

Adaptive Mesh Refinement and Turbulence Modeling

Michael E. Olsen¹

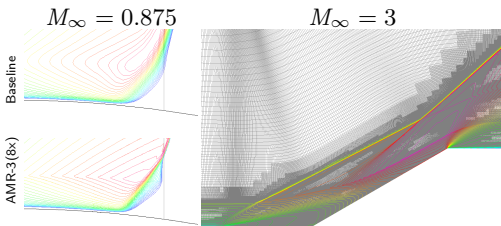
¹NASA Ames Research Center, Moffett Field, CA 94035

ICCFD11



Turbulence modeling: Nonlinear PDE solved with discretization
How to deal with the problem of truncation error?

- Classic version: ($\Delta x \mapsto \frac{1}{2}\Delta x$; $N_p \mapsto 4 \times N_p$; $\epsilon_n \mapsto \frac{1}{4} \times \epsilon$) Enormous fast!
- AMR computational efficiency ("Exact" solution/miniumum cost)
- AIAA-2016-3326: AMR Capability (Buning/Pulliam OVERFLOW)
- AIAA-2018-3858: Current methodology outlined



- AMR $\iff$ Classic version
- Sub-, Trans-, Super-sonic
- Field variables converge last
- Shocks, BL edge: refine!

AMR ready for more complex turbulence models

- Revisit AIAA-2005-101 "High Speed Turbulence" (defacto Lag- ν_T definition)
 - Flowfields of increasing complexity
 - Kussoy/Horstman $M = 7$ cylinder/flare
 - More complex models useful?
- Lag models:
 - Wilcox $k-\omega$ (1988) at core
 - Eddy viscosity, R_{ij} , TTR(Transport T_{ijk} , and TAO(High Re) versions
 - Additional field equations (e.g. Lag- ν_T):

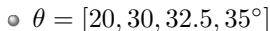
$$\frac{D\nu_T}{Dt} = \omega (\nu_T - \nu_T^e)$$

- No limiters
- No wall distance
- URANS: Grid and time converged solutions (Apollo, etc.)
- RHS source terms based on exact equations
- Most advanced (TAO) includes High Re anisotropy match
- Simplest works more universally than alternative models

4/16

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Conclusions



attached ... separated

- Water cooled walls, long run time,
- Surface pressure, heat transfer
- Canonical high speed flow case

$$M_\infty = 7.04$$

$$u_{\infty} = 1127 \frac{\text{m}}{\text{s}}$$

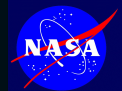
$$T_w = 311 \text{ K}$$

$$T_{\infty} = 81.2 \text{ K}$$

$$p_{\infty} = 576 \text{ Pa}$$

$$\tau_{w\infty} = 25 \text{ Pa}$$

$$\rho_{\infty} = 0.02522 \text{ kg/m}^3 \quad Re = 5.8 \times 10^{-6} \frac{1}{\text{m}} \quad \dot{q}_{w\infty} = 9300 \text{ W/m}^2$$



Solver: Overflow 2.2k[modified/stock]

- Stock: verified SST, SA implementations
- Modified: Lag variants
- Cases steady (so far)
- Coarser starting grid (computational efficiency)
- General ethos:
 - Low dissipation
 - no multigrid
 - Well converged (solution)

AMR: "meta" algorithm

- Cauchy sequence? (grid convergence)
- Classic refinement comparison
- Where refinement? ("bespoke" grids)
- AMR sensor: linearity in $[\xi, \eta]$

$$S = \max_{i=j,k,l} \left\{ \max_{q=[\rho, \rho u, \dots]} \left[\left(\frac{q_{i-1} - 2q_i + q_{i+1}}{2q_{ref}} \right)^2 \right] \right\}$$

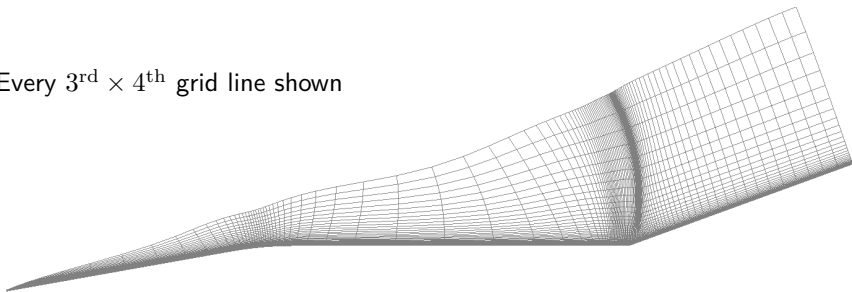
Baseline grid and solution domain

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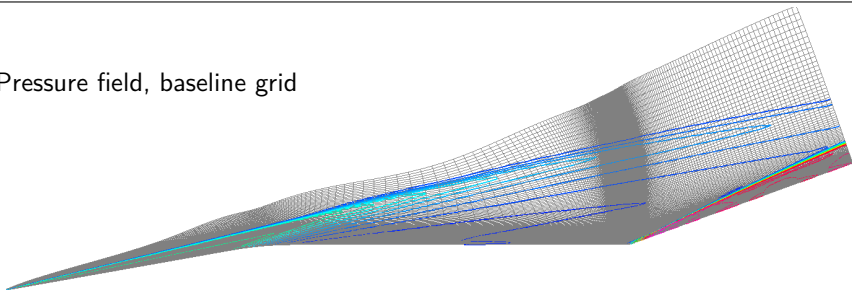
6/16



Every 3rd × 4th grid line shown



Pressure field, baseline grid



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Introduction

Method

Experiment

Computation

Grid

Results

$\theta = 20^\circ$

$\theta = 35^\circ$

Conclusions

Additional

Material

Grid, Solution, Refinement, $\theta = 20^\circ$ (attached)

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7/16



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Modeling

Olsen

Introduction

Method

Experiment

Computation

Grid

Results

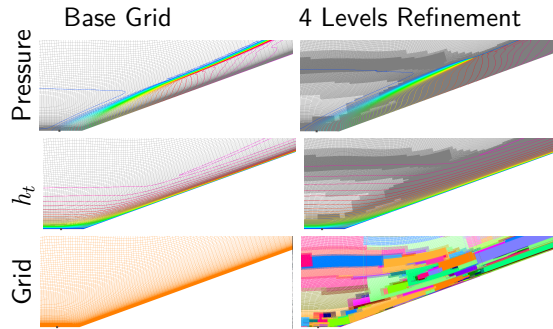
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Conclusions

Additional

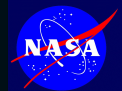
Material



- Compression waves
 $\mapsto$ shock
- Boundary layer
 edge refined
- ∞ ($x = -6$ cm)
 visible

- Boundary layer edge habitually overlooked (important in hindsight)
- "proto-shock" region refinement focus
- Some regions remain unrefined (under proto-shock/boundary layer edge)
- Successive refinement informative

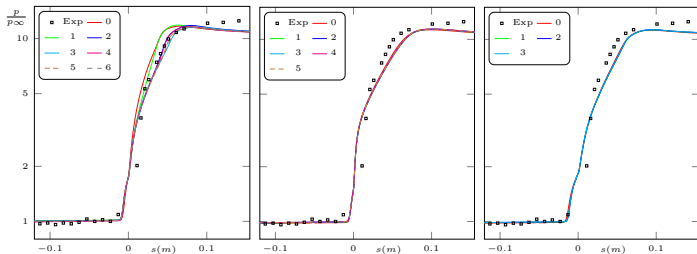
Results: $\theta = 20$



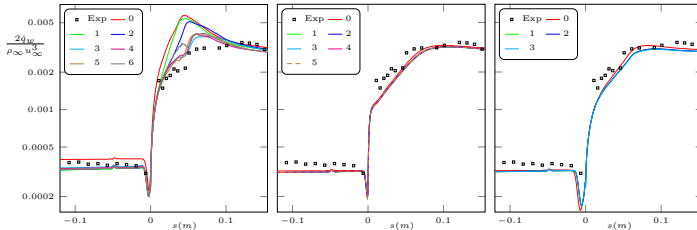
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8/16

Pressure



Heating



Lag- ν_T

SA

SST

- Pressure results very consistent with 2005 results
- Heating results improved
- 6 levels $\mapsto$ 4096 grid increase

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Modeling

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Introduction

Method

Experiment

Computation

Grid

Results

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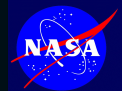
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Conclusions

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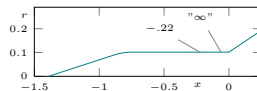
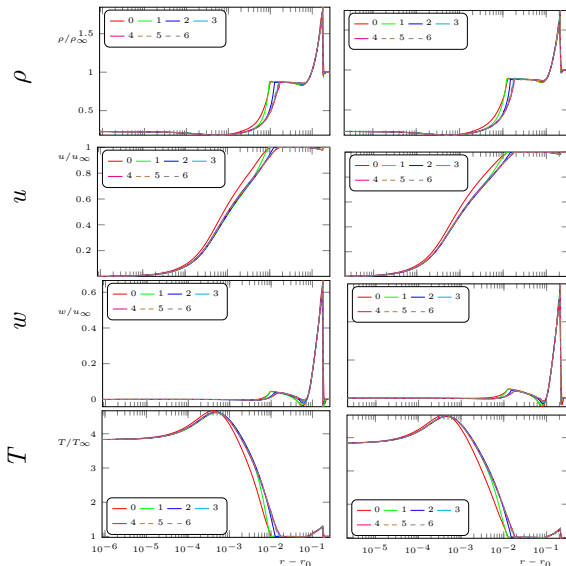
Material

Upstream Flowfield: $(\infty) \theta = 20$



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9/16



- 4th and higher refinements
- Boundary layer edge (and external shock) last to "grid converge"
- Surface quantities first to "grid converge"
- Consistent with 2018 findings

$x = -0.22 \text{ m}$

$x = -0.06 \text{ m} (" \infty ")$

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Modeling

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Introduction

Method

Experiment

Computation

Grid

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Conclusions

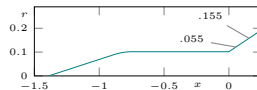
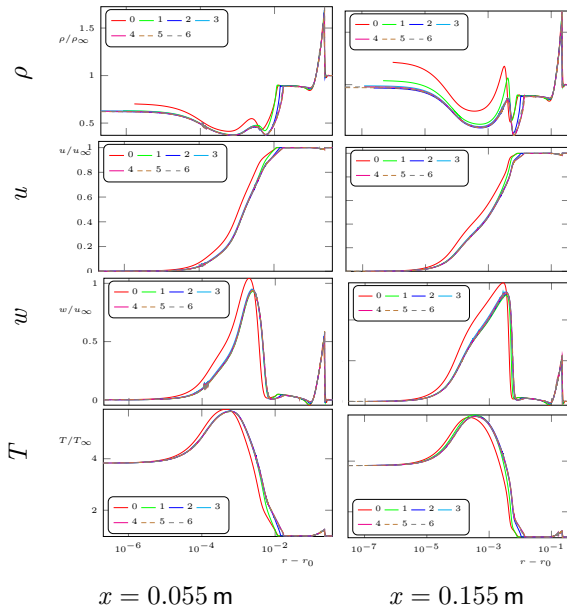
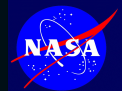
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Material

Flare(Downstream) Flowfield: $\theta = 20^\circ$

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10/16



- Further downstream: more sensitive to refinement (ρ)
- Even surface changing at $x = 0.155$ m
- Fixed Wall T is a boundary condition
- Larger differences than upstream

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Introduction

Method

Experiment

Computation

Grid

Results

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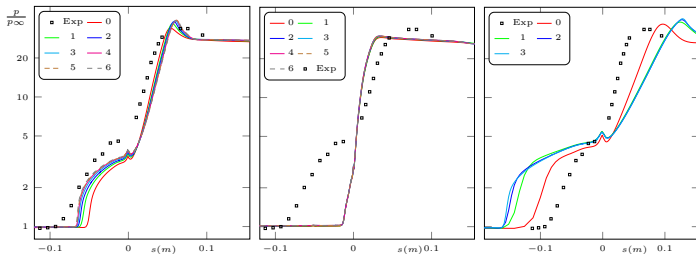
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Conclusions

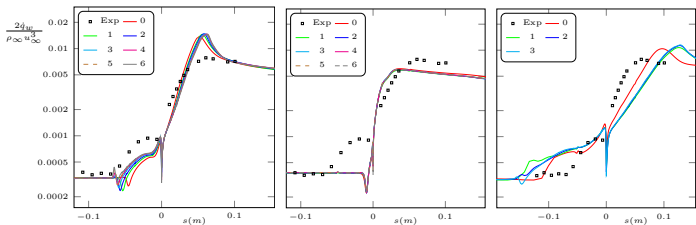
Additional

Material

Pressure



Heating



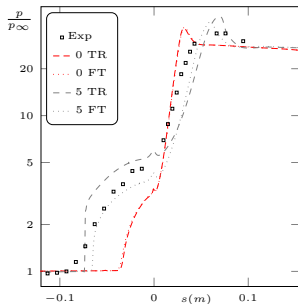
Lag- ν_T

SA

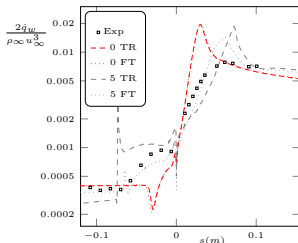
SST(extended)

- Pressure results much improved
- Heating results improved
- 6 levels $\mapsto 2^{12} = 4096$ grid size increase

Pressure



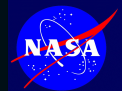
Heating



FT ≡ "Fully turbulent"

TR ≡ "Transitional"

- Baseline grid relatively transition insensitive
- Refined grid sensitive
- Other terms (σ_k) now matter
- Improved edge turbulent state of more advanced models(TTR)?
- Hindsight: Flowfield slatlike... (AMR allows accurate propagation)



AMR:

- Provided better predictions
- Allows accurate information propagation
- Showed inviscid/viscous interactions not seen on baseline (compression $\mapsto$ shock)
- Removes preconception bias (searching under the streetlamp)
- "cosmetic" choices now important and tunable

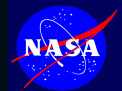
Forward:

- Even more refinement (levels, "errest")
- Assess the now important parameters, tune them
- More complex models (do they work, improve things, create craters?)
- 3D
- At higher refinement, unsteady?

Interaction Region, $h_t \theta = 20^\circ$ (attached)

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14/16



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Modeling

Olsen

Introduction

Method

Experiment

Computation

Grid

Results

$\theta = 20^\circ$

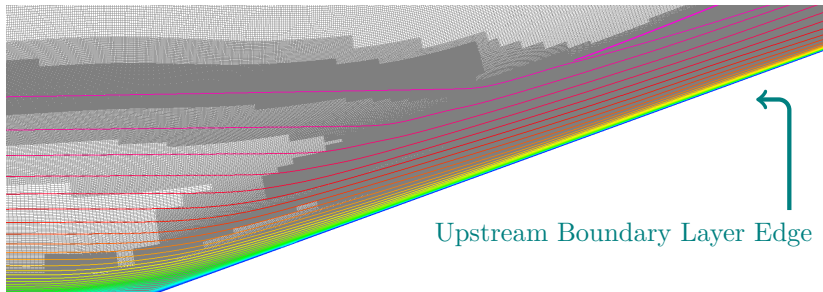
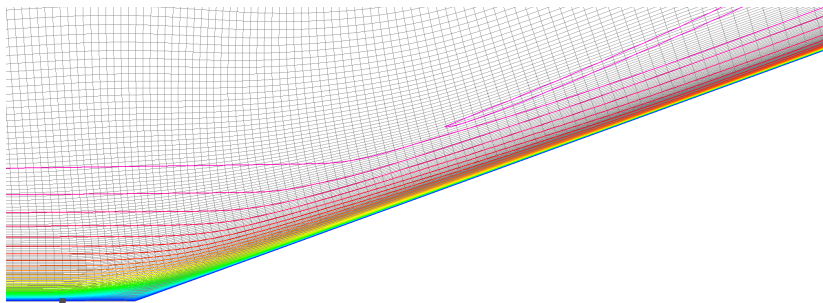
$\theta = 35^\circ$

Conclusions

Additional
Material

Back

4 Levels Refinement



Upstream Boundary Layer Edge

AMR and pressure details, Interaction region $\theta = 20^\circ$ (attached)

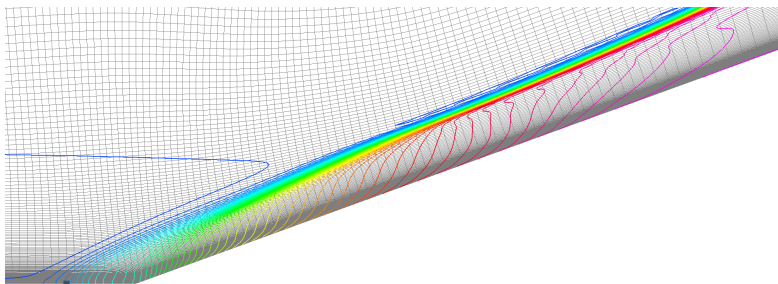


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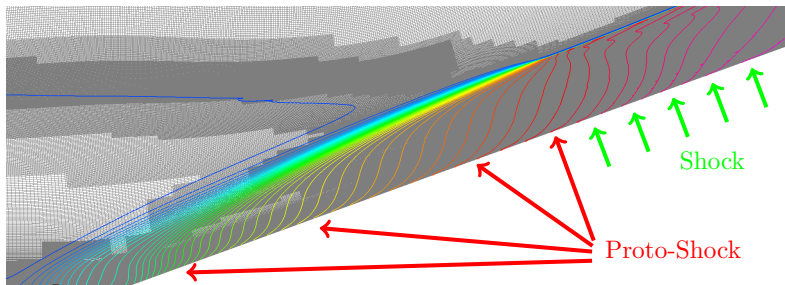
15/16

Base Grid

Back



4 Levels Refinement



AMR/Turb
Modeling

Olsen

Introduction

Method

Experiment

Computation

Grid

Results

$\theta = 20^\circ$

$\theta = 35^\circ$

Conclusions

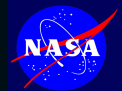
Additional

Material

AMR Grid as abstract art $\theta = 20^\circ$ (attached)

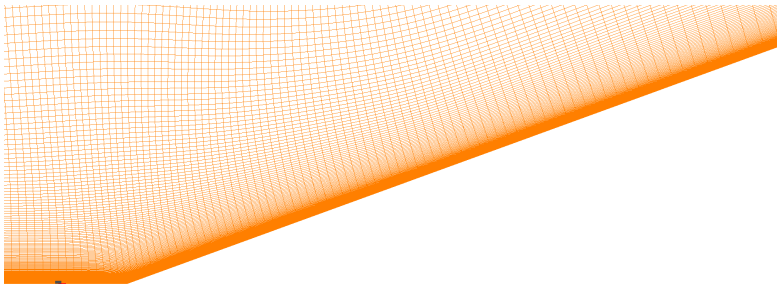
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16/16

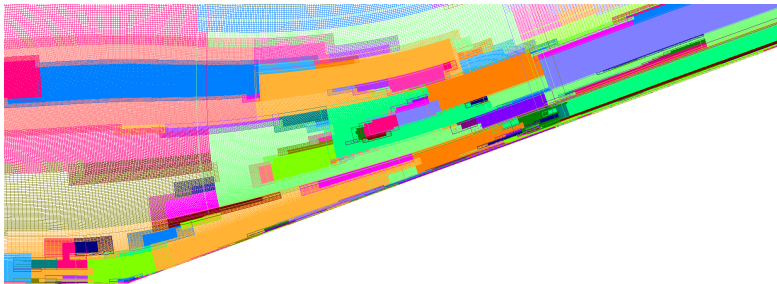


Back

Base Grid



4 Levels Refinement



AMR/Turb
Modeling

Olsen

Introduction

Method

Experiment

Computation

Grid

Results

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Conclusions

Additional
Material