



NETS

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**NUCLEAR and
EMERGING
TECHNOLOGIES for
SPACE**



Nuclear Electric Propulsion Modular Power Conversion Model

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Agenda

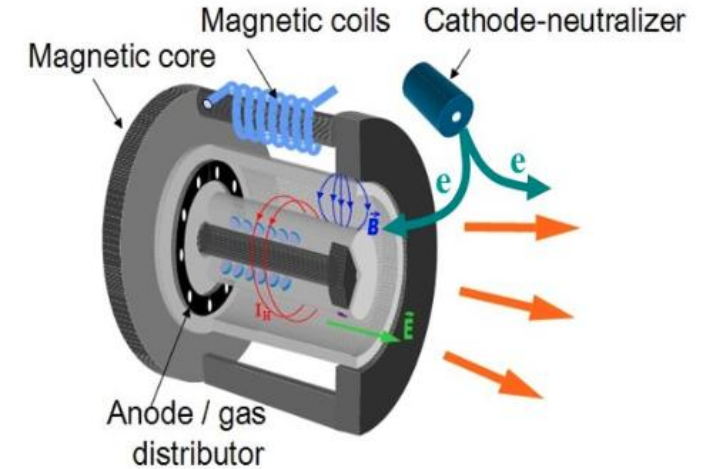
- Introduction
- Working Fluids Considered
- Heat Transfer
- Turbomachinery
- Integrated Model
- Results
- Conclusion/Future Work



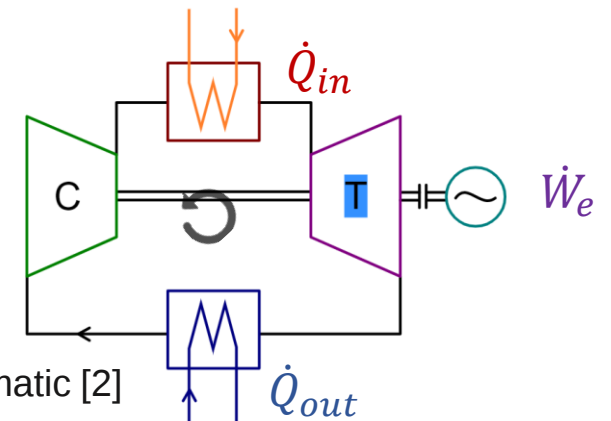
Introduction

Nuclear Electric Propulsion (NEP) – nuclear power plant for electricity production

- NEP uses a nuclear reactor to produce electricity for electric thrusters to accelerate heavy noble gases to provide thrust.
- There are multiple ways of converting thermal energy into electricity for space applications:
 - Brayton
 - Stirling
 - Rankine
- Current research focuses on the Brayton cycle due to scalability, single-phase working fluid, and high TRL.



Hall Thruster Diagram [1]

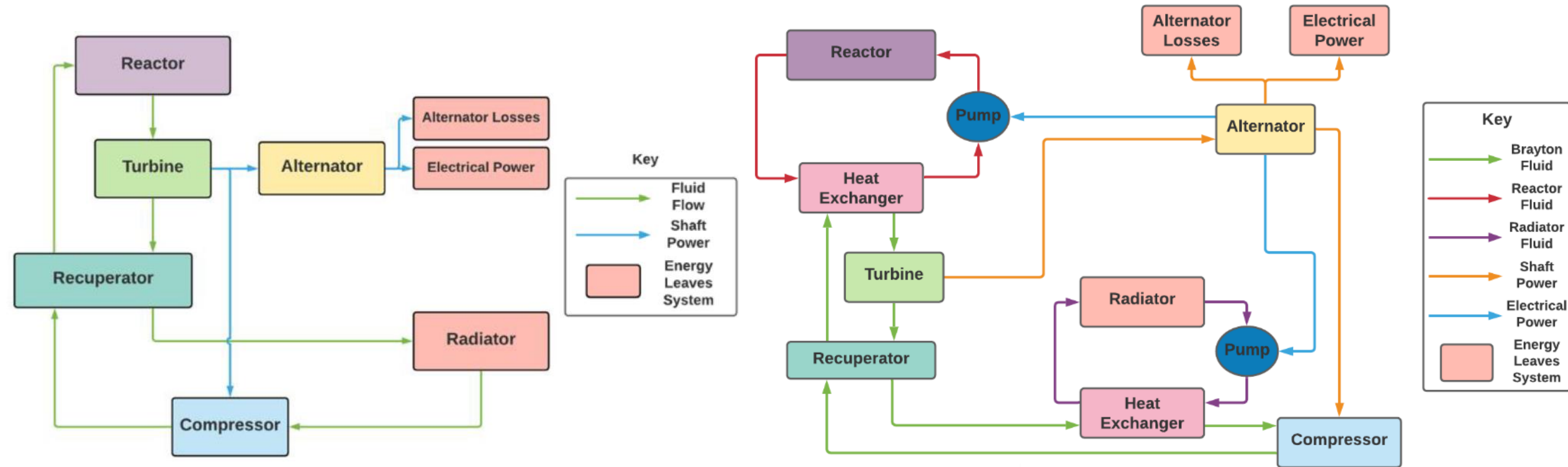


Brayton Cycle Schematic [2]



Brayton Power Conversion Loop Options

Heat source is the nuclear reactor, heat sink is the radiator



High pressure losses could be incurred at the reactor and radiator, therefore, separate loops with different fluids are considered



Working Fluids

Fluid property libraries allow for variable property considerations

- Brayton Fluid: Helium (72%) + Xenon (28%) to yield 40 g/mol consistent with the BRU studies [3]
 - Properties for individual fluids are taken from CoolProp [4] and REFPROP [5].
 - To consider mixture ratios:
 - Thermophysical properties use the mass fraction lever rule
 - Transport property mixture correlations developed from kinetic theory [6-8]
 - Future work will consider other mixture ratios of these fluids.
- Reactor Fluid: Lithium
- Radiator Fluid: Eutectic NaK
- Liquid alkali metal properties are taken from Meisl [9].

Fluid property libraries allow for variable property considerations



Heat Transfer Components

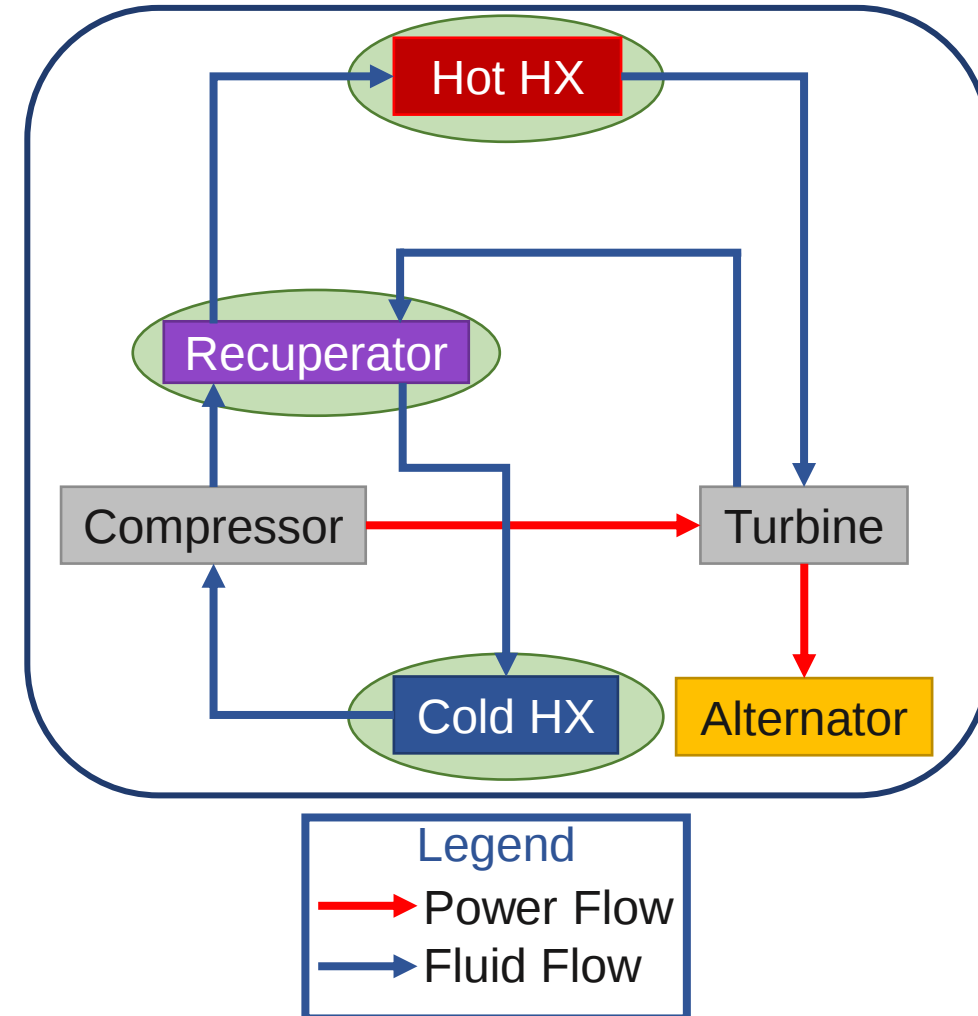
Simple models pave the way for complex component models

- Reactor
 - Power is based on 1st law enthalpy.
 - Pressure losses are assumed.
- Radiator
 - Area is iteratively scaled
 - Frictional pressure losses are calculated.
- Recuperator and Heat Exchangers
 - Based on NTU method.
 - Effectiveness is assumed.
- Future work will consider higher fidelity models of these components.

$$\dot{Q} = \dot{m}(h_{out} - h_{in})$$
$$T = T(h, P)$$

$$\Delta P = f \frac{\rho V^2}{2D}$$

Although simple, each component is self-contained and can grow in complexity



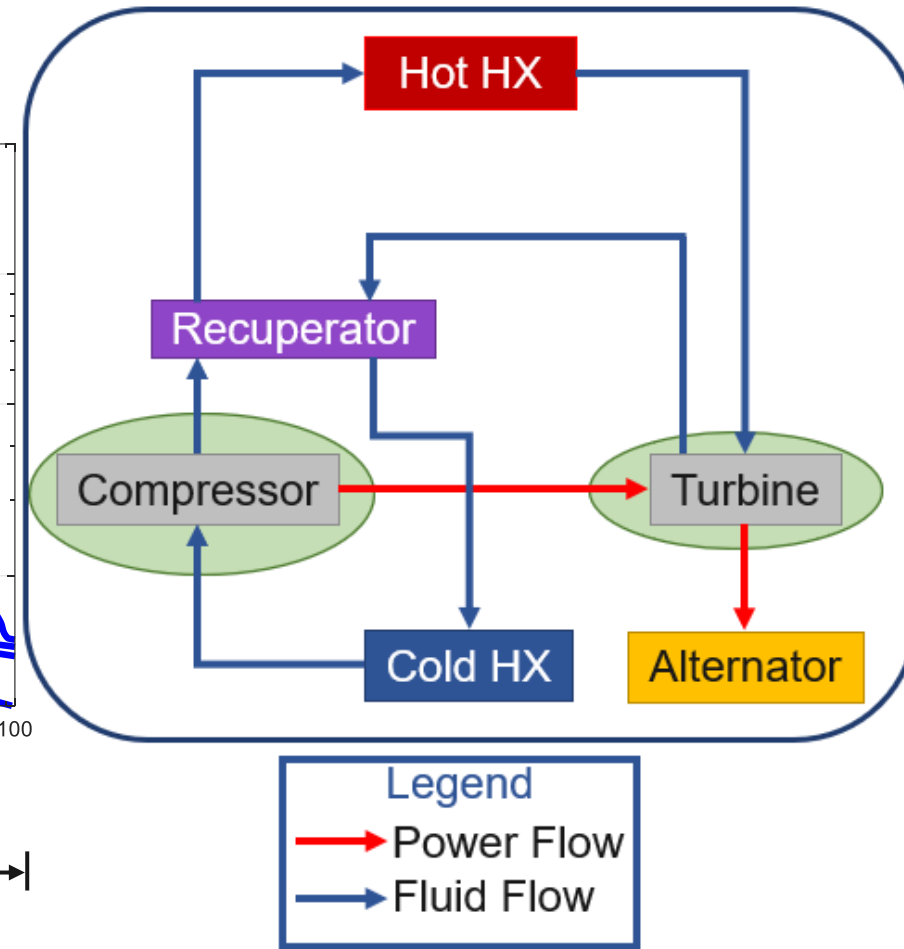
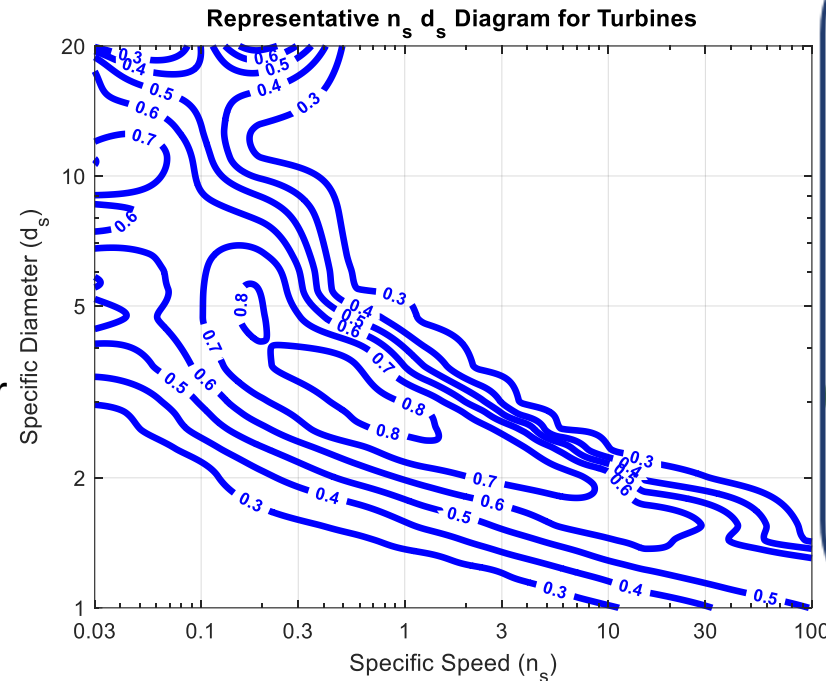
Turbomachinery

Complex component models can inform off-nominal operation

- **Defined by:**
 - Shaft speed ω
 - Efficiency η
 - Outlet pressure/pressure ratio
- **Solves for:**
 - Diameter D
 - Specific speed n_s
- Specific speed and specific diameter d_s are related to each other through efficiency η .

$$n_s = \frac{\omega \sqrt{\dot{V}}}{(g_0 H)^{3/4}} = \frac{\omega \sqrt{\dot{m}}}{\sqrt{\rho} (h_{in} - h_{out})^{3/4}}$$

$$d_s = \frac{D (g_0 H)^{1/4}}{\sqrt{\dot{V}}} = \frac{D \sqrt{\rho} (h_{in} - h_{out})^{1/4}}{\sqrt{\dot{m}}}$$



Turbomachinery Validation

- Validation was performed against a NASA Fission Surface Power study [11].
- Efficiency contour plot [10] had to be corrected by 6.5% to better match the results.

COMPRESSOR (Pressure Ratio = 2.065; 65,694 RPM)					
Inlet Temperature (K)		Inlet Pressure (kPa)		Mass Flow Rate (kg/s)	
360.93		330.94		0.54	
Parameter	Reference	Current Model	Difference (%)	Current Model (Corrected)	Difference (%)
Efficiency	84.23	79.13	6.05	84.23	0.00
Power	33339.80	36173.60	8.50	33979.94	1.92
Exit Temperature	428.15	433.40	1.23	429.30	0.27

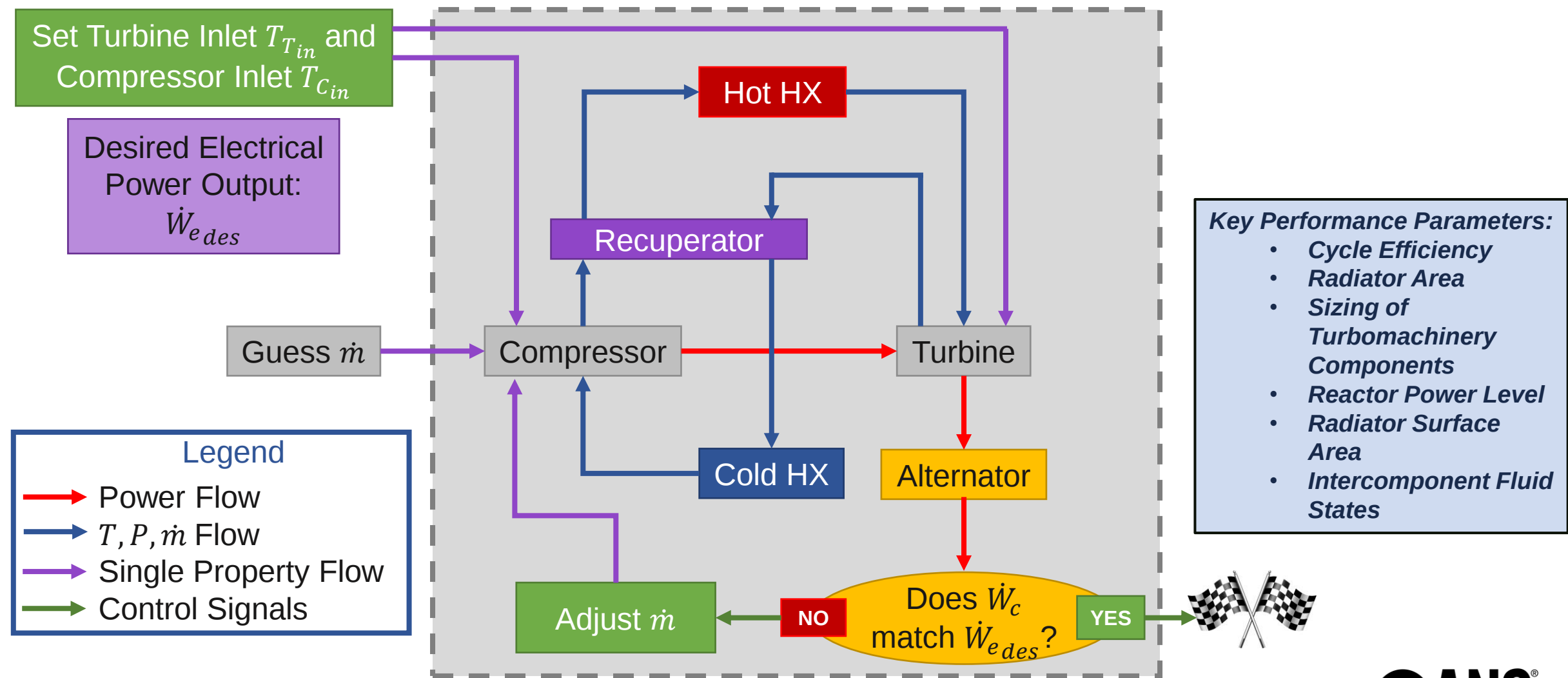
TURBINE (Pressure Ratio = 2.067; 65,694 RPM)					
Inlet Temperature (K)		Inlet Pressure (kPa)		Mass Flow Rate (kg/s)	
844.26		682.58		0.54	
Parameter	Reference	Current Model	Difference (%)	Current Model (Corrected)	Difference (%)
Efficiency	86.10	80.25	6.79	86.10	0.00
Power	50285.00	47090.00	6.35	50520.00	0.47
Exit Temperature	763.71	768.90	0.68	763.40	0.04

As a “Rule-of-Thumb”, model-model validation is achieved at less than 4% error while model-experiment validation is achieved at less than 8% error. [12]



Solution Method

Iterative solution converging on the cycle mass flow rate



Model Input GUI

Species 1
CO2

1

Species 2
None

0

Species 3
None

0

Mixture Type

Molar

Mass

Turbine Diameter (m)
0.147974

Turbine ns
0.453248

of Turbines
1

Solve Turbine

Pass

Solve

Turbine Pressure Ratio
2.7

Turbine Efficiency (%)
80

Compressor Diameter (m)
0.089

Compressor ns
0.376712

of Compressors
1

Solve Compressor

Pass

Solve

Shaft RPM
50000

Compressor Efficiency (%)
80

System Pressure Type
Turbine Inlet

System Pressure (MPa)
20

Brayton Mass Flow Rate (kg/s)
(Initial Condition)
27.15971

Alternator Efficiency (%)
92

Desired Electrical Power (kW)
1000

Max System Iterations
2

System Thermal Losses kW
5

Data Output

Write

Sheet #
1

Row Start
2

Run Number
1

Pass

FILE NAME

Input GUI

Radiator

Radiator Pressure Loss Type
Absolute

Percent

Radiator Pressure Loss (kPa or %)
1

Radiator Outlet T (K)
500

Emissivity
0.9

T Sink
4

View Factor
0.85

Number of Radiator Pipes
2

Radiator Pipe Diameter (m)
0.1

Radiator Pipe Length (m)
120

Area Step (m^2)
5

Maximum Iterations
100000

Radiator Loop
NaK

RADIATOR LOOP

Reactor

Reactor Pressure Loss Type
Absolute

Percent

Reactor Pressure Loss (kPa or %)
800

Reactor Outlet T (K)
1300

Reactor Loop
Lithium

REACTOR LOOP

m_dot Error Tolerance (%)
0.01

T_turbine Error Tolerance (%)
0.05

Recuperator

Pressure Loss Type
Absolute

Percent

Hot Pressure Loss (kPa or %)
1.5

Cold Pressure Loss (kPa or %)
1.5

Efficiency (%)
85

CALCULATE

Display Diagnostics in:
MATLAB

Simulink

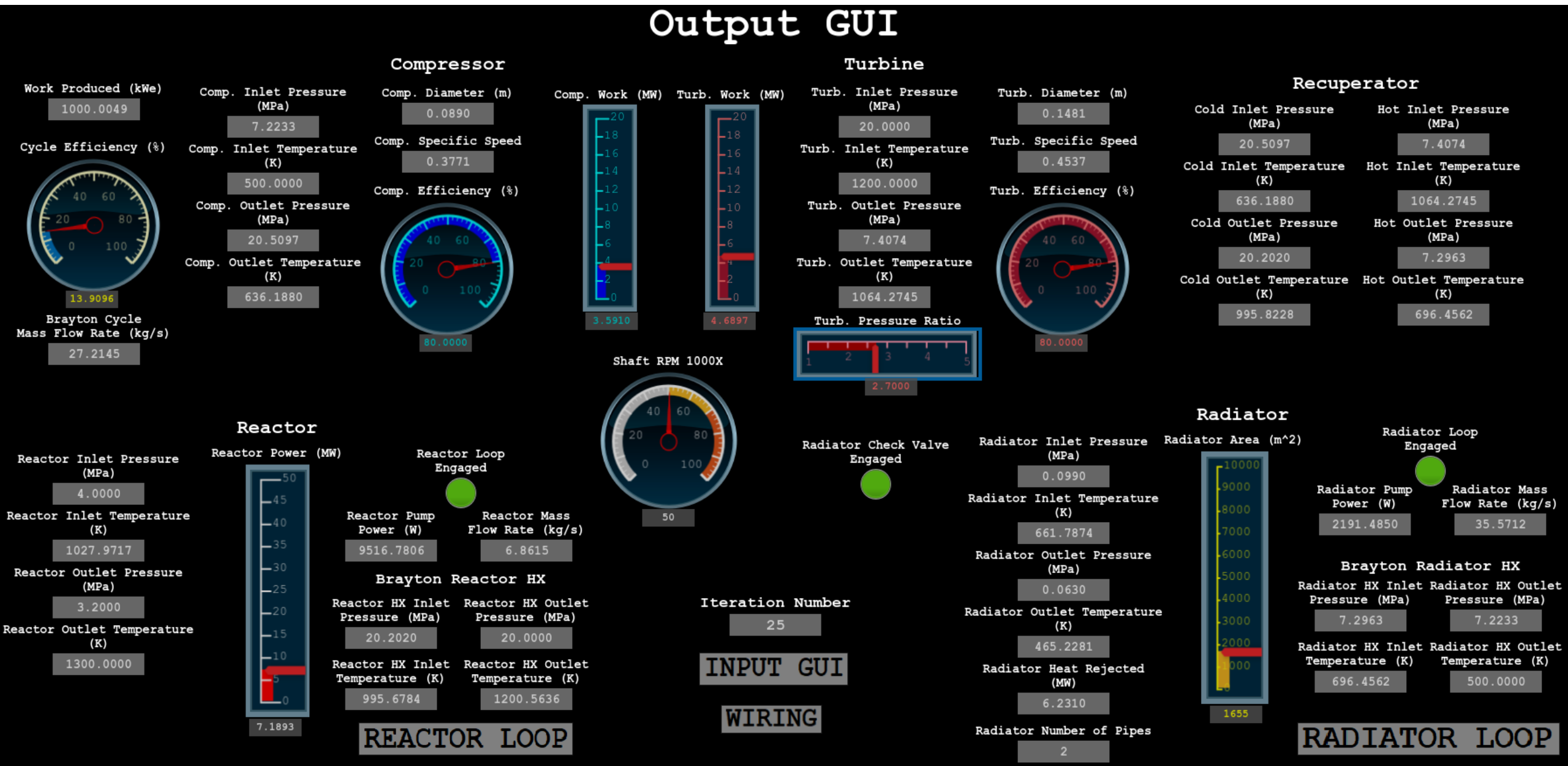
Start

Stop

OUTPUT GUI

WIRING

Model Output GUI

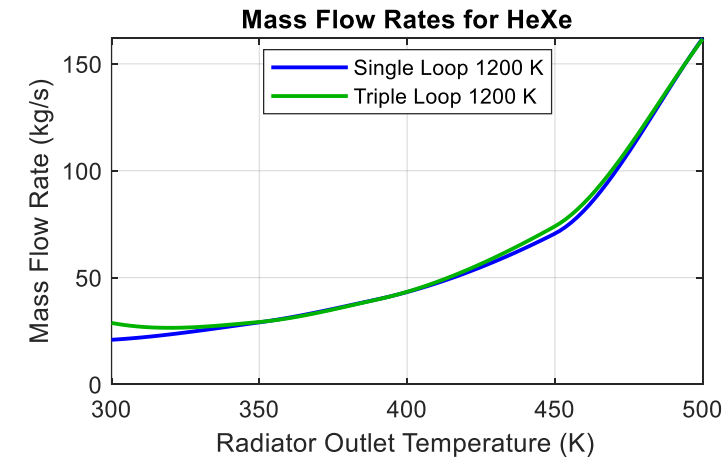
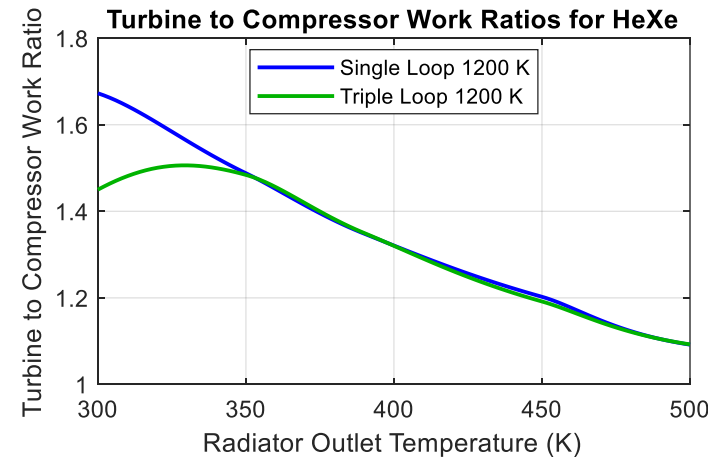
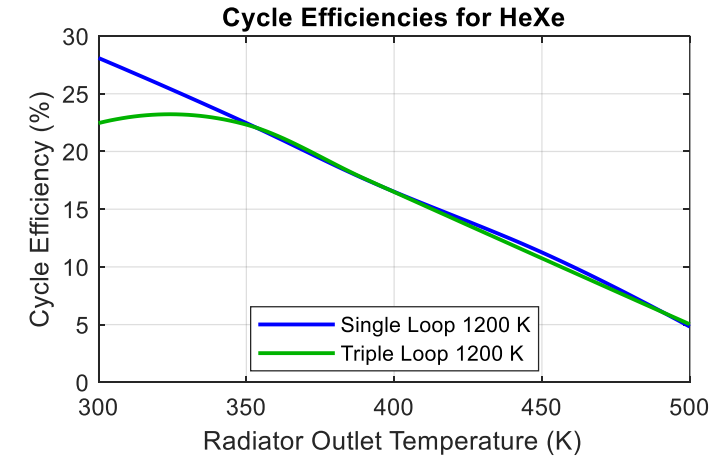
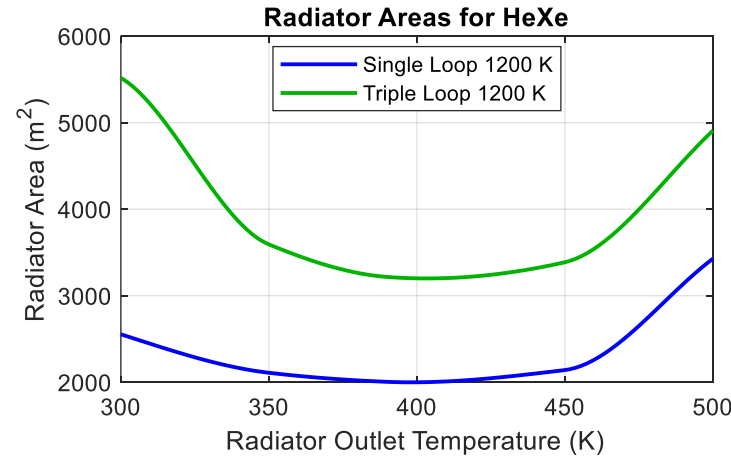


Results for Varying Radiator Outlet Temperature

Low velocities require large components

- Electrical power produced was set at 1 MWe.
- Different turbine inlet temperatures and fluid loops were considered.
- The radiator area affects the mass the most and has a minimum value.
- By decreasing the radiator outlet temperature, and thereby decreasing the cycle ΔT , the cycle efficiency decreases.

At low radiator outlet temperatures, the cycle efficiency is lower for the triple loop due to additional power load from electric pumps.

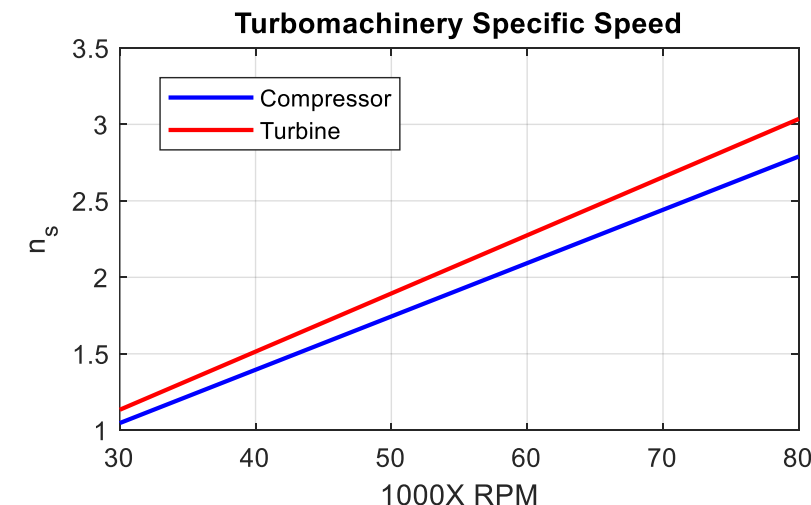
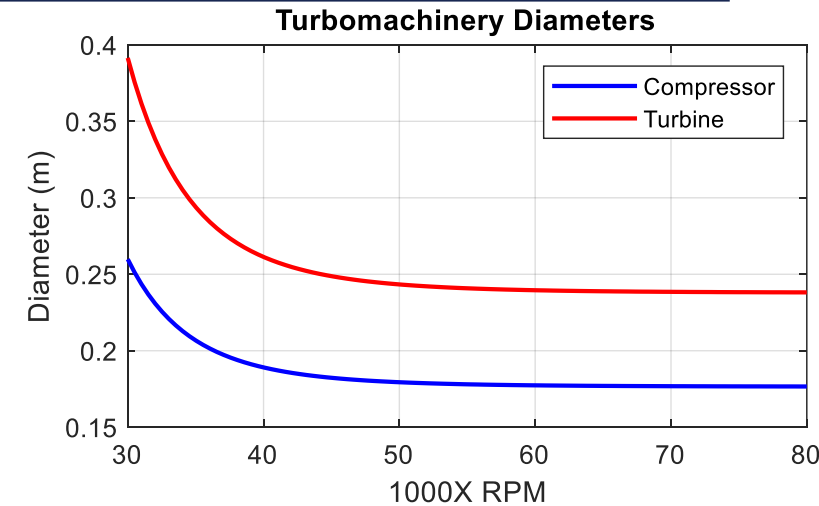


Results for Varying Shaft Speed

Low velocities require larger components

- Turbomachinery diameters are secondary mass drivers
- Considered: 1 MWe and 80% turbomachinery component efficiency.
- Higher velocities show to decrease the turbomachinery diameters but increase the strain on the roots of the blades.
- Specific speed increases linearly.

Depending on the material chosen for these components, a mass estimation can be made using these values.



Conclusions / Future Work

NEP modular power conversion model

- Higher fidelity turbomachinery informs system masses and can predict off-nominal performance.
- Different options in the GUI allow for different use cases to be examined and design methodologies implemented.
- Future work will consider:
 - High fidelity heat exchanger and reactor neutronics spline fit results.
 - Trades involving different types of heat exchangers.
 - Reactor heat pipe blocks and accompanying heat exchanger.
 - Different HeXe mixture concentrations.



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