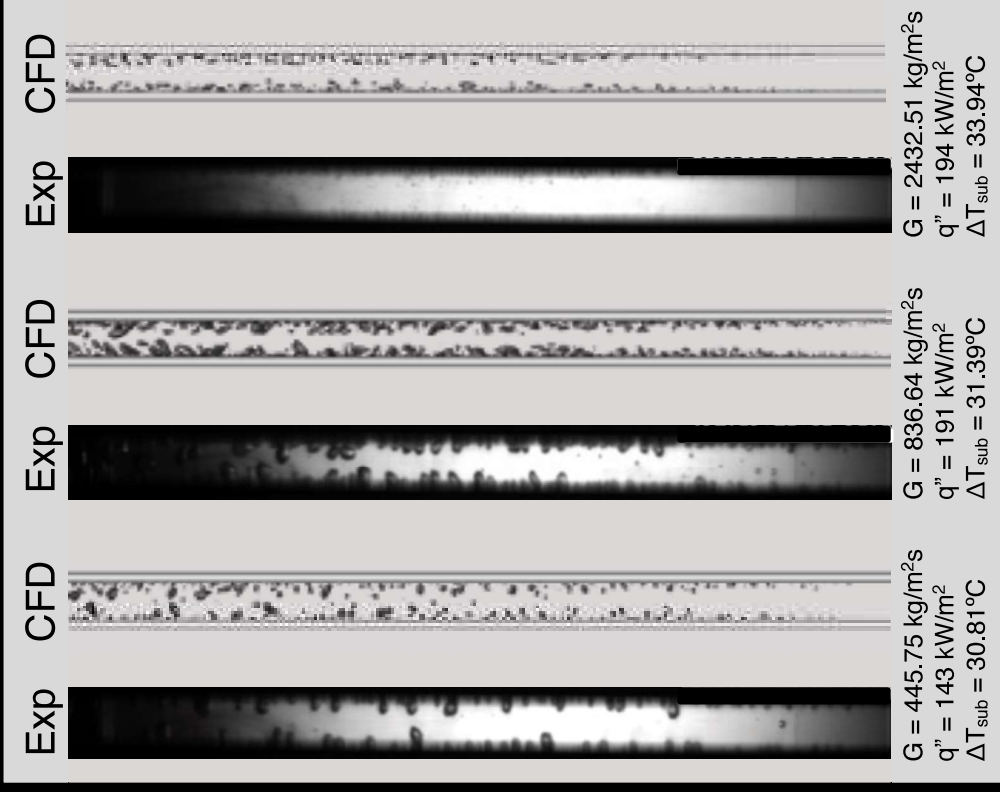


Distance from Heated Inlet, z [mm]

Measured wall temperature

Video-captured interfacial structure

CFD results must be validated against BOTH



Purdue University (16):

Principal Investigator: Issam Mudawar

Zhang, Hui (Ph.D.)
 Kim, Sung-Min (Ph.D.)
 Lee, Hyoung-Soon (Ph.D.)
 Konishi, Christopher (Ph.D.)
 Mascarenhas, Nikhin (Ph.D.)

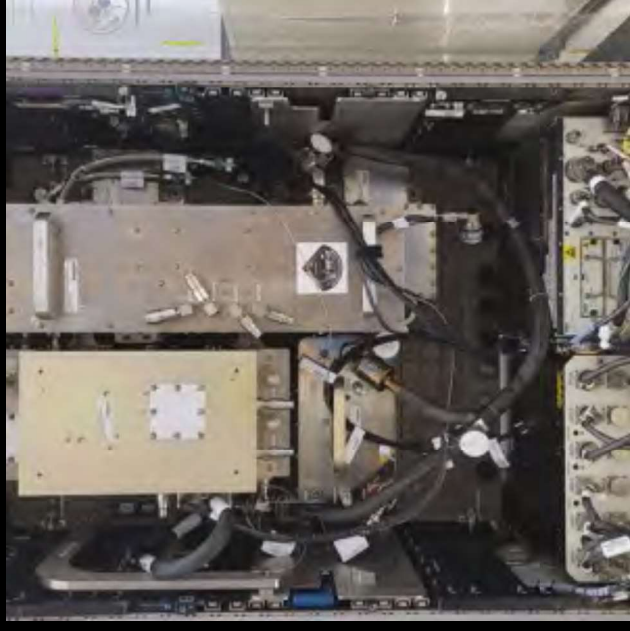
Park, Ilchung (Ph.D.)
 Kharangate, Chirag (Ph.D.)
 Lee, Seunghyun (Ph.D.)
 O'Neill, Lucas (Ph.D.)
 Devahdhanush, V.S. (Ph.D. candidate)

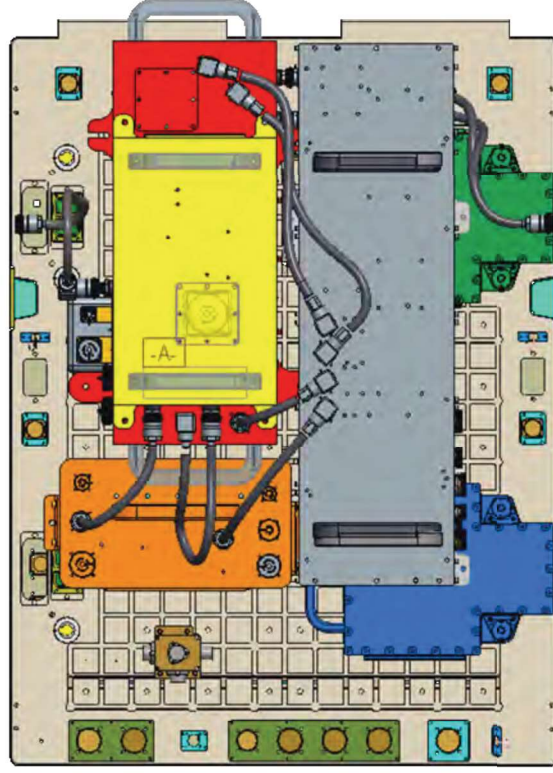
Lee, Jeongmin (Ph.D. candidate)
 Ganesan, Vishwanath (Ph.D. candidate)
 Dandle, Nishad (Ph.D. candidate)
 Kim, Sunjae Kim (Ph.D. candidate)
 Patel, Raj (M.S. candidate)

NASA Glenn (37):

Project Management	
Project Manager	Nancy Hall
Configuration Management	Kathy Kachmar
Configuration Management	Barb Wamsley
FCF	Andrea Marchica
Scheduler	Erin Wood
Science Team	
Co-Principal Investigator	Mojib Hasan
Project Scientist	Henry Nagra
Research Scientist	Balasubramaniam Ramaswamy
Engineering Team	
Chief Engineer	Monica Guzik
Chief Safety Officer	Martin Bradish
AST, S&MA	Brandon White
Lead Systems Engineer	Tim Schuler
V&V Lead	Mark Sorrells
AI&T Engineer	Mark Lefebvre
Diagnostics	Chris Lant
Diagnostics Discipline Lead & TMA Product Lead	Jeff Mackey
Electrical	Glenn Lindamood

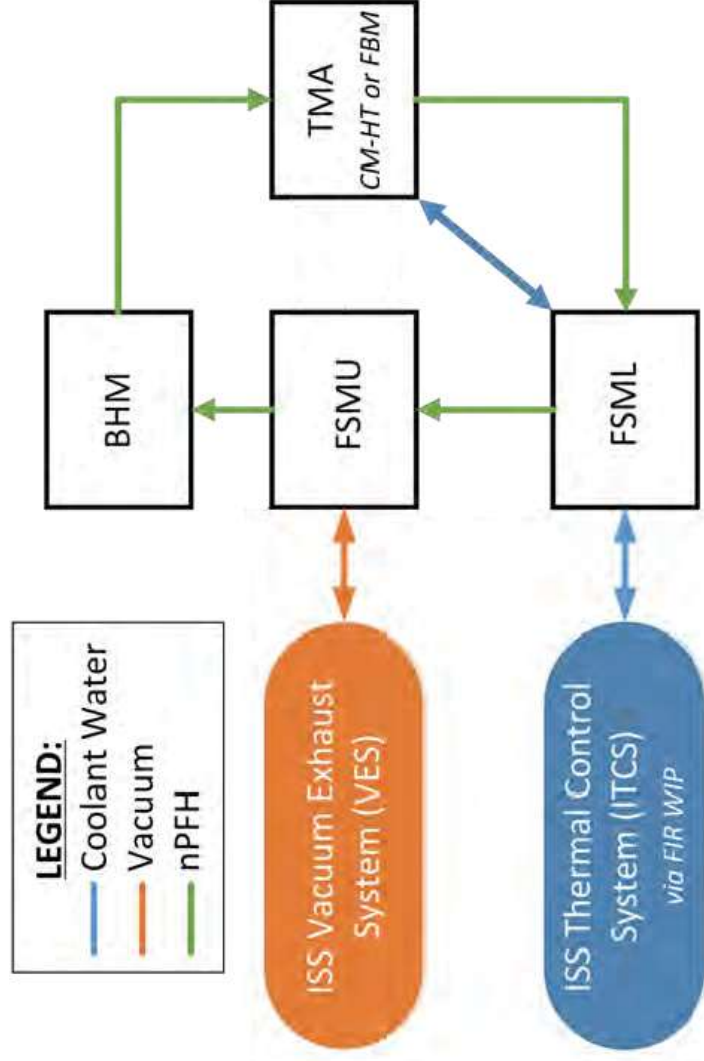
Electrical	Nick Purpera
Electrical	Issam Boukabou
Electrical Lead	Hector Dominguez
Fluid Systems Discipline Lead	Jesse Defiebre
Payload Lead	Monica Guzik
Fluids Integrated Rack Support	Chris Rogers
Mission Ops	Chanisara Netsuwan
Fluids Integrated Rack Support	Brandon Wagner
Mechanical Designer Discipline	Dave Nawrocki
RDAQM Product Lead	Bob Dolesh
Software (Flight Software)	Phil Gonia
Software Product Lead/SW Discipline Lead	Rochelle May
Thermal Discipline Lead	Erik Stalcup
Safety and Mission Assurance	
System Safety Lead	Deboshri Sadhukan
Software Safety Mgr./Software QA	Rick Plastow
Materials and Processes	Logan Micham
Quality Assurance Engineer	Brian Loucks
Risk Management	Bennett Straker
Bldg 110 Lab Technicians	
Mechanical Engineering	Dan Gedeon
Electronics Technician	Bob Paulin
Electronics Technician	Tiffany Vanderwyst





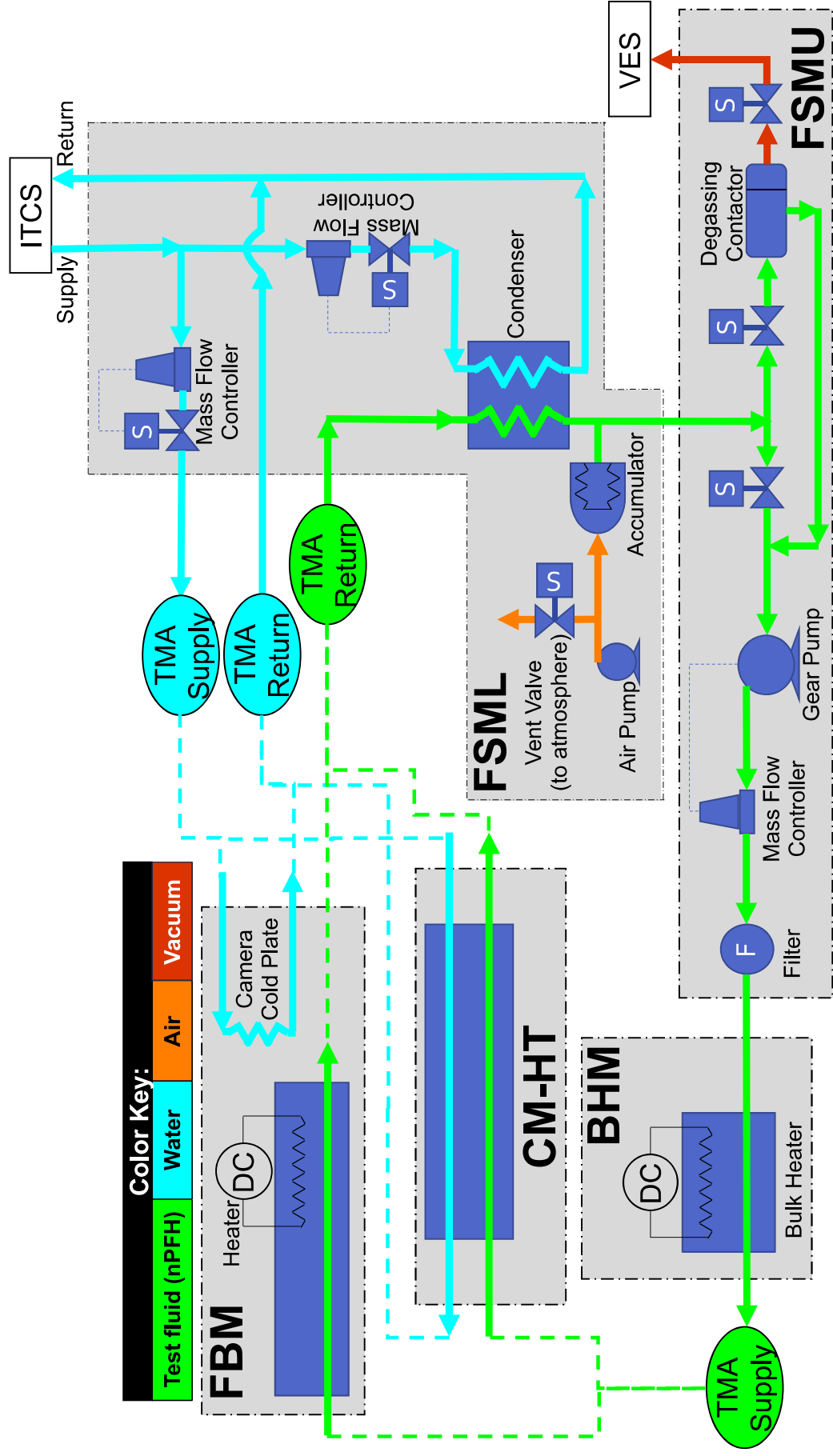
FBCE Modules:

- ▶▶▶ **BHM** – Bulk Heater Module
- ▶▶▶ **FSMU** – Fluids System Module - Upper
- ▶▶▶ **FSML** – Fluids System Module - Lower
- ▶▶▶ **RDAQM 1** – Remote Data Acquisition Module 1
- ▶▶▶ **RDAQM 2** – Remote Data Acquisition Module 2
- ▶▶▶ **TMA** – Test Module Assembly (1 of 2 installed):
 - ▶▶▶ **FBM** – Flow Boiling Module
 - ▶▶▶ **CM-HT** – Condensation Module - Heat Transfer

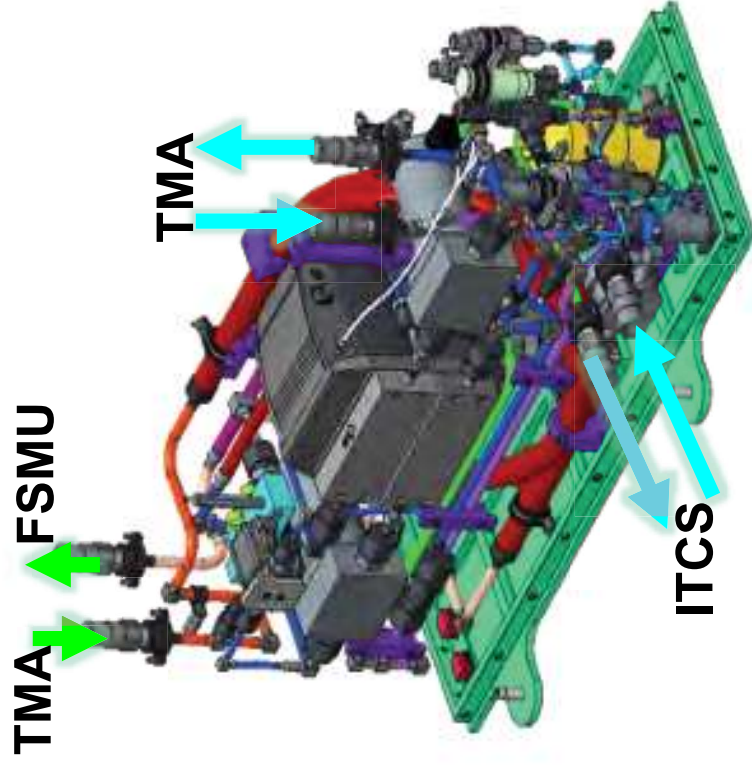


FIR Provided Hardware:

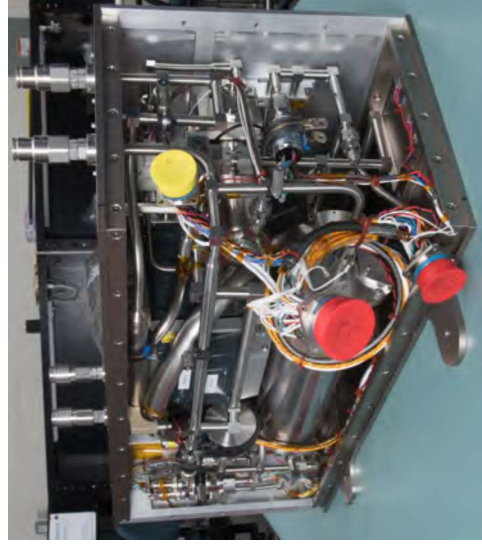
- **SAMS** – Space Acceleration Measurement System
- **CCU** – Confocal Control Unit (on back of rack)
- **IPSU-CL** – Imaging Processing Storage Unit – Camera Link (on back of rack)



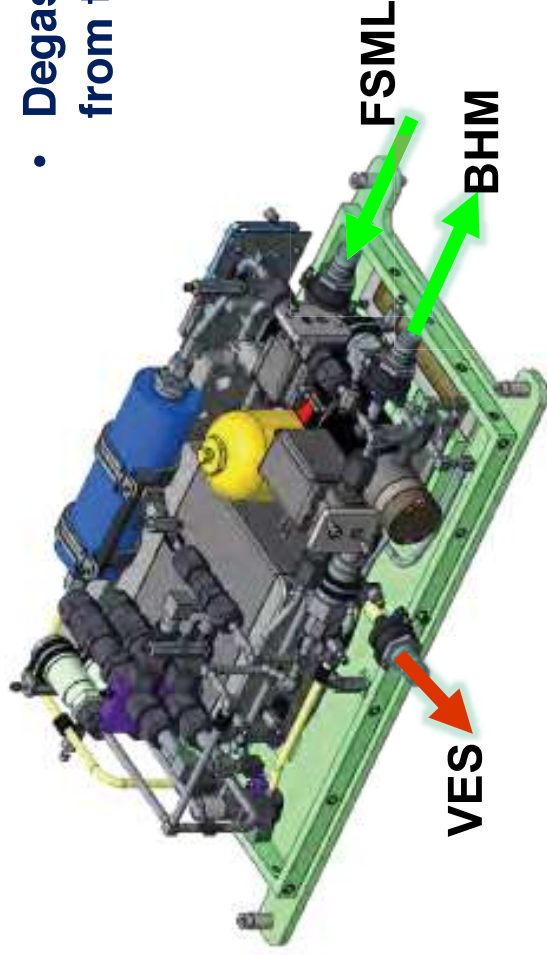
- Provides primary cooling for the test fluid exiting the test section, and the test section itself
- System pressure set by pressurizing or venting the air-side of a bellows accumulator



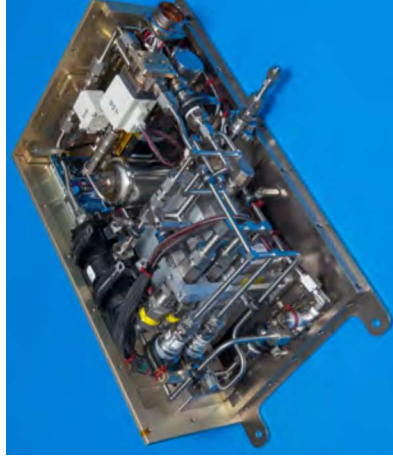
Color Key:	
Test fluid (nPFH)	Water
	Air



- Mass flow controller drives a gear pump to provide flow throughout the closed loop system
- Multiple controls in place to prevent over-pressurization
- Degassing contactor removes dissolved gases from test fluid when membrane exposed to vacuum



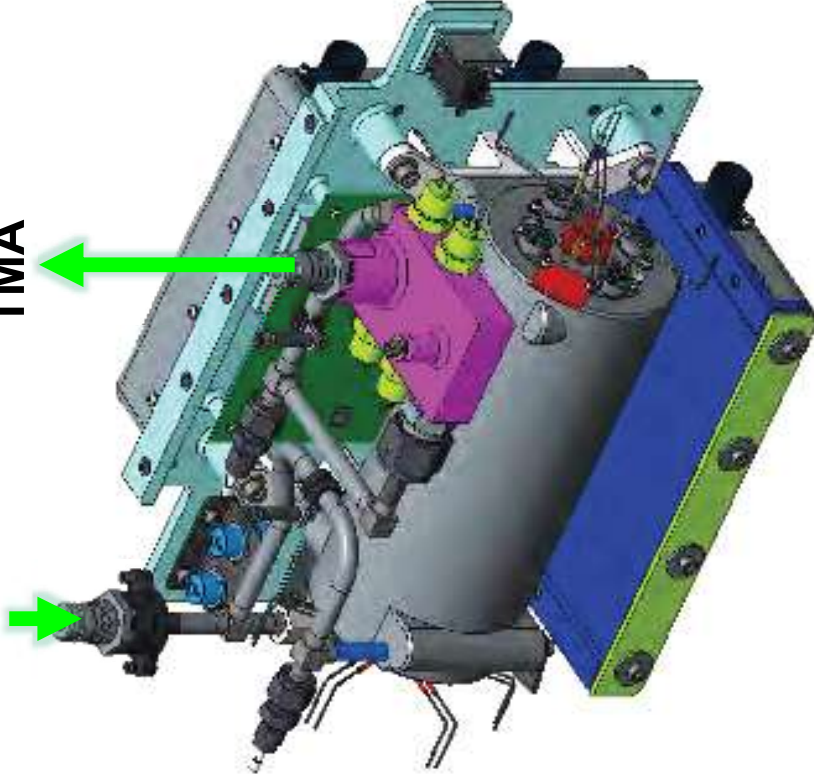
Color Key:	
Test fluid (nPFH)	Vacuum



- Primary source of heating to condition test fluid to required test section inlet conditions
- Three 120V primary heaters and three 28V booster heaters can be operated at any time, with backup heaters available

FSMU

TMA



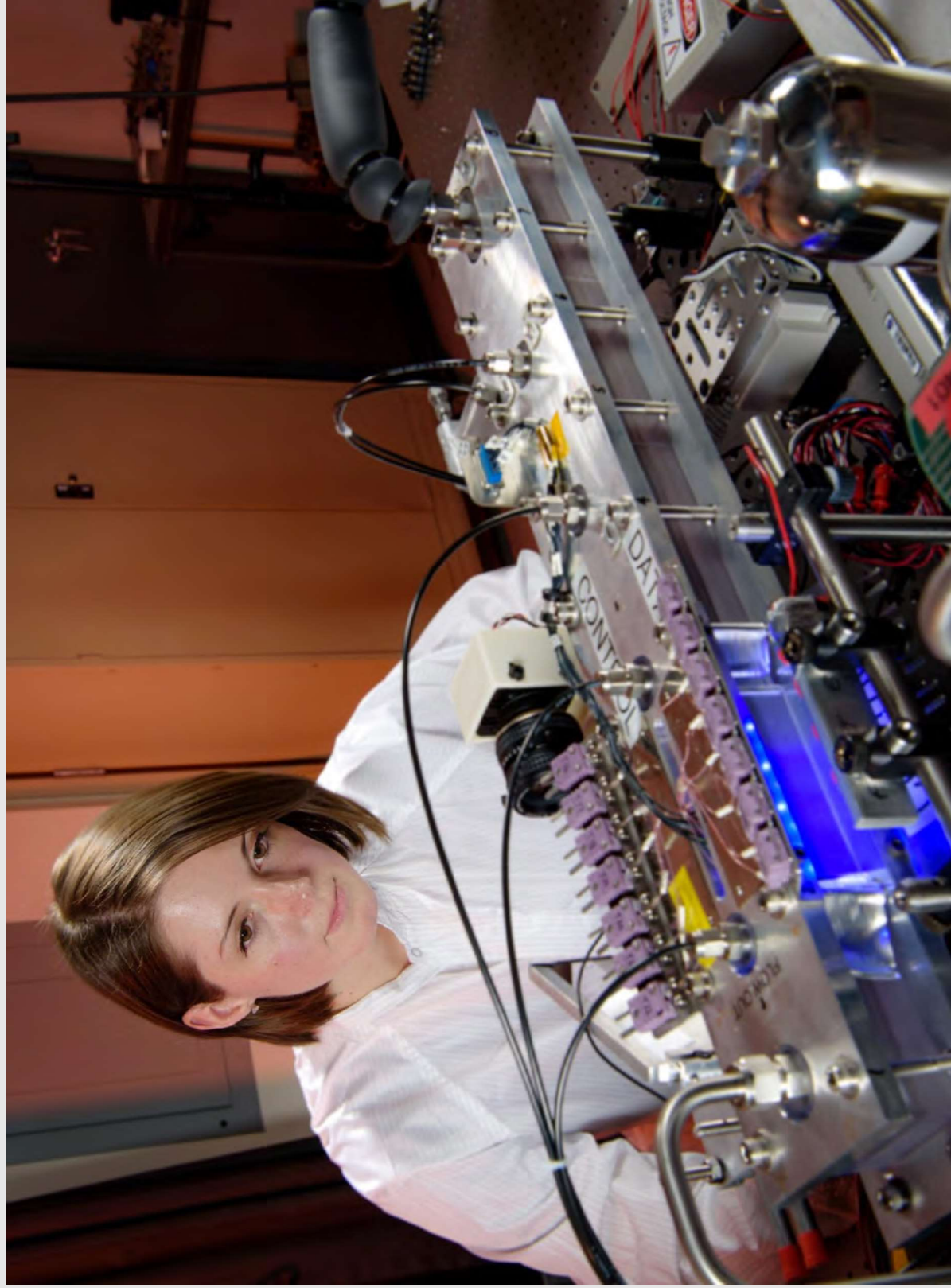
Color Key:

Test fluid (nPFH)

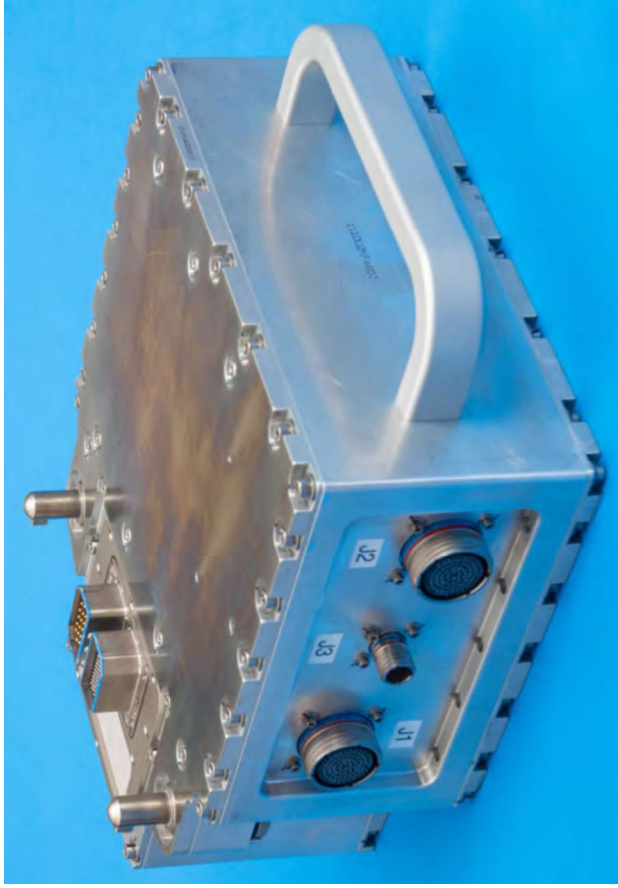




Flow Boiling Module (FBM)

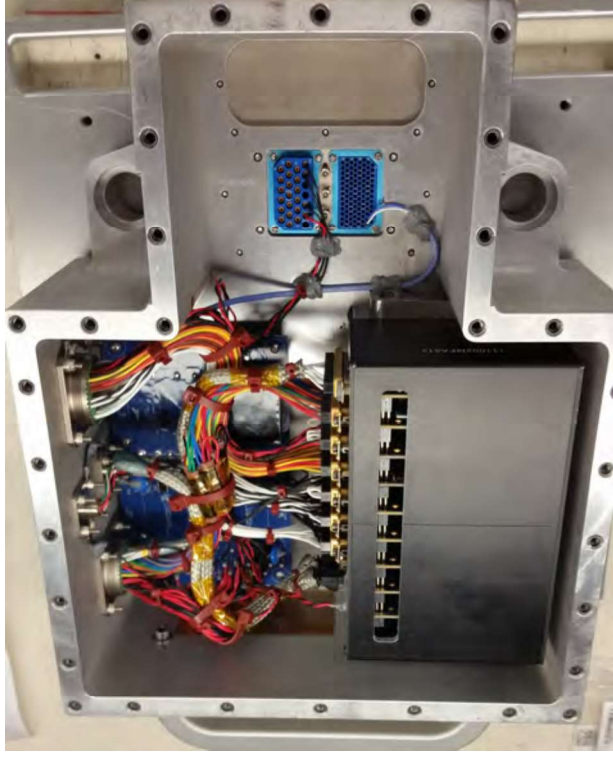


Remote Data Acquisition Module 1 (RDAQM1)



UEI Data Cubes (Thermocouple Signal Conditioning)

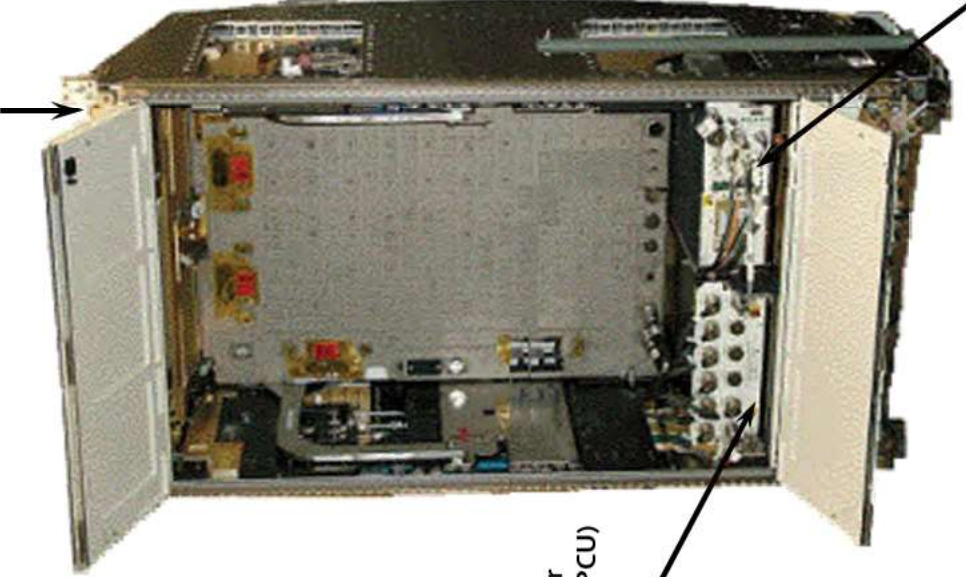
Remote Data Acquisition Module 2 (RDAQM2)



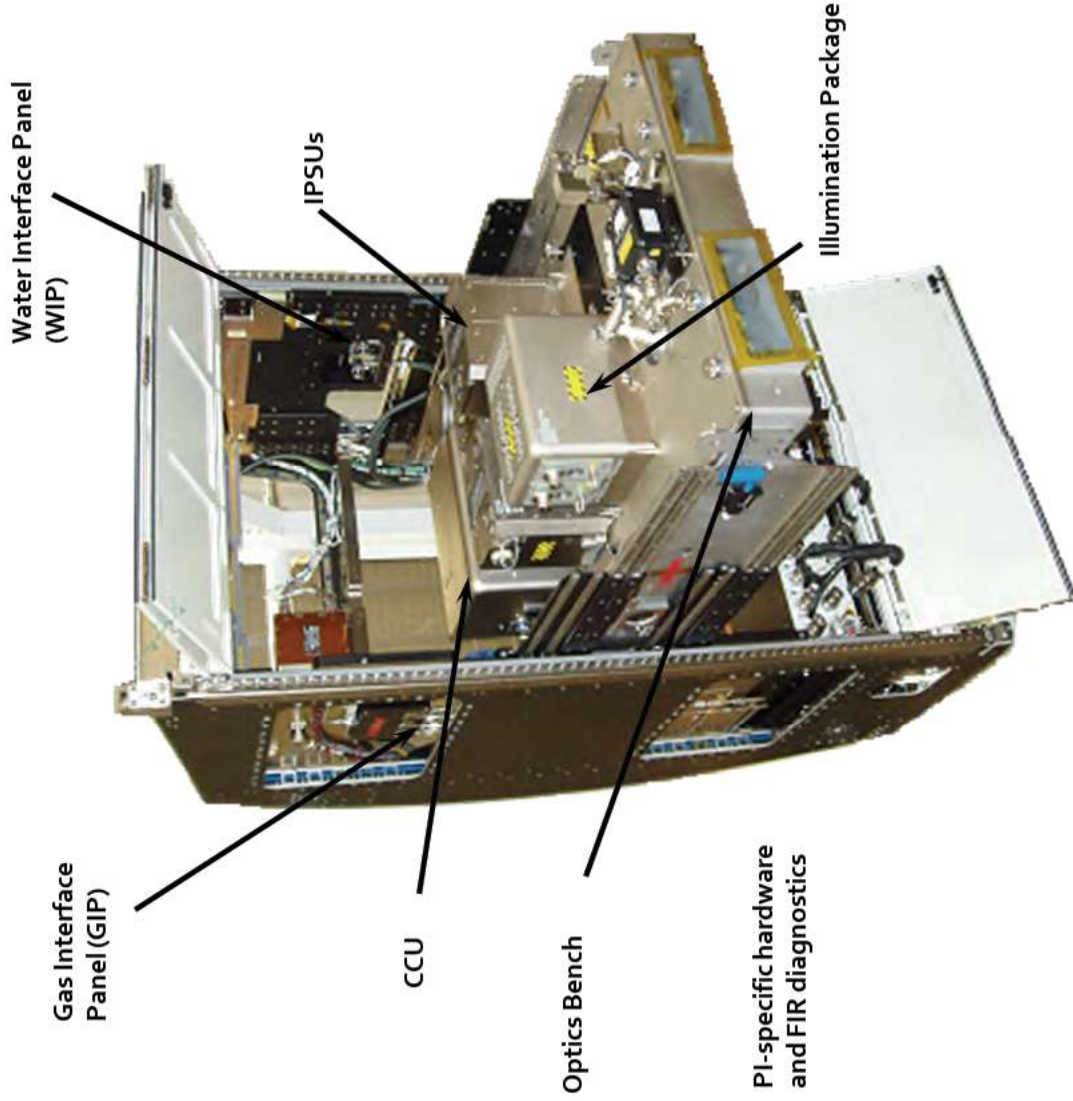
UEI Data Cube and Custom Sensor Supply Printed
Circuit Board
(Signal Conditioning and Power Distribution)

Environmental Control (ECS)

- Air Thermal Control
- Fire Detection & Suppression
- Water Thermal Control
- Gas Interfaces (GN₂, VES, VRS)



Electrical Power Control Unit (EPCU)



Water Interface Panel (WIP)

Gas Interface Panel (GIP)

CCU

IPSUs

Optics Bench

PI-specific hardware and FIR diagnostics

Illumination Package



NG-16 Cygnus

SS-Elilson Onizuka

Operator
Northrop Grumman

Launch site
Launch Pad 0A
Wallops Island, Virginia

Launch vehicle
Antares 230+

ISS docking location
Unity nadir

Cargo mass
~3,700 kilograms

What's aboard?
(Not an exhaustive list)

Pressurized Cargo Module

- ▶ Cardinal Muscle evaluation
- ▶ Redwire Regolith Print study
- ▶ The Flow Boiling and Condensation Experiment
- ▶ Kentucky Re-Entry Probe Experiment
- ▶ Four Bed CO2 Scrubber
- ▶ Blob investigation
- ▶ Slingshot Deployment System
- ▶ ISS Power Augmentation Mod Kit
- ▶ Upgraded acrylic scratch panels for Cupola windows
- ▶ Airlock Stowage Platform

Service Module

- ▶ 2 UltraFlex solar arrays
- ▶ Nanorecs External
- ▶ CubeSat Deployer

6.39 meters

3.1 meters

SEA *Space Environment Assessment*





**Largest Cygnus cargo ever
launched to ISS (3,723 kg)**



Launch (August 10, 2021, 6:01 pm ET)



Arrival at ISS (August 12, 2021, 6:10 am ET)

