



## In-situ Measurements using a Configurable Architecture Additive Testbed System

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- Summary



# NASA Transformational Tools and Technologies (TTT) Project



#### Introduction







#### **Objectives:**

Reduce the total Life Cycle Costs by:

- 1. Enabling Certification by Analysis to reduce surprises during flight tests
  - Develop and validate eddy resolving methods for airframe and propulsion system applications
  - Design and execute CFD validation experiments
  - Develop pressure & temperature sensitive paints to support dynamic measurements
  - Develop applicable velocimetry techniques for time-resolved unsteady flow
- 2. Increase manufacturing rate and reduce weight of materials during production
  - Develop computational validation of additive and other advanced manufacturing processes
  - Advance rapid manufacturing of composite unitized structures
  - Develop advanced materials and structural concepts
- 3. Decreasing the amount of required maintenance during Operations and Maintenance Phase
  - Enable predictive maintenance methods through advances in data fusion methods and techniques



## NASA Transformational Tools and Technologies Project



### Additive Manufacturing (Metals)

TACP - Transformational Tools & Technologies Project





## In-situ Measurements using Configurable Architecture Additive Testbed (CAAT)



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#### Objectives

- Investigate the use of a low cost in-situ near infrared (NIR) sensor for real time measurement of the thermal history for improved additive manufactured builds.
- Calibrate the NIR sensor and investigate the measured melt pool size based on varying process parameters.
- Compare the melt pool width with microscopy measurements.

#### Payoffs

• Additively manufactured parts must be certified for broad application onto aircraft structures. By documenting the thermal history, process parameters for microstructure can be evaluated and real time inspections can be performed during the AM build. These results can be used to validate thermal models and build process parameters.



#### CAAT System Layout





![](_page_7_Picture_0.jpeg)

## **Co-axial NIR Optical Path**

![](_page_7_Picture_2.jpeg)

![](_page_7_Figure_3.jpeg)

![](_page_7_Figure_4.jpeg)

• NIR camera has 640 x 480 FPA, maximum frame rate = 751 Hz, pixel pitch is 4.8 x 4.8 um, configured with focusing optics and 880 nm narrow bandpass filter (875-884nm), resolution approximately 8.55 microns, ROI for images 144 x144, and provides frame rate of approximately 2,000 Hz.

![](_page_8_Picture_0.jpeg)

![](_page_8_Picture_1.jpeg)

# Effective Radiance and Calibration

$$Radiance = \frac{1}{2} \int_{\lambda_1}^{\lambda_2} \frac{c_1}{k^5 \left(e^{\frac{c_2}{\lambda(T+273.15)}} - 1\right)} * sensor(\lambda) * filter(\lambda) * d\lambda \quad \text{where } c_1 = 2 * h * c^2 \quad \text{and} \quad c_2 = \frac{h * c}{k}$$

![](_page_8_Figure_5.jpeg)

![](_page_8_Picture_6.jpeg)

- Spectral band 875 to 884 nm defined by the 880 nm narrow bandpass filter.
- •Camera frame rate approximately 2,000. Hertz with ROI pixel array size of 144x144.
- •Temperatures used were 900, 1000, 1100, 1200, 1300, 1400, and 1500 degrees C for integration times were varied 59, 75, 100, 150, 300, 500, 700, 900, 1200, and 1500 micro-seconds.

![](_page_9_Picture_0.jpeg)

![](_page_9_Picture_2.jpeg)

![](_page_9_Figure_4.jpeg)

![](_page_10_Picture_0.jpeg)

## In-situ NIR Melt Pool Imaging Results

![](_page_10_Picture_2.jpeg)

![](_page_10_Figure_3.jpeg)

Pixel Position (microns)

0.000

![](_page_11_Picture_0.jpeg)

![](_page_11_Picture_2.jpeg)

- Radiometric calibration for interpretation of camera imagery.
- Thermal camera pixel resolution Measured Pixel Resolution Approximately 8.55 microns.
- Solidus temperature value 1605 Degrees C (Ti-6Al-4V).
- Blurring due to movement of laser beam vs. camera integration time.
- Surface emissivity value (vary with material, surface geometry and temperature).
- Accurate destructive measurements using microscopy.

![](_page_12_Picture_0.jpeg)

#### Melt Pool Imagery (Laser Scanning 500 mm/sec) for Various Emissivity Values Compared to Optical Microscopy – <u>Blurring Uncorrected</u>

![](_page_12_Picture_2.jpeg)

![](_page_12_Figure_4.jpeg)

Melt Pool Imagery (Laser Scanning 750 mm/sec) for Various Emissivity Values Compared to Optical Microscopy – <u>Blurring Uncorrected</u>

![](_page_13_Picture_1.jpeg)

![](_page_13_Figure_3.jpeg)

![](_page_14_Picture_0.jpeg)

![](_page_14_Picture_1.jpeg)

# Removal of Blurring using Inverse Filtering

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- Laser velocity of 500 and 750 mm/sec combined with camera integration time (200 microseconds) results in ~ 12 pixel and ~ 18 pixel blur respectively.
- Use Weiner inverse filtering technique to remove camera blur.

$$W(u,v) = \frac{H^{*}(u,v)}{|H(u,v)|^{2} + K(u,v)}$$

Deblurred Image (u, v) = W(u, v)BlurredImage (u, v)

![](_page_14_Figure_8.jpeg)

![](_page_15_Picture_0.jpeg)

Melt Pool Imagery (Laser Scanning 500 mm/sec) for Various Emissivity Values Compared to Optical Microscopy – <u>Blurring Corrected</u>

![](_page_15_Picture_2.jpeg)

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![](_page_15_Figure_4.jpeg)

X Position (microns)

# Melt Pool Imagery (Laser Scanning 750 mm/sec) for Various Emissivity Values Compared to Optical Microscopy – <u>Blurring Corrected</u>

![](_page_16_Picture_1.jpeg)

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![](_page_16_Figure_3.jpeg)

 Inverse deblurring filter helps with agreement, however other factors might be contributing to these errors such as plume effects, calibration errors, sensor blooming, etc.

![](_page_17_Picture_0.jpeg)

![](_page_18_Picture_0.jpeg)

![](_page_18_Picture_2.jpeg)

![](_page_18_Figure_3.jpeg)

![](_page_18_Figure_4.jpeg)

227 Celsius

 The COMSOL model uses a volumetric heat source and was calibrated to the optical microscopy measurements. The gray center in the middle shows the melt pool and semi-solid regions.

![](_page_19_Picture_0.jpeg)

# Preliminary Comparison of Measured Radiance to Model for

![](_page_19_Picture_2.jpeg)

Melt Pool Width

![](_page_19_Figure_4.jpeg)

![](_page_19_Figure_5.jpeg)

- Comparison of in-situ measured melt pool width to model predictions is progressing.
- Radiometric calibration allows for initial comparisons to models however, emissivity, plume effects, powder splatter, varying melt properties, etc. can make things challenging.

# **Most Recent Results**

![](_page_20_Picture_2.jpeg)

- Higher speed cameras installed for improved temporal and spatial imaging.
- Registration of in-situ measurements to Xray CT.
- Future work: continue/refine comparison of melt pool width measurements to FEM models for given process parameters.

![](_page_20_Picture_6.jpeg)

![](_page_20_Picture_7.jpeg)

![](_page_20_Picture_8.jpeg)

![](_page_21_Picture_0.jpeg)

![](_page_21_Picture_1.jpeg)

### **Recent Fabrication using CAAT System**

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Built Example

![](_page_21_Figure_5.jpeg)

![](_page_21_Figure_6.jpeg)

**Designed Part** 

 Disk slices represent different build parameters denoted by circumferential numbering scheme.

![](_page_22_Picture_0.jpeg)

![](_page_22_Picture_1.jpeg)

## In-situ Monitoring Mapping of Built Part

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#### As built example part

![](_page_22_Picture_5.jpeg)

#### Melt pool image, 3kHz sampling rate @ 12bit

![](_page_22_Figure_7.jpeg)

![](_page_22_Figure_8.jpeg)

![](_page_23_Picture_0.jpeg)

![](_page_23_Picture_2.jpeg)

![](_page_23_Figure_4.jpeg)

# Porosity segmented X-Ray computed tomography

![](_page_23_Figure_6.jpeg)

![](_page_24_Picture_0.jpeg)

## Summary

![](_page_24_Picture_2.jpeg)

- A low cost NIR camera was calibrated and used to measure the width of the melt pool on a Ti-6Al-4V plate.
- Blurring effects, due to relatively long integration time, was reduced by inverse filtering.
- Optical microscopy measurements were used to compare the NIR melt pool width with marginal agreement. Need to investigate error in optical microscopy measurements to validate NIR melt pool width measurements.
- CAAT system operational for building AM parts with high-speed cameras used for in-situ measurements.
- Registered in-situ infrared measurements with X-ray CT for volume comparisons.