

Enabling automated metric-based mesh adaptation for US3D

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- ① Why anisotropic mesh adaptation?
- ② Serial implementation
- ③ Parallel implementation
- ④ Numerical examples
 - Supersonic flow past the MSL entry capsule
 - Subsonic flow past the Earth Entry Vehicle (EEV)
- ⑤ Conclusions

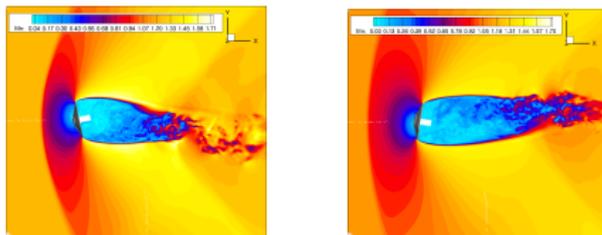
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Why anisotropic mesh adaptation?

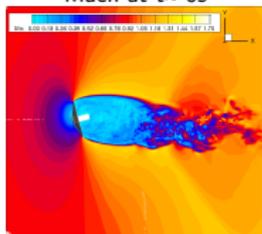
Goals

- Simplify the mesh generation process for unsteady flows past complex geometries.
- Improve the resolution of free-flight CFD simulations of atmospheric entry vehicles using US3D.

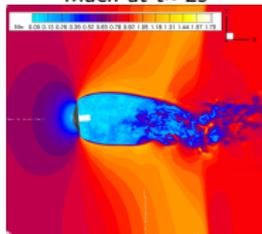


Mach at $t \approx 0s$

Mach at $t \approx 2s$

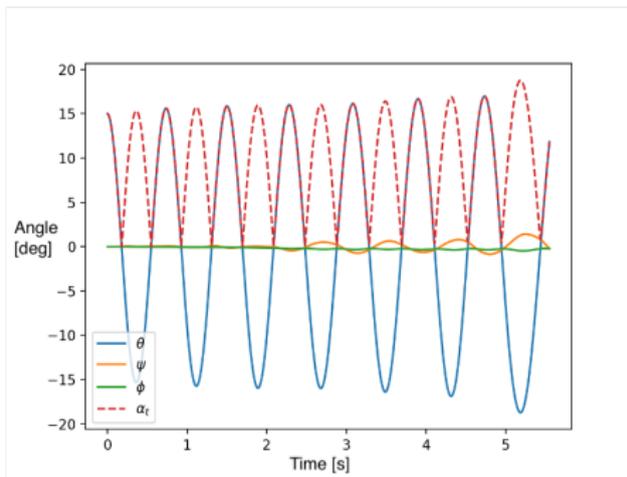


Mach at $t \approx 4s$



Mach at $t \approx 5s$

Mach solution for ADEPT at three different time instances.



Time history of the attitude for the ADEPT geometry.

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Serial implementation

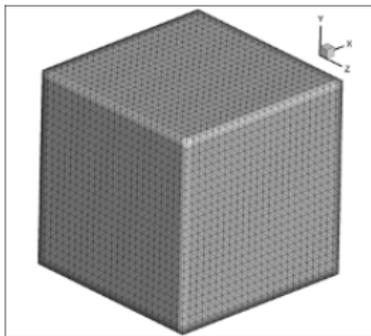
Required developments

- Calculate metric data based on a US3D flow solution that can drive anisotropic mesh adaptation.
- Implemented a prismatic boundary layer domain that is kept fixed.
- Linked US3D to MMG and demonstrated iterative adaptation in serial.

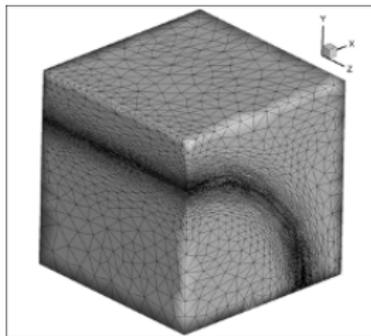
The aim of metric-based mesh adaptation is to control the local error by aligning the local size and directionality of the mesh edges/elements. Based on a given state/derived variable u we can calculate/reconstruct the metric tensor field that prescribes the preferred direction and size of the local edges/elements^a:

$$M_{LP} = D_{LP} (\det \|H_u\|)^{\frac{-1}{2p+3}} \mathbf{R}_u^{-1} \|\Lambda\| \mathbf{R}_u \quad (1)$$

Pass the metric tensor field to a adaptive capability that computes an aligned mesh.



Initial mesh that consists of 82000 tetrahedra.

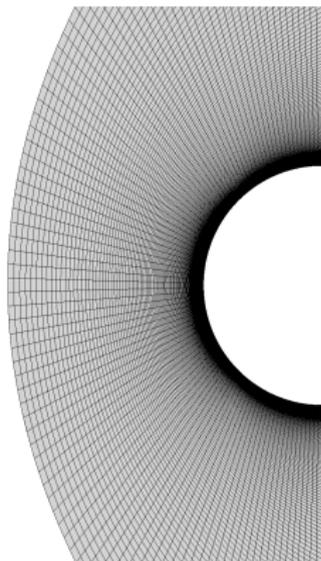


Adapted mesh that consists of 72000 tetrahedra.

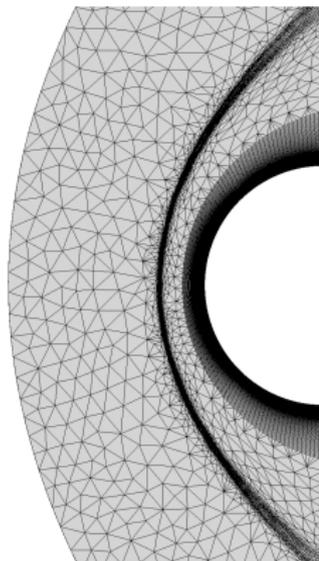
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Original hexahedral mesh.



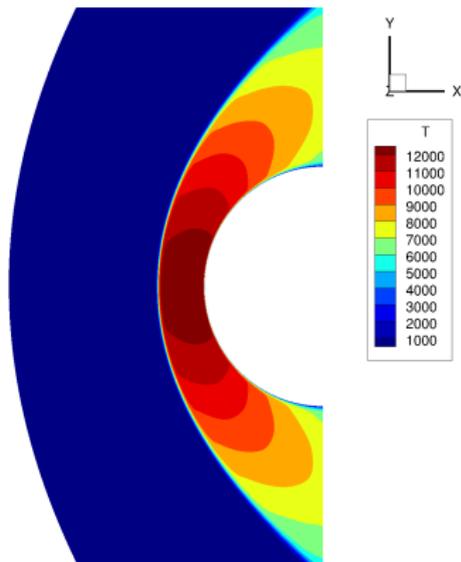
Final hybrid (prisms+tetrahedra) mesh.



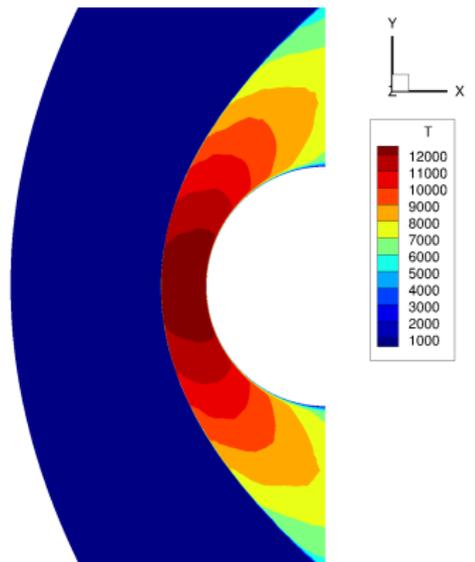
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Temperature computed using original hexahedral mesh.

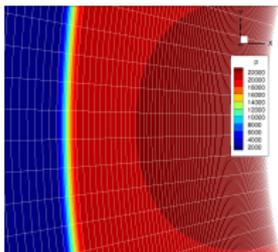


Temperature computed using the final hybrid mesh.

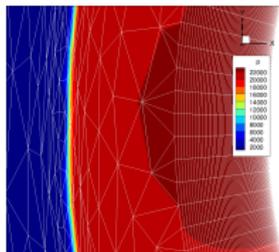
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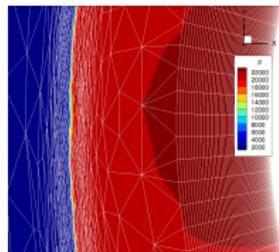
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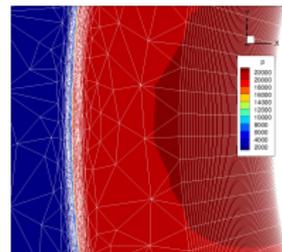
Mesh 1 (hexahedra)



Mesh 2
(prisms+tetrahedra)



Mesh 3
(prisms+tetrahedra)

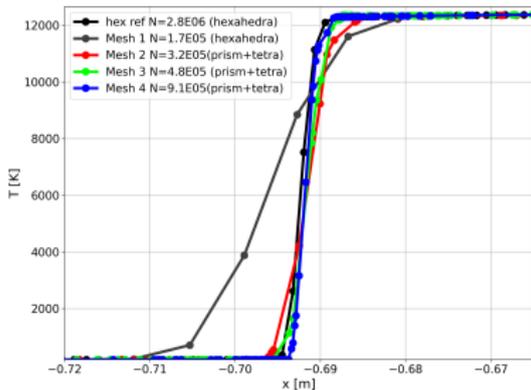


Mesh 4
(prisms+tetrahedra)

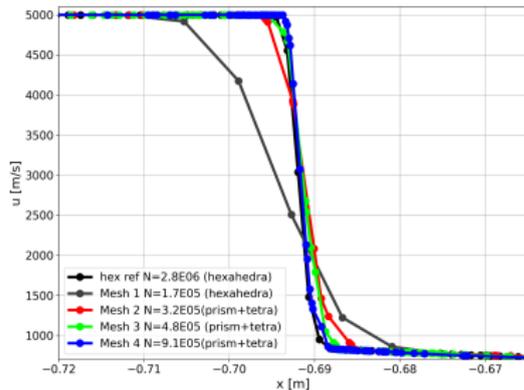
Recap

Required developments

- Calculate metric data based on a US3D flow solution that can drive anisotropic mesh adaptation.
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Temperature profile along the stagnation line.

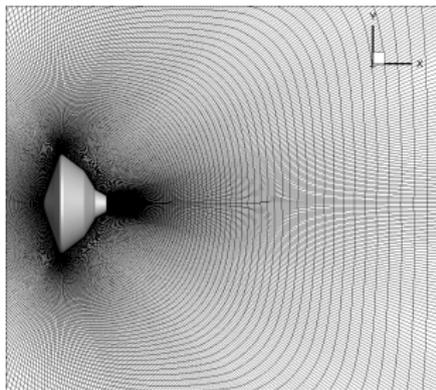


u velocity along the stagnation line.

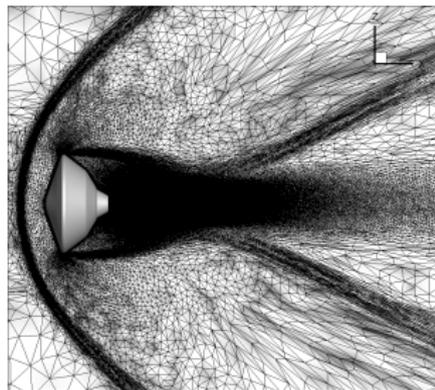
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Initial mesh (hexahedra).

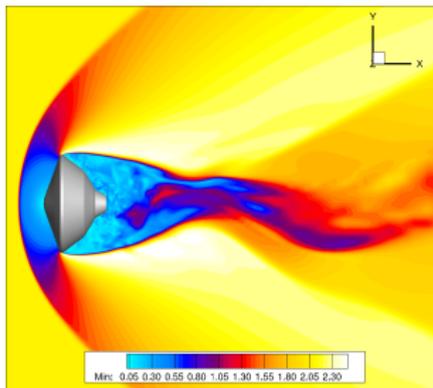


Adapted mesh (prisms+tetrahedra).

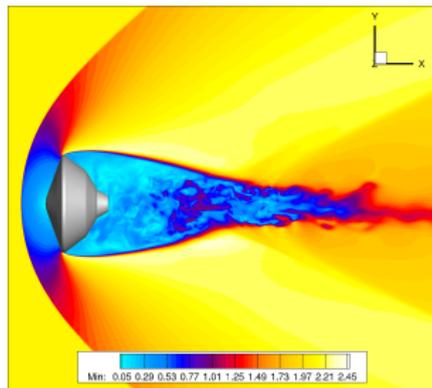
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Initial mesh (hexahedra).



Adapted mesh (prisms+tetrahedra).

Limitations

- Adapting a mesh that consists of approximately 50×10^6 elements takes about 1.5 hours in serial using MMG.
- Memory usage is limited being to able to just use one node.

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Parallel implementation

Serial implementation

- Parallel reading from HDF5.
- Parallel reconstruction of the Hessian on a hybrid (prisms+tetrahedra) meshes and hexahedral meshes.
- Prism layer extraction from hexahedral meshes.
- Serial adaptation using MMG.
- Serial writing to HDF5 format compatible with US3D.

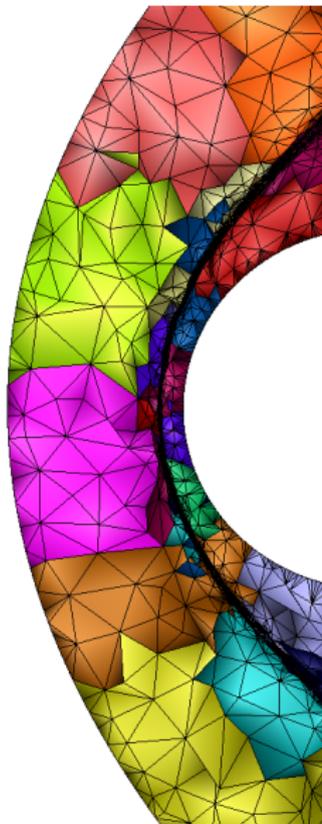
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New features

- **Adapt the tetrahedra in parallel using ParMMG.**
 - **Repartition/redistribute the tetrahedra since ParMMG does not accept prisms.**
 - **Determine the correct shared interfaces between partitions.**
- Patch the adapted tetrahedra topology onto the fixed prismatic boundary layer topology.
- Apply wake refinement by letting the Turbulent Kinetic Energy (TKE) drive isotropic refinement.
- Output the distributed mesh into a single "grid.h5" file that is compatible with US3D.



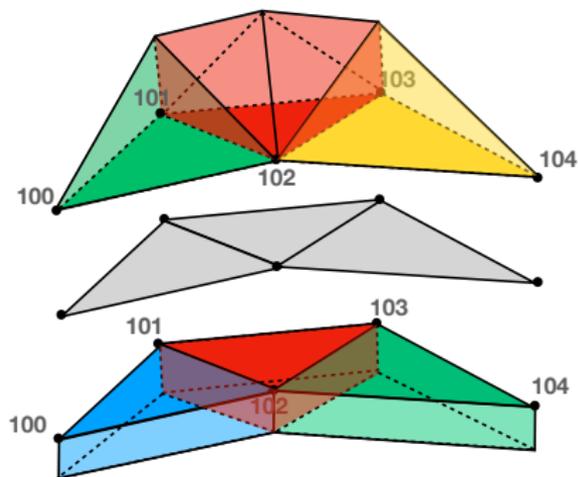
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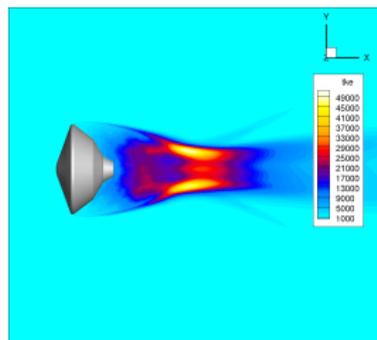
The anisotropic mesh refinement is driven by the metric term that relates the local mesh sizing and directionality to the local spatial linear interpolation error:

$$M_{LP} = D_{LP} (\det \|H_u\|)^{\frac{-1}{2p+3}} \mathbf{R}_u^{-1} \|\Lambda\| \mathbf{R}_u \quad (2)$$

The anisotropic mesh adaptation based on the Mach number is now combined with isotropic mesh adaptation based on the Turbulent Kinetic Energy (TKE).

$$M_t = (\xi - 1)M_{LP} + \xi M_i \quad (3)$$

where the weights $\xi = f(k_t/k_{t,max})$ are determined linearly based on the TKE.



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$$M_{LP} = D_{LP} (\det \|H_u\|)^{\frac{-1}{2p+3}} \mathbf{R}_u^{-1} \|\Lambda\| \mathbf{R}_u \quad (4)$$

The anisotropic mesh adaptation based on the Mach number is now combined with isotropic mesh adaptation based on the Turbulent Kinetic Energy (TKE).

$$M_t = (\xi - 1)M_{LP} + \xi M_i \quad (5)$$

where the weights $\xi = f(k_t/k_{t,max})$ are determined linearly based on the TKE.

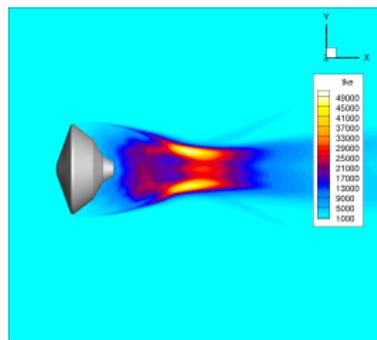
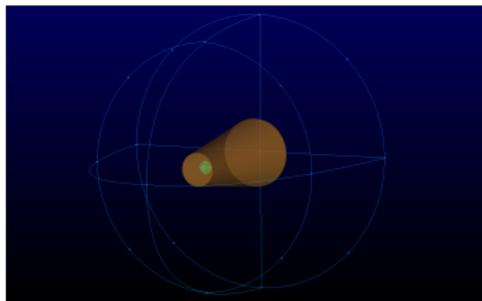
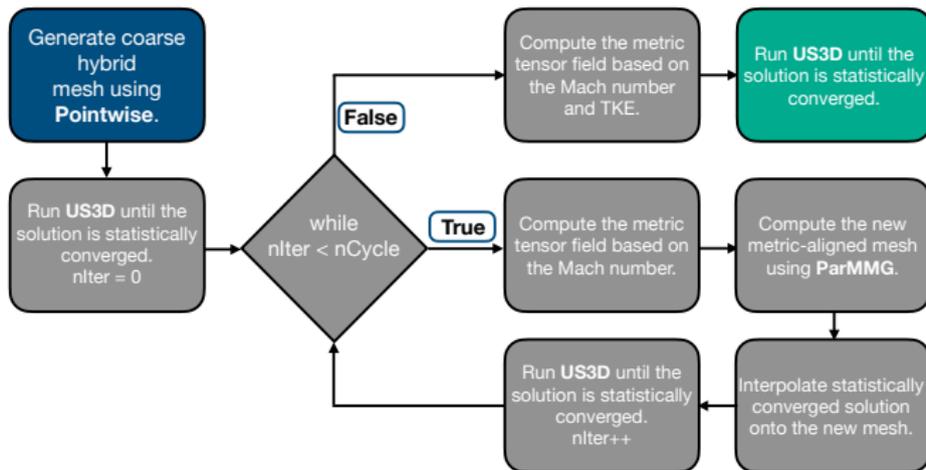


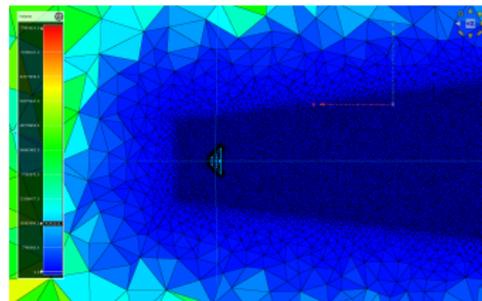
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Numerical examples



Initial mesh definition in Pointwise



A cut of the coarse initial volume mesh.

Numerical examples

```
#PBS -S /bin/bash
#PBS -N eev_adaptionCycle
#PBS -q devel
#PBS -l select=100:ncpus=40:mpiprocs=40:model=sky_ele
#PBS -l walltime=2:00:00
```

```
export FOCUS=/modules/./test15
```

```
mkdir adaptCycle
cd adaptCycle
mkdir inputs
cd inputs
ln -s ../../grid.h5 grid.h5
ln -s ../../conn.h5 conn.h5
ln -s ../../data.h5 data.h5
cp -r ../../metric_new.inp metric.inp
cd ..
cp -r ../input.inp .
```

```
mpiexec -np 560 $FOCUS > adaption.log
```

```
mpiexec -np 40 us3d-prepar --grid=grid.h5 --conn=conn.h5 >
connBuild.log
```

```
mpiexec -np 1 us3d-interp --sdir=../ --ddir=../
adaptCycle_r2 --method=1 > interpolation.log
```

```
mv data.h5 data_restart.h5
```

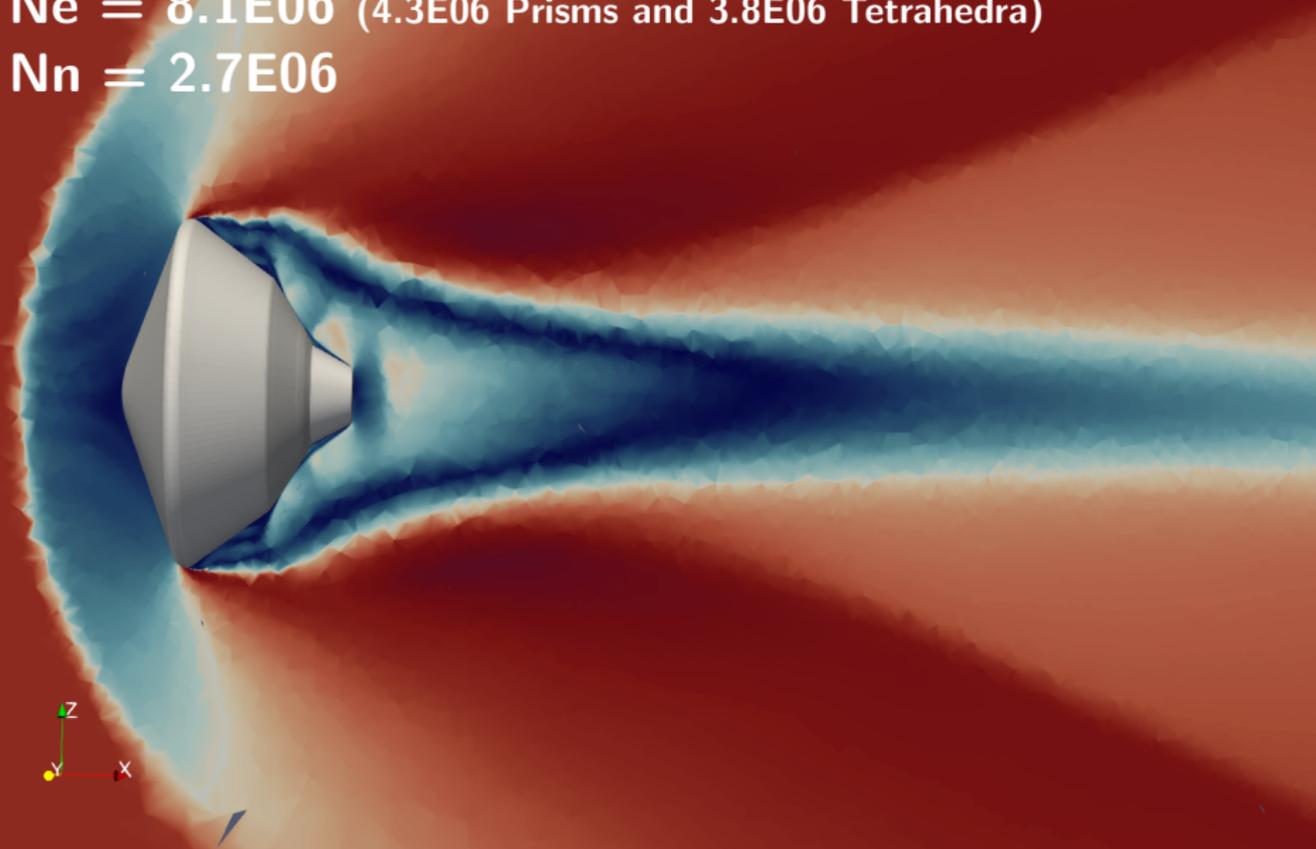
```
mpiexec -np 4000 us3d --grid=grid.h5 --conn=conn.h5 --
restart=data_restart.h5 --data=data.h5 > wash.log
```

example .pbs file

Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

$Ne = 8.1E06$ (4.3E06 Prisms and 3.8E06 Tetrahedra)

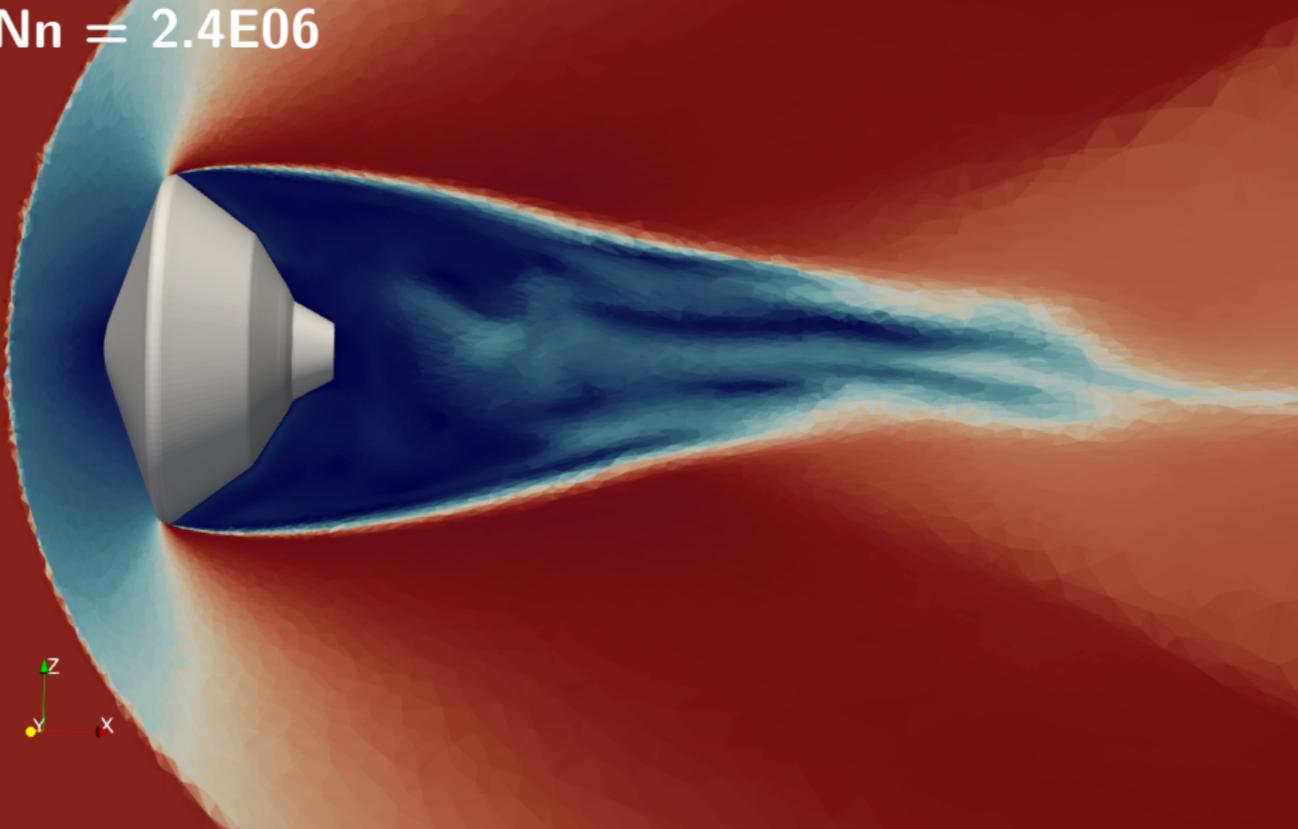
$Nn = 2.7E06$



Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

$Ne = 6.2E06$ (4.3E06 Prisms and 1.9E06 Tetrahedra)

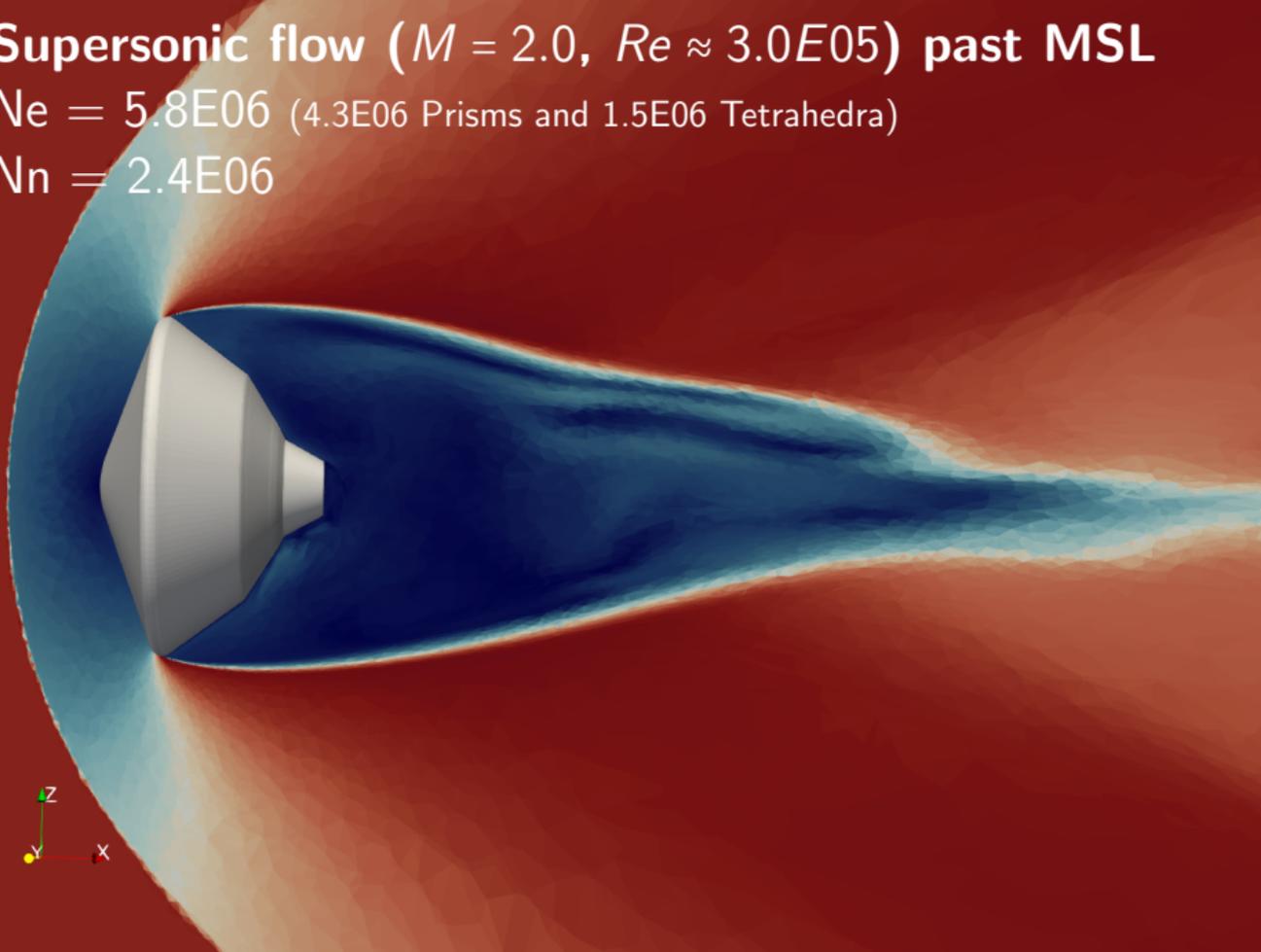
$Nn = 2.4E06$



Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

$N_e = 5.8E06$ (4.3E06 Prisms and 1.5E06 Tetrahedra)

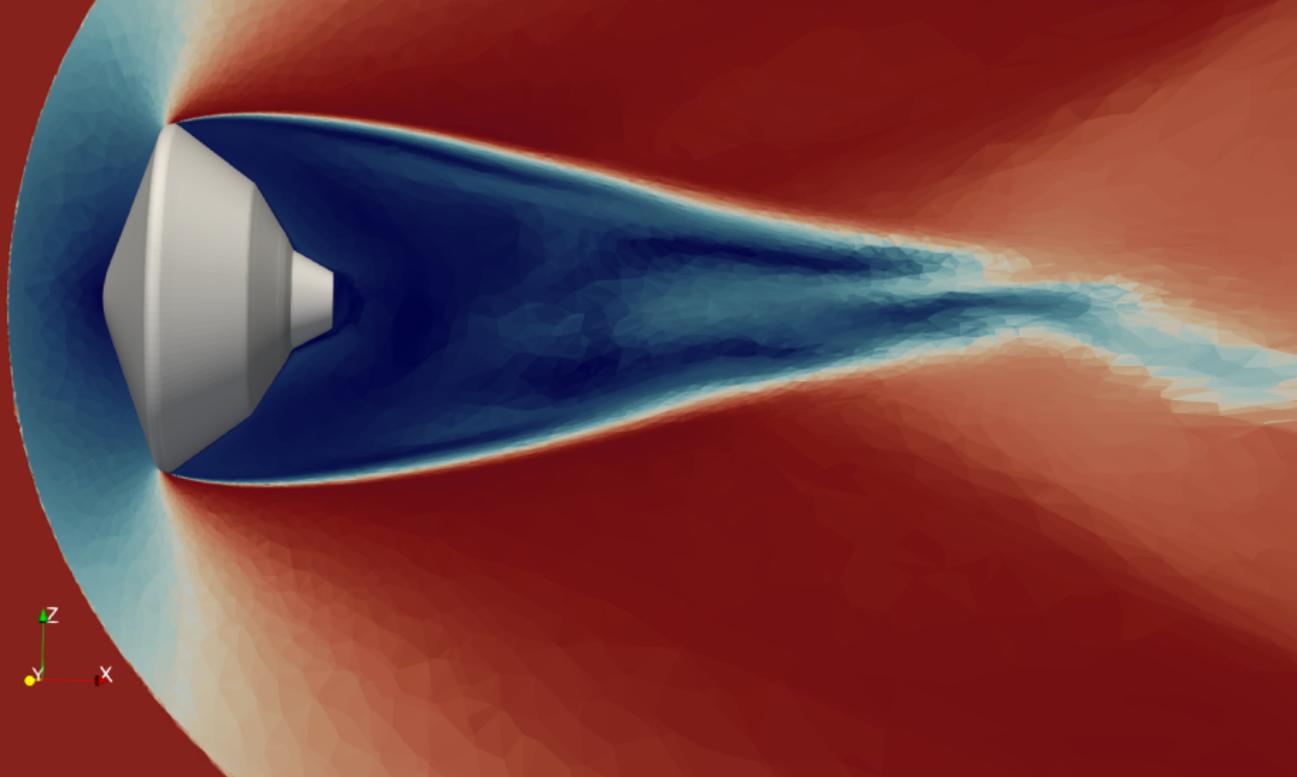
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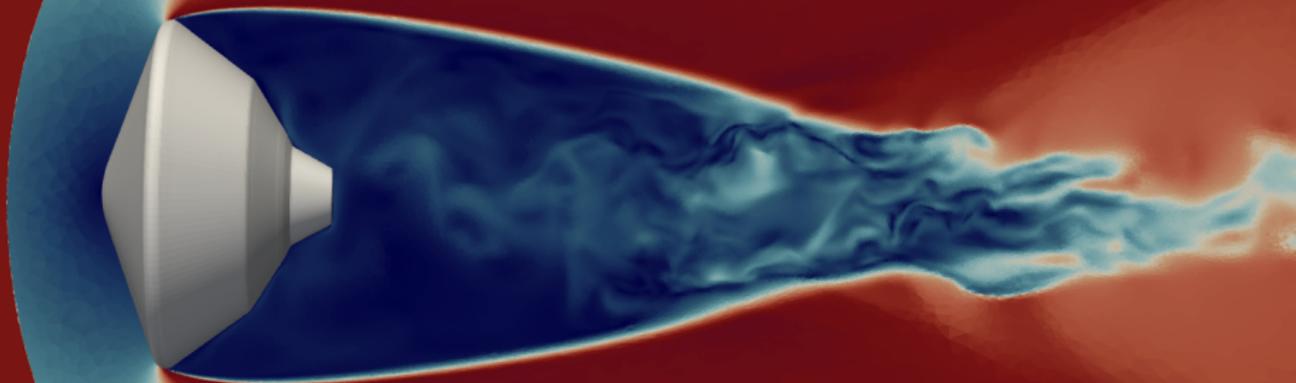
$Nn = 2.4E06$



Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

$Ne = 27.0E06$ (4.3E06 Prisms and 22.5E06 Tetrahedra)

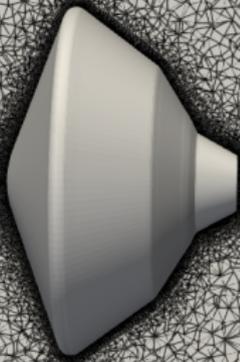
$Nn = 5.9E06$



Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

\mathcal{T}_0 has $N_e = 8.1E06$ (4.3E06 Prisms and 3.8E06 Tetrahedra)

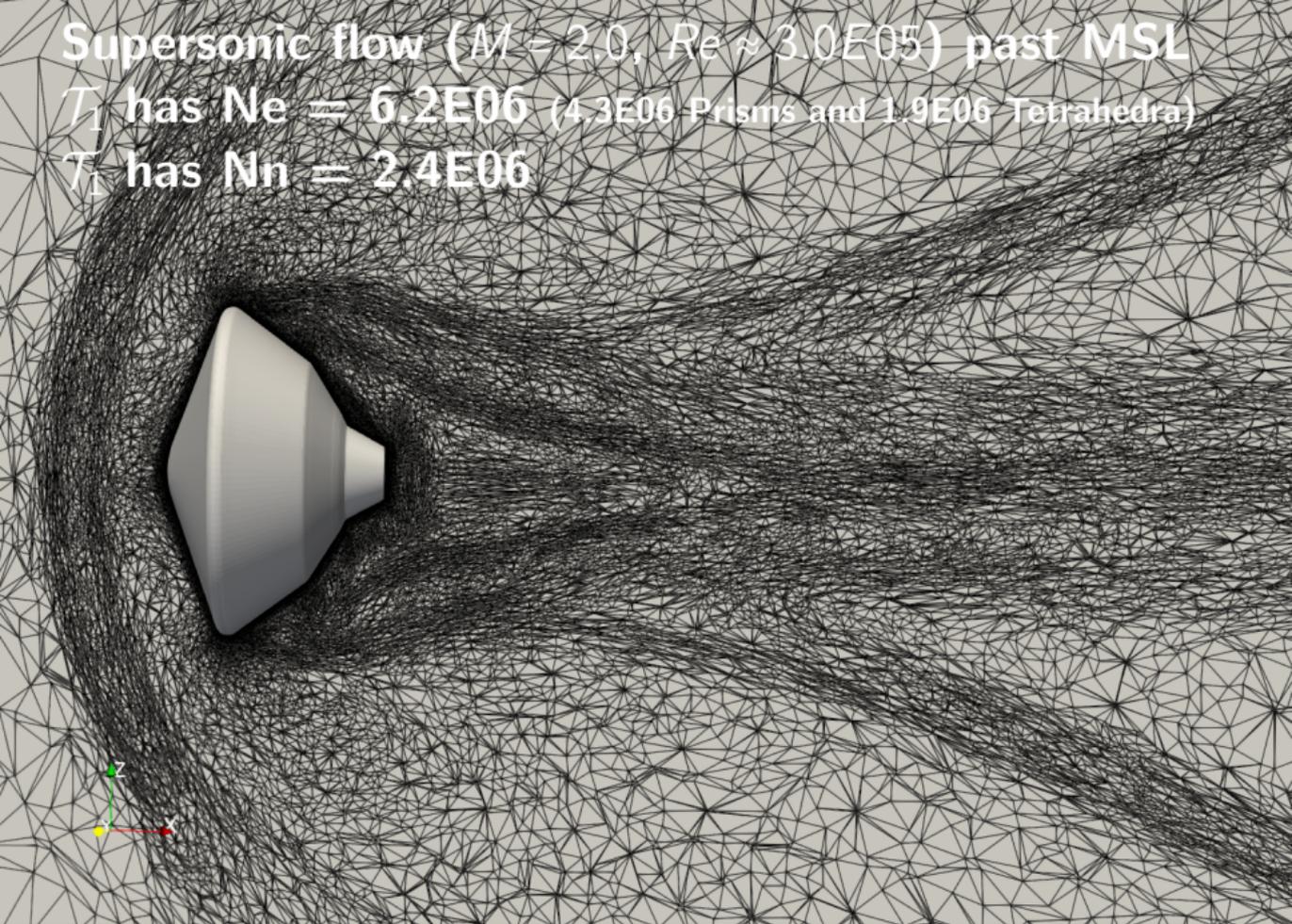
\mathcal{T}_0 has $N_n = 2.7E06$



Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

T_1 has $N_e = 6.2E06$ (4.3E06 Prisms and 1.9E06 Tetrahedra)

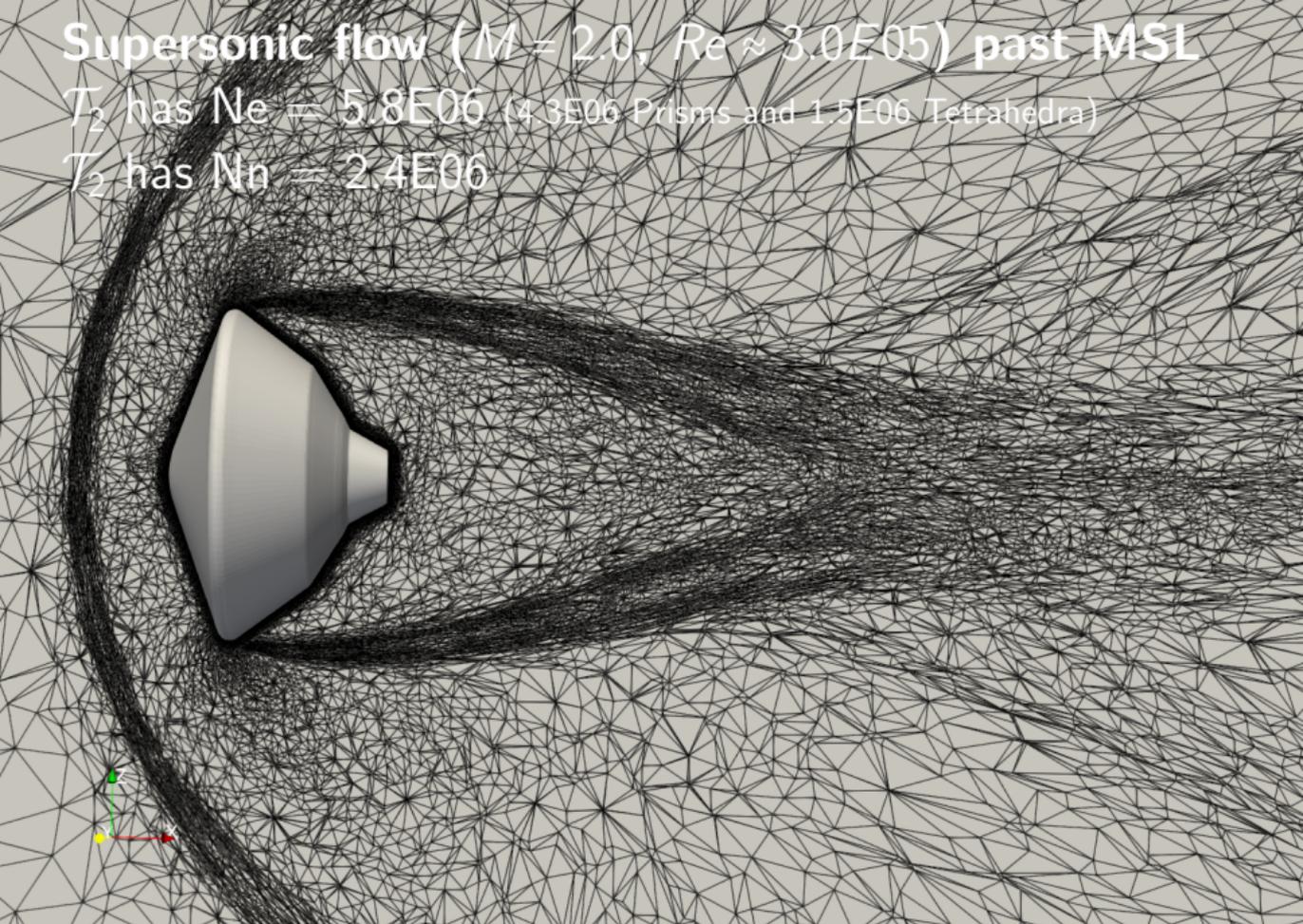
T_1 has $N_n = 2.4E06$



Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

T_2 has $N_e = 5.8E06$ (4.3E06 Prisms and 1.5E06 Tetrahedra)

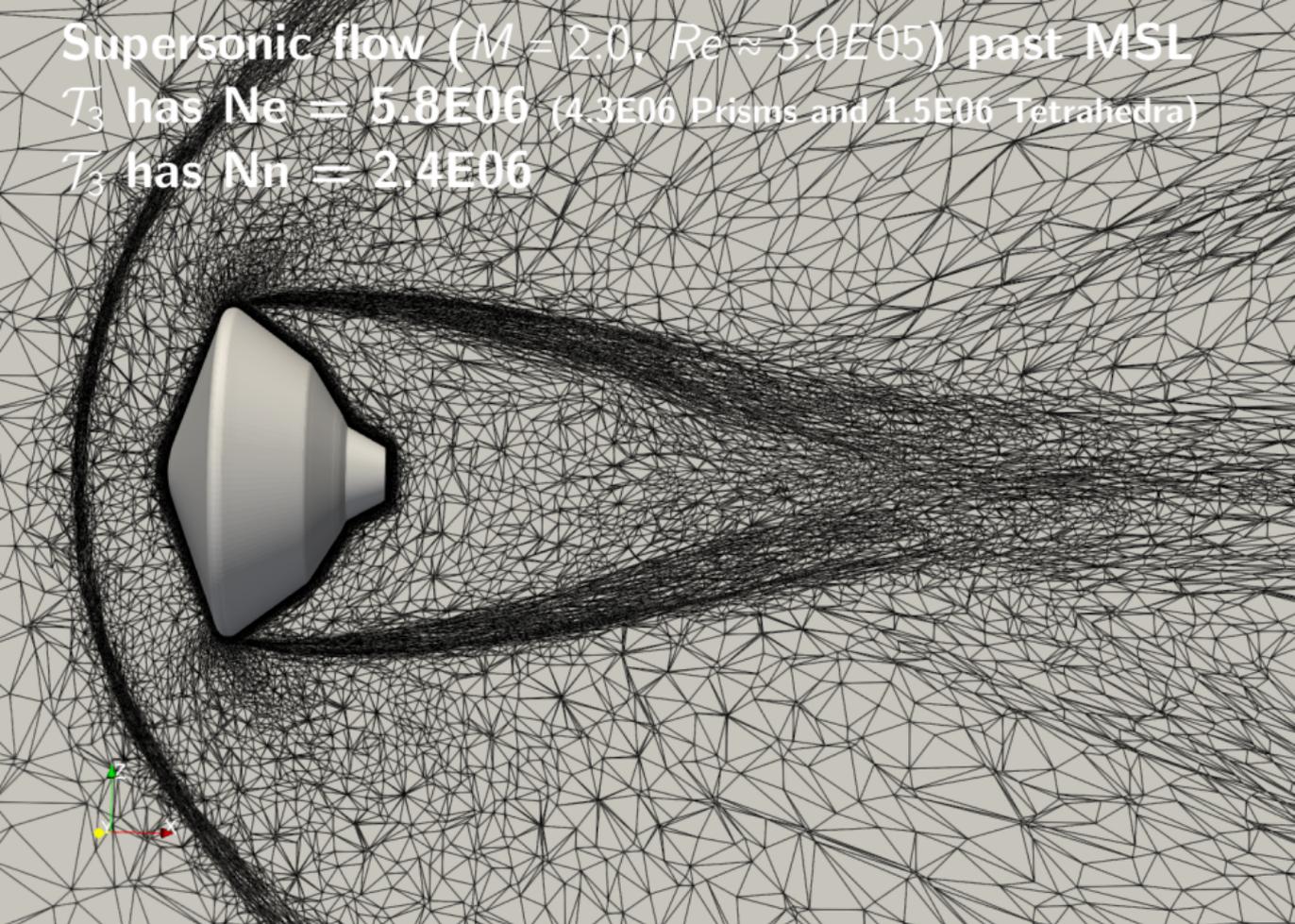
T_2 has $N_n = 2.4E06$



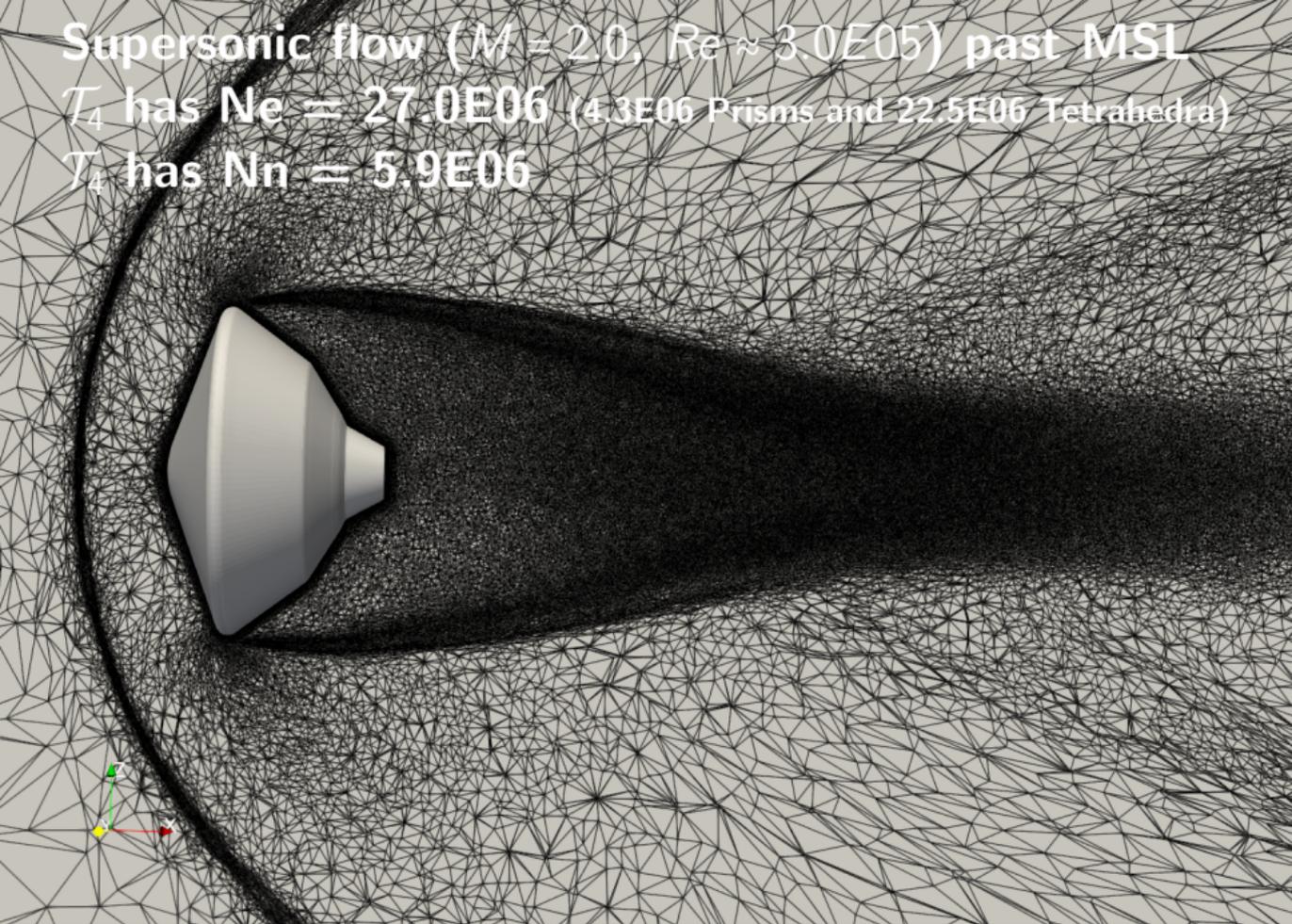
Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL

T_3 has $N_e = 5.8E06$ ($4.3E06$ Prisms and $1.5E06$ Tetrahedra)

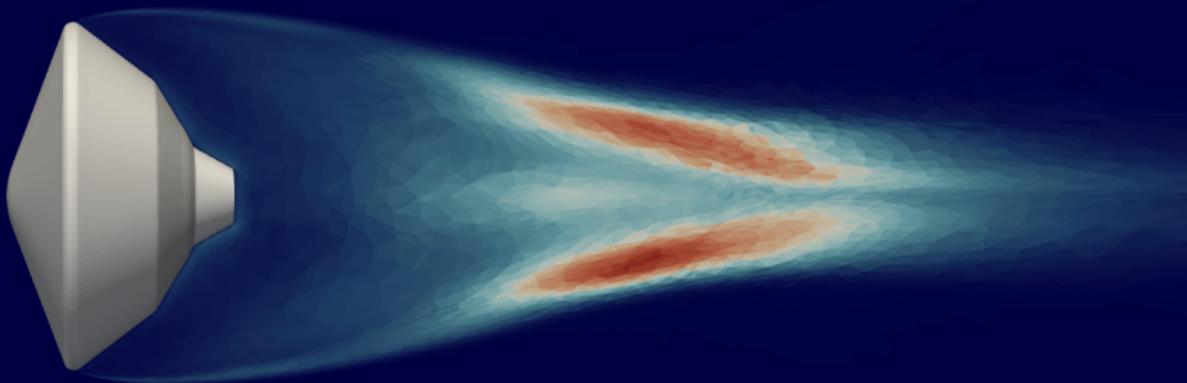
T_3 has $N_n = 2.4E06$



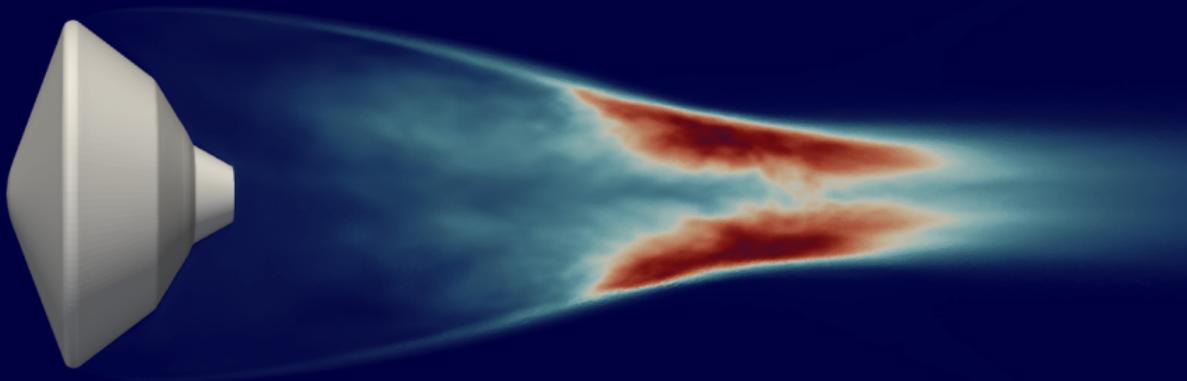
Supersonic flow ($M = 2.0$, $Re \approx 3.0E05$) past MSL
 T_4 has $N_e = 27.0E06$ (4.3E06 Prisms and 22.5E06 Tetrahedra)
 T_4 has $N_n = 5.9E06$



TKE on \mathcal{T}_3



TKE on \mathcal{T}_4



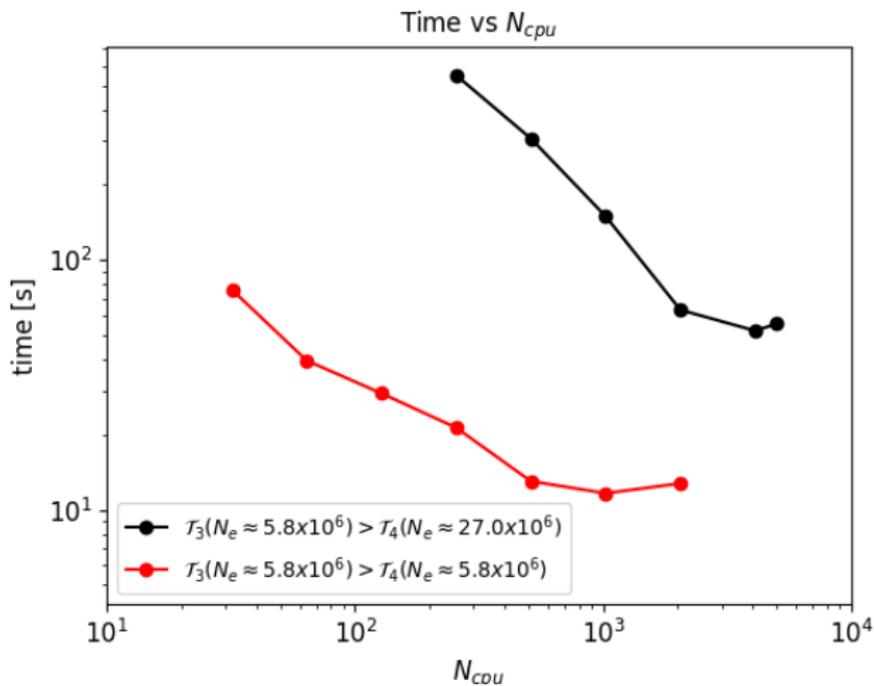
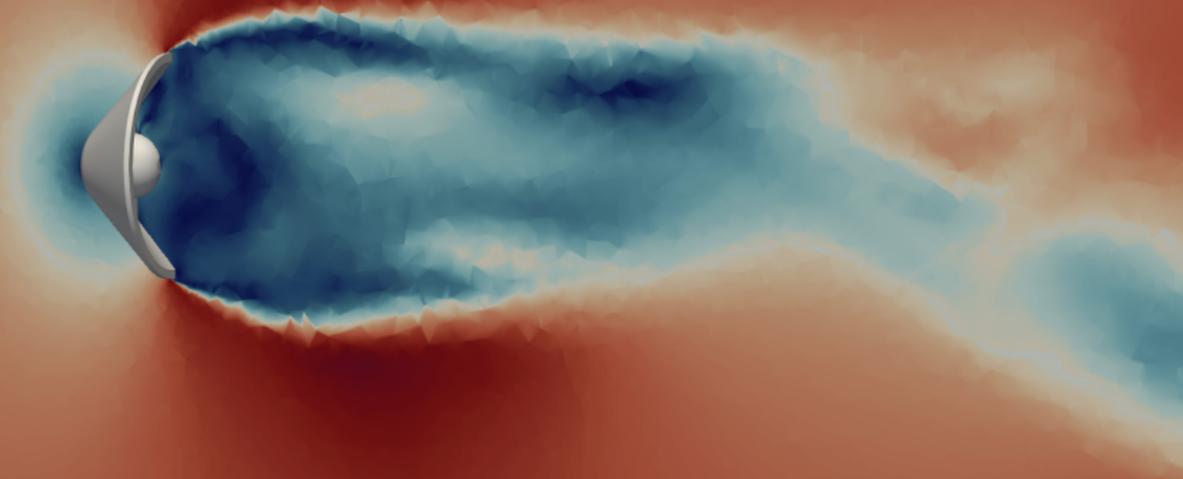
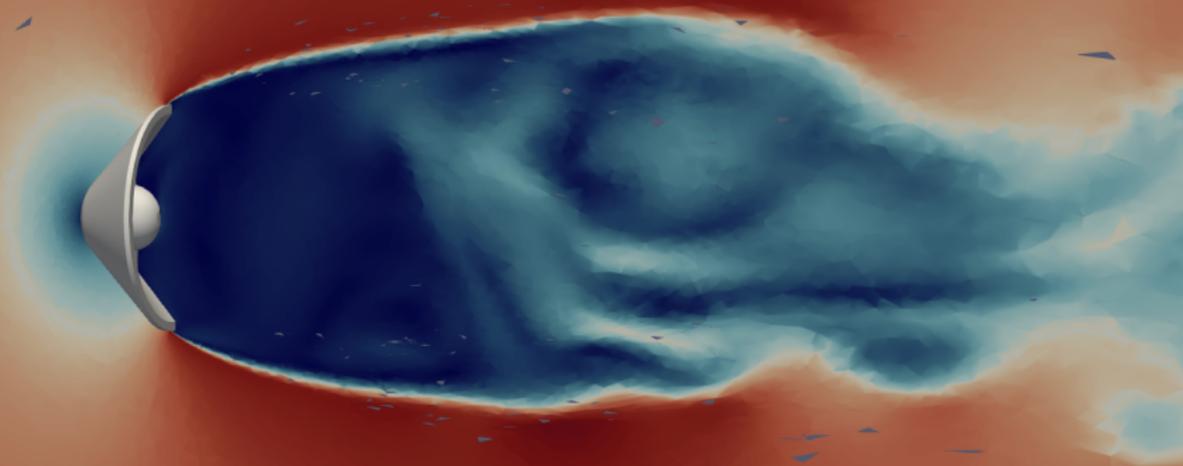


Figure: Time versus number of CPUs used to perform the adaptation for the last two adaptation iterations for supersonic flow past the MSL geometry.

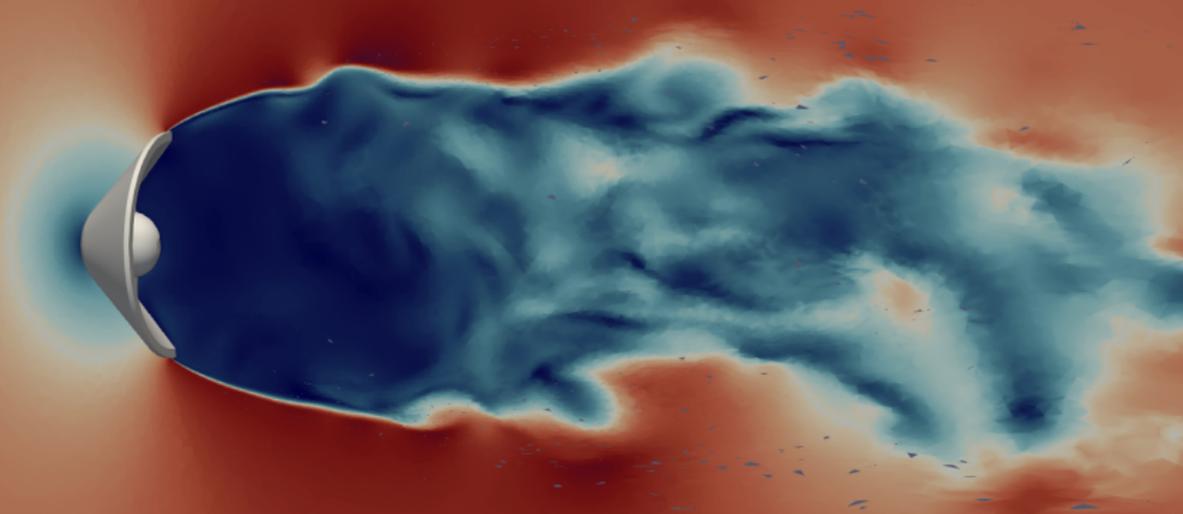
Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
Ne = 42.7E06 (37.6E06 Prisms and 5.1E06 Tetrahedra)
Nn = 19.9E06



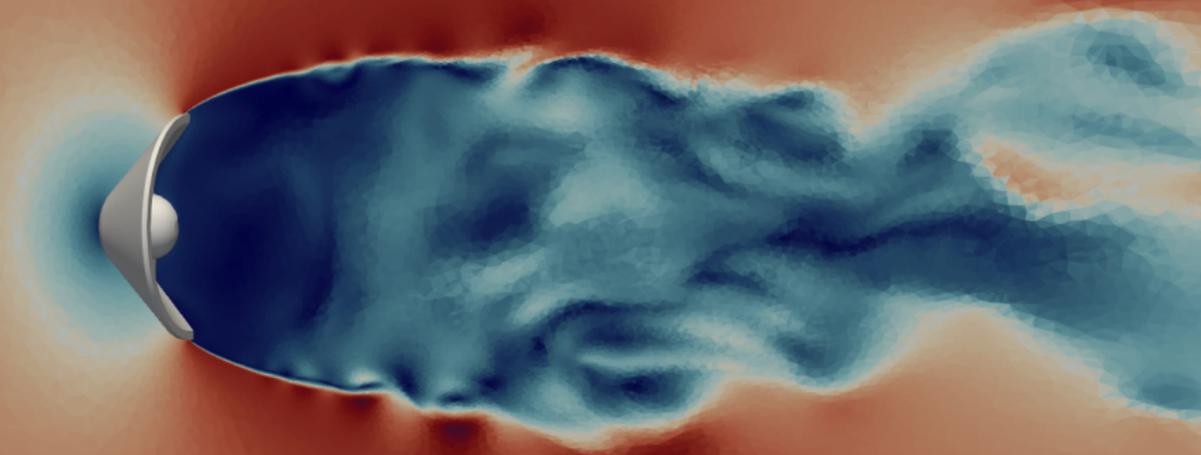
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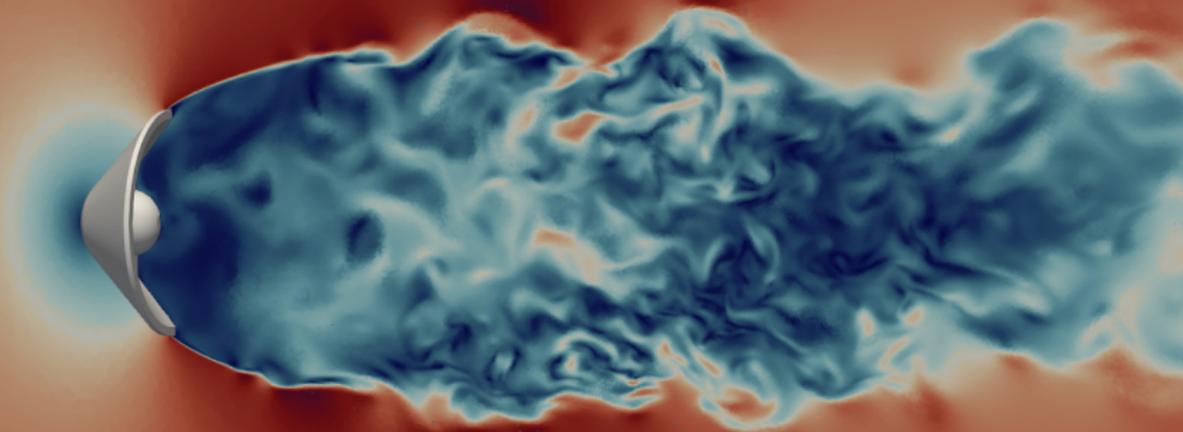
Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
 $Ne = 48.4E06$ (37.6E06 Prisms and 10.8E06 Tetrahedra)
 $Nn = 20.7E06$



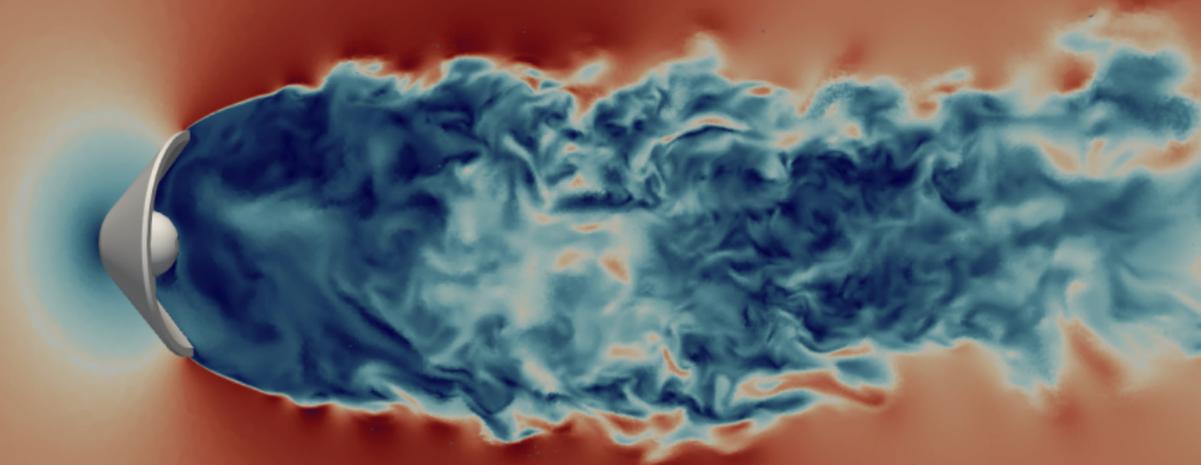
Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past **EEV**
 $Ne = 47.5E06$ (37.6E06 Prisms and 9.9E06 Tetrahedra)
 $Nn = 20.6E06$



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past **EEV**
 $Ne = 101.2E06$ (37.6E06 Prisms and 63.6E06 Tetrahedra)
 $Nn = 29.6E06$



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
Ne = 101.2E06 (37.6E06 Prisms and 63.6E06 Tetrahedra)
Nn = 29.6E06
KEC flux



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
Ne = 42.7E06 (37.6E06 Prisms and 5.1E06 Tetrahedra)
Nn = 19.9E06



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
 $N_e = 42.1E06$ (37.6E06 Prisms and 4.6E06 Tetrahedra)
 $N_n = 19.7E06$



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
 $N_e = 48.4E06$ (37.6E06 Prisms and 10.8E06 Tetrahedra)
 $N_n = 20.7E06$



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
 $N_e = 47.5E06$ (37.6E06 Prisms and 9.9E06 Tetrahedra)
 $N_n = 20.6E06$



Transonic flow ($M = 0.8$, $Re \approx 4.0E05$) past EEV
 $N_e = 101.2E06$ (37.6E06 Prisms and 63.6E06 Tetrahedra)
 $N_n = 29.6E06$



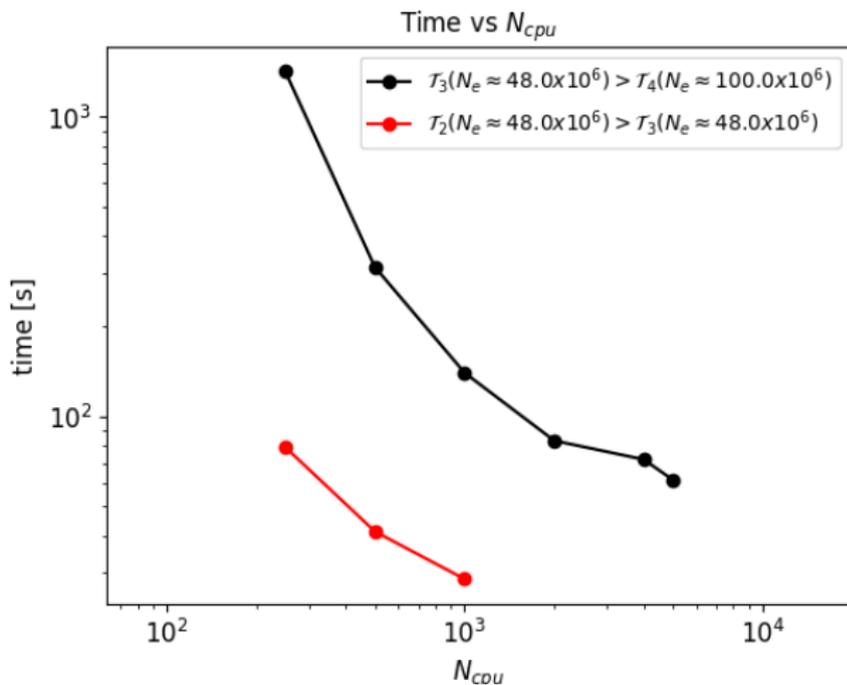


Figure: Time versus number of CPUs used to perform the adaptation for the last two adaptation iterations for supersonic flow past the EEV geometry.

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In summary...

Conclusions

- We currently have an anisotropic mesh adaptation utility that is compatible with US3D and is able to compute a solution-informed adapted mesh for realistic applications that are of interest to the EDL community.
- We have demonstrated a simplified simulation strategy that starts with a small and coarse mesh and applies iterative mesh adaptation to improve the resolution of the simulation while keeping the element count low.
- Currently we are able to generate a anisotropic adapted mesh of approximately 100×10^6 elements in 60 seconds.

Future work

- Streamline the workflow process of running the adaptive capability with US3D to improve usability of the tool.
- Improve the error estimation and include a temporal component to the metric tensor field computation.
- Potentially start employing anisotropic mesh refinement to the dynamic stability calculations for the Earth Entry Vehicle geometry.