



Computationally Guided Design of Polymer-Coated Microparticles as Reusable Materials

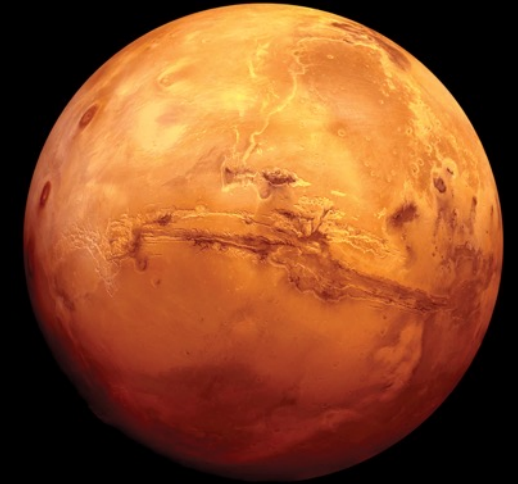
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³National Institute of Aerospace, ⁴William & Mary, ⁵NASA Langley Research Center

Materials innovation needed for sustainable exploration



- Long-duration human exploration necessitates a reduced dependency on Earth supply
- Reusable and in-situ materials are critical for sustainability



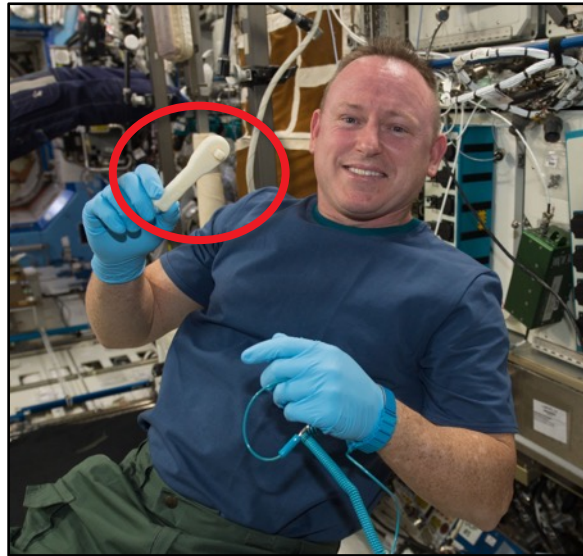
Transit time:
~6 months

Mission duration:
~2-3 years

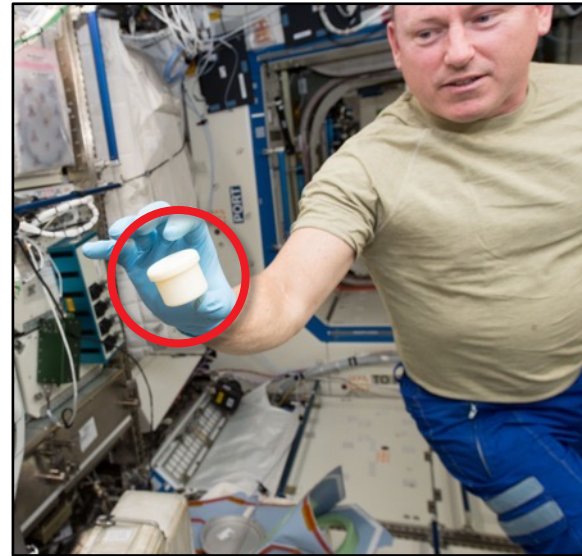
Additive manufacturing capabilities enhanced by recycling



- In-space manufacturing (ISM) allows for on-demand fabrication of articles to reduce mission mass and risk
- Enabling Sustained Presence Using Recyclables (ESPUR) project focuses on development of reusable feedstocks

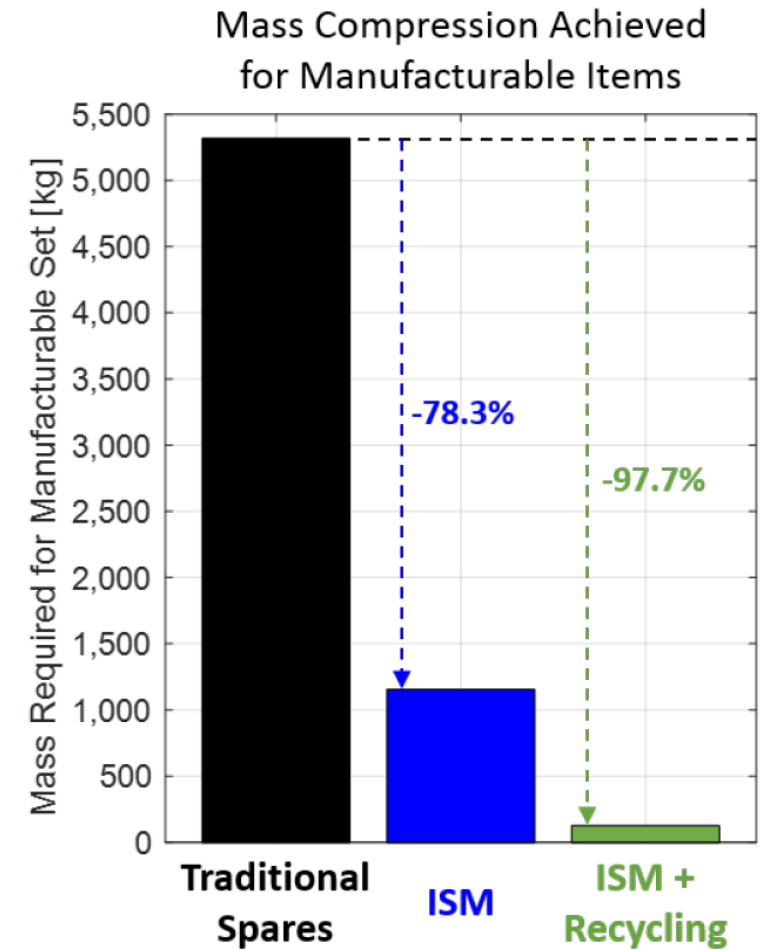


3D-printed ratchet wrench



3D-printed sample container

Image credits: NASA

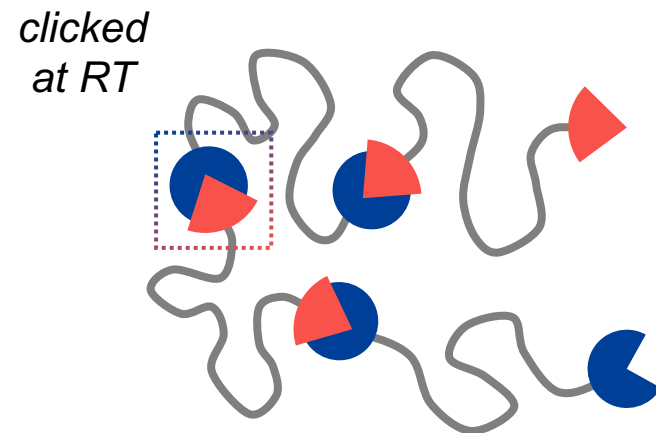
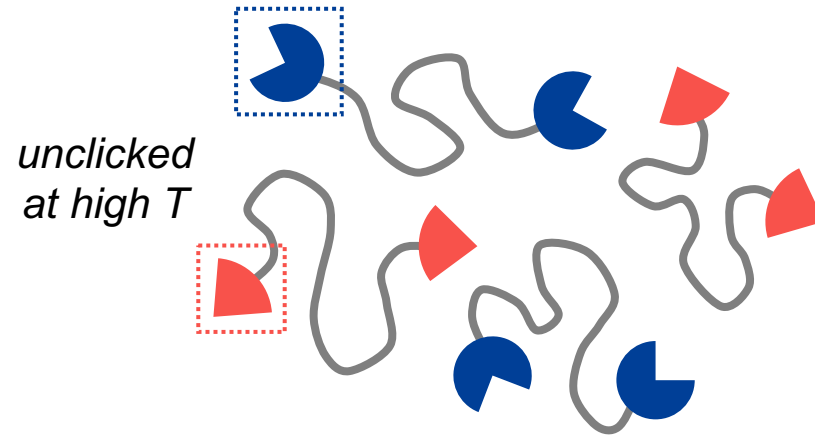
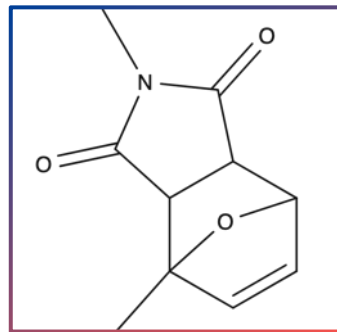
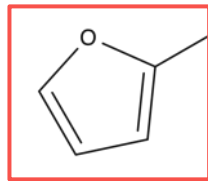
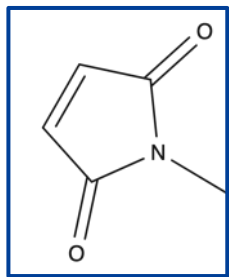


Owens and Weck, AIAA SPACE 2016

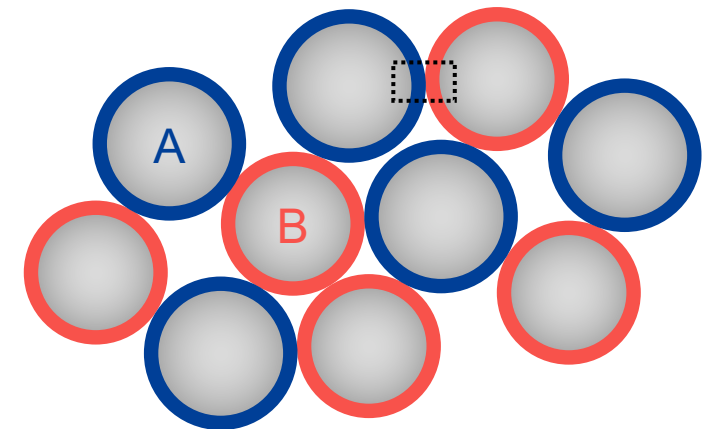
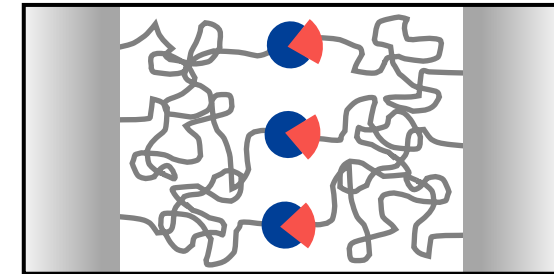
Reusable material concept via reversible click chemistry



ESPUR materials
incorporate thermoreversible
Diels-Alder reactions



Microparticle building blocks feature
complementary polymer coatings

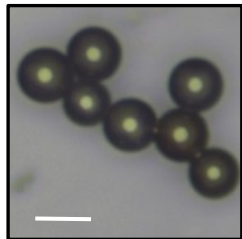


Tunability possible within the large design space

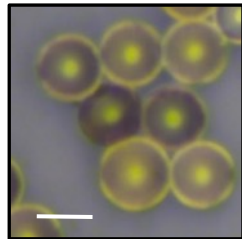


Epoxy Microparticles

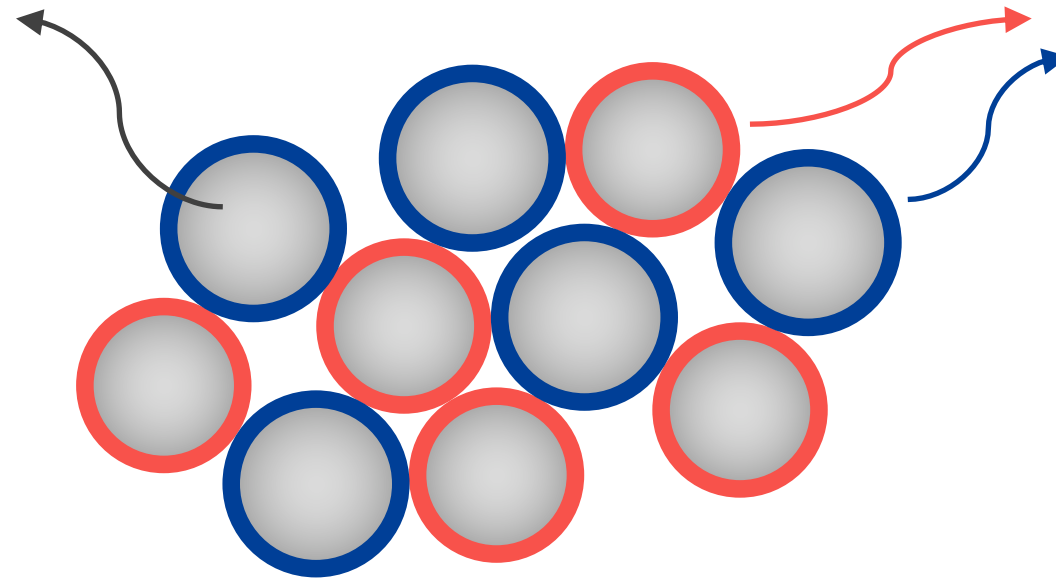
- Epoxy chemistry
- Microparticle size
- Coating thickness



Uncoated

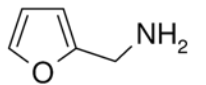
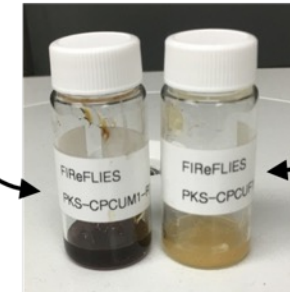
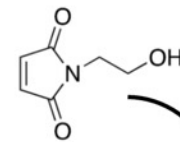


Coated



Polymer Coatings

- Polymer chemistry
- Molecular weight
- Reversible chemistry



Today at 2:25 pm...

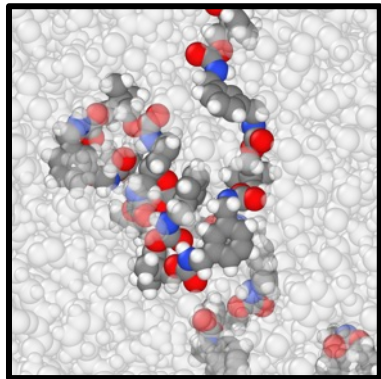
M. Beaudry et al. Recent advances of the ESPUR reversibly assembling materials project.

Materials characterization undertaken across scales



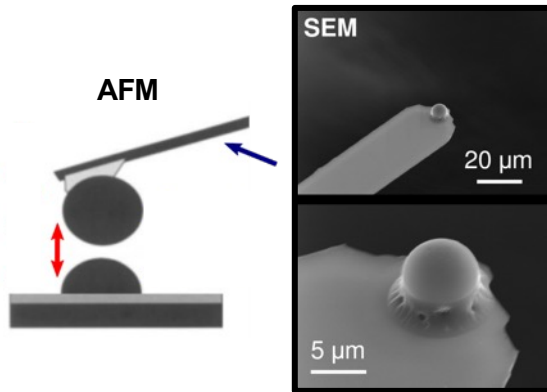
Molecular models for molecular interactions

NASA Ames



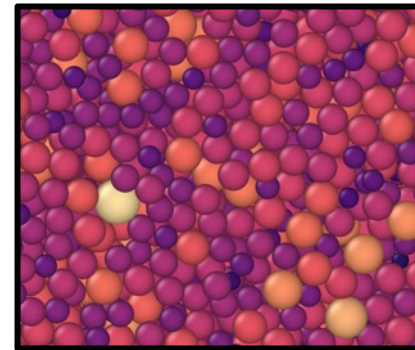
Atomic force microscopy for microparticle interactions

William & Mary

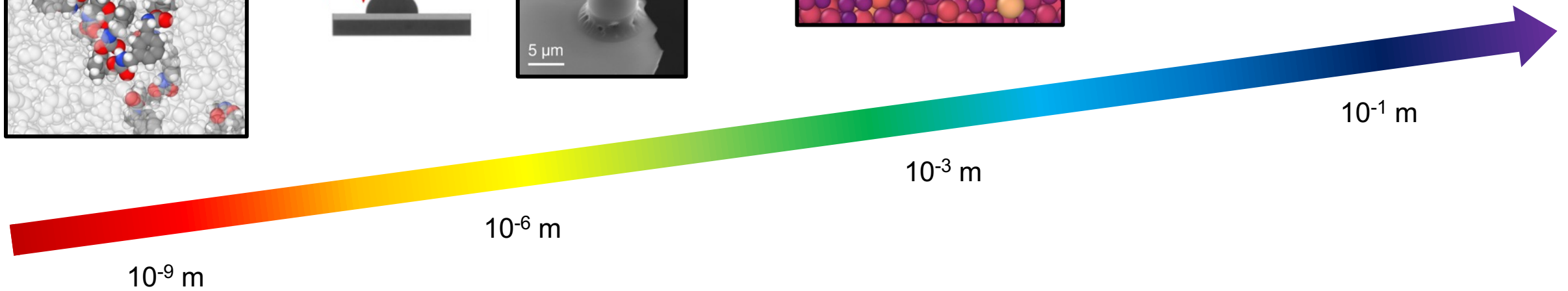
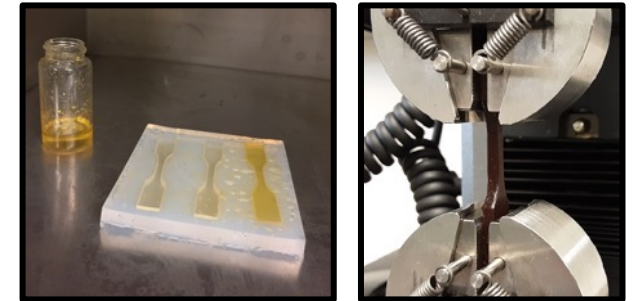


Discrete element models for microparticle packing

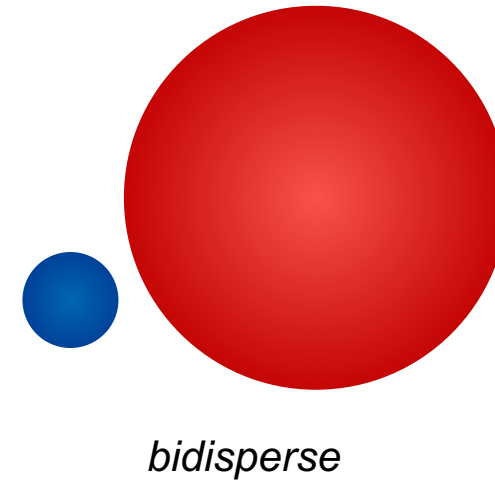
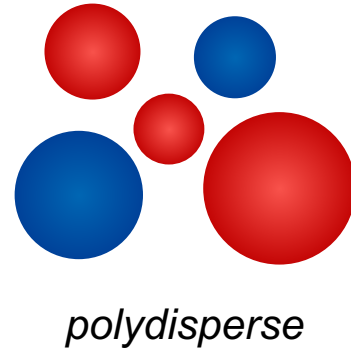
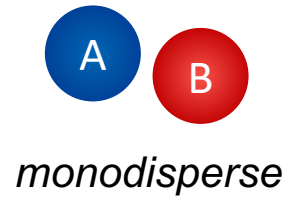
NASA Ames



Mechanical testing for material property calculation
NASA Langley, William & Mary



Influence of microparticle size dispersity on packing



Can we tune particle sizes to:

Maximize
A-B contacts

+

Minimize
void volume

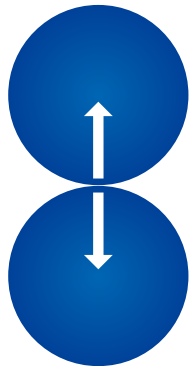


Increase
mechanical
strength

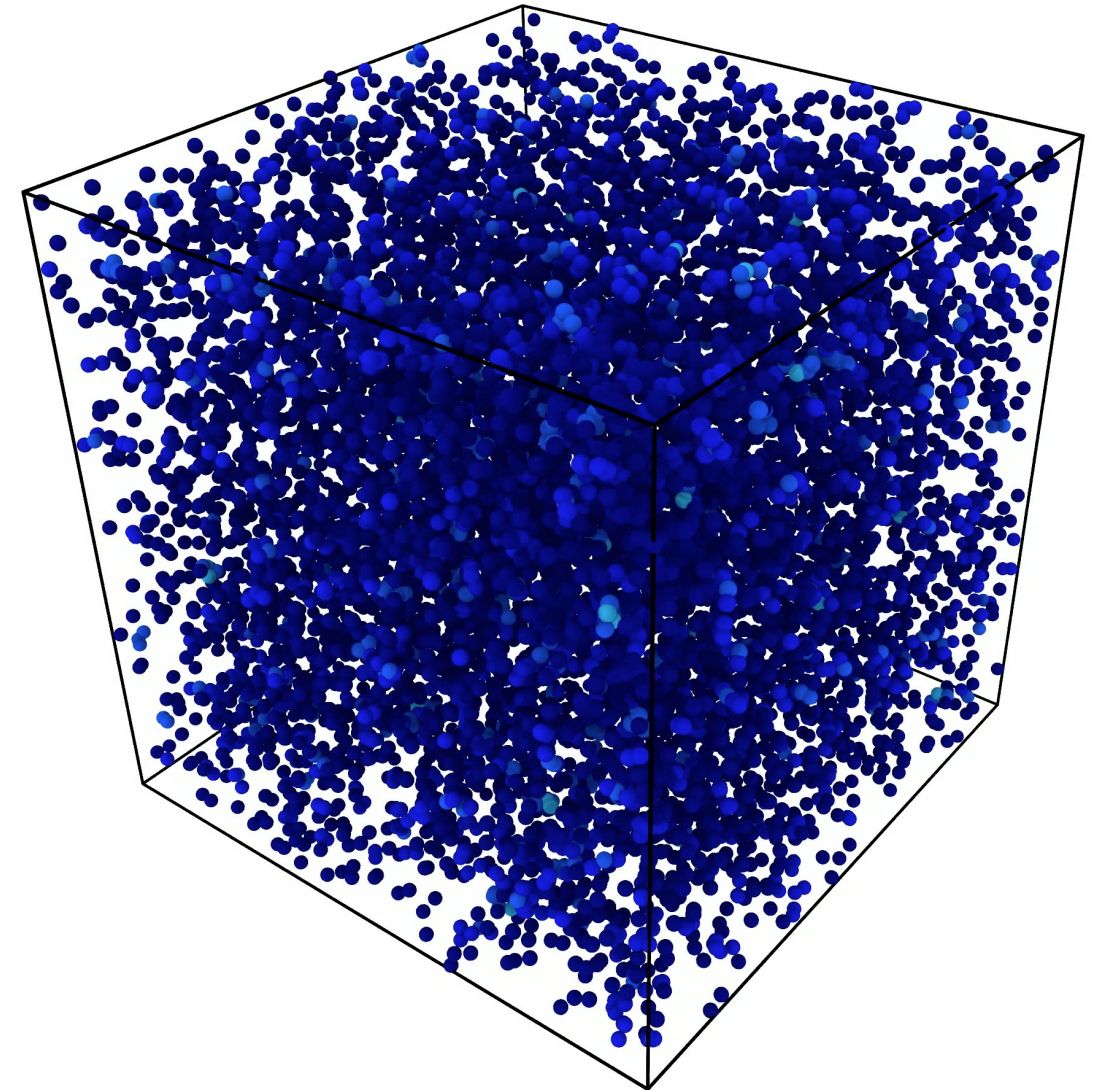
Discrete element method (DEM) simulations



- Box contains at least 1000 each of type A and B particles, up to 10 million total
- Contact mechanics described with Hertzian model, experimentally relevant parameters
- Compress dilute to dense final packing
- Periodic boundary conditions
- LAMMPS



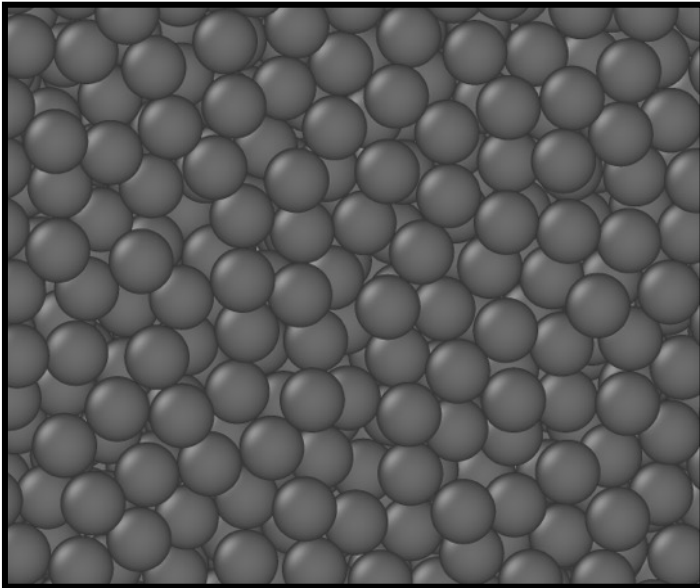
Property	Model parameter	
Young's modulus	k_n	4.808 GPa
Poisson's ratio	k_s	4.345 GPa
Coeff. of restitution	γ_n	$0.009404 \mu\text{m}^{-1} \text{ns}^{-1}$
Density	m_{eff}	$1.1 \text{ pg } \mu\text{m}^{-3}$
Diameter	R_{eff}	$10 \mu\text{m}$



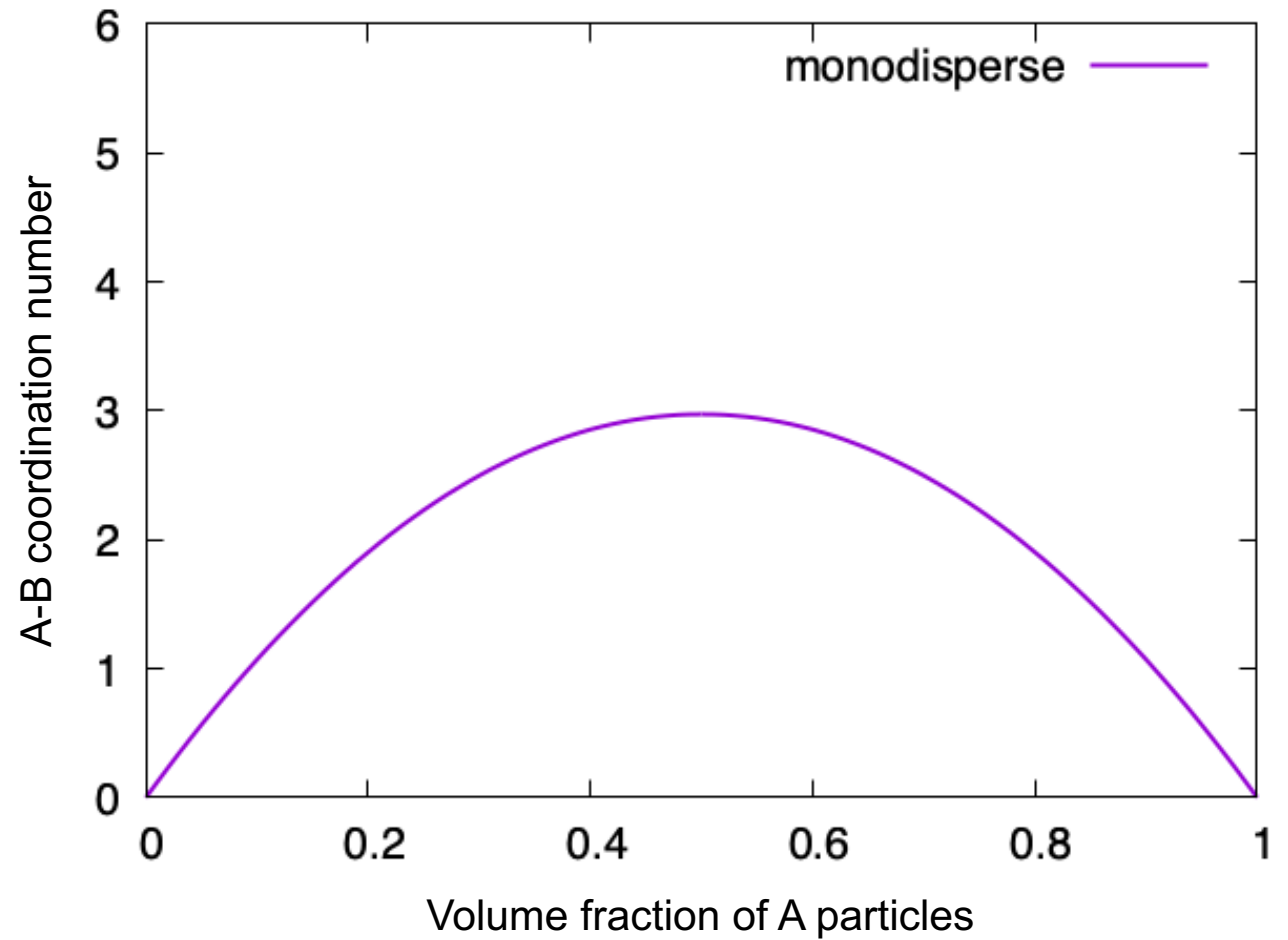
Monodisperse microparticles: the baseline case



- Maximum A-B contacts with 50:50 mix of A and B
- Packing density of ~64%



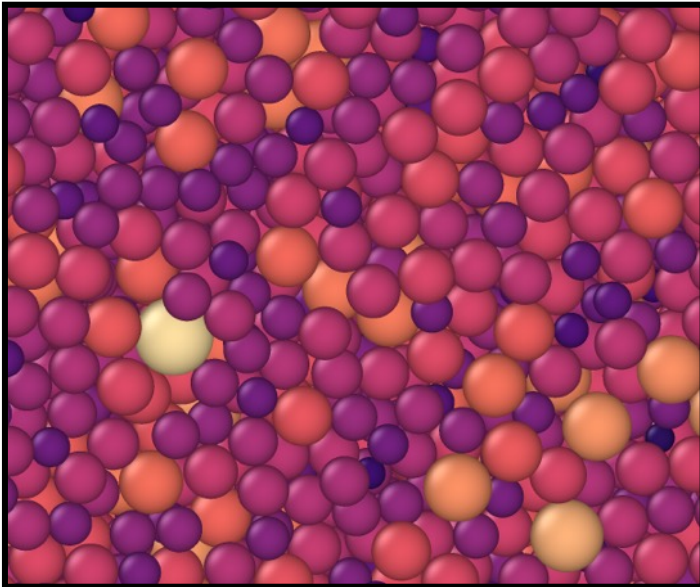
$$D_A = D_B = 10 \mu\text{m}$$



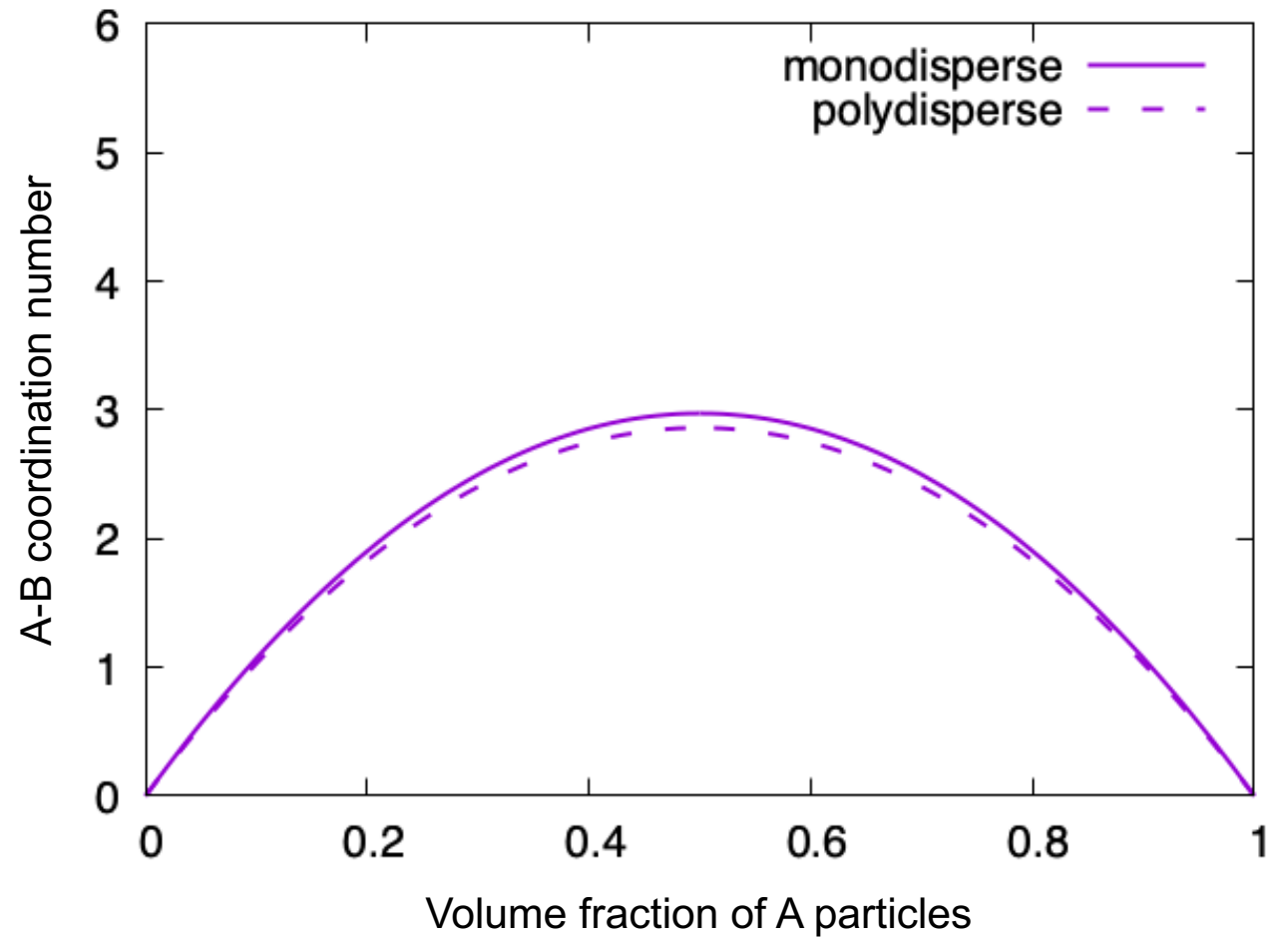
Polydisperse microparticles: experimentally informed



- Slight decrease in contacts, still maximum at 50:50 mix
- Slight increase in packing density



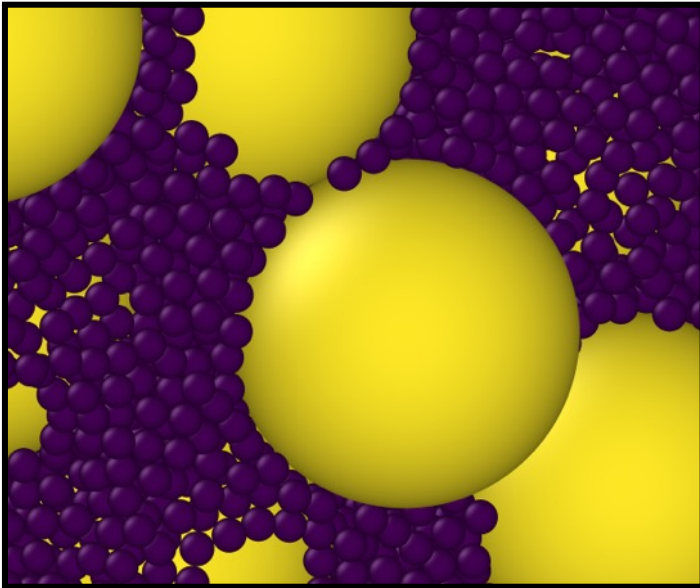
$D_A, D_B \sim N(10 \mu\text{m}, 1.5 \mu\text{m})$



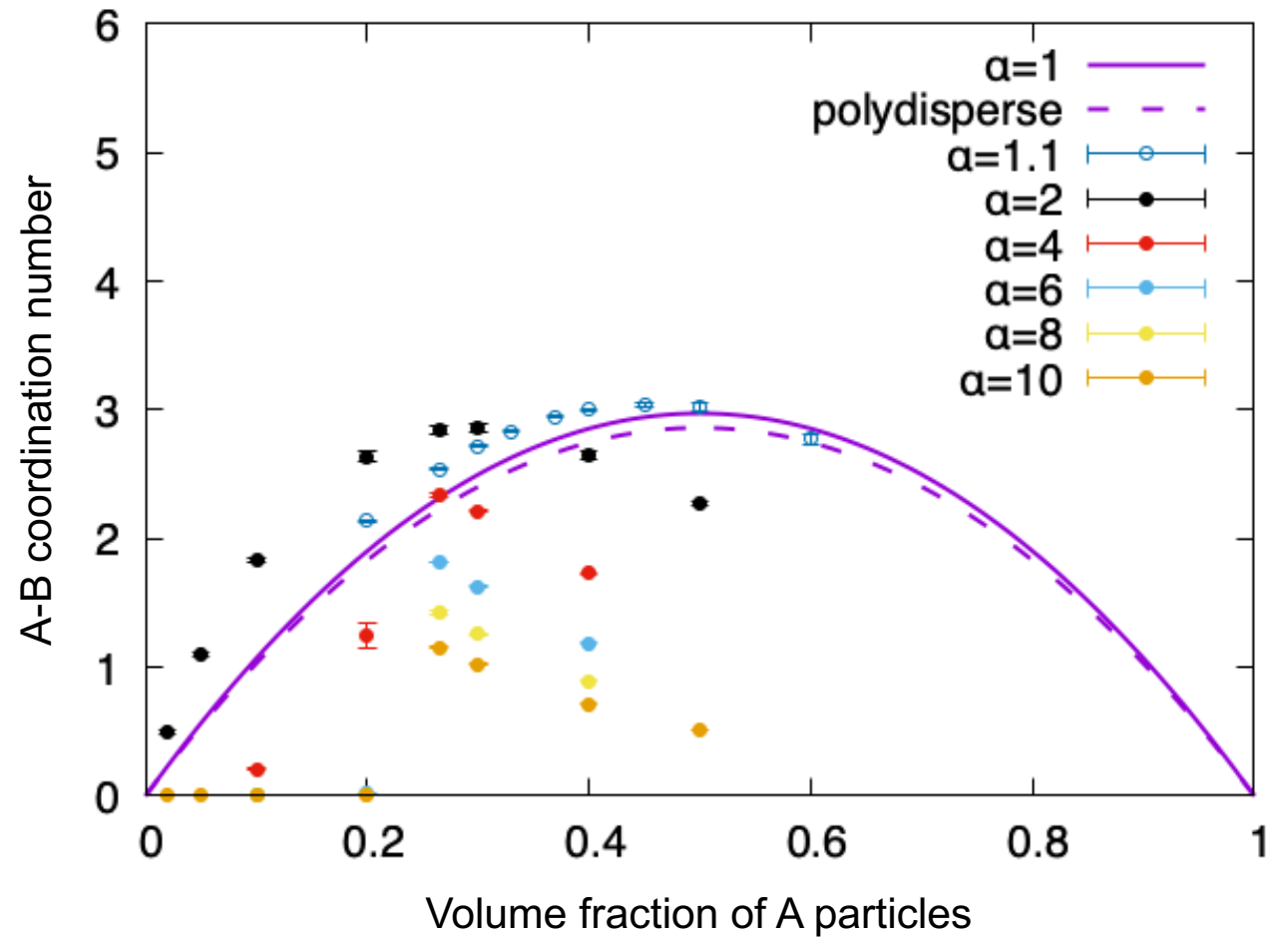
Bidisperse microparticles: guiding future design



- Shift of maximum to lower volume fractions of A particles
- Smaller size ratios \rightarrow more contacts



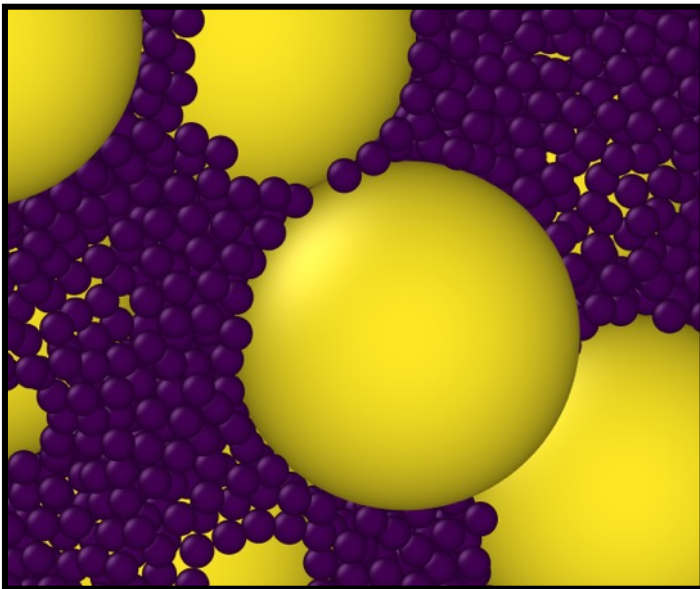
$$D_A = 10 \mu\text{m}, D_B = \alpha D_A$$



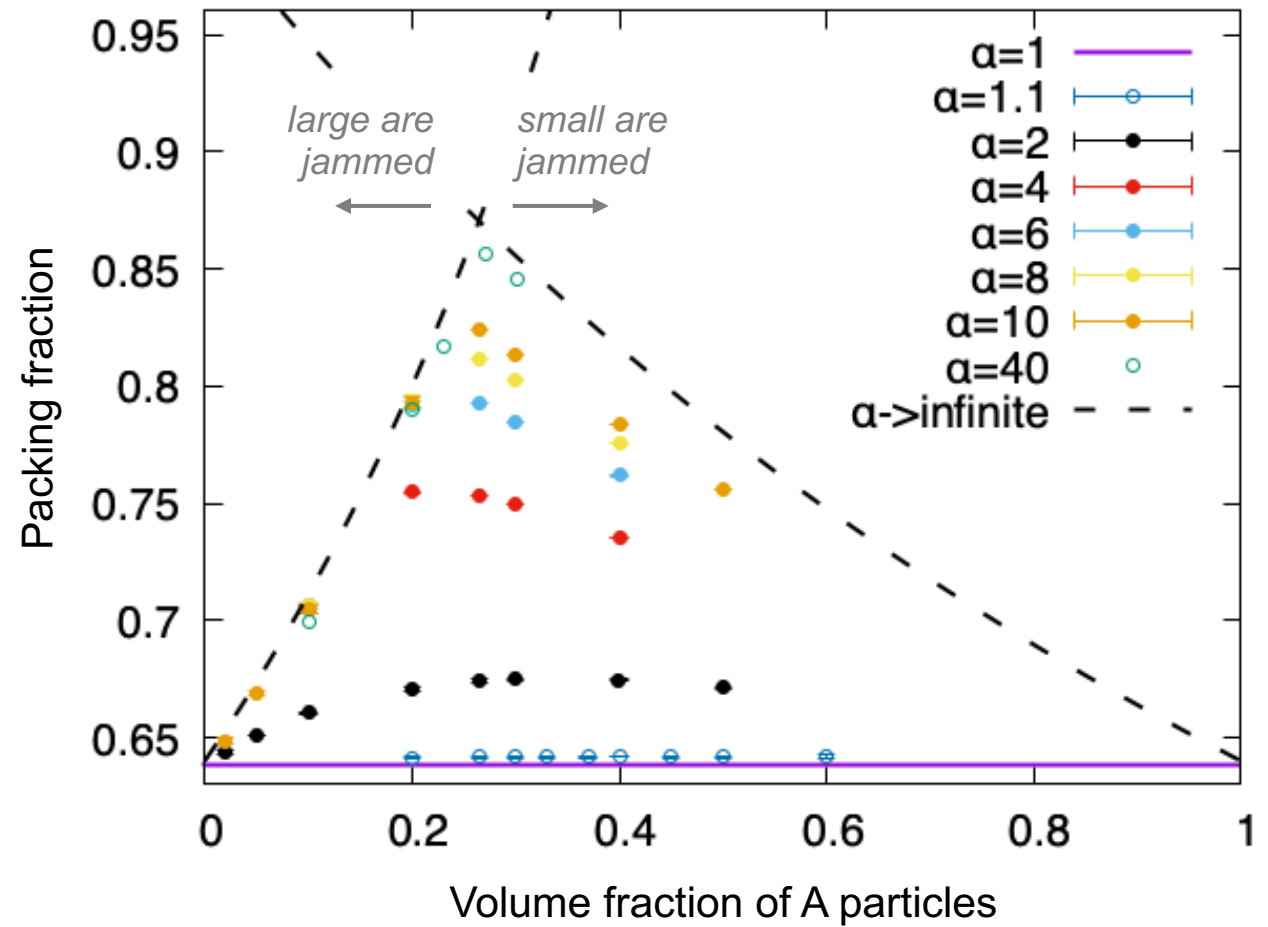
Bidisperse microparticles: guiding future design



- Maximum contacts consistent with maximum packing fraction
- Larger size ratios \rightarrow fewer voids



$$D_A = 10 \mu\text{m}, D_B = \alpha D_A$$



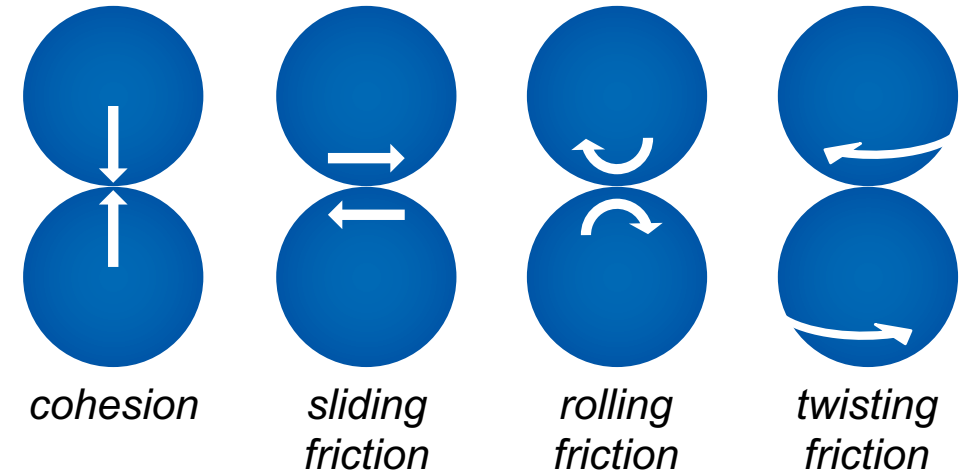
Key takeaways from the microparticle simulations



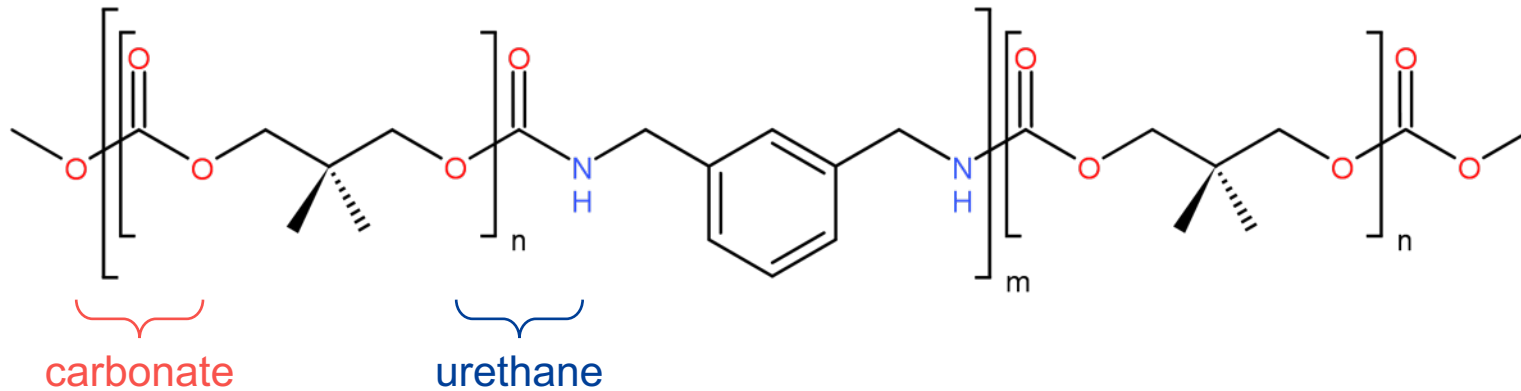
- The optimal A:B mixture depends on the particle size distribution
- The peak volume fraction corresponds with a peak in A-B contacts for bidisperse packings
- Increasing the A:B size ratio causes the volume fraction to increase and A-B contacts to decrease → an expected trade-off for mechanical properties

Next steps:

- Improve discrete element model with addition of cohesion and friction
- Leverage atomic force microscopy data to refine model parameters for microparticle interactions
- Calculate mechanical properties to elucidate expected trade-off behavior for bidisperse packings



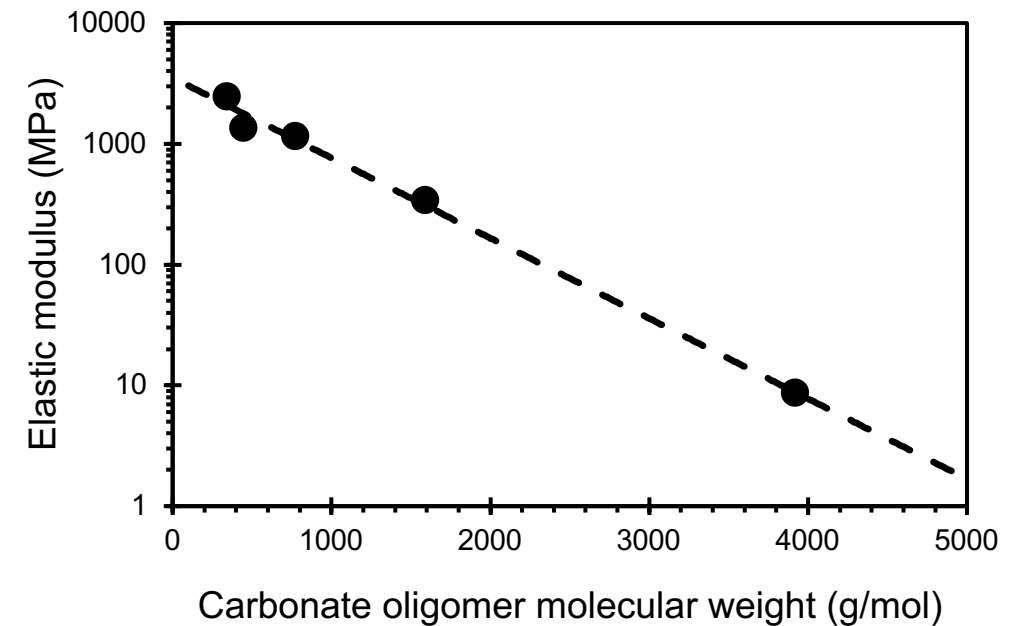
Influence of polymer chemistry on properties



**Copoly(carbonate urethane)
(CPCU)**

How does copolymer composition affect:

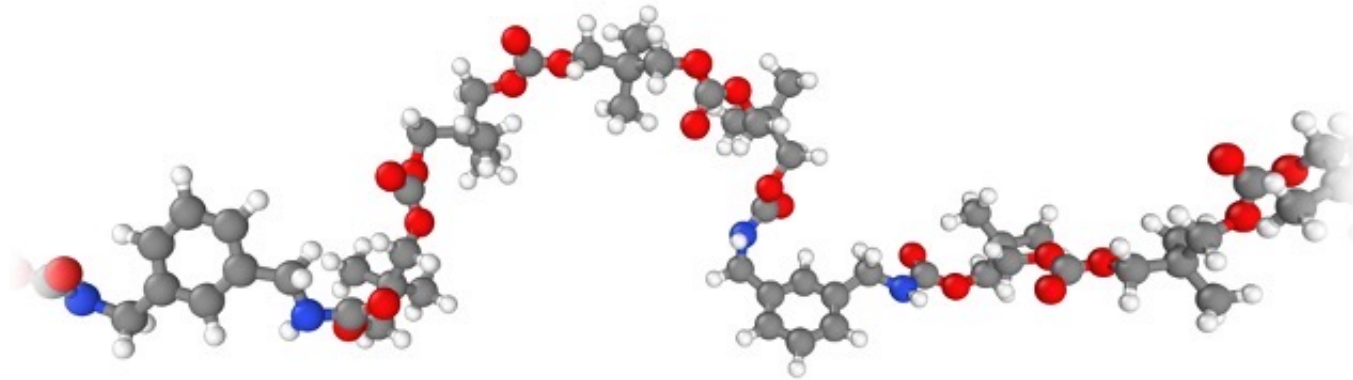
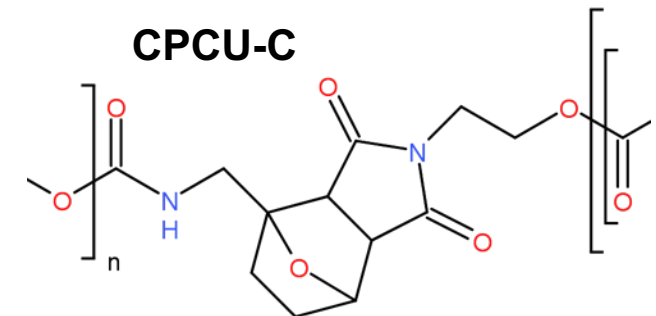
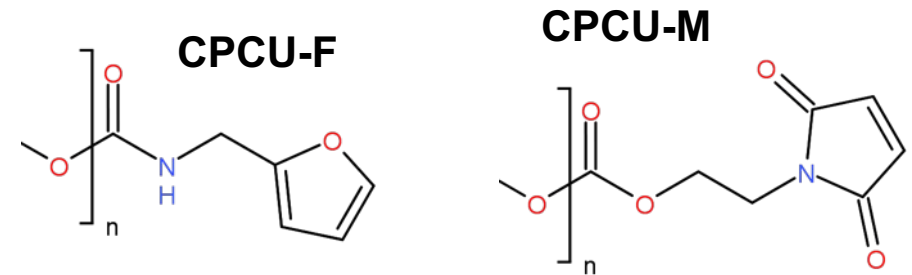
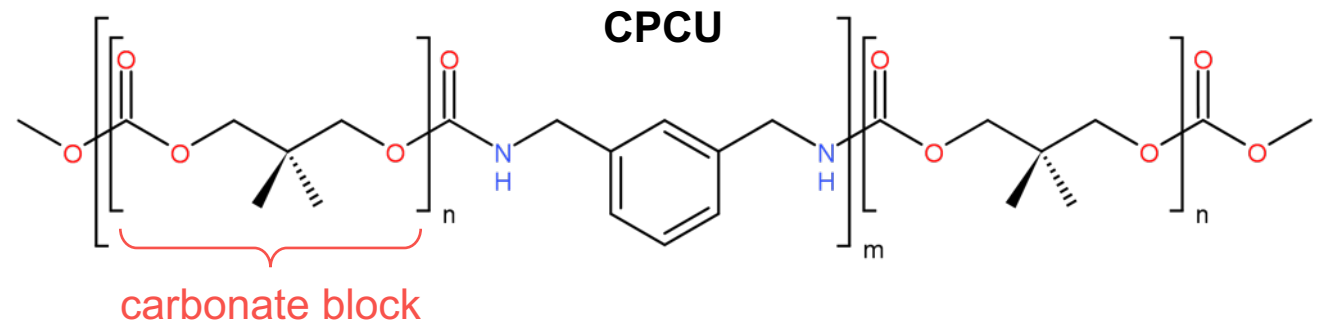
- Molecular interactions
- Polymer properties



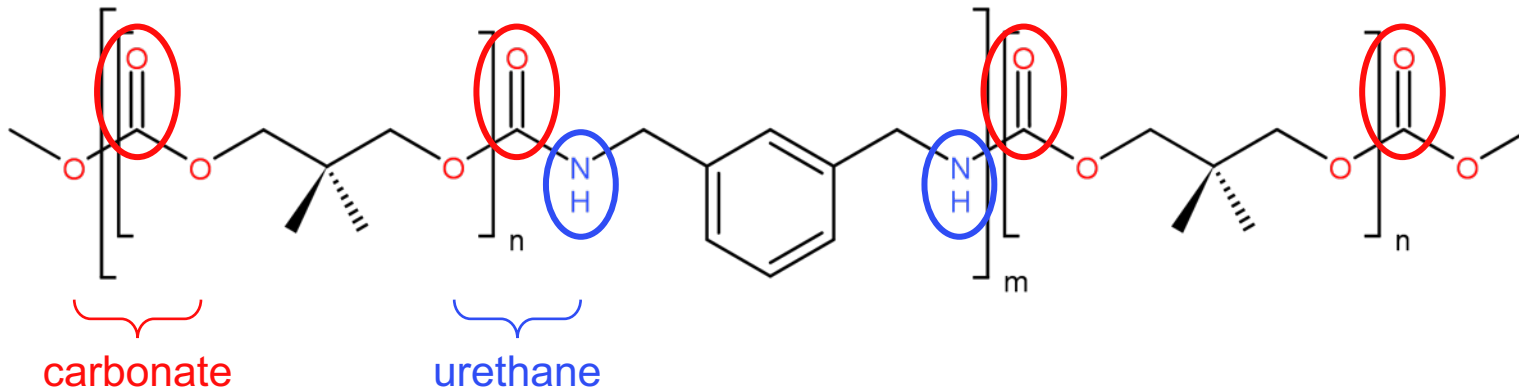
Molecular dynamics (MD) simulations



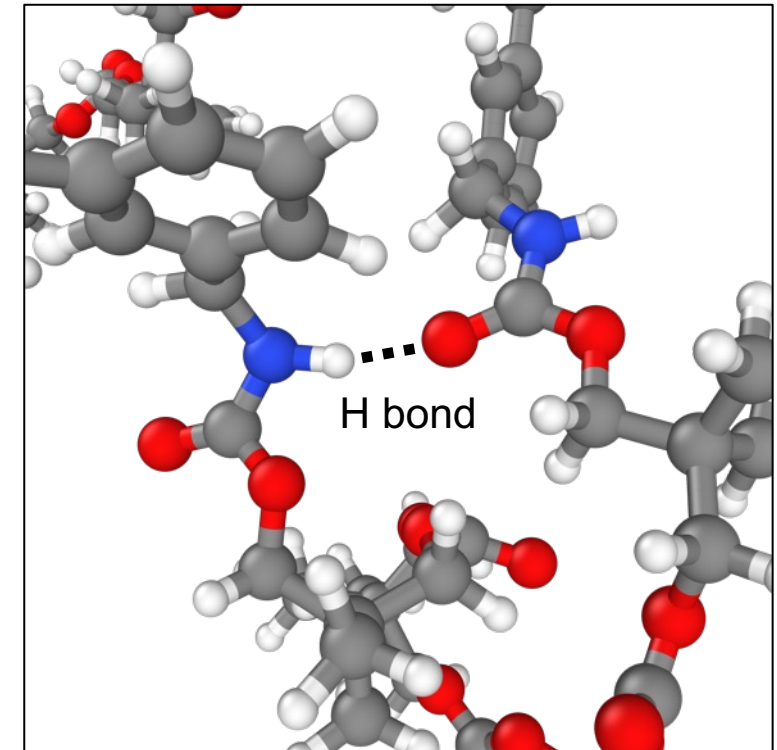
- Varying the carbonate block ($n = 1$ or $n = 4$), similar polymer backbone length
- Varying the end-group functionalization
- Simulations contain ~ 17 - 20 K atoms
- Polymer interactions described with polymer consistent force field (PCFF)
- Periodic boundary conditions
- LAMMPS



Hydrogen bonds play a key role in polymer interactions



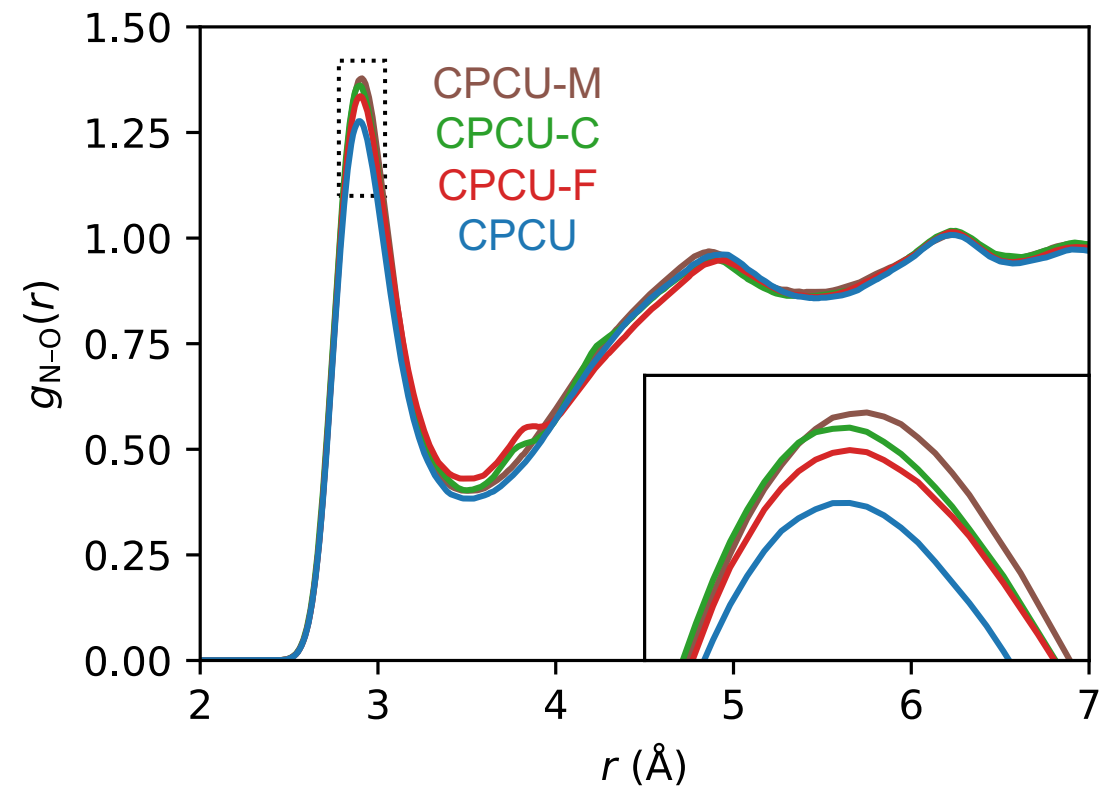
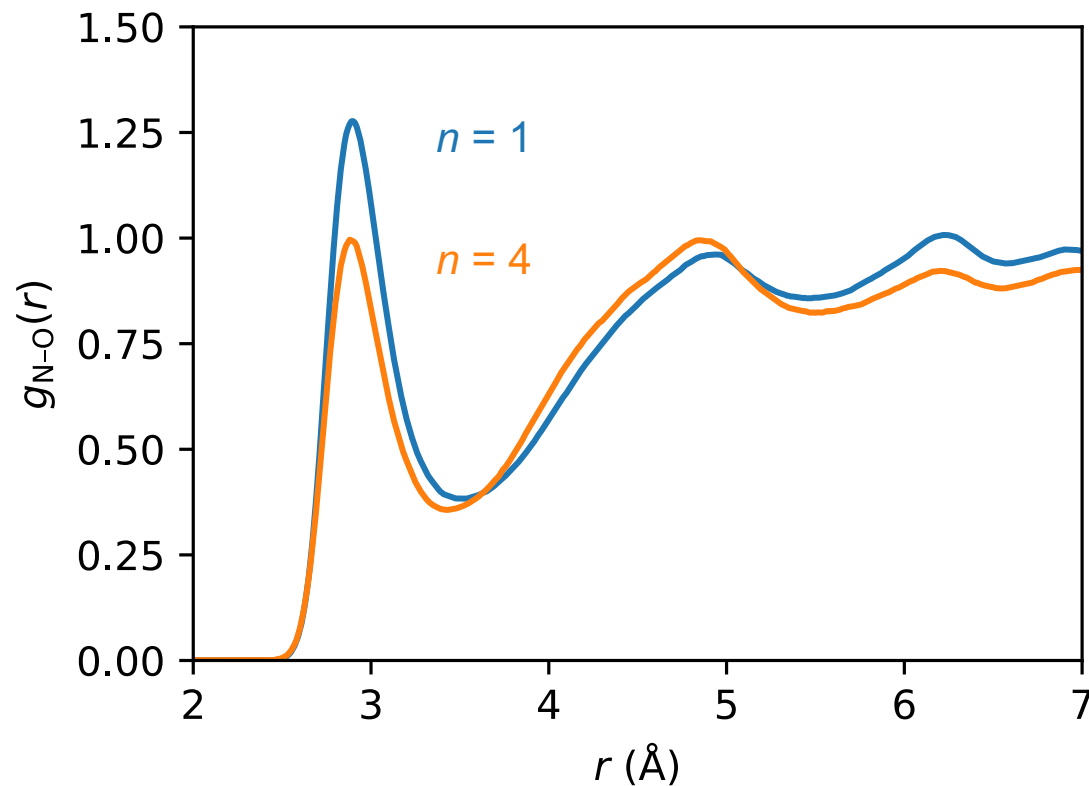
- Hydrogen bonding **C=O** groups in both carbonate and urethane linkages
- Hydrogen bonding **NH** groups in urethane linkage only
- Increasing the carbonate block length decreases the frequency of **NH** groups along the backbone



Copolymer composition affects H-bond interactions



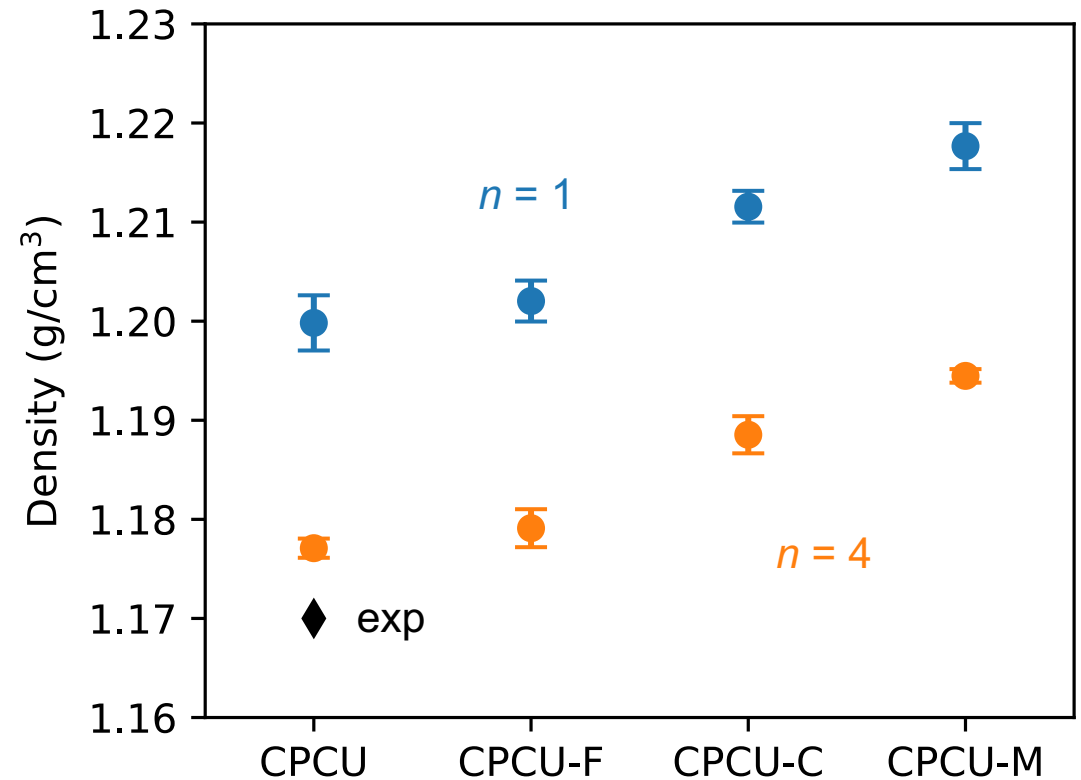
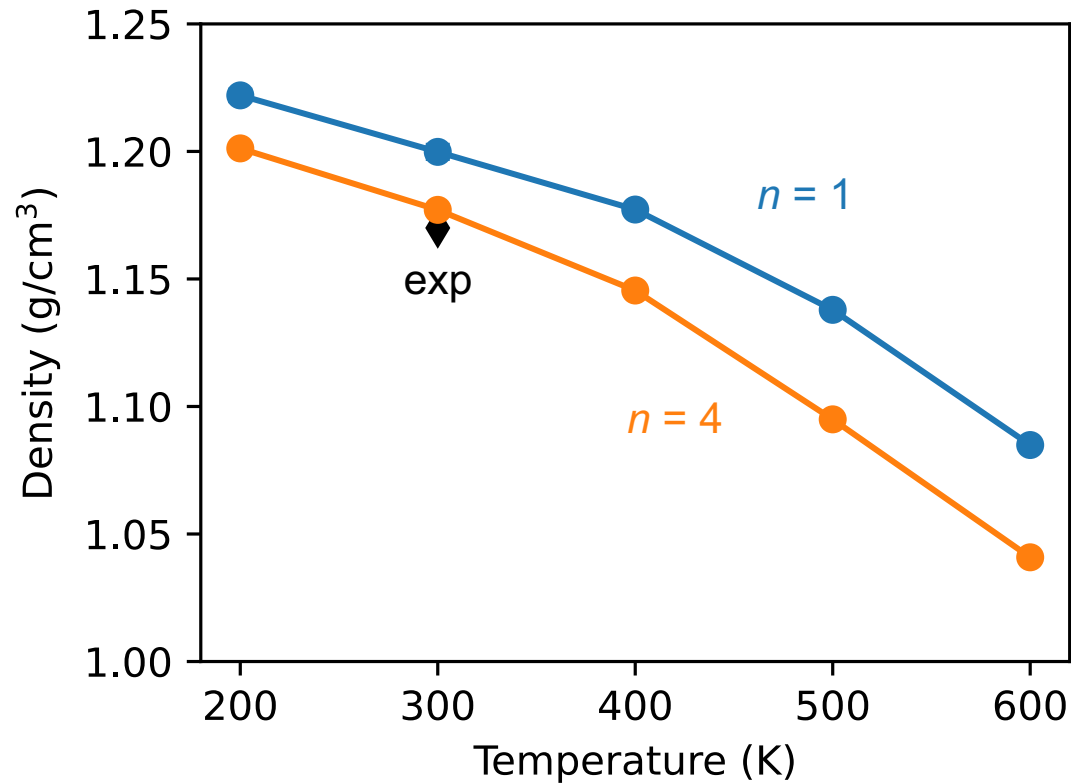
- The first peak in the N-O radial distribution function arises from O...HN hydrogen bonds
- Increasing the carbonate molecular weight reduces the extent of hydrogen bonding
- End functionalization increases the extent of hydrogen bonding



Increased H-bond interactions yield higher densities



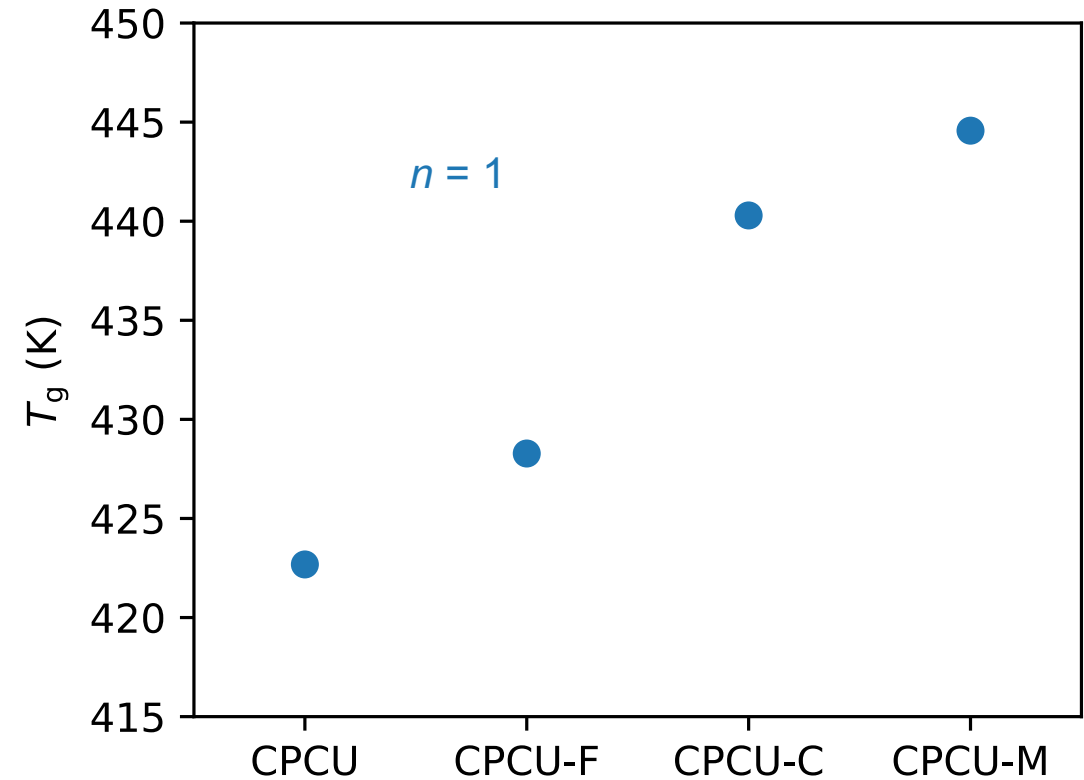
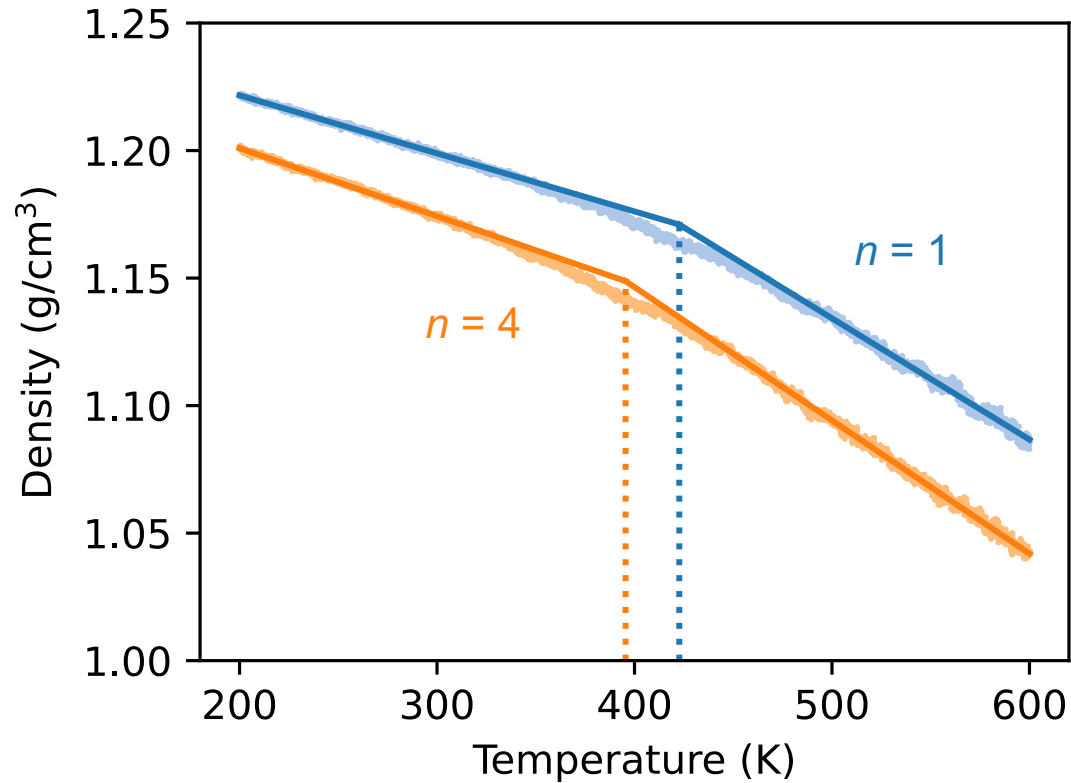
- CPCUs with a greater extent of hydrogen bonding tend to have higher densities
- The experimentally measured density of a CPCU ($n \approx 3-4$) is consistent with the simulations



Increased H-bond interactions yield higher glass transitions



- CPCUs with a greater extent of hydrogen bonding tend to have higher glass transition temperatures
- The glass transition is observed at high temperatures in the simulations due to the fast heating rate



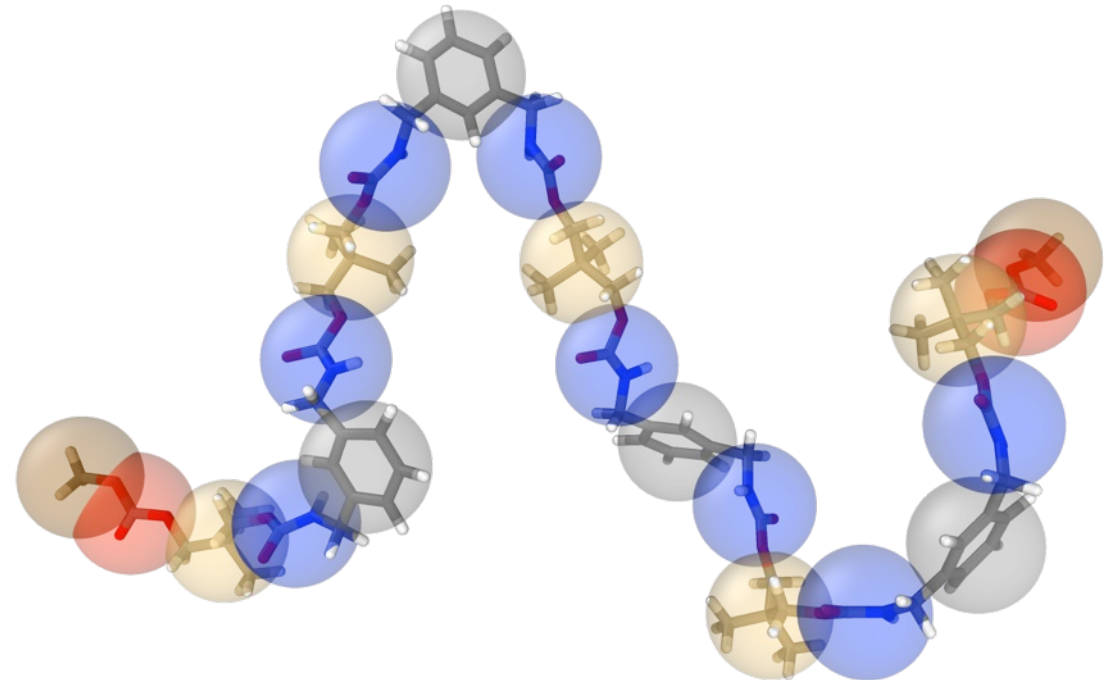
Key takeaways from the polymer simulations



- The CPCU chemistry can be tailored to adjust the hydrogen bonding interactions
- Increasing the extent of hydrogen bonding results in increased densities and higher glass transition temperatures

Next steps:

- Use coarse-grained models to run larger and longer simulations
- Investigate influence of copolymer composition on mechanical properties
- Incorporate click chemistry reactions



Summary



- Computational materials modeling provides important insights to guide materials design, limiting unnecessary experimental efforts
- Discrete element simulations pinpoint the optimal mixtures of functionalized microparticles to increase the mechanical properties
- Molecular dynamics simulations elucidate the extent of hydrogen bonds and their affect on the properties of the CPCU polymer coatings