



# ICAM 2021

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## Validation and application of crystal plasticity simulations to study effect of process-specific defects in additively manufactured polycrystalline materials

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## Saikumar “Sai” Yeratapally

### Work Experience:

Research engineer at National Institute of Aerospace (NIA) (10/2017- current)

Post-doctoral Research Associate at NIA (3/2016 – 10/2017)

### Education:

Ph.D. in Aeronautics and Astronautics Engineering from Purdue University (12/2015)

M.S. in Mechanical Engineering from Carnegie Mellon University (12/2010)

B.E. (Honors) in Mechanical Engineering from Birla Institute of Technology and Science (Goa, India) (8/2009)

### Research Interests:

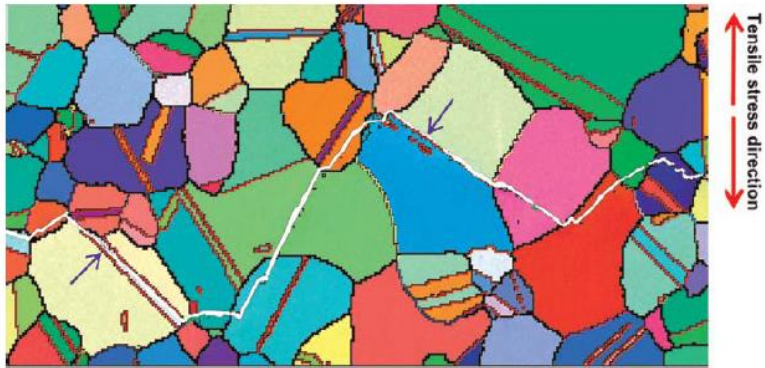
Microstructure-performance linkage using crystal plasticity models

Effect-of-defects in additively manufactured polycrystalline materials



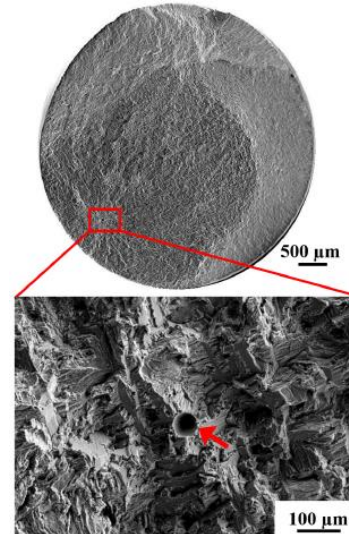
- Fatigue crack initiation (FCI) in polycrystalline materials is primarily dependent on microstructure, inclusion and defect attributes, in addition to other factors

*FCI at twin boundaries*



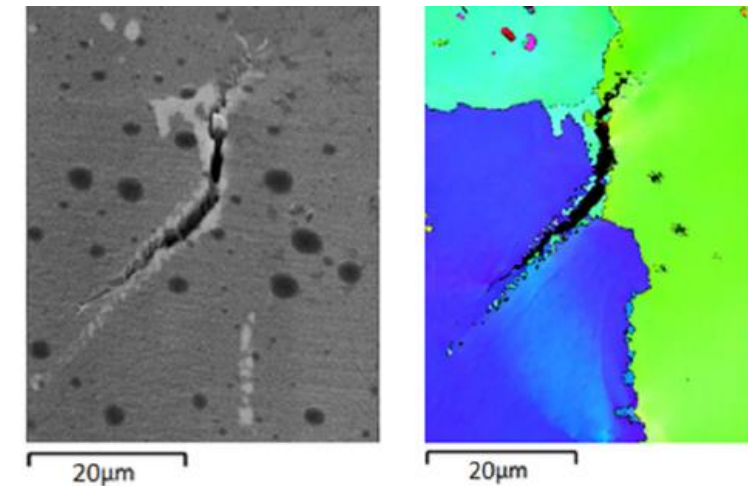
*Jiang et al. (2015)*

*FCI at pore*



*Shamir et al. (2020)*

*FCI at inclusion*

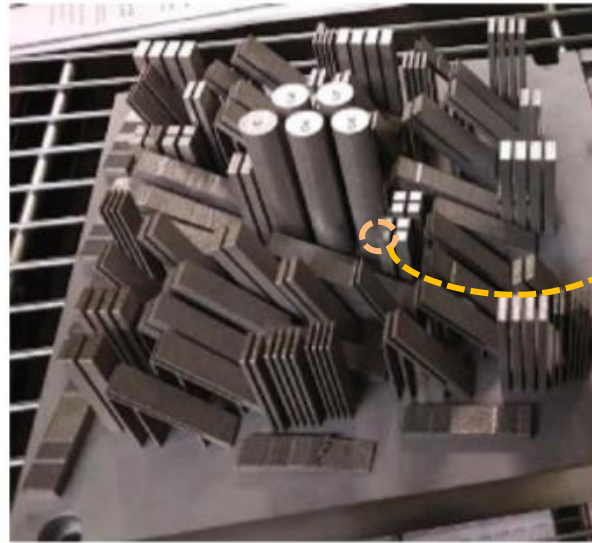


*Yeratapally et al. (2017)*

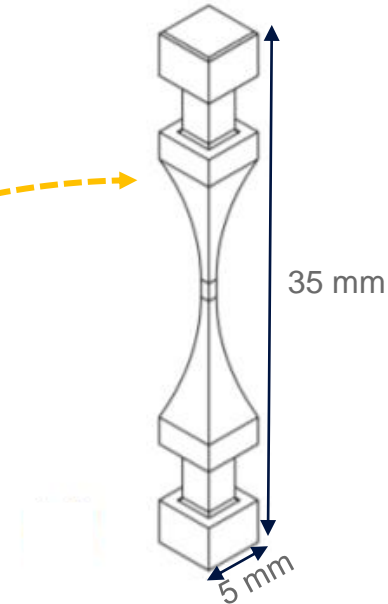
- Linking defect/microstructure attributes to failure mechanisms and hence performance is essential for rapid qualification
- Crystal plasticity (CP) simulations provide a platform to quantitatively link defect/microstructure attributes to performance
- Validation of CP models is important to be able to quantitatively understand the underpinning mechanisms of crack initiation

- Additive manufacturing (AM) modeling challenge
  - Comparing crystal plasticity finite element (CPFE) predictions with high-energy X-ray measurements
- CP-based investigation of process-specific defects Ti-6Al-4V alloy

*Final build*



*Fully machined tensile coupon*



**Material / AM Process:** Inconel 625 (IN625) produced through Laser powder-bed fusion (L-PBF)

**Machine:** EOS M280

**Powder:** Commercially available IN625 gas atomized powder

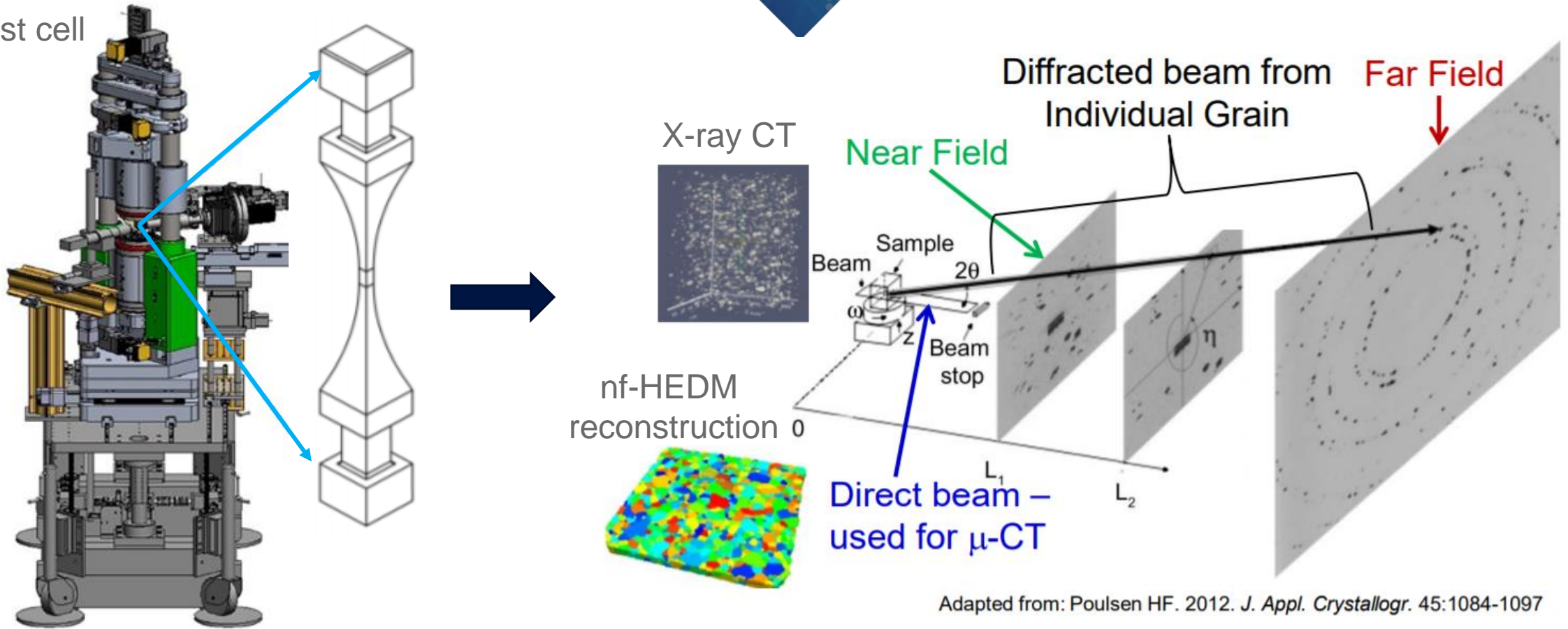
**Processing parameters:** Nominal processing parameters

**Machining:** The sample was fully machined by wire electrical discharge machining (EDM)

**Post processing:** Stress relieved (SR)+ heat treated (HT)+ hot isostatic pressing (HIP), no surface treatment

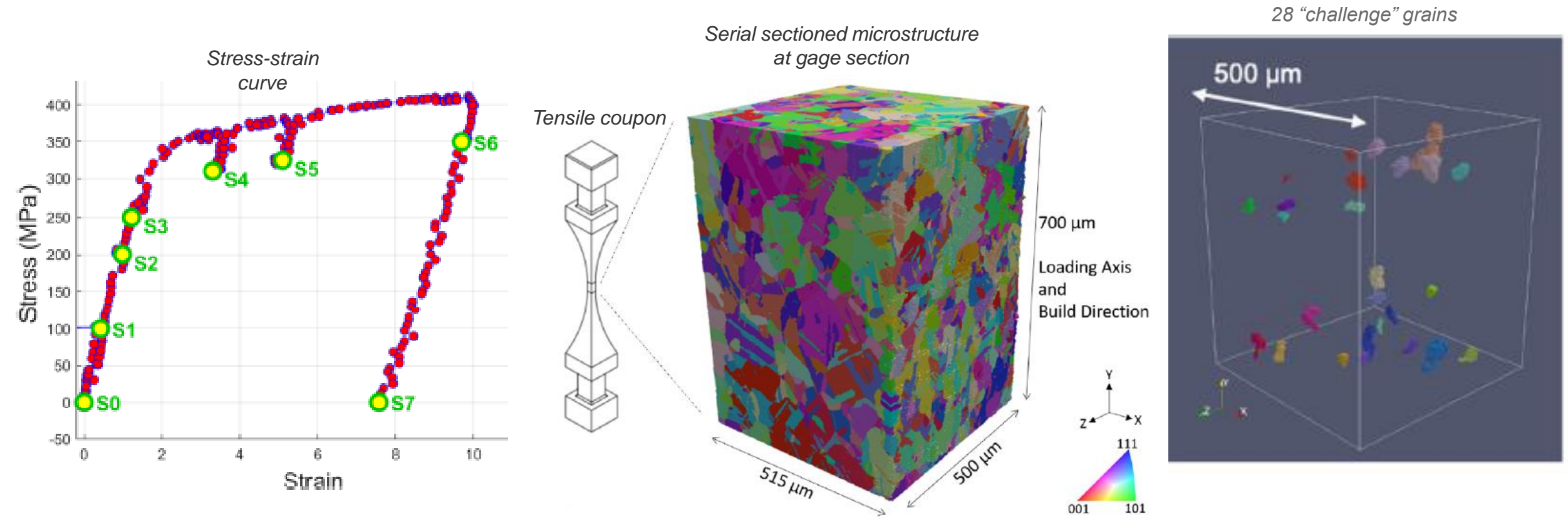
# AM modeling challenge: High energy X-ray diffraction | CAM 2021

Test cell



Variants of high-energy X-ray diffraction (HEDM) technique:

- 1) **near-field HEDM (nf-HEDM)**: provides data to reconstruct individual grain morphologies
- 2) **far-field HEDM (ff-HEDM)**: provides grain average orientations, elastic strains and centroids

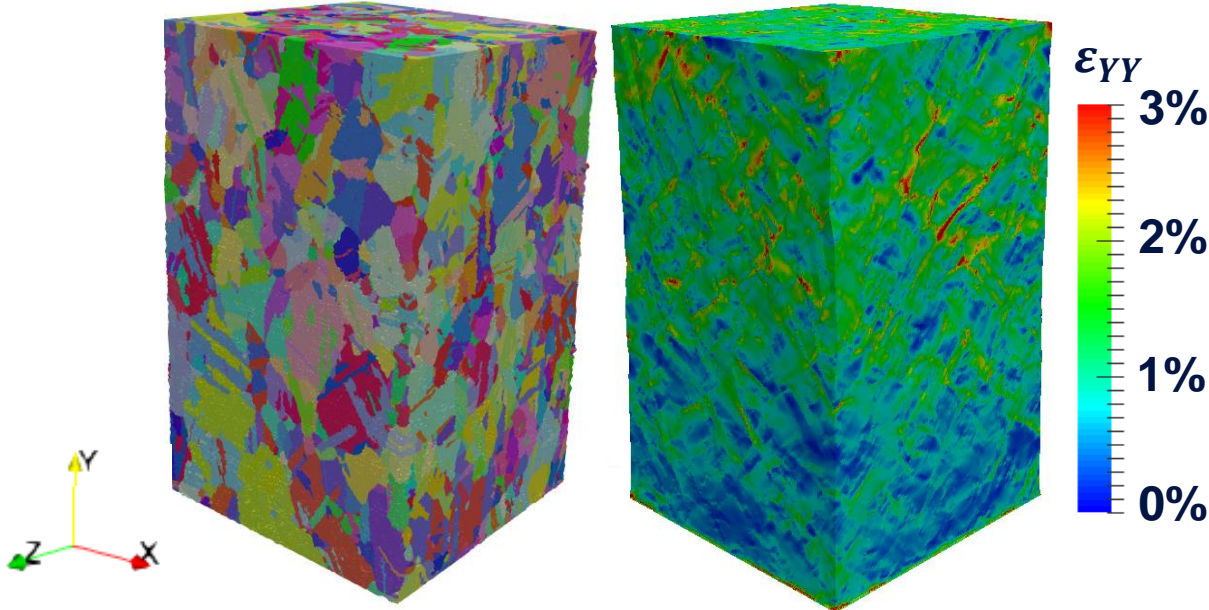


**Challenge problem:** Given the stress strain curve, serial-sectioned and reconstructed 3D microstructure, predict grain-average elastic strain tensor for 28 “challenge” grains at six different macroscopic load states, S1 through S6

- Additive manufacturing (AM) modeling challenge
  - Comparing crystal plasticity finite element (CPFE) predictions with high-energy X-ray measurements
- CP-based investigation of process-specific defects Ti-6Al-4V alloy



## SciFEN: Scalable Implementation of Finite Elements by NASA



- SciFEN<sup>1</sup> is built on PETSc<sup>2</sup>
- Leverages a suite of data structures and routines to achieve scalability.
- Utilizes open-source libraries like MOAB<sup>3</sup> and HDF5<sup>4</sup> for parallel I/O operations.
- Scales well over thousands of processors, compared to commercial packages
- Includes phenomenological CP models
- Interfaces with DREAM.3D<sup>5</sup>, Gmsh<sup>6</sup> and SPPARKS<sup>7</sup>

- 3D microstructure\* of IN625 obtained from serial-sectioning has 29,662 grains
- Finite element mesh has ~85 million degrees of freedom
- Global strain applied in YY direction: 1%
- CP model: Strain-gradient based<sup>8</sup>
- Simulation time: ~44 hours on 640 Intel Xeon E5-2670 processors

### Boundary conditions:

- Fully fixed bottom (-Y) face
- Free X and Z faces
- Applied Y-displacement on top (+Y) face

1. <https://software.nasa.gov/software/LAR-18720-1>

2. Scalable solutions for PDEs, [www.mcs.anl.gov/petsc/](http://www.mcs.anl.gov/petsc/)

3. Mesh-Oriented dataBAse, <http://sigma.mcs.anl.gov/moab-library/>

4. Parallel file I/O, [www.hdfgroup.com](http://www.hdfgroup.com)

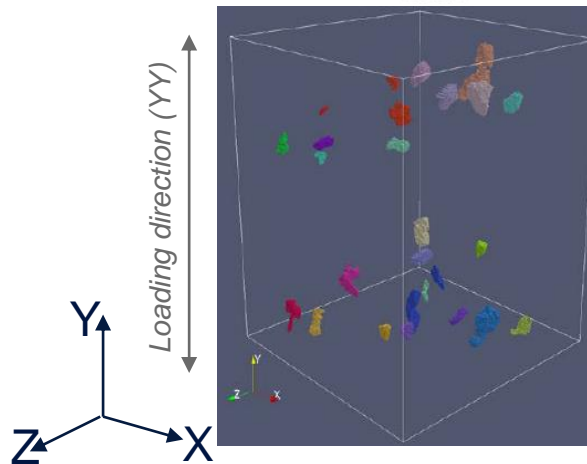
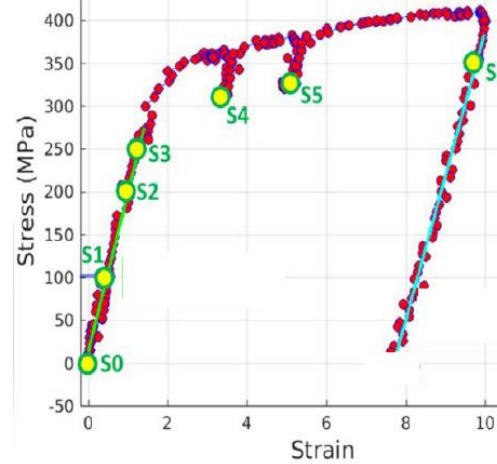
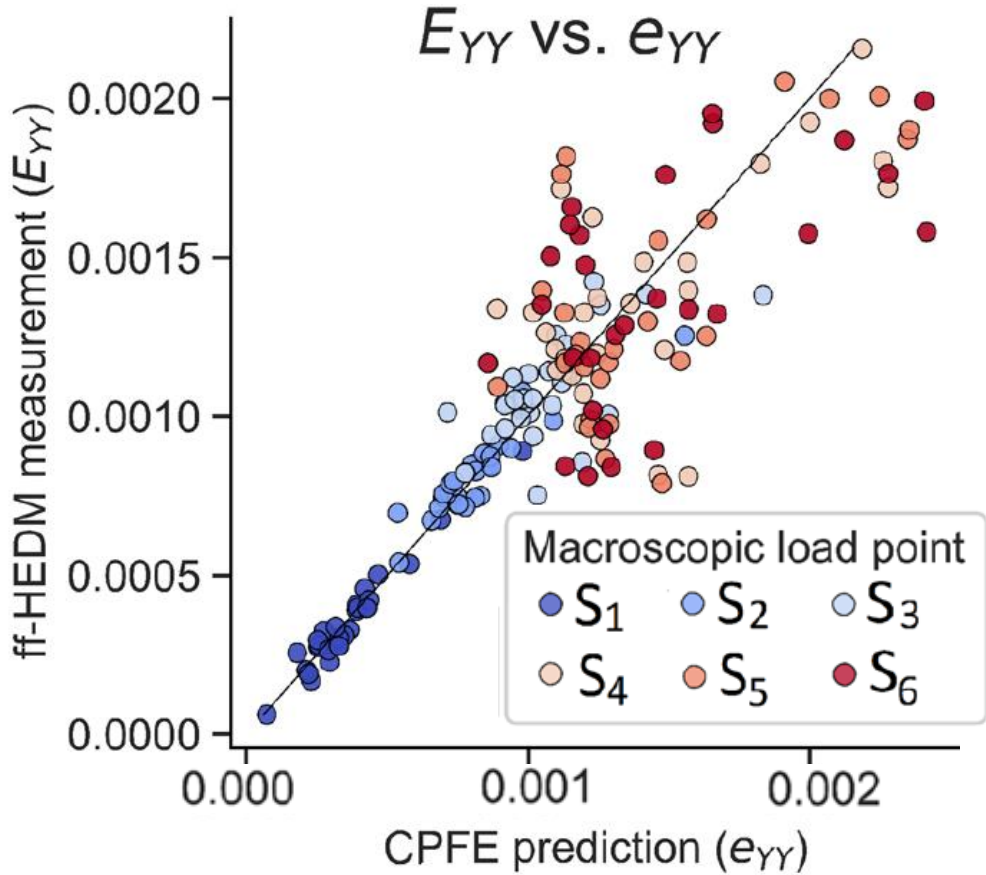
5. DREAM.3D <http://dream3d.bluequartz.net/>

6. Gmsh, <https://gmsh.info/>

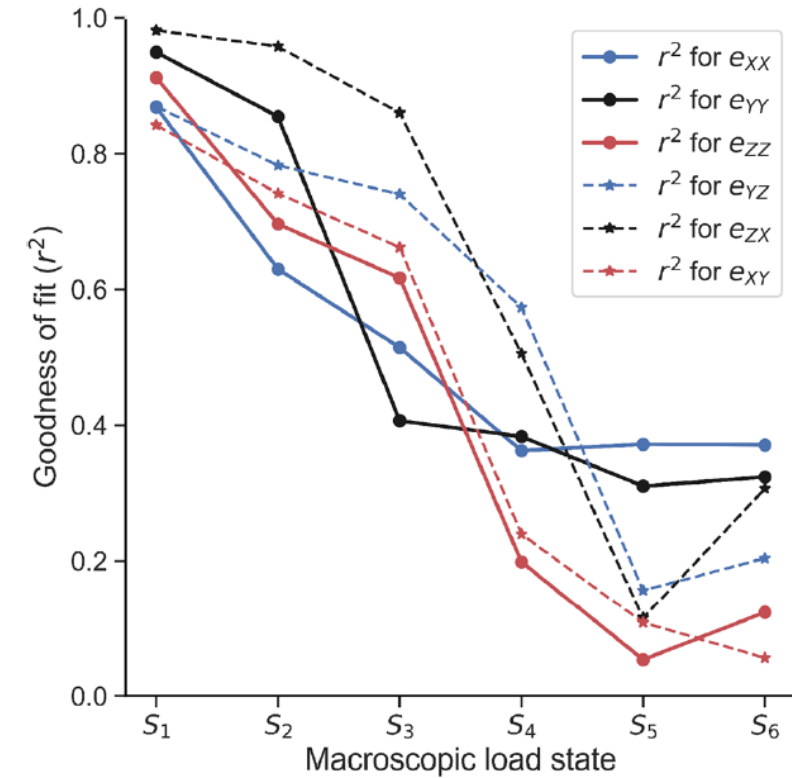
7. SPPARKS, <https://spparks.github.io/>

8. Acharya et al. (2000), J. Mech. Phys. Solids, 48(10), pp:2213-2230

CP predictions vs. ff-HEDM measurements

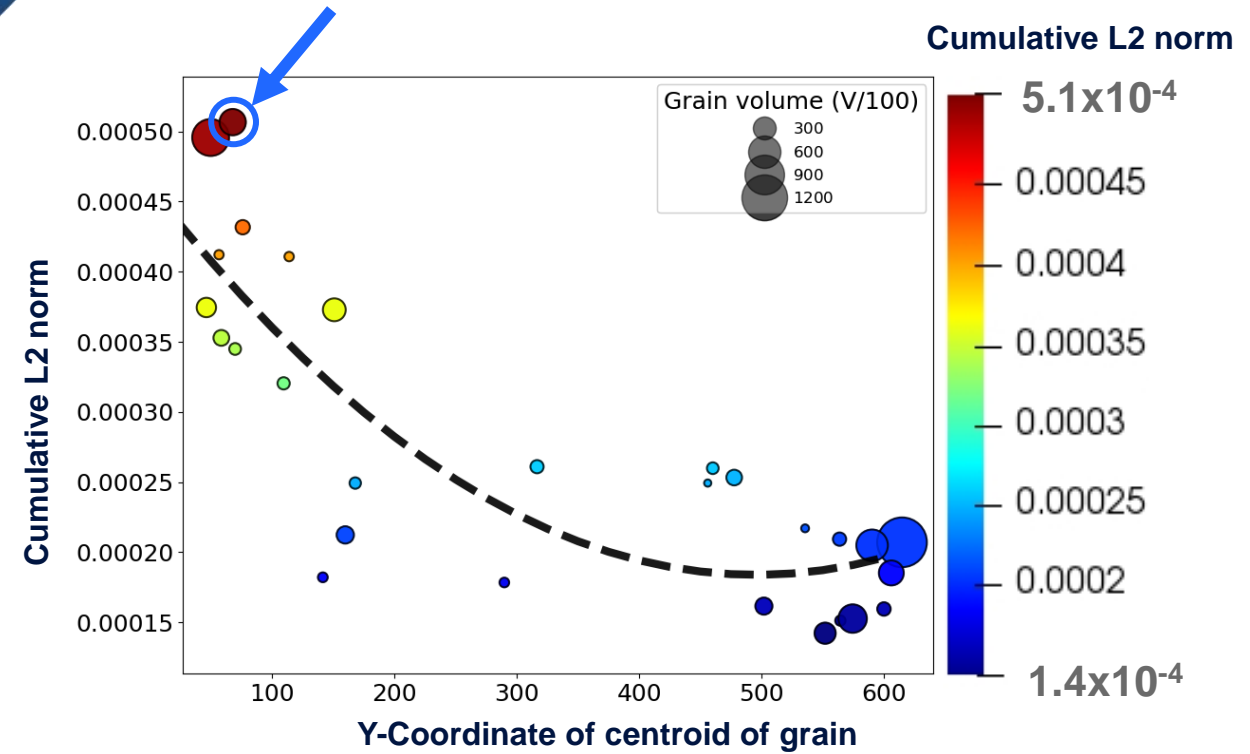
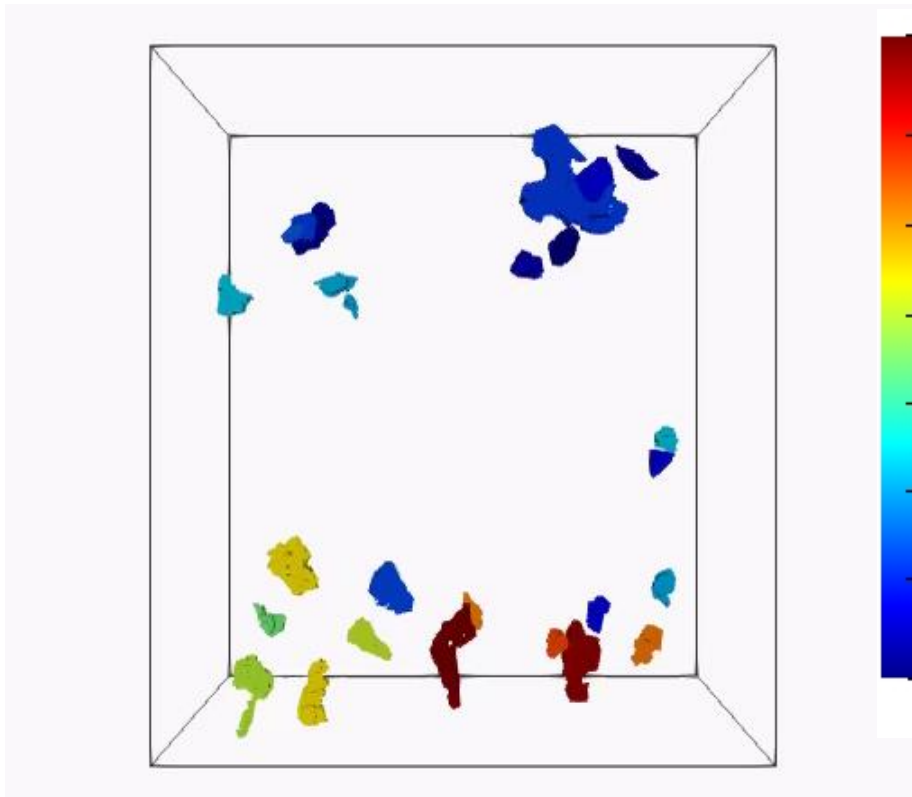


Goodness-of-fit



## Observations:

- There is a good agreement between CP predictions and ff-HEDM measurements in the elastic regime ( $S_1$ - $S_3$ )
- Deviations start to develop in plastic regime ( $S_4$ - $S_6$ )

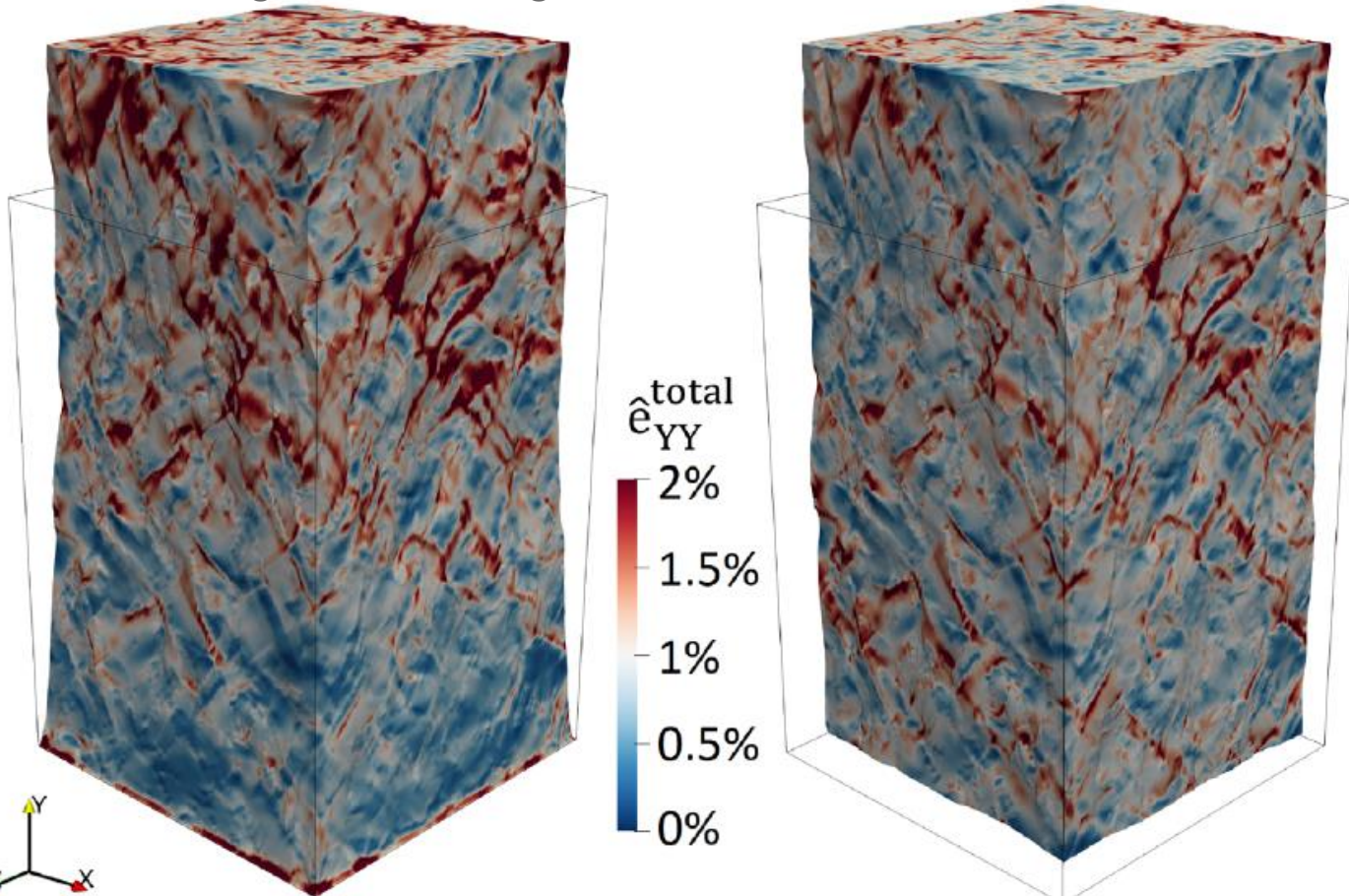


## Boundary conditions:

- Fully fixed bottom (-Y) face
- Free X and Z faces
- Applied Y-displacement on top (+Y) face

# Discrepancy 1: Boundary conditions

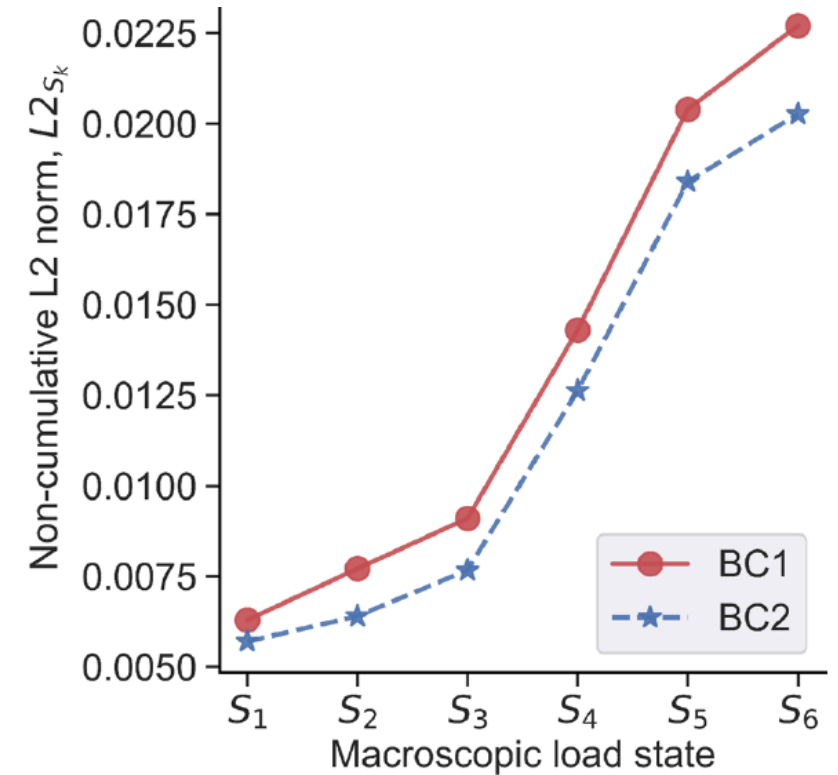
Strain maps of total strain in YY direction, generated at global strain of 1%



**BC1:** Fully constrained bottom face

**BC2:** Relaxed boundary conditions  
(Only one corner node on -Y face fully fixed and one edge fixed in X and Y directions)

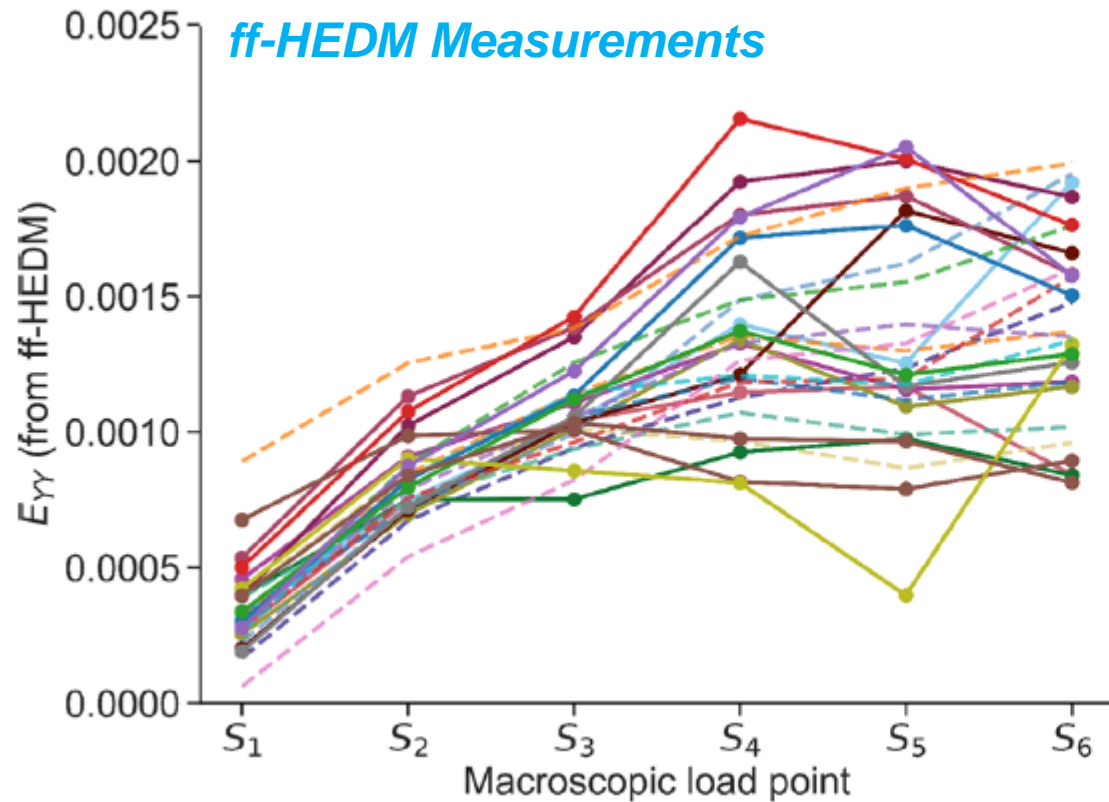
Non-cumulative L2 norm calculated at each macroscopic load state,  $S_k$



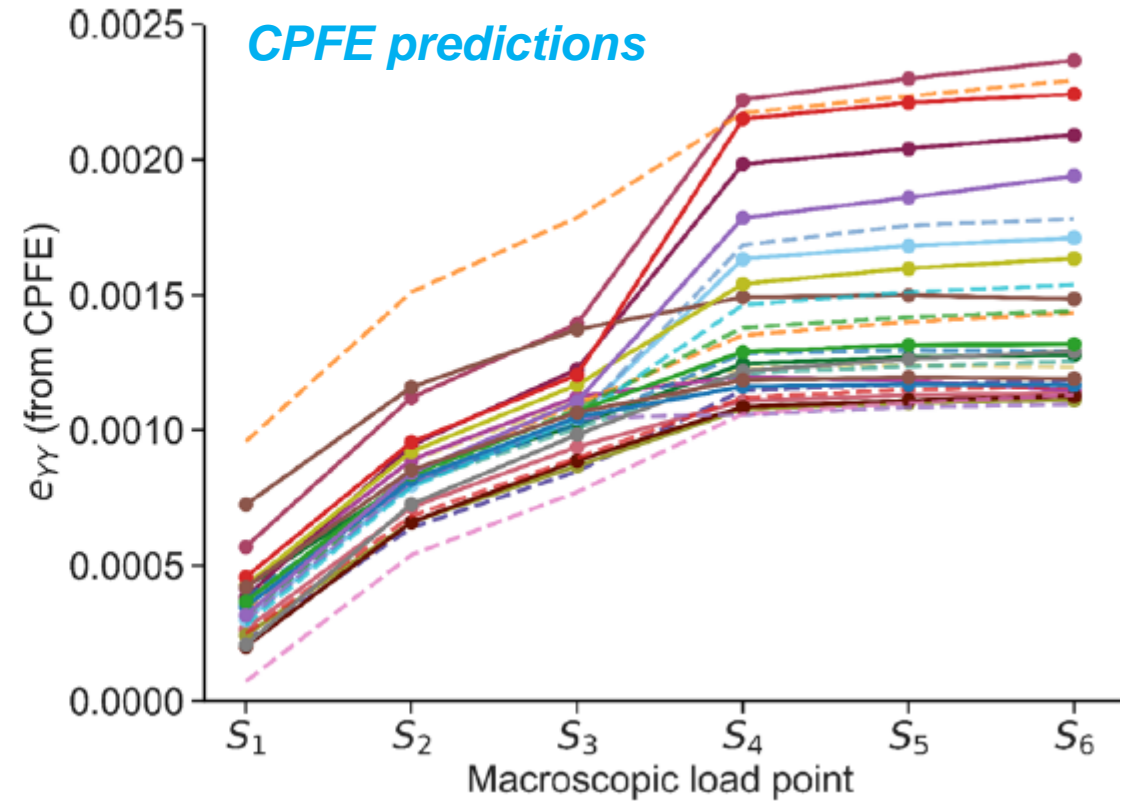
$$L2_{S_k} = \sum_{n=1}^N \sqrt{\sum_{i=1}^6 \left( (E_i)_{S_k}^{g_n} - (e_i)_{S_k}^{g_n} \right)^2}$$

$(E_i)_{S_k}^{g_n}$  is ff-HEDM measurement;  $(e_i)_{S_k}^{g_n}$  is CP prediction;  $N$  is # grains  
 $S_k$  is macroscopic stress state;  $g_n$  is grain ID

*ff-HEDM measurement of evolution of YY component of grain-average elastic strain in each of the 28 grains*

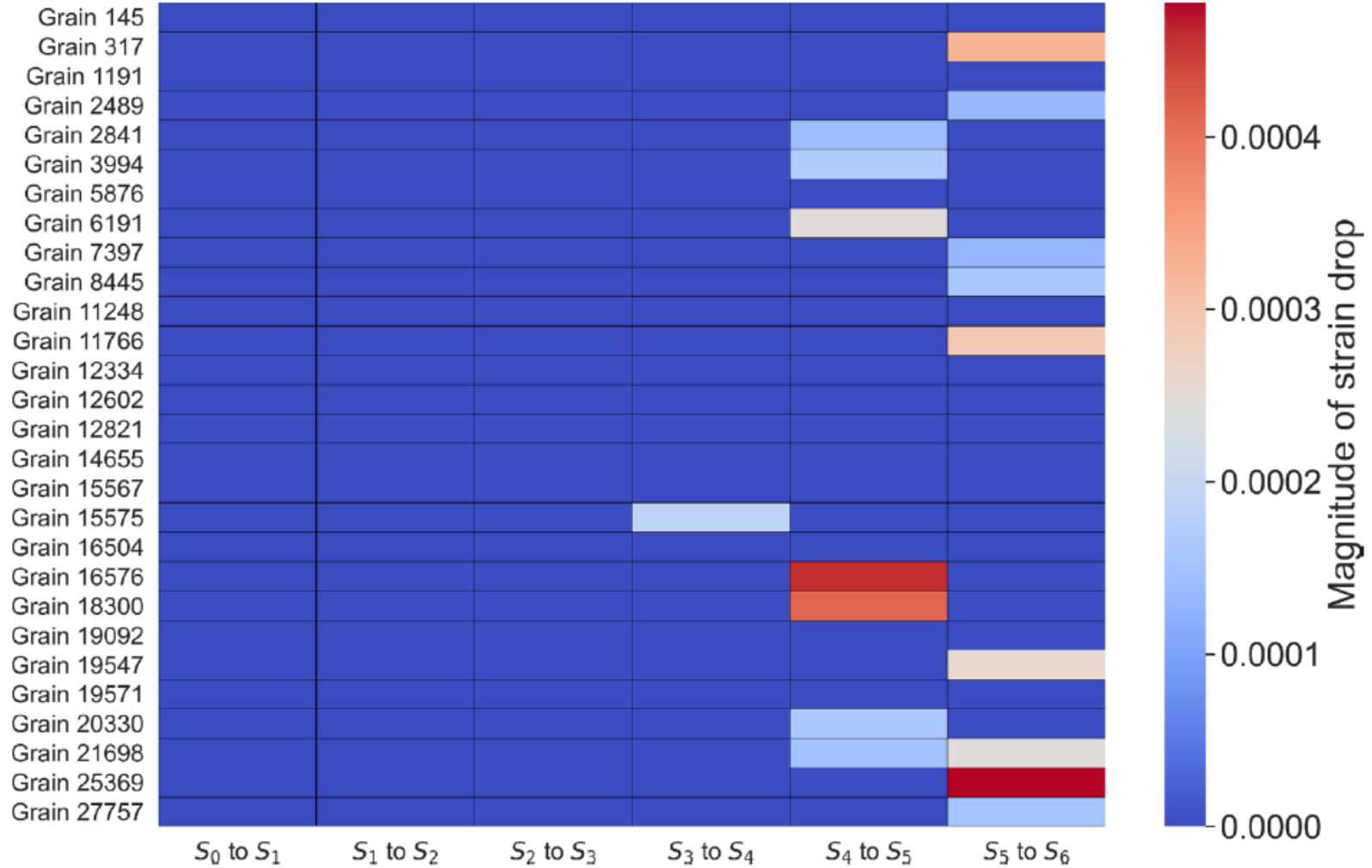
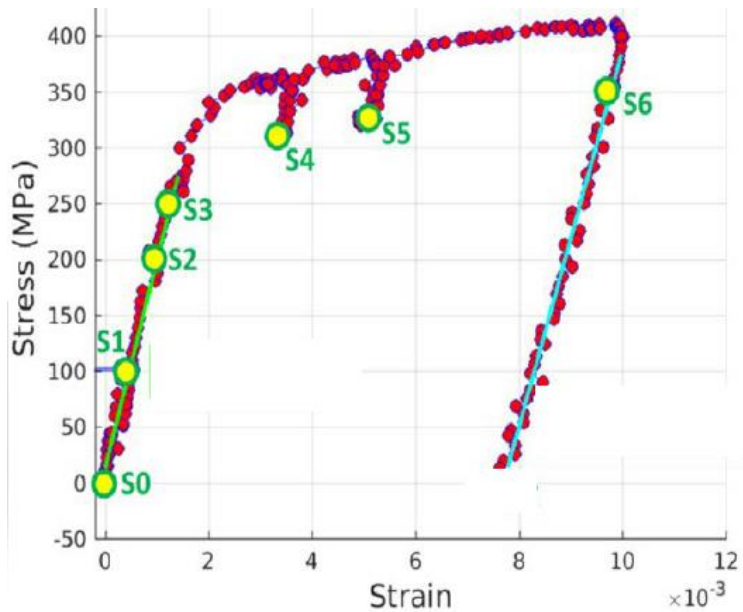


*CPFE prediction of evolution of YY component of grain-average elastic strain in each of the 28 grains*

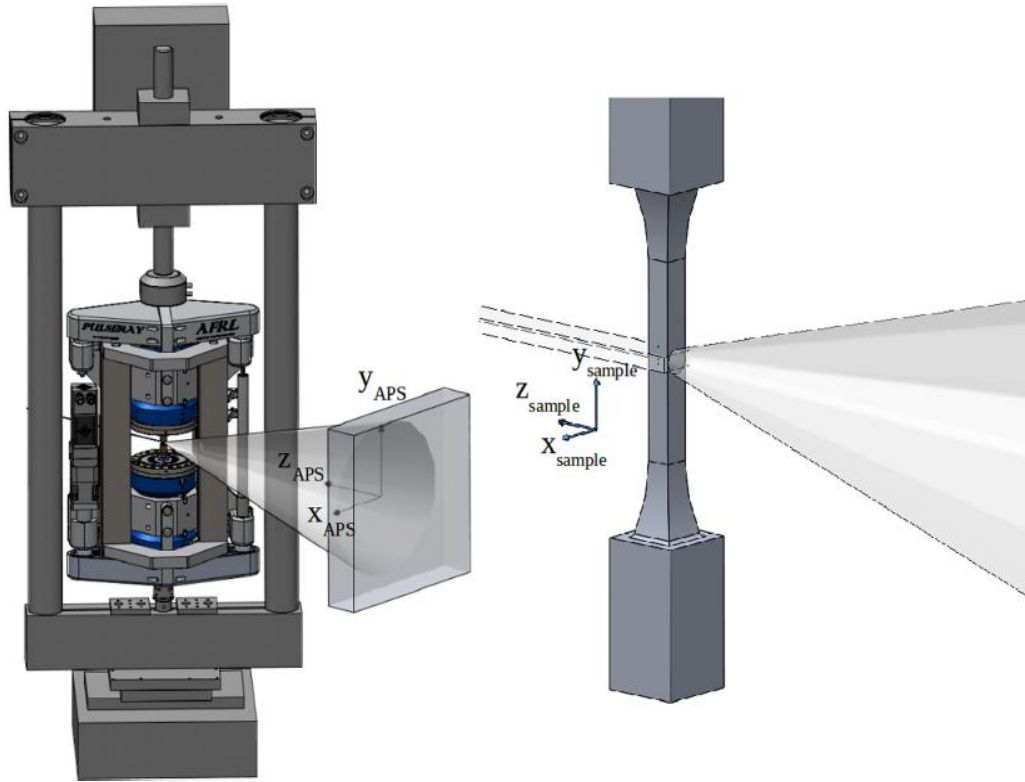


**Observation:** Phenomenological CP model used is unable to predict stress relaxation

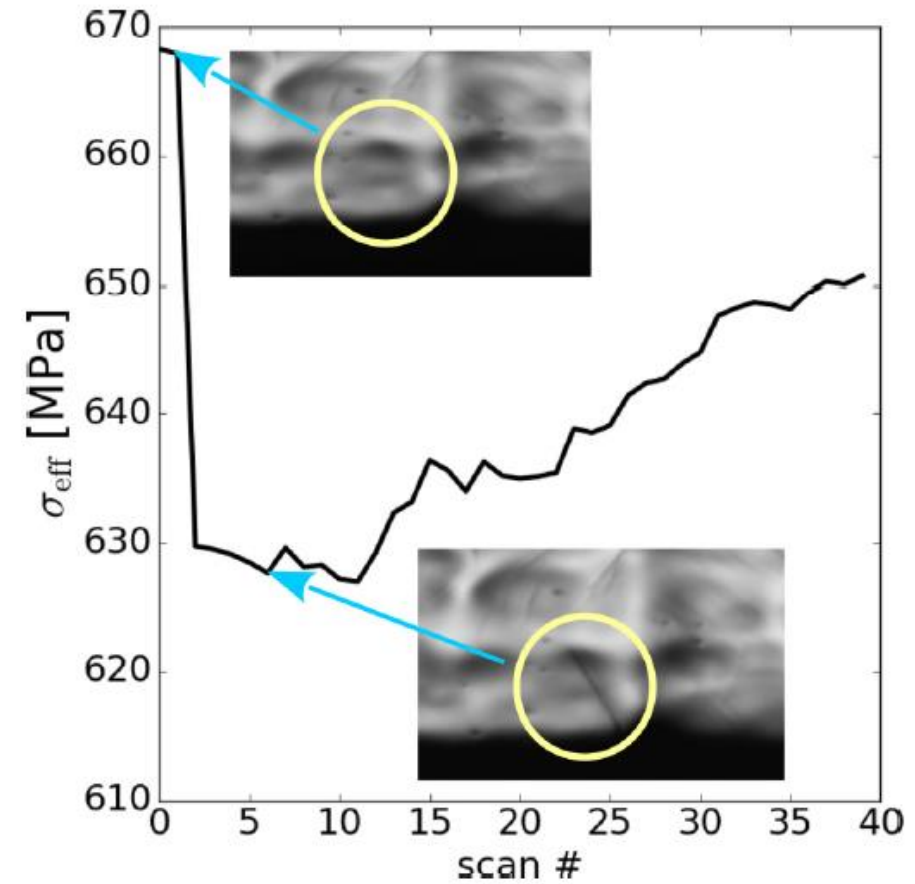
- Heatmap showing strain drop in grains
- Heatmap created using ff-HEDM data.



**Observation:** Stress relaxation is predominant in the plastic regime and is non-existent in the elastic regime



Setup of creep experiment at advanced photon source (APS)



- Stress relaxation during creep loading at 85% of the yield stress
- Corresponding slip band developed at the location of the grain

Source: Beaudoin et al. Physical Review B. 96, 174116 (2017)

**Saikumar R. Yeratapally**, Albert R. Cerrone, Edward H. Glaessgen, “*Discrepancy between crystal plasticity simulations and far-field high energy X-Ray diffraction microscopy measurements*” Integrating Materials and Manufacturing Innovation 2021; 10(2):196-217.  
DOI: 10.1007/s40192-021-00216-5

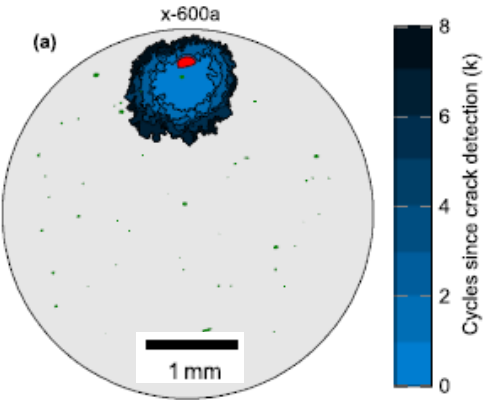
Journal: Integrating Materials and Manufacturing Innovation (IMMI)

Special Issue: Metal Additive Manufacturing Modeling Challenge Series 2020



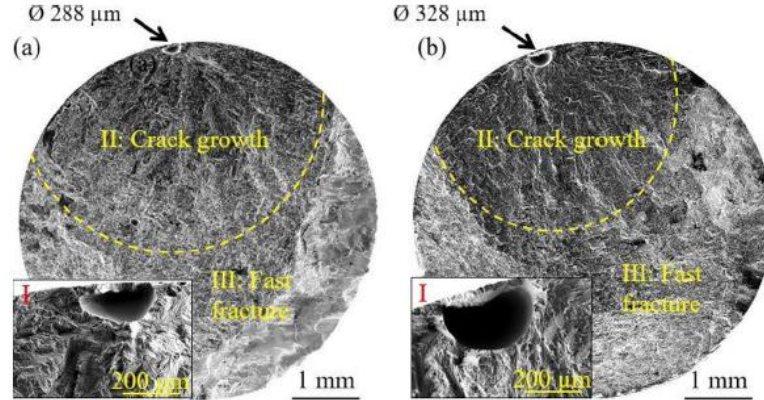
- Additive manufacturing (AM) modeling challenge
  - Comparing crystal plasticity finite element (CPFE) predictions with high-energy X-ray measurements
- CP-based investigation of process-specific defects Ti-6Al-4V alloy

## Ti6Al4V, EBM



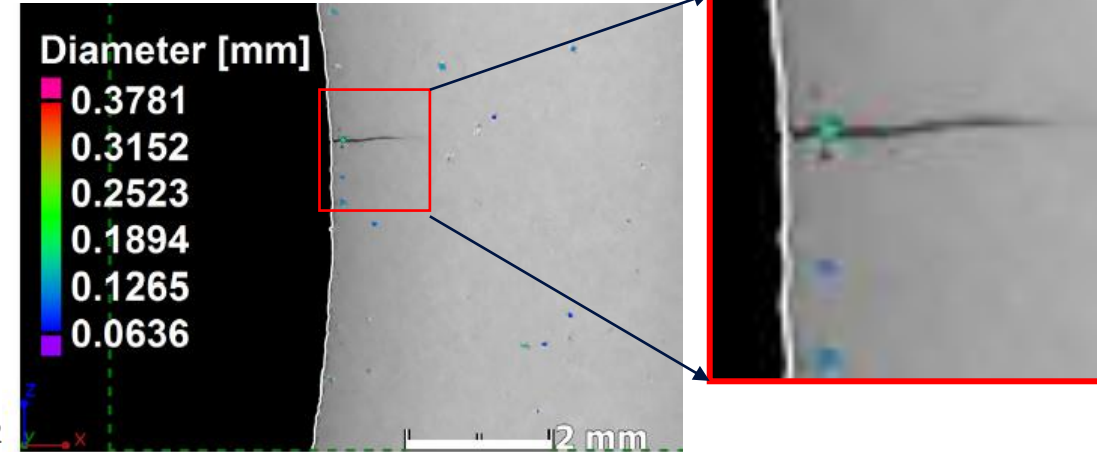
Williams et al. (2017) Scientific Report | 7: 7308

## Ti6Al4V, WAAM



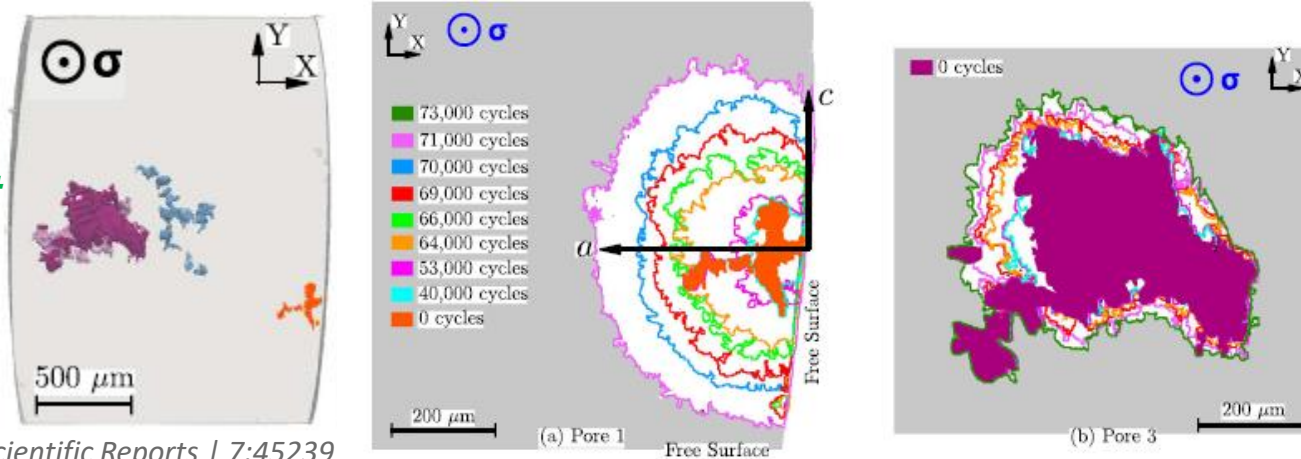
Biswal et al. (2019) Additive Manufacturing 28:517–52

## AlSi10Mg, L-PBF



Du Plessis et al. (2020) Materials and Design 187 (2020) 108385.

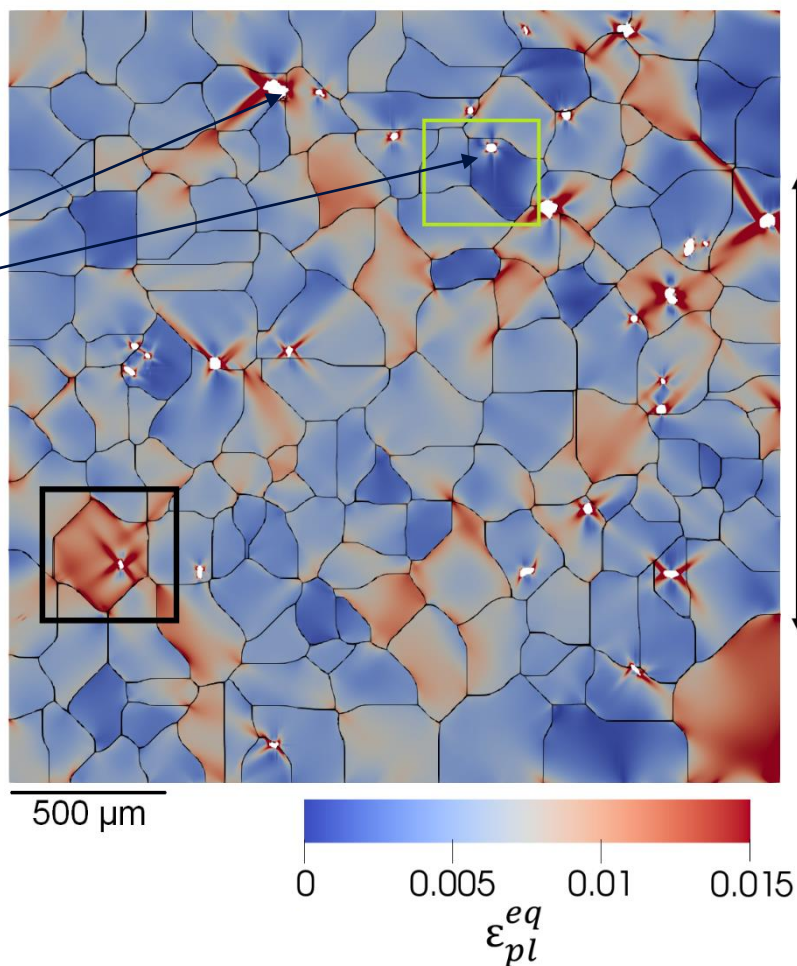
## A357-T6, Cast



Munoz et al. (2016) Scientific Reports | 7:45239

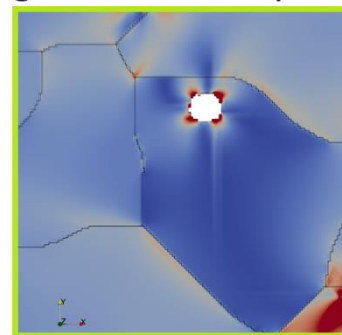
EBM: electron beam melting  
WAAM: wire arc additive manufacturing  
L-PBF: Laser powder-bed fusion

Equivalent plastic strain map  
(at 1% global strain)

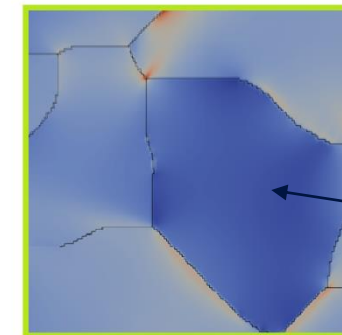


L-PBF process-specific pores in as-built Ti-6Al-4V alloy, obtained from backscatter electron images of metallographic sections

Strain map in local neighborhood of *pore 1*

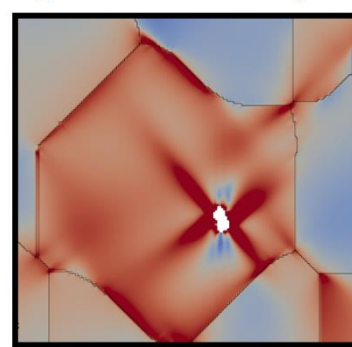


Strain map when there is no pore

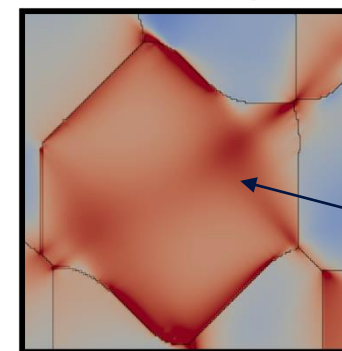


Pore 1 is embedded in a "hard" grain

Strain map in local neighborhood of *pore 2*

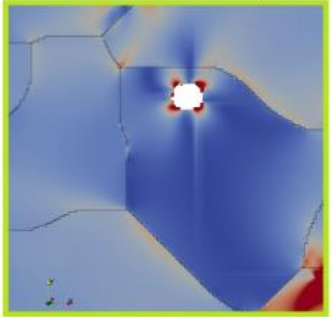


Strain map when there is no pore

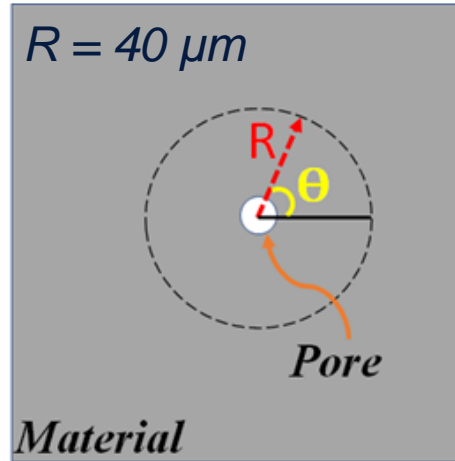
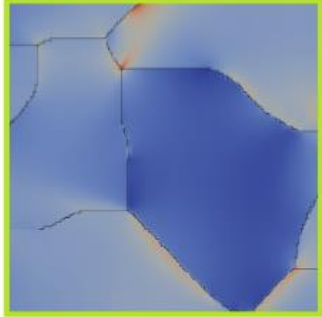


Pore 2 is embedded in a "soft" grain

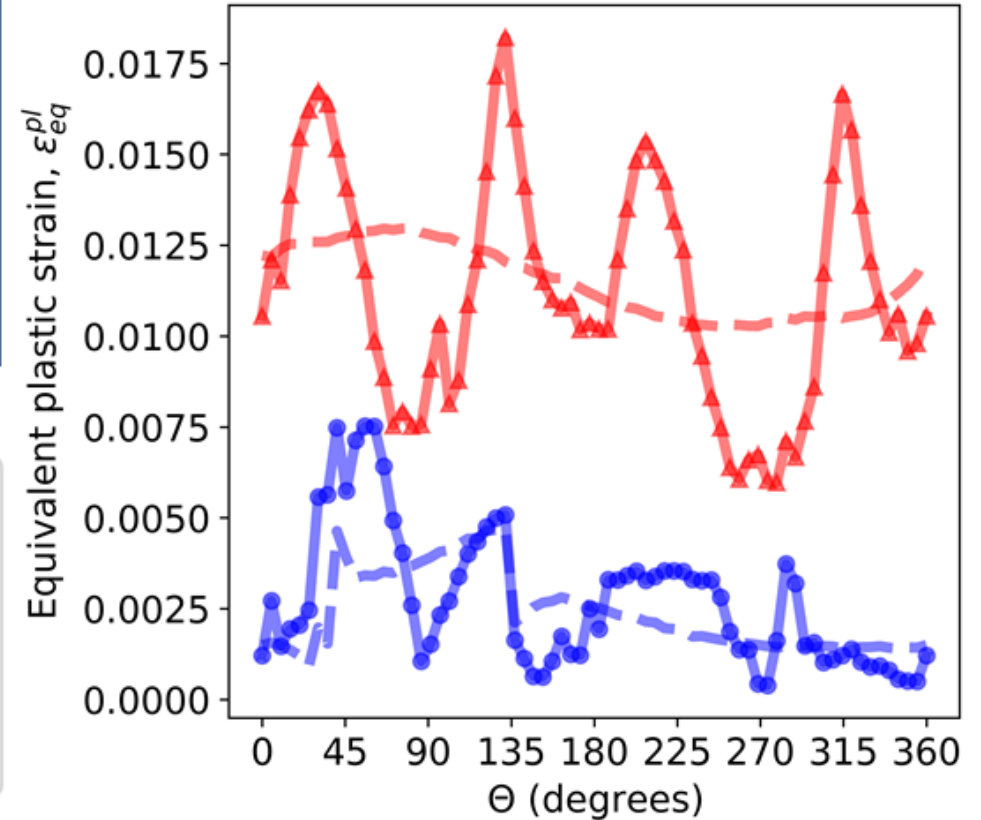
Strain map in local neighborhood of *pore 1*



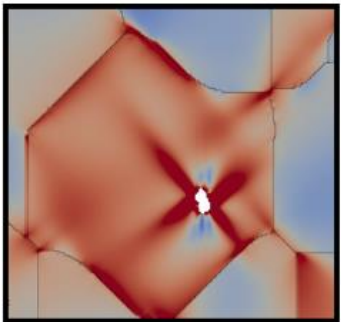
Strain map when there is no pore



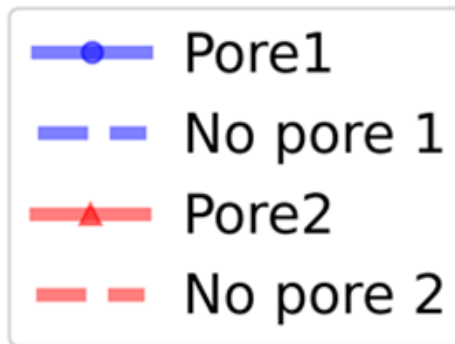
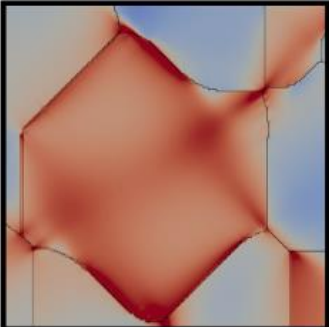
Comparing strain accumulation in vicinity of two pores



Strain map in local neighborhood of *pore 2*



Strain map when there is no pore



**Observation:** Pore fully embedded in “soft” grain accumulates significant plastic strain in its vicinity compared to a similar sized pore located within a “hard” grain

- Grain-average elastic strain measurements from crystal plasticity finite element (CPFE) are compared with far-field high energy X-ray diffraction (ff-HEDM) measurements.
  - ScIFEN's CPFE solver predictions (in the elastic regime) agree with ff-HEDM measurements
  - The results qualitatively agree in the elastic regime, but increased level of discrepancy is observed in the plastic regime
  - Sources of discrepancy between CPFE and ff-HEDM are discussed
- CP simulations are used to understand the influence of local microstructure on the accumulation of plastic strain.
  - Pore fully embedded in “soft” grain accumulates significant plastic strain compared to a similar sized pore located within a “hard” grain
- Ongoing work to validate and apply high-fidelity CP models will be used to develop certification by analysis

The work presented is supported by NASA Aeronautics Research Mission Directorate's (ARMD) Transformative Tools and Technologies (TTT) project



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## Thank you.

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