

A Strategy to Optimize Local Phase Transformation Strengthening for Next Generation Superalloys

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Motivation for Mechanistic Studies

(°C)



- Material advancements are required to accommodate the higher compressor exit temperatures in jet turbine engines (>700°C near the rotor rim) for improved efficiency and pollution reduction.

- New deformation mechanisms will become dominant at these higher operating temperatures along with a need for improved creep properties in these disk alloys.

- New understanding and materials will be needed for future advancements



Segregation along Stacking Faults



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Segregation along superlattice stacking faults has been observed in numerous Ni and **Co-based** superalloys.



Phase Transformation Strengthening



S202



New insight into alloy effects:

• Segregation of γ formers in ME3 promotes microtwinning

 Formation of η phase at faults in ME501 inhibits microtwinning and improves creep strength

Material Preparation







ME3 Average Grain Diameter = $59.2 \mu m$ LSHR Average Grain Diameter = $59.9 \mu m$



Alloy	Secondary γ' VF	Tertiary γ' VF	Total γ' VF	Average Secondary γ' Size	Average Tertiary γ' Size
ME3	43.97 ± .6	2.65 ± .4	46.61 ± 1.0	135 nm	15.4 nm
LSHR	43.52 ± 1.7	2.27 ± .1	45.80 ± 1.8	154 nm	15.9 nm



The two alloys are microstructurally comparable!

Smith, et al. Acta Materialia, 2019

Creep Performance of ME3 and LSHR





- Creep tests were performed at 760°C under a stress of 552MPa
- LSHR has consistently performed better in creep compared to ME3 in this temperature regime. Why?

Phase Transformation Softening – γ Phase



γ phase formation along SISF promotes stacking fault ribbon shear

SISF = Superlattice Intrinsic stacking Fault



Phase Transformation Strengthening – χ Phase





χ phase formation along SISF inhibits stacking fault ribbon shear

SISF = Superlattice Intrinsic stacking Fault



Phase Transformation Strengthened Superalloys





Can the η and χ phase transformation strengthening mechanisms be combined into a single alloy without precipitating bulk topologically close packed (TCP) phases?





Development of Transformation Strengthened NASA Alloys (TSNA)

Alloy	Cr	Со	AI	Ti	Nb	Мо	Та	W	Hf	В	С	Ni
LSHR	12.5	20.4	3.5	3.5	1.5	2.7	1.5	4.3	0	0.03	0.045	Bal
ME3	13	21	3.4	3.8	0.8	3.7	2.4	2.1	0	0.02	0.05	Bal
TSNA-1	10.9	19	2.9	3	1.4	2.6	5.0	4.5	0.37	0.025	0.05	Bal









Avg. Grain Size: 60um Avg. Grain Size:

Avg. Grain Size: 19.2um Avg. Grain Size: 19.8um

Alloy	Secondary γ' VF	Tertiary γ' VF	Total γ' VF	Average Secondary γ' Size	Average Tertiary γ' Size
ME3	44.8 ± 0.5 %	2.6 ± 0.2 %	47.4 ± 0.6 %	234 nm	36.4 nm
LSHR	45.4 ± 1.8 %	3.4 ± 0.4 %	48.7 ± 1.3 %	243 nm	39.8 nm
TSNA-1	54.0 ± 0.2 %	0.6 ± 0.2 %	54.5 ± 0.3 %	311 nm	38.5 nm

By not forging the TSNA-1 alloy, grain sizes remained fine in comparison to LSHR. A fine grain LSHR was produced for a better comparison.



Creep Properties





TSNA-1 presents significantly better creep properties over current state of the art alloys through possible phase transformation strengthening

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Creep Deformation in TSNA-1





Deformation was dominated by isolated faulting in the γ' precipitates and dislocations gliding in the matrix.



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Ordered segregation observed in HAADF images of both fault types

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Phase Transformations in TSNA-1 - SISF







γ' to χ phase transformation confirmed along SISFs

Phase Transformations in TSNA-1 - SESF





γ' to η phase transformation confirmed along SESFs





Density Functional Theory Calculations



Binary $L1_2$, $D0_{19}$, and $D0_{24}$ cells were produced for energy calculations



Density Functional Theory Calculations





National Aeronautics And Space Administration

Future Work: Molecular Dynamic Models – Nb Segregation along SISFs



T = 1000 K

Ni and Al atoms not shown

Substituted 10% AI in precipitate with Nb



National Aeronautics And Space Administration

Future Work: Molecular Dynamic Models - χ Phase Effect on Dislocation Motion







sxz = 400 MPa syz = 693 MPa stot = 800 MPa T = 1000 K

Ni atoms not shown

0% Nb

sxz = 400 MPa syz = 693 MPa stot = 800 MPa T = 1000 K

Ni atoms not shown

7.5% Nb





Why Phase Transformations?









D0₂₄





Local crystal structure + composition + observed Z contrast ordering = Local phase transformation along faults

Future Work



Forged TSNA-1





ELEBRATI



Conclusions



- The creep performance of TSNA-1 is significantly better compared to LSHR and ME3 despite testing conducted on an overall similar, though not yet optimized, microstructure.
- The creep deformation at 760°C/552MPa in TSNA-1 is dominated by dislocation glide in the γ channels and isolated faulting in the γ ' precipitates.
- High resolution STEM analysis reveals the formation of χ phase along SISFs and η phase along SESFs for TSNA-1.
- The formation of these phases along the faults may explain the superior creep properties exhibited by TSNA-1, as the grain and γ' microstructure fail to do so.
- The strengthening η and χ phase transformations can be combined in future Ni-base disk alloy compositions for improved creep properties





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