



# Conflict Resolution Strategies for Balloon-Airship Encounters in Upper Class E Traffic Management (ETM)

Abraham K. Ishihara (Presenter)

KBR Wyle Services, LLC.  
Moffett Field, CA

Min Xue

NASA Ames Research Center  
Moffett Field, CA

AIAA Aviation Forum, 2022

*This material is a work of the U.S. Government and is not subject to copyright protection in the United States.*

# Introduction and Motivation

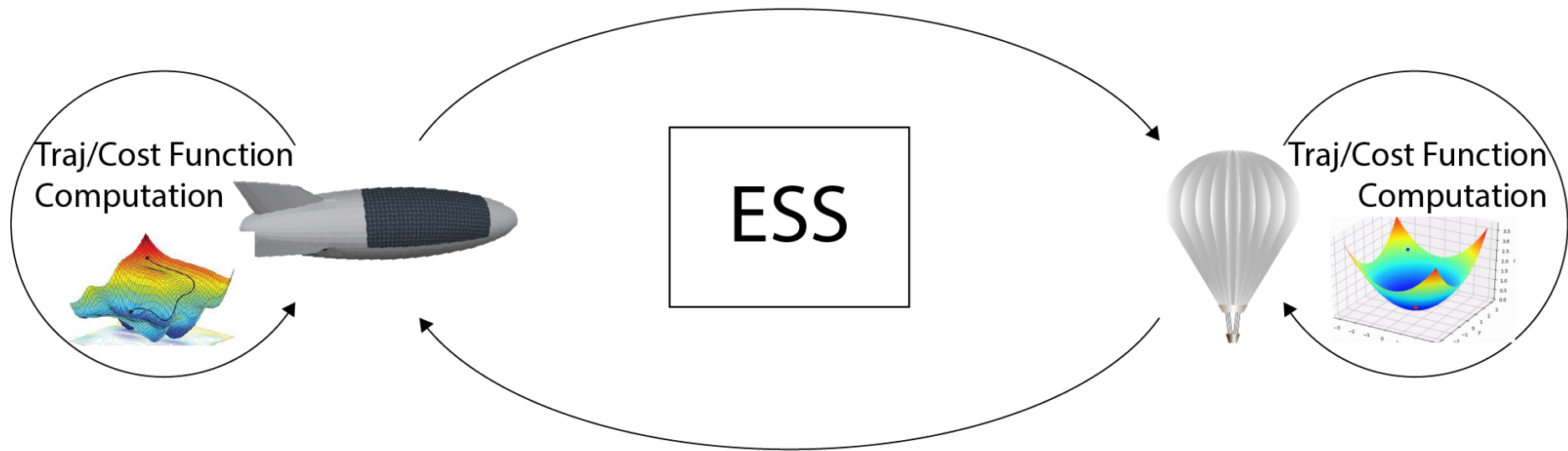
- HAPS market revenue of \$4 billion by 2029
- No specific provisions for air traffic management systems above 60,000 ft.
- NASA and FAA are investigating air-traffic management strategies for this emerging market.  
This is termed **ETM** or Upper Class **E Traffic Management**
- This presentation focuses on conflict resolution strategies for airship-balloon interaction leveraging optimal control and negotiation.



*2021 Upper Class E Traffic Management Workshop 2021*

# Organization

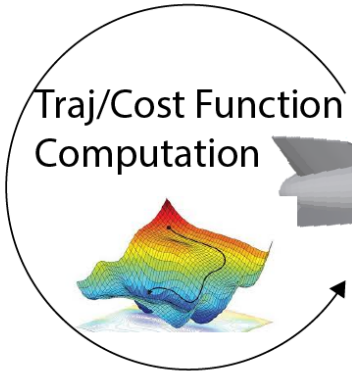
- Big Picture
- Balloon and Airship Dynamics
- Optimal Control Problem Formulation and Numerical Solutions
- Main Results
- Conclude



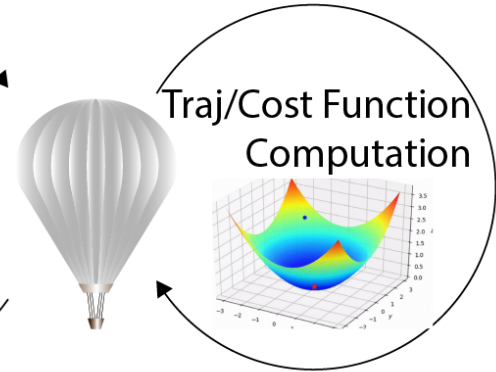
Propose Trajectory  
Compute Utility

1

$$(T_i^{(a)}, U_a(T_i^{(a)}))$$

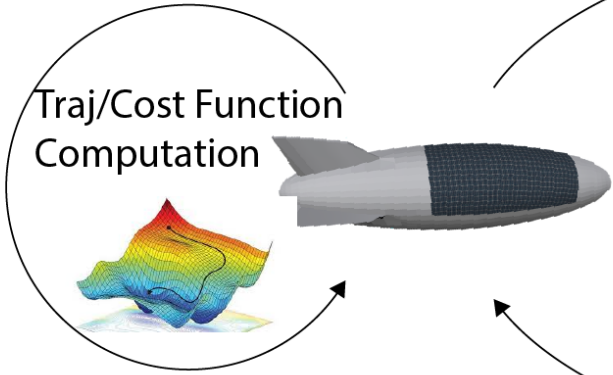


ESS



1  
Propose Trajectory  
Compute Utility

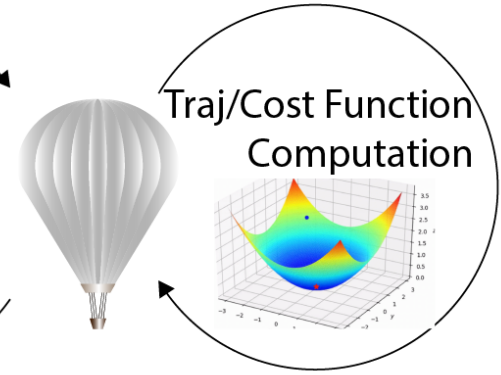
$$(T_i^{(a)}, U_a(T_i^{(a)}))$$

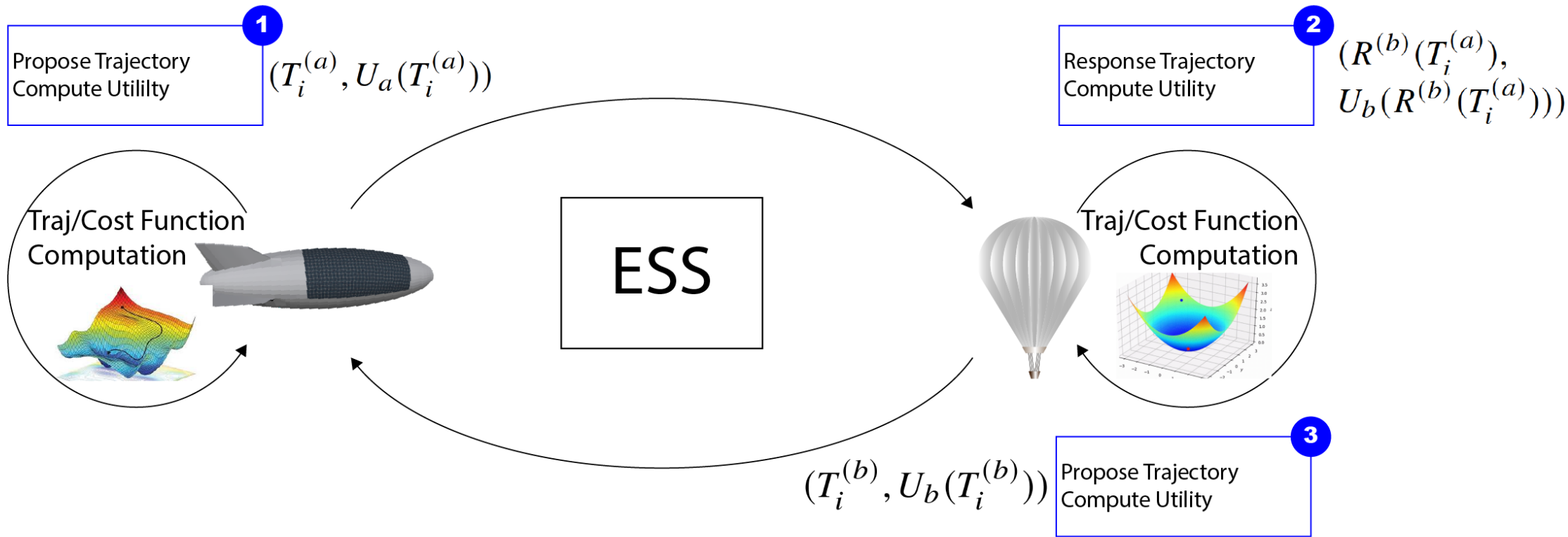


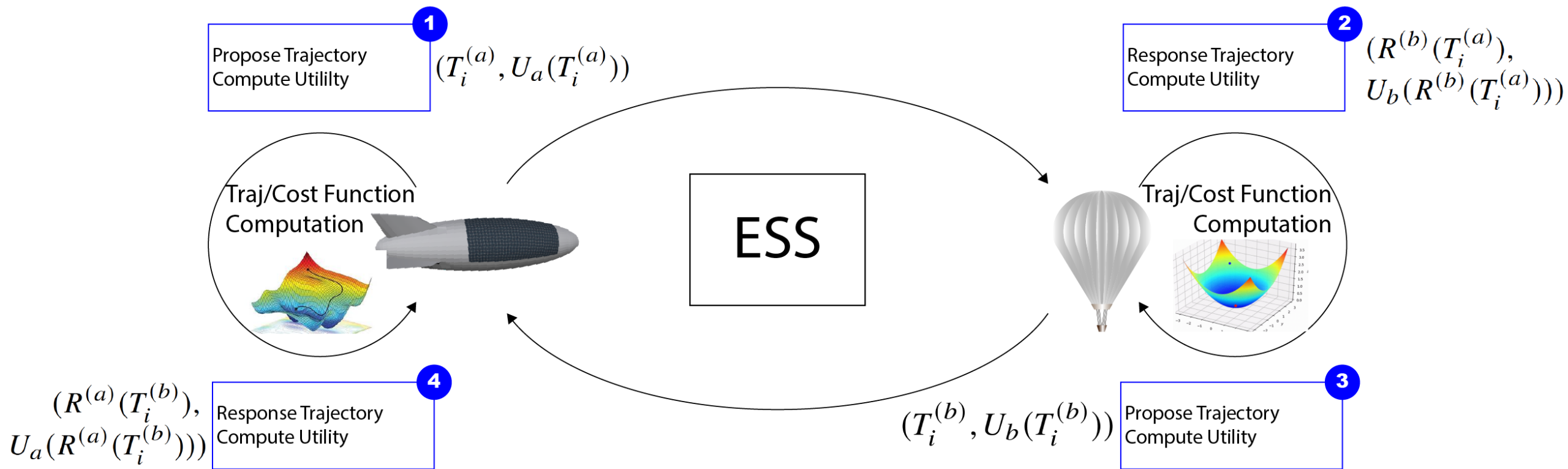
ESS

2  
Response Trajectory  
Compute Utility

$$(R^{(b)}(T_i^{(a)}), U_b(R^{(b)}(T_i^{(a)})))$$







Pritchett, A. R., & Genton, A. (2017). Negotiated decentralized aircraft conflict resolution.

Wollkind, S., Valasek, J., & Ioerger, T. (2004, August).

Zlotkin, G., & Rosenschein, J. S. (1989, August)

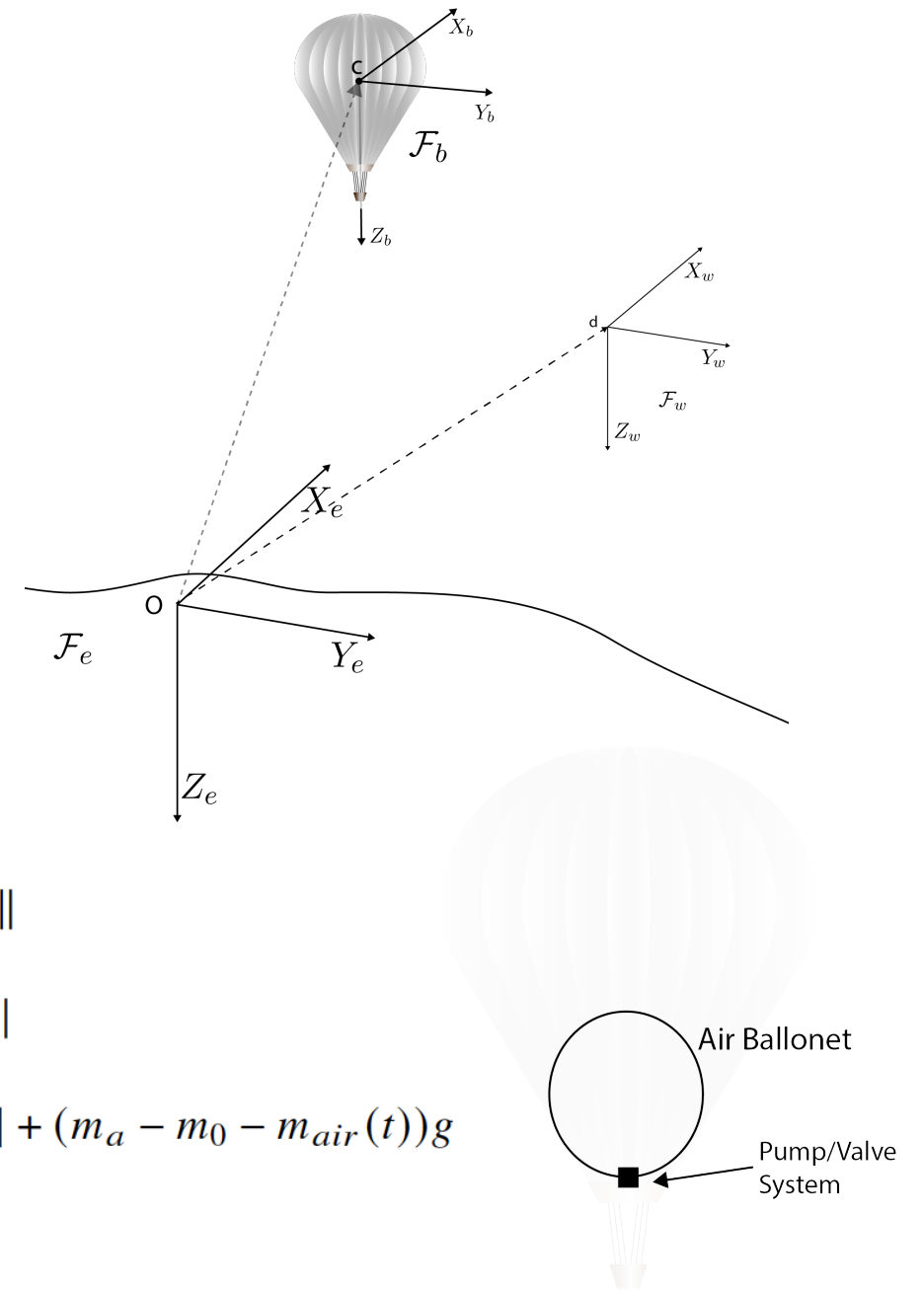


# Balloon Dynamics

Forces acting on the balloon

$$\vec{F}^{(e)} = \vec{F}_{aero}^{(e)} + \vec{F}_{buoy}^{(e)} + \vec{F}_g^{(e)}$$

$$\left\{ \begin{array}{l} \dot{x}_b = v_{bx} \\ \dot{y}_b = v_{by} \\ \dot{z}_b = v_{bz} \\ \frac{d}{dt} ((m_0 + m_{air}(t) + \eta m_a) (v_{bx} - \zeta_x)) = -\bar{q}_b S_b C_d (v_{bx} - \zeta_x) / \|\vec{V}_{rel}\| \\ \frac{d}{dt} ((m_0 + m_{air}(t) + \eta m_a) (v_{by} - \zeta_y)) = -\bar{q}_b S_b C_d (v_{by} - \zeta_y) / \|\vec{V}_{rel}\| \\ \frac{d}{dt} ((m_0 + m_{air}(t) + \eta m_a) (v_{bz} - \zeta_z)) = -\bar{q}_b S_b C_d (v_{bz} - \zeta_z) / \|\vec{V}_{rel}\| + (m_a - m_0 - m_{air}(t))g \\ \dot{m}_{air}(t) = u(t) \end{array} \right.$$



# Airship Dynamics

$$\begin{bmatrix} mI_{3 \times 3} & mD_{cg} \\ -mD_{cg} & I \end{bmatrix} \begin{bmatrix} \dot{\vec{v}}_{\zeta}^{(b)} \\ \dot{\vec{\omega}}^{(b)} \end{bmatrix} + \begin{bmatrix} \vec{H}^{(F)} \\ \vec{H}^{(M)} \end{bmatrix} + m \begin{bmatrix} \vec{A}_{cg} \\ \vec{B}_{cg} \end{bmatrix} = \begin{bmatrix} \vec{F}^{(b)} \\ \vec{M}^{(b)} \end{bmatrix}$$

$$\vec{\omega}^{(b)} = [p \ q \ r]^T \quad \text{angular rates}$$

$$\vec{v}_{\zeta}^{(b)} := [u + \zeta_x \quad v + \zeta_y \quad w + \zeta_z]^T \quad \text{body velocities with wind}$$

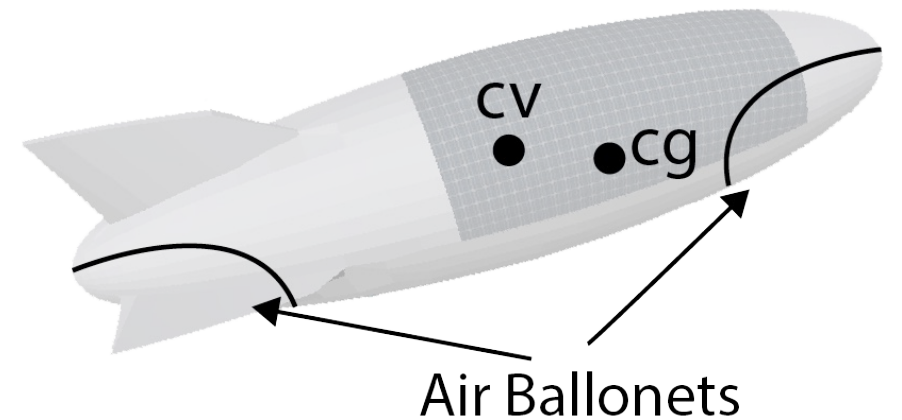
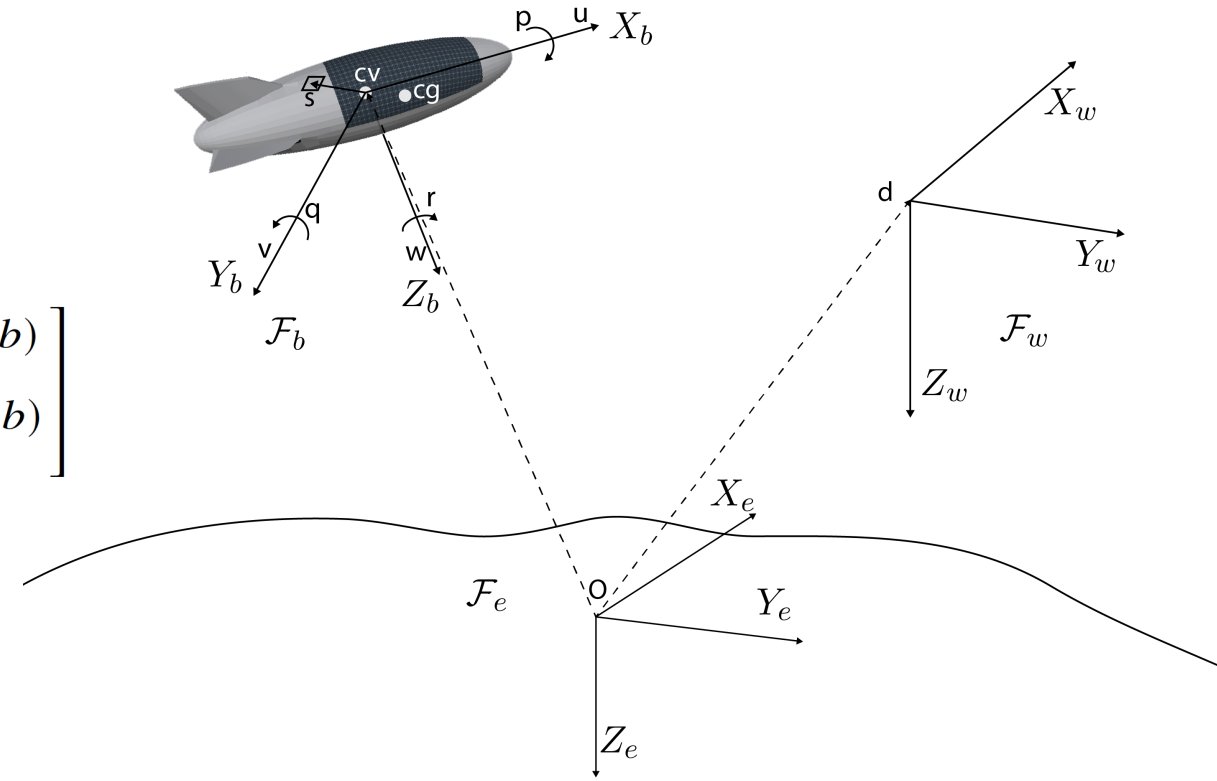
$$D_{cg} = \begin{bmatrix} 0 & d_z & -d_y \\ -d_z & 0 & d_x \\ d_y & -d_x & 0 \end{bmatrix}$$

$$\vec{H}_F = m\vec{\omega}^{(b)} \times \vec{v}_{\zeta}^{(b)}$$

$$\vec{H}_M = \vec{\omega}^{(b)} \times I\vec{\omega}^{(b)}$$

$$\vec{A}_{cg} = \begin{bmatrix} -d_x(q^2 + r^2) + d_y pq + d_z pr \\ -d_y(p^2 + r^2) + d_z rqd_x pq \\ -d_z(p^2 + q^2) + d_x pr + d_y qr \end{bmatrix}$$

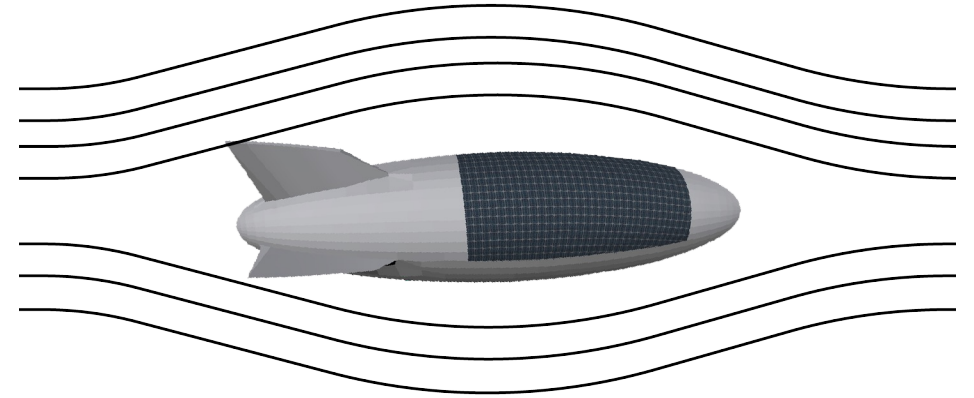
$$\vec{B}_{cg} = \begin{bmatrix} d_y(pv_{\zeta} - qu_{\zeta}) - d_z(ru_{\zeta} - pw_{\zeta}) \\ d_z(qw_{\zeta} - rv_{\zeta}) - d_x(pv_{\zeta} - qu_{\zeta}) \\ d_x(ru_{\zeta} - pw_{\zeta}) - d_y(qw_{\zeta} - rv_{\zeta}) \end{bmatrix}$$



# Virtual Mass/Inertia

$$\vec{F}_v^{(b)} = \Gamma_1 \dot{\vec{v}} + \Gamma_2 \dot{\vec{\omega}} + E_F$$

$$\vec{M}_v^{(b)} = \Gamma_3 \dot{\vec{v}} + \Gamma_4 \dot{\vec{\omega}} + E_M$$

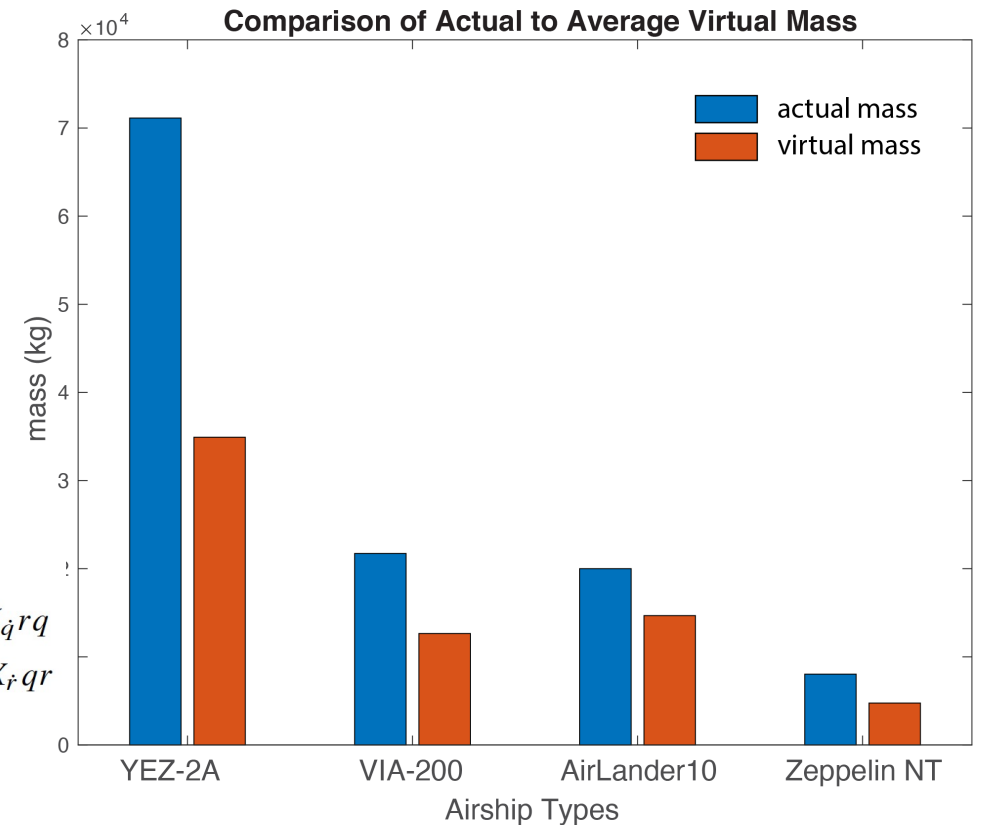


$$\Gamma_1 = \begin{bmatrix} X_{\dot{u}} & X_{\dot{v}} & X_{\dot{w}} \\ X_{\dot{v}} & Y_{\dot{v}} & Y_{\dot{w}} \\ X_{\dot{w}} & Y_{\dot{w}} & Z_{\dot{w}} \end{bmatrix} \quad \Gamma_2 = \begin{bmatrix} X_{\dot{u}} & X_{\dot{v}} & X_{\dot{w}} \\ X_{\dot{v}} & Y_{\dot{v}} & Y_{\dot{w}} \\ X_{\dot{w}} & Y_{\dot{w}} & Z_{\dot{w}} \end{bmatrix} \quad E_F = \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}$$

$$E_x = Z_{\dot{w}}qw + Z_{\dot{q}}q^2 + X_{\dot{w}}qu - Y_{\dot{v}}rv - Y_{\dot{p}}rp - Y_{\dot{r}}r^2 - X_{\dot{v}}ru - Y_{\dot{w}}rw - (Y_{\dot{q}} - Z_{\dot{r}})rq$$

$$E_y = X_{\dot{v}}rv - Y_{\dot{w}}pv - Z_{\dot{p}}p^2 + X_{\dot{r}}r^2 + (X_{\dot{p}} - Z_{\dot{r}})pr - X_{\dot{w}}pu + X_{\dot{w}}rw - Z_{\dot{w}}pw + X_{\dot{u}}ru - Z_{\dot{q}}pq + X_{\dot{q}}rq$$

$$E_z = -X_{\dot{w}}qw - X_{\dot{u}}qu - X_{\dot{q}}q^2 + Y_{\dot{v}}pv + Y_{\dot{r}}rp + Y_{\dot{p}}p^2 + Y_{\dot{w}}pw + X_{\dot{v}}pu - X_{\dot{v}}qv - (X_{\dot{p}} - Y_{\dot{q}})pq - X_{\dot{r}}qr$$



# Optimal Control

- Non-Dimensionalization

$$\begin{cases} \dot{x} = f(t, x, u) \\ x(t_0) = x_0 \end{cases}$$

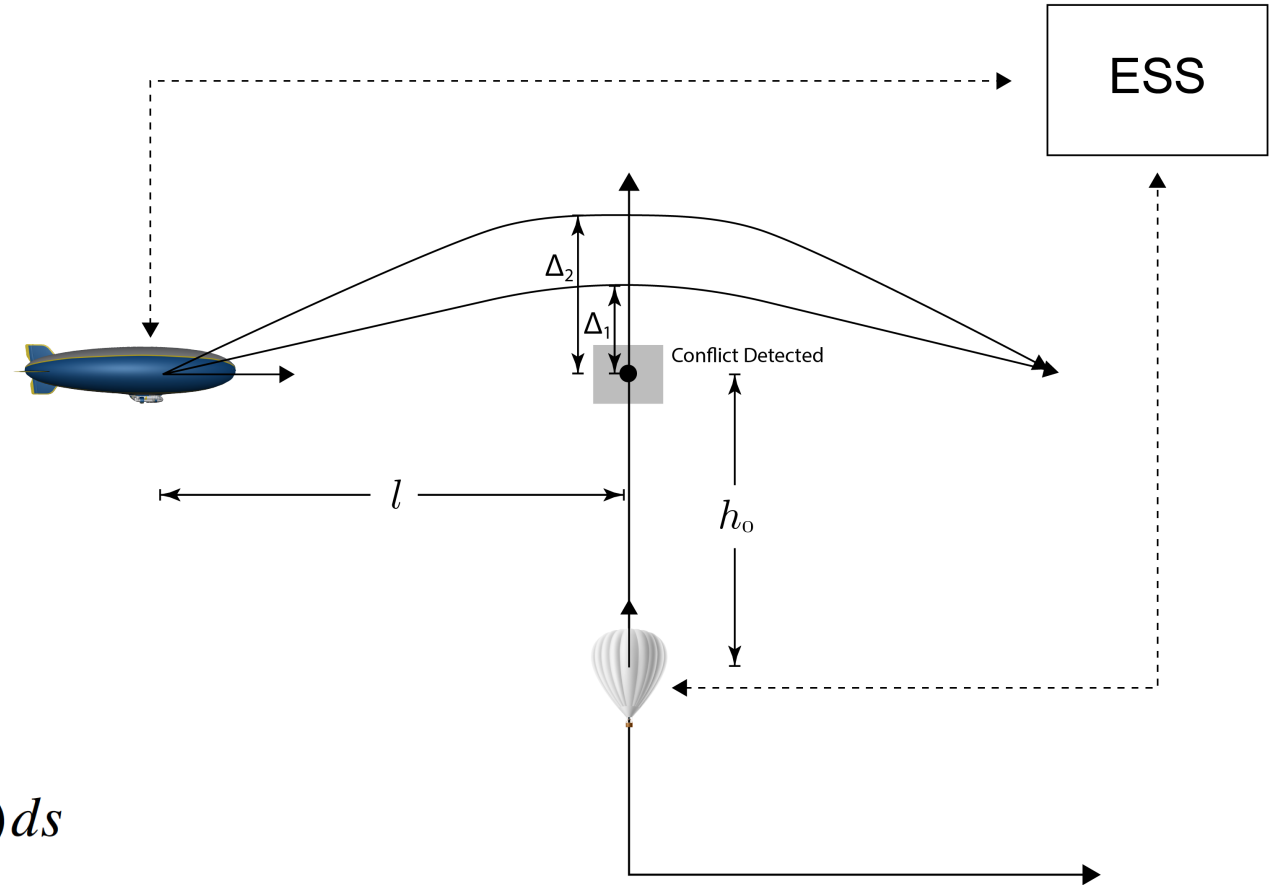
Plant Dynamics

$$\begin{cases} \dot{p} = -\frac{\partial H}{\partial x} \\ p(t_f) = -\frac{\partial \phi(x(t_f))}{\partial x} \end{cases}$$

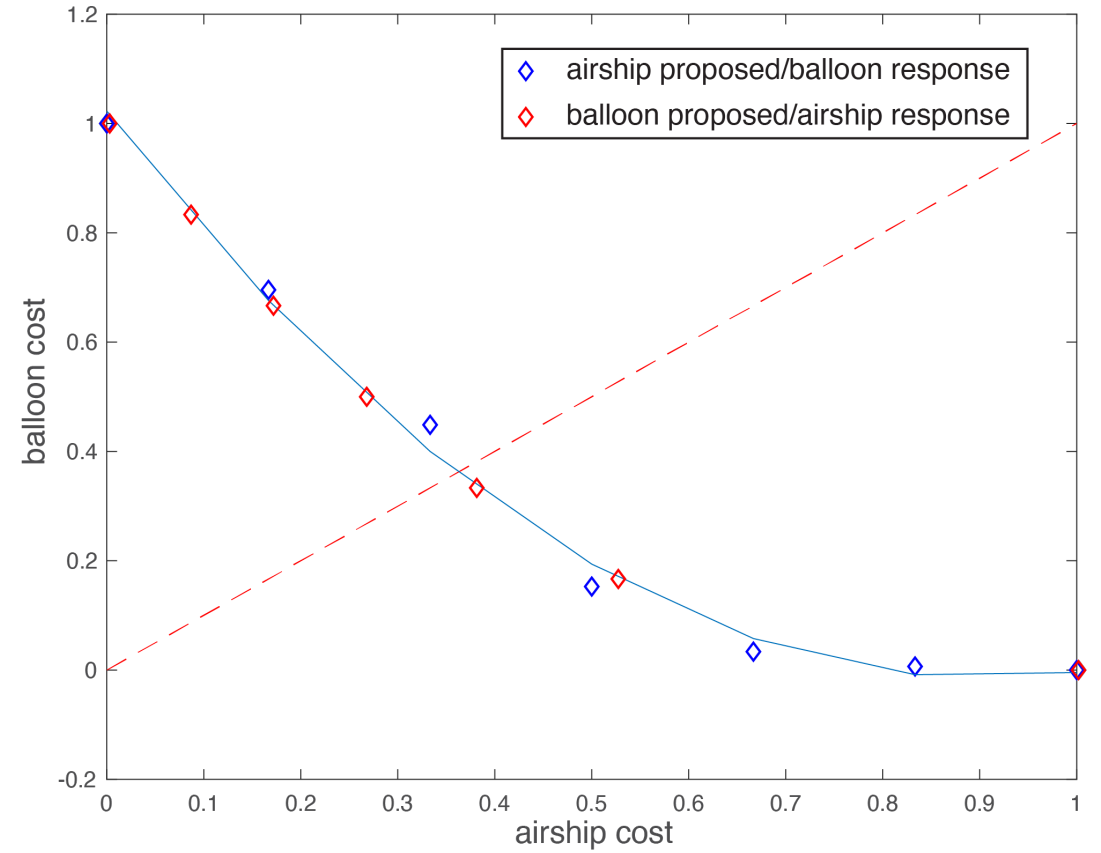
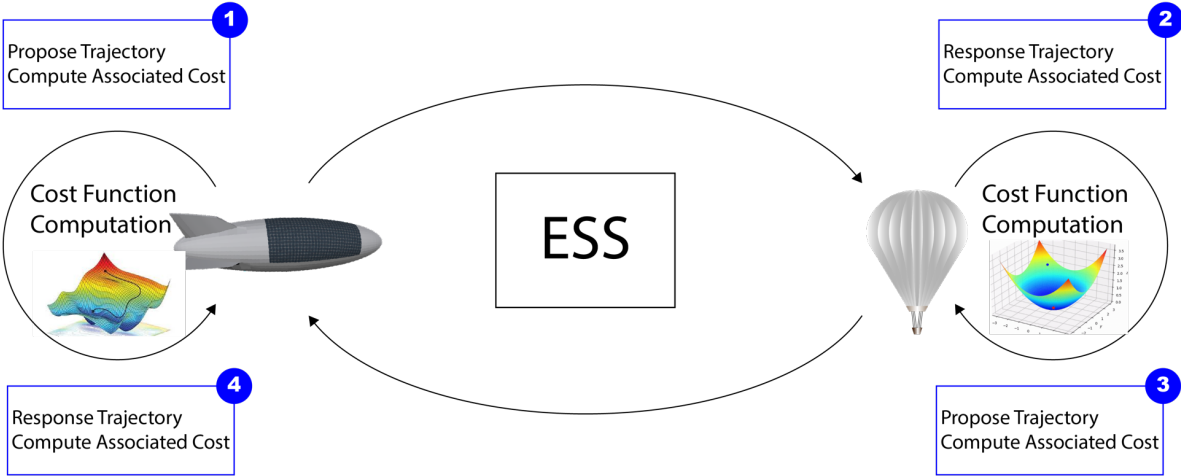
Co-State Dynamics

$$J[\bar{u}] := \int_0^{\tau_f} (1 - \gamma)|\bar{u}| + \gamma\bar{u}^2 + \alpha\bar{R}(\tau, \bar{x}) ds$$

$$H(\tau, x(\tau; t_0, x_0, u^*), u^*(\tau), p(\tau)) \geq H(\tau, x(\tau; t_0, x_0, v), v, p(\tau))$$



# Results



iteration	airship proposed cost	balloon response cost	balloon proposed cost	airship response cost
1	0.00	1.00	0.00	1.00
2	0.17	0.70	0.17	0.53
3	0.33	0.45	0.33	0.38
4	0.50	0.15	0.50	0.27

# Conclusions

- There is a need for new approaches to traffic management in this emerging airspace
- A system modeled after UTM (UAS Traffic Management) terms ETM is currently being investigated.
- We presented an optimal control approach that could facilitate negotiation and conflict resolution between operators.
- Future work includes (1) analysis of convergence properties of the proposed framework, (2) exploration of different combinations of vehicles types, (3) real-time optimal control solutions.