

Evaluation of Voronoi Meshes for Large Eddy Simulations of High Lift Aerodynamics

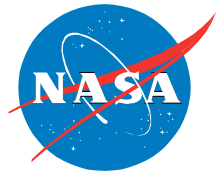
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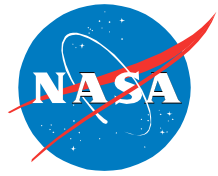
AIAA SciTech Forum, National Harbor, MD

01/23/2023

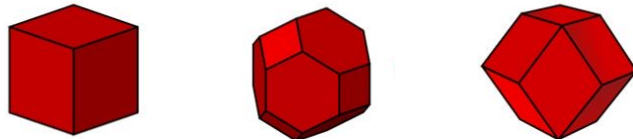


- LES addresses major challenges faced by RANS in shear-dominant flows such as take-off and landing of airplanes with deployed high-lift devices
- And it is becoming feasible at practical scale thanks to advancements in high-performance computing
- AIAA 4th High-Lift Prediction Workshop (HLPW4)
 - Nine participants submitted WMLES results, of which 6 used unstructured meshes
 - In contrast, HLPW3 had no WMLES submissions
- Results are extremely encouraging, but success highly depends on mesh density and quality
- High quality unstructured meshes can be generated at scale using Voronoi methods

Voronoi Mesh Properties

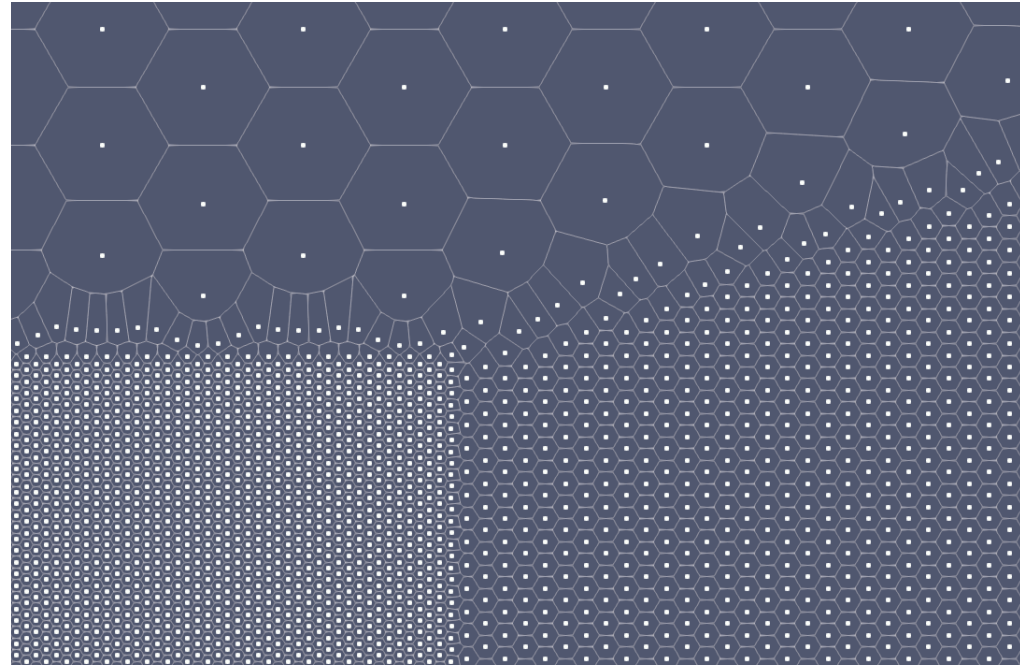
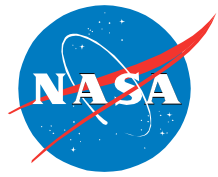


- Voronoi diagrams have inherent special properties:
 - Cells are guaranteed to be convex
 - Faces are planar
 - Faces are located halfway between seed points
 - Faces are orthogonal to the vector connecting the two seeds on either side
- These properties act to significantly improve robustness and reduce dissipation in CFD
- Various cell types can be generated:
 - Cartesian seeding – Cubic cells
 - Body-centered Cubic (BCC) – Truncated octahedral cells
 - Face-centered Cubic (FCC) – Rhombic dodecahedral cells

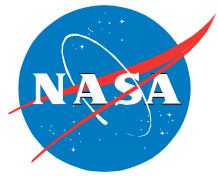


https://en.wikipedia.org/wiki/Voronoi_diagram

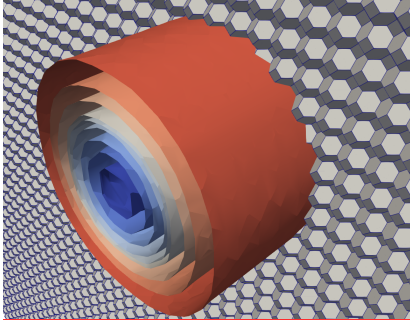
Voronoi Mesh Smoothing



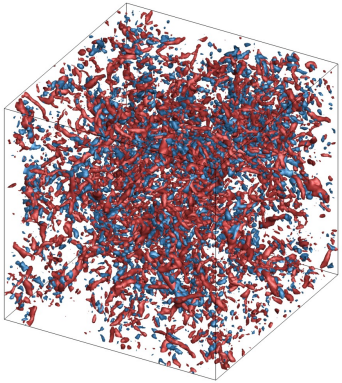
- Coarse/fine interfaces, or irregular point distributions can be naturally smoothed
 - Lloyd procedure iteratively moves seed points to the generated cell's centroid
 - Results in a regularized point distribution
 - Cells converge towards a centroidal shape
- In practice, we apply the smoothing in a limited zone around mesh size transitions
 - Majority of the regularly seeded mesh is unaffected



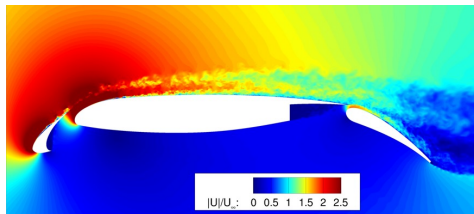
- LAVA Unstructured solver was used
 - Developed at NASA Ames Research Center
 - A decade of successful use for RANS simulations using arbitrary polyhedral meshes
 - Recently refactored and highly optimized for modern CPU's
- 2nd order accurate cell-centered finite volume method
- Sensor based, blended upwind/central convective flux scheme
- Vreman Sub-Grid Scale (SGS) turbulence model
- Explicit 3rd order accurate time integration with a strong stability preserving, 3-stage Runge-Kutta scheme
- Blended log-layer explicit wall model



- Isentropic vortex propagation
 - Demonstrate kinetic energy preservation
 - Investigate effects of different Voronoi mesh types
 - Study coarse/fine interface effects

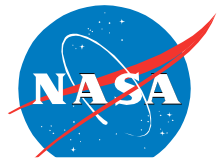


- Homogeneous Isotropic Turbulence (HIT)
 - Test SGS for non-linear robustness
 - Study the turbulent energy cascade

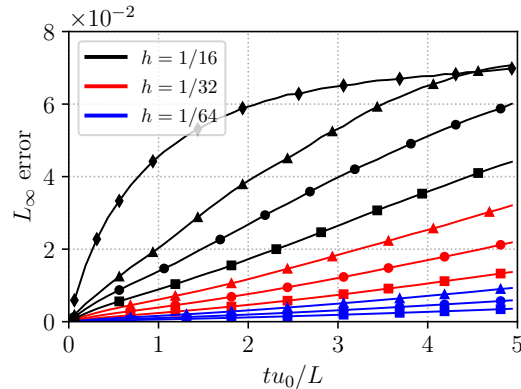
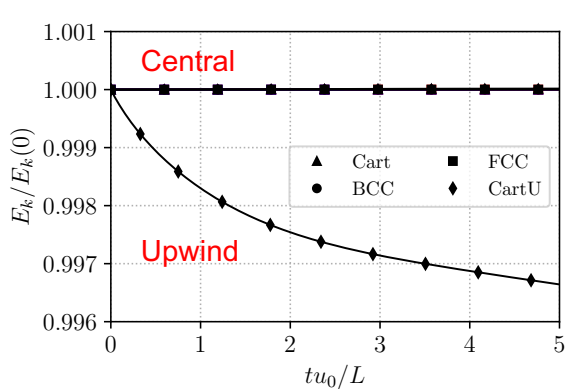
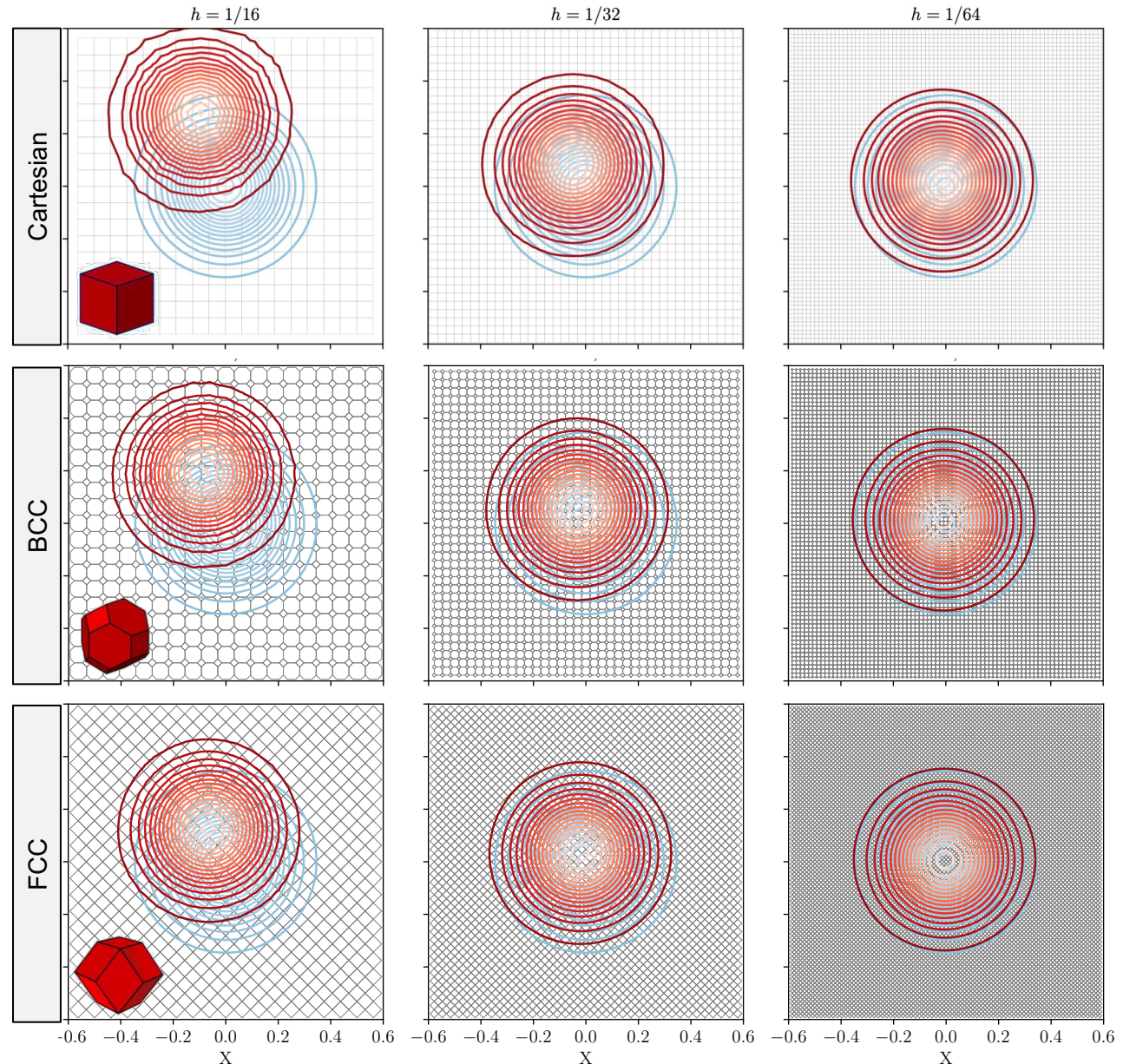


- McDonnell Douglas 30P30N multi-element airfoil
 - Compare high-lift aerodynamics predictions to experimental data
 - Demonstrate results for different Voronoi mesh types
 - Verify current numerical approach's suitability for WMLES

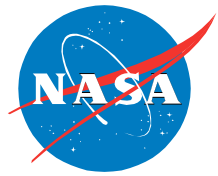
Isentropic Vortex Propagation – Uniform Mesh Results



- Inviscid vortex tube traveling in x-direction
 - Triply periodic domain with extents $[-2, 2]$
 - Measured integrated kinetic energy and pressure error for 5 pass-through periods
- Voronoi mesh types: Cartesian, BCC & FCC
- Central convective flux is non-dissipative, with 2nd order solution error convergence for all grid types
- Dispersion errors manifest as drift
- For the same grid spacing, Cartesian has the largest error, FCC has the least

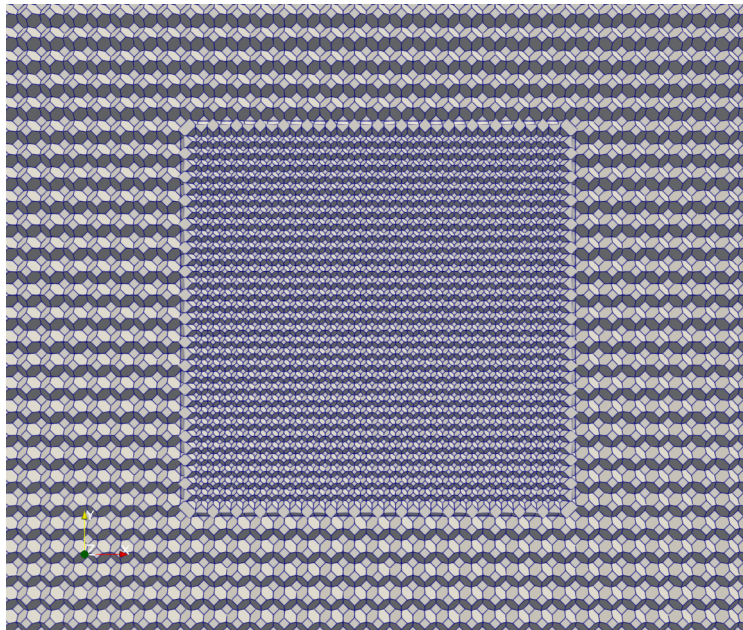


Isentropic Vortex Propagation – Coarse/Fine Interfaces

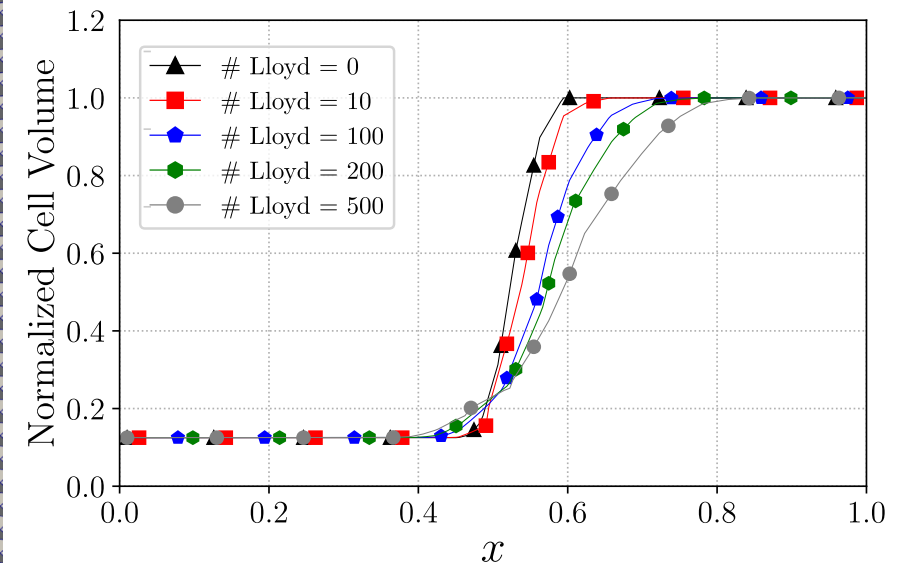
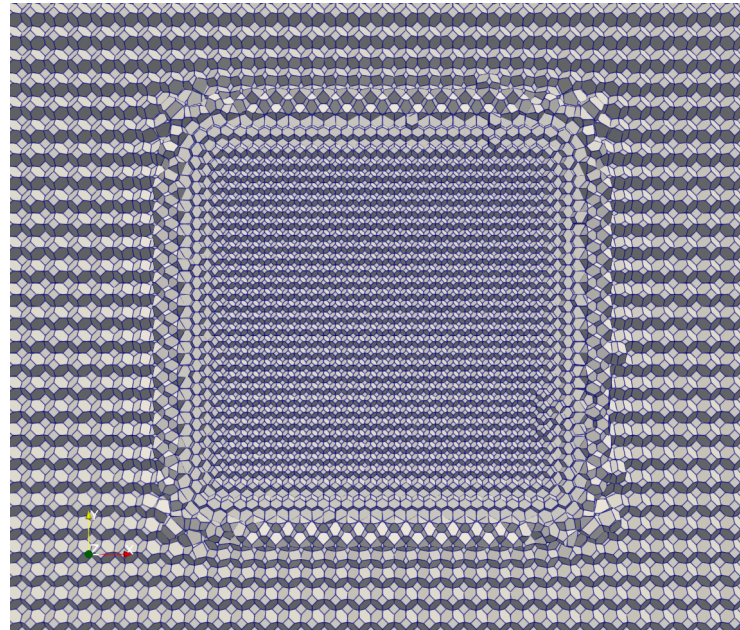


- A 1:2 coarse/fine interface was studied by embedding a cubic refinement region in the domain
- Interfaces of varying smoothness are generated via Lloyd iterations

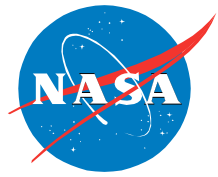
0 Lloyd Iterations



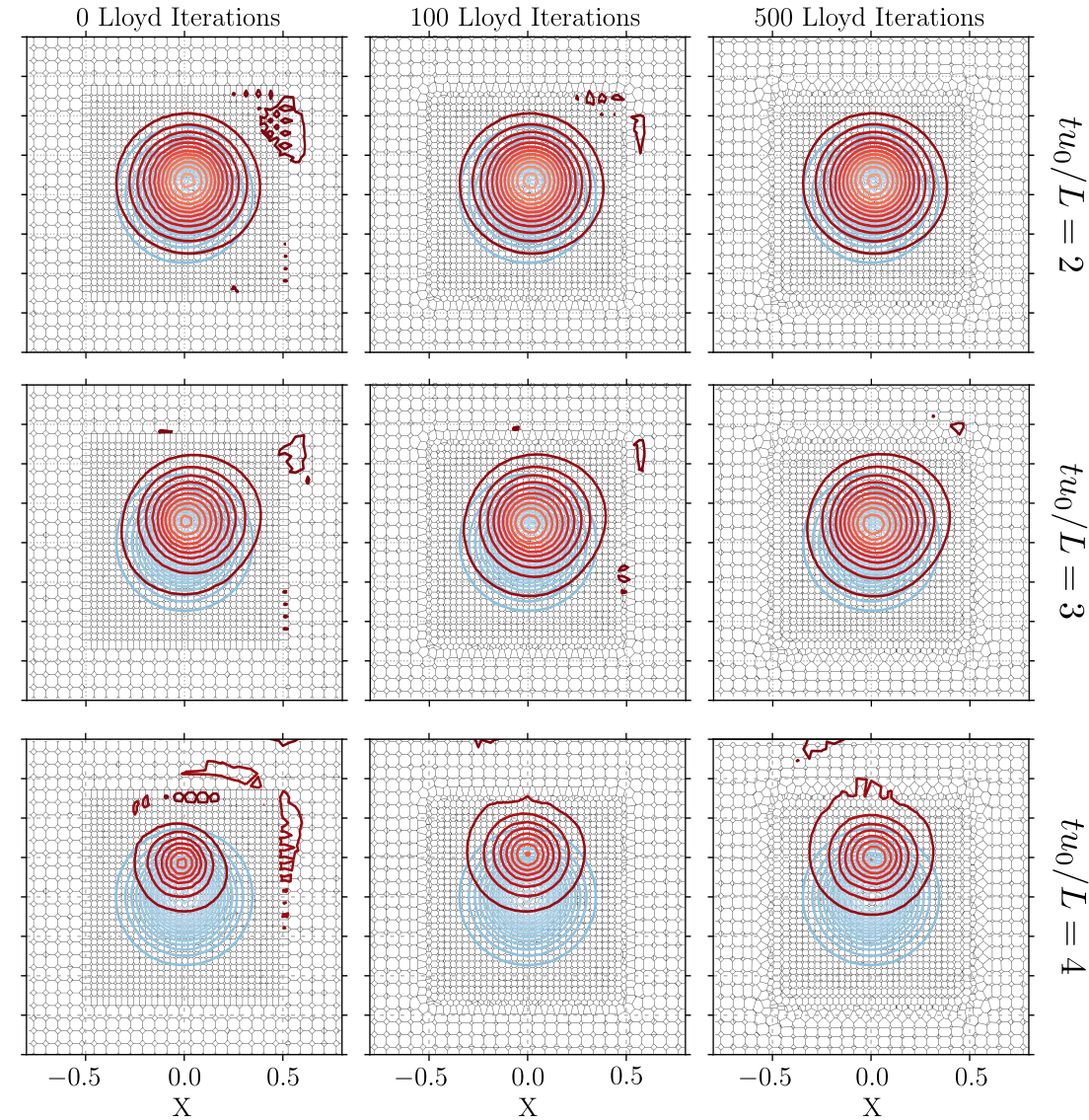
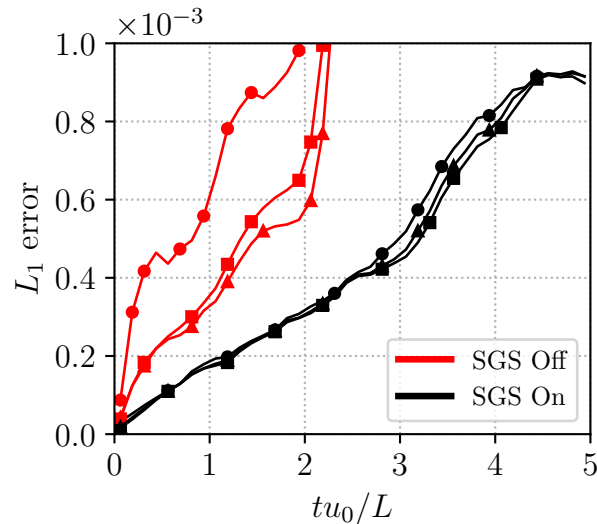
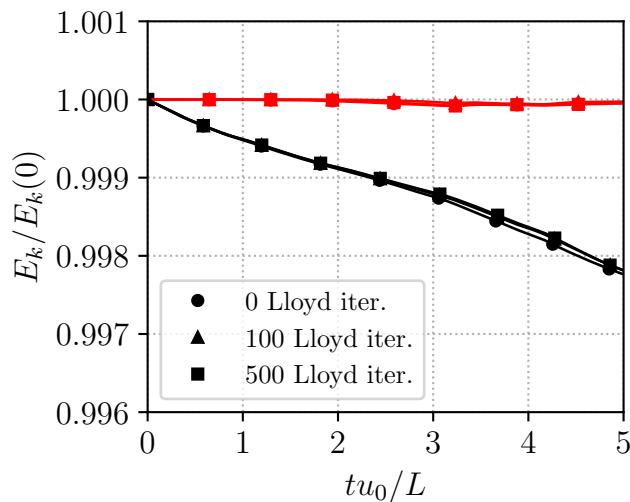
500 Lloyd Iterations



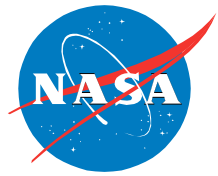
ISENTROPIC VORTEX PROPAGATION – COARSE/FINE INTERFACES



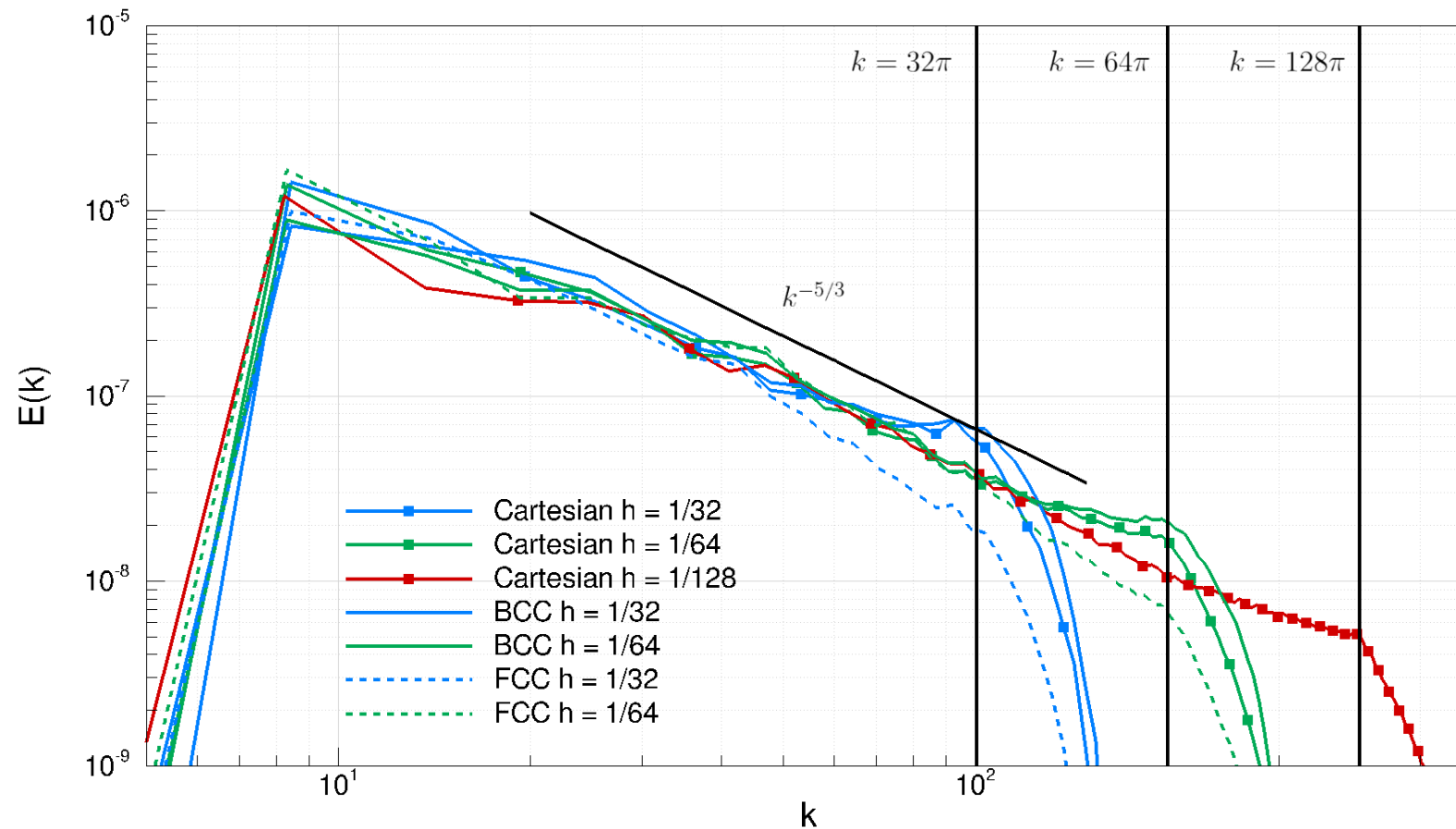
- Only BCC Voronoi meshes were used in this test
- Simulations without SGS is not stable when coarse/fine interface present
 - No mechanism to attenuate the errors due to the interface
 - Kinetic energy is preserved
- SGS was provided sufficient stability without any upwinding
- Smoother interface: Less energy decay, and less pressure error
- But the difference is marginal



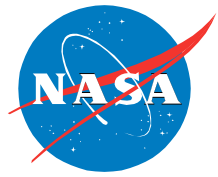
Homogeneous Isotropic Turbulence (HIT)



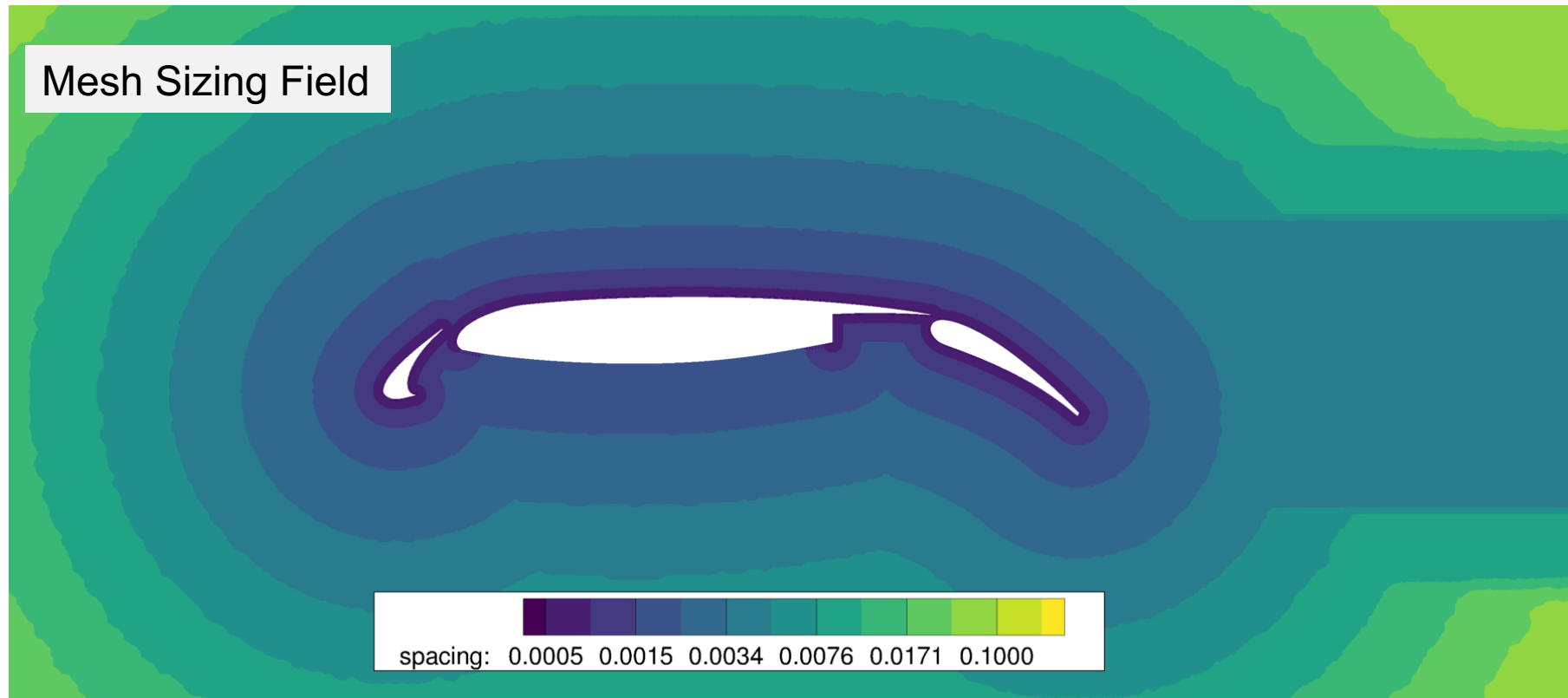
- HIT with a momentum forcing source was studied
- Energy decay rate at the inertial rate is correctly predicted
- Onset of rapid dissipation at the sub-grid scale is captured at correct Nyquist wave numbers



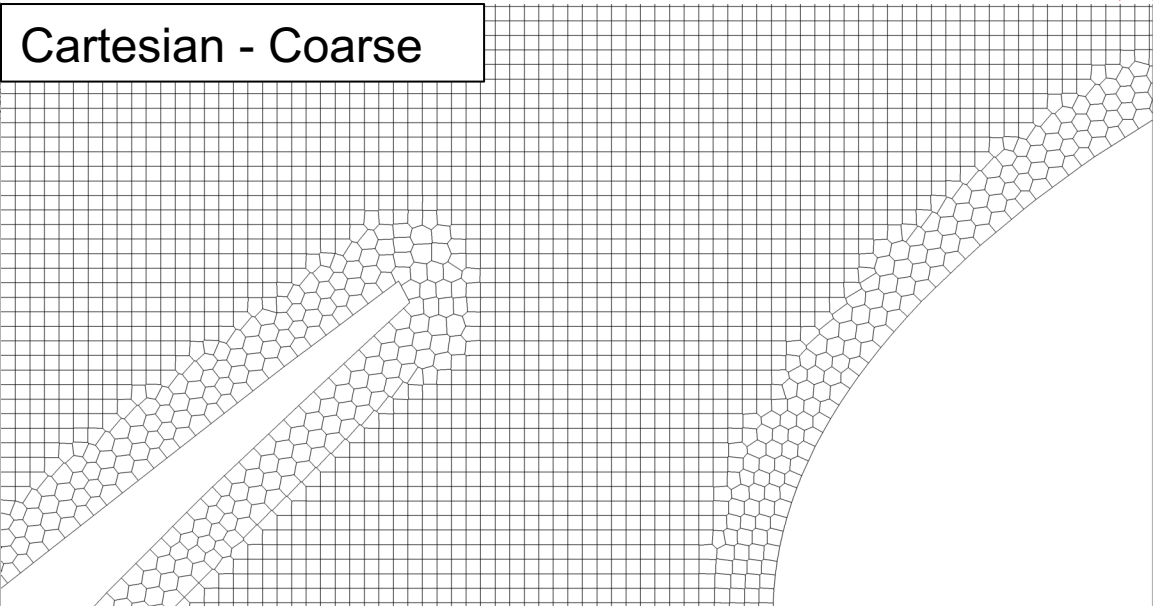
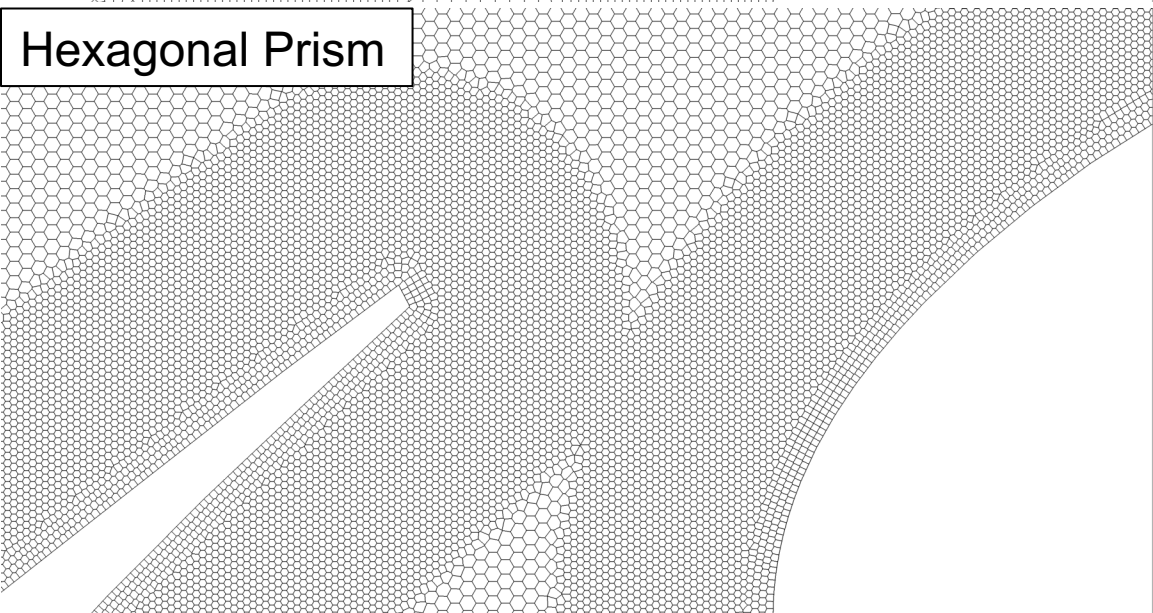
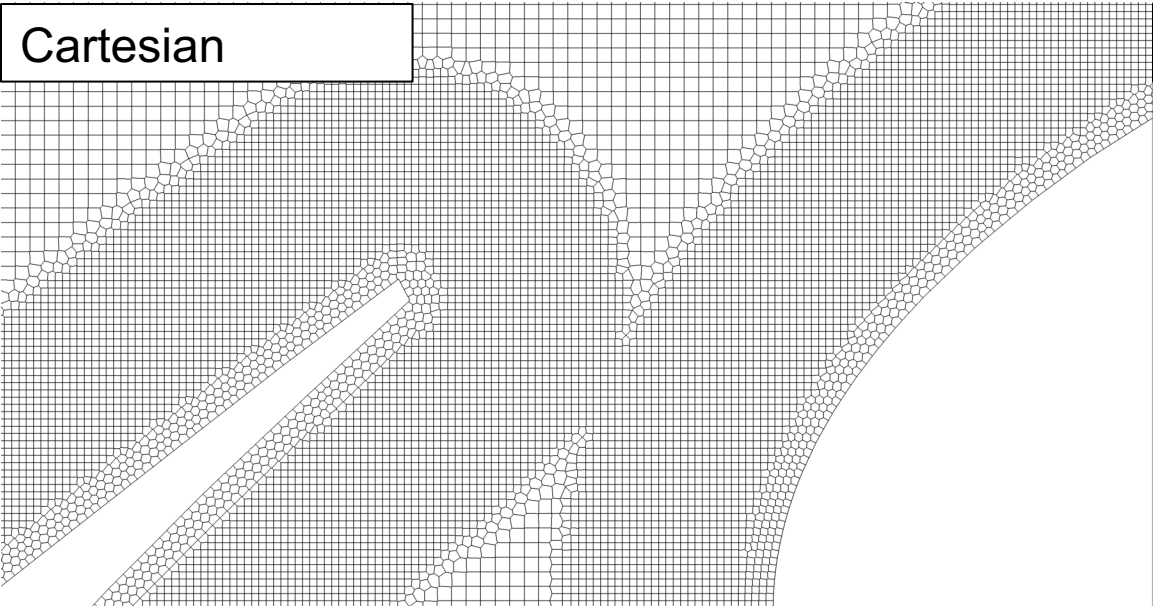
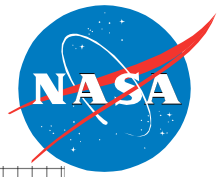
30P30N Setup



- $Ma = 0.2$, $Re = 9e6$
- 10% c span length simulated with periodic boundary conditions on end planes
- Meshes are created in 2D, extruded spanwise with a constant spacing of $1e-3c$
- Two different Voronoi mesh types tested: Cartesian seeded and Hexagonal seeded



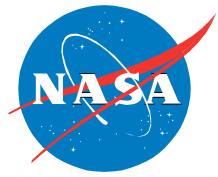
30P30N Meshes – Slat Gap Close-up



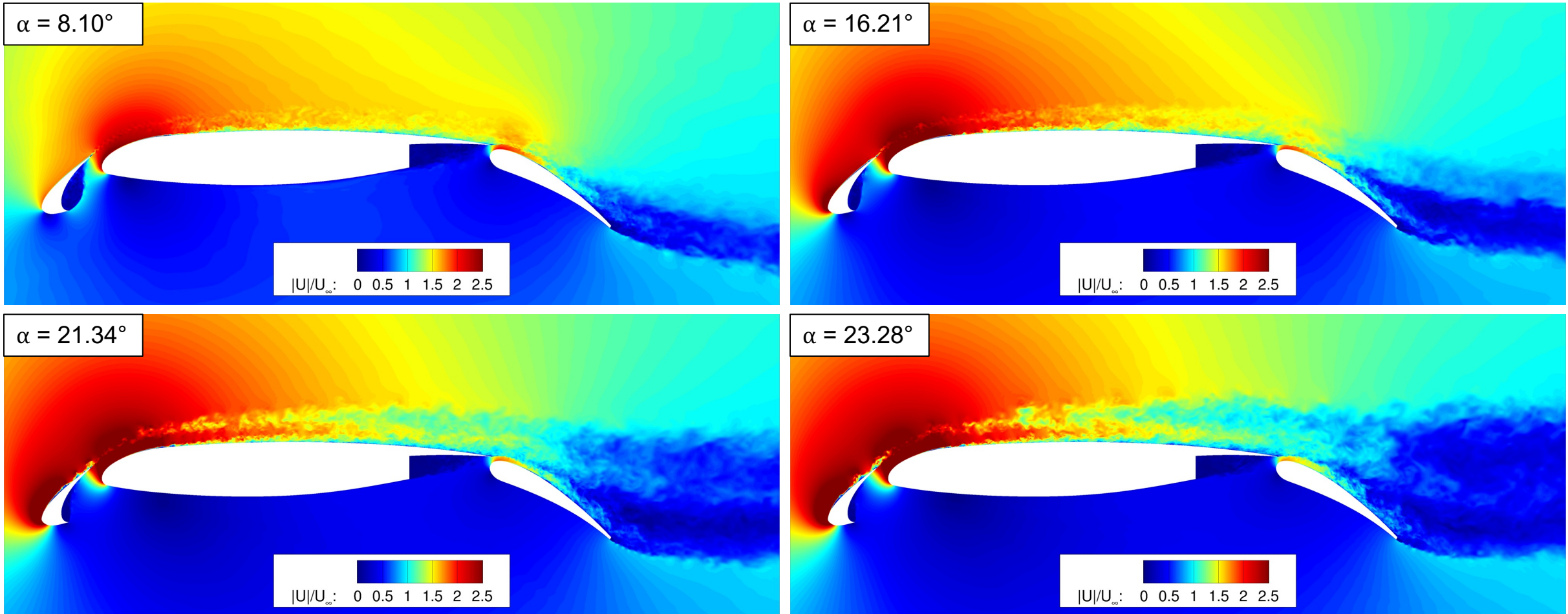
- Refinement regions of same sizing contoured around different elements seamlessly join together
- 4 wall-aligned layers, 15 Lloyd smoothing iterations
- Smoothed cells in Cartesian mesh naturally morph into hexagonal cells and other transitional cell types
- Cartesian – Coarse mesh simply skips the finest sizing region

Mesh	Spacing (chord normalized)					# Cells (million)	# Faces (million)
	Slat	Main Upper	Main Lower	Flap	Spanwise		
Cartesian Voronoi - Coarse	1e-3	1e-3	2e-3	1e-3	1e-3	31.8	101.3
Cartesian Voronoi	5e-4	5e-4	2e-3	5e-4	1e-3	41.7	133.8
Hexagonal Prism Voronoi	5e-4	5e-4	2e-3	5e-4	1e-3	50.9	198.3

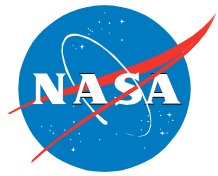
30P30N Results – Instantaneous Velocity Magnitude Field



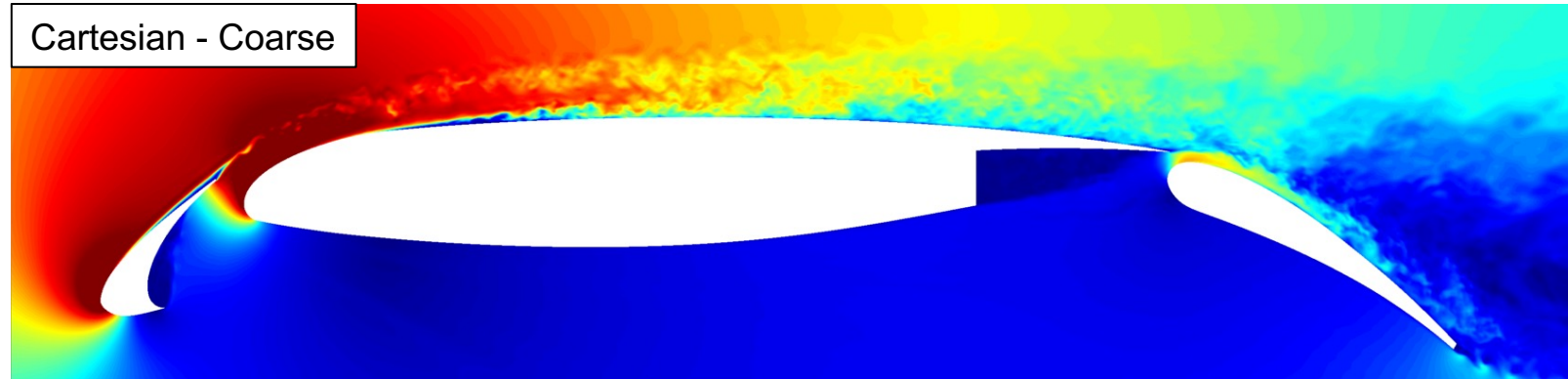
- Instantaneous velocity magnitude contours shown for the hexagonal prism mesh



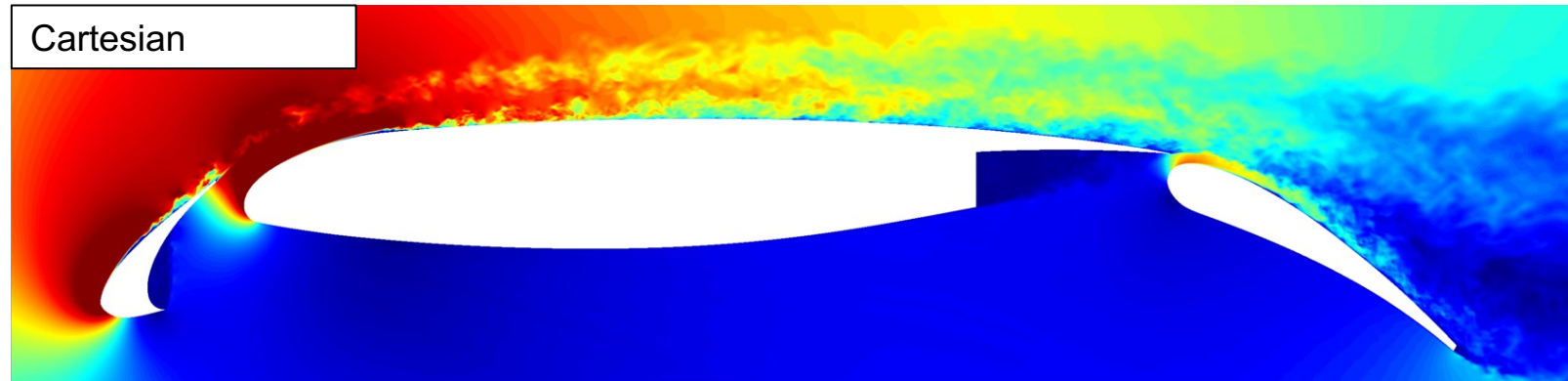
30P30N Results – Mesh Sensitivity at $C_{L,max}$ ($\alpha = 21.34^\circ$)



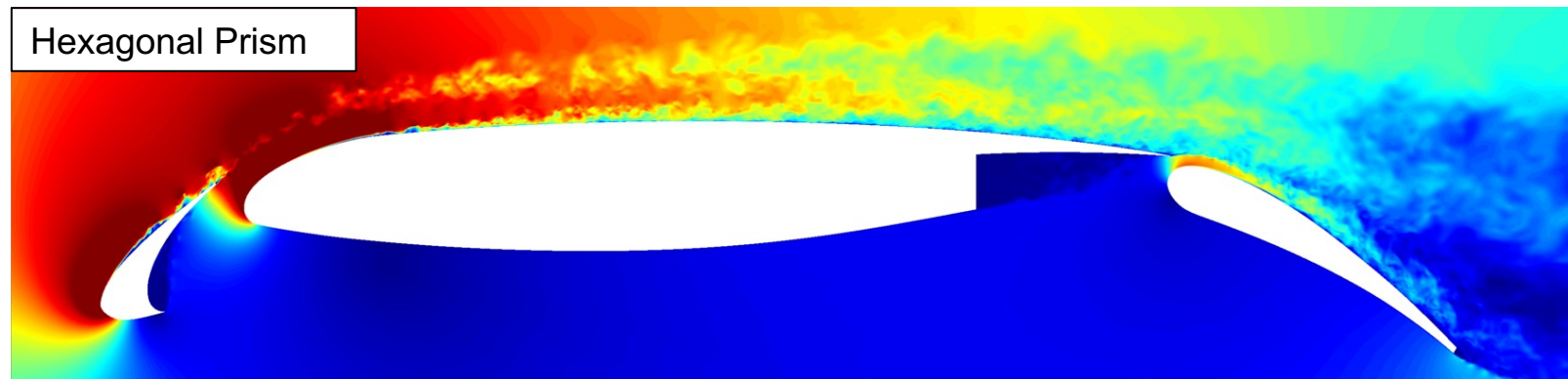
- Slat upper surface stays laminar and attached



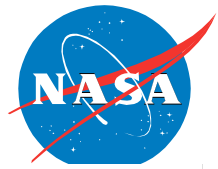
- Onset of transition over the slat
- Earlier transition over the main element



- Finer scale turbulence over the main element boundary layer
- Further breakdown of slat boundary layer
- Better definition near flap upper surface

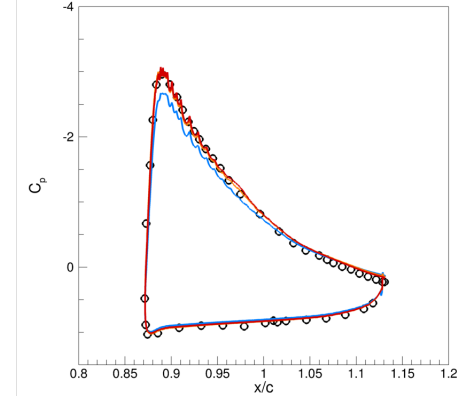
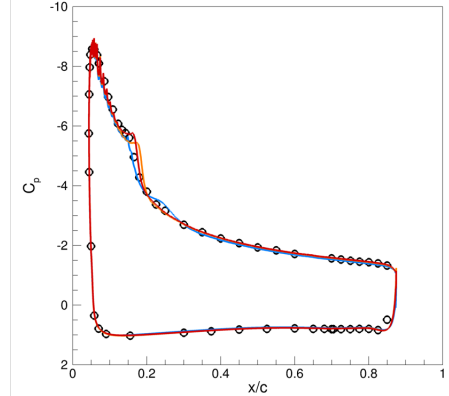
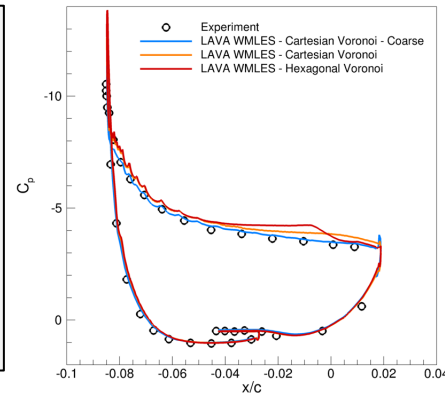


30P30N Results – Pressure Coefficient Distributions

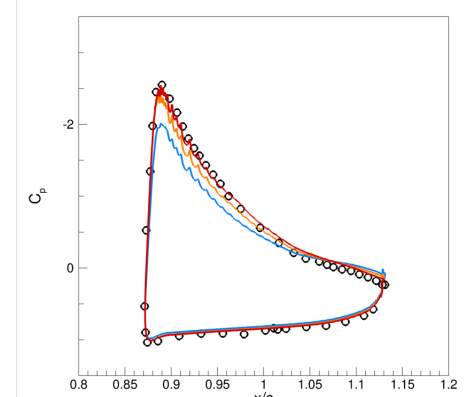
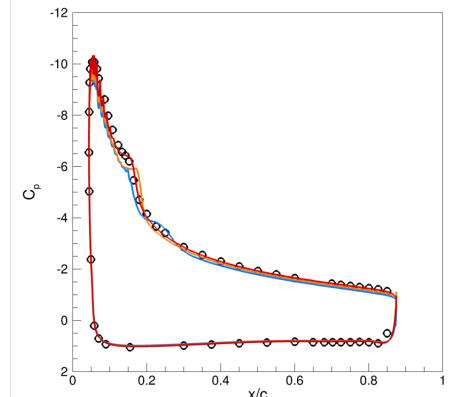
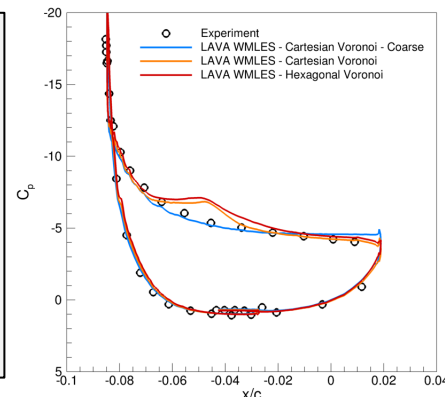


- Time-averaged (~50 CTU's) pressure field, extract at mid-span
- Excellent agreement with the experiment over the main element
 - Hexagonal mesh doing slightly better
- Slat is transitional, while experiment doesn't show a sign of this
 - Coarse mesh doesn't show transition until the highest angle
 - Transition onset location moves upstream with refinement
 - Hexagonal mesh exhibits higher resolution compared to Cartesian mesh of same spacing
- Great agreement over the flap until post-stall
 - Results display higher mesh sensitivity compared to the main element
 - Predictions trend towards the experiment with mesh refinement
 - Hexagonal mesh results better capture the suction peak
 - Slight under-prediction at highest angle

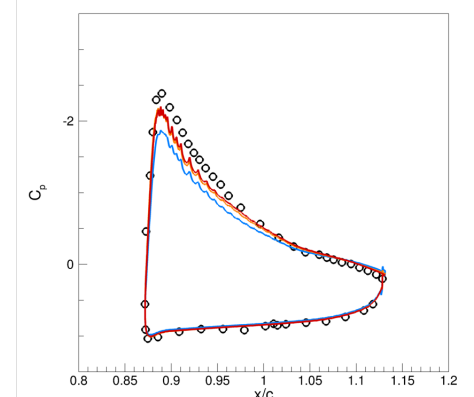
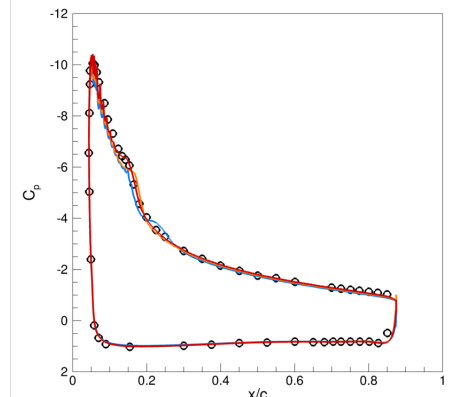
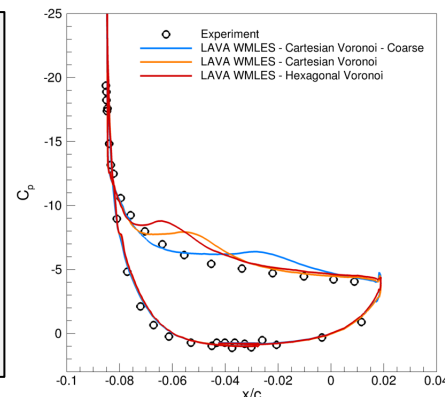
$\alpha = 16.21^\circ$



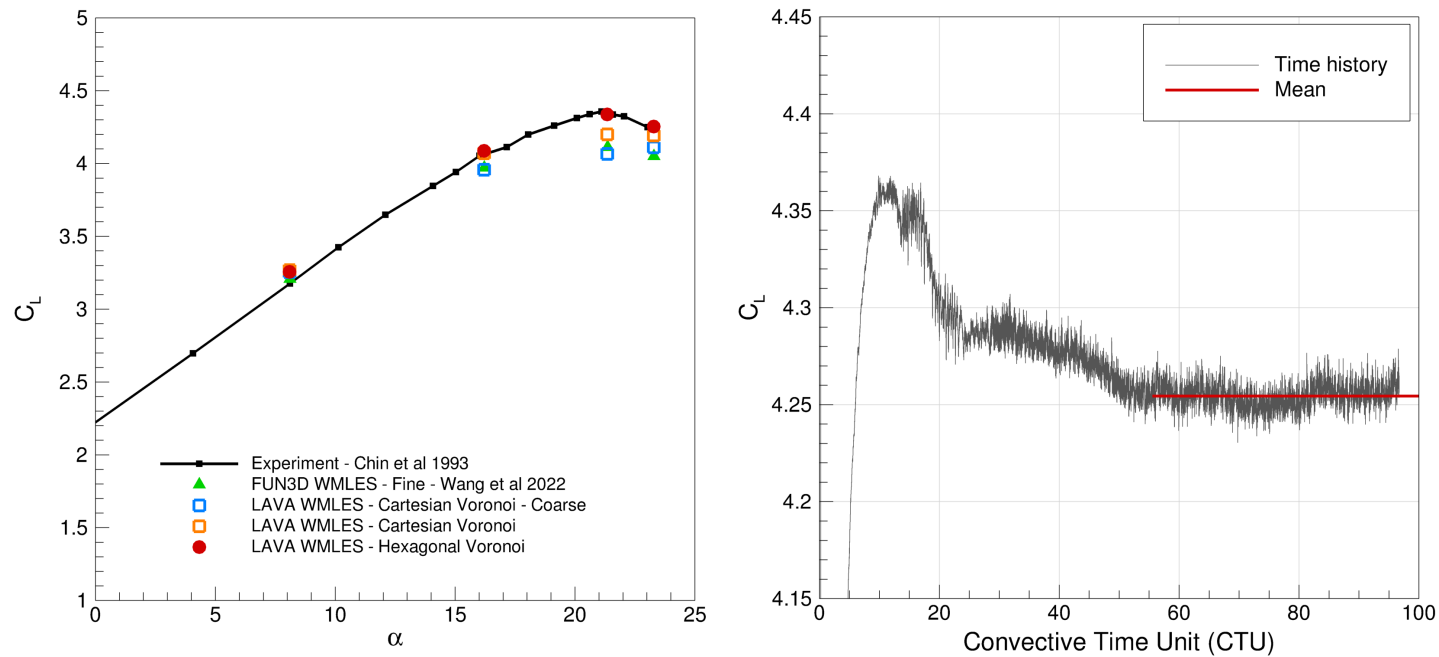
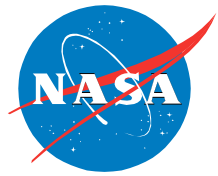
$\alpha = 21.34^\circ$



$\alpha = 23.28^\circ$

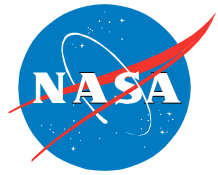


30P30N Results – Lift Curve



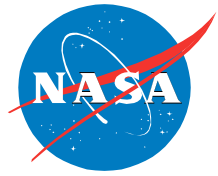
- Integrated aerodynamic forces are time-averaged for about 50 CTU's
- Hexagonal mesh shows excellent agreement with the experimental lift
 - Slight overprediction at the lowest angle for all meshes
- Cartesian meshes underpredicts the lift at high angles
 - Mesh refinement trends toward experimental values

Summary & Conclusions



- A 2nd order accurate cell-centered finite volume unstructured scheme suitable for large eddy simulations has been presented and tested with model problems of increasing complexity.
- Isentropic vortex propagation:
 - The central scheme was able to preserve the integrated kinetic energy for all Voronoi mesh types tested
 - For the same mesh spacing, Cartesian mesh had the highest error, followed by BCC and FCC
 - When there is a coarse/fine interface, SGS was sufficient to stabilize the scheme
 - Coarse/fine interface smoothing made little difference; more smoothing → marginally less error
- Homogeneous isotropic turbulence:
 - SGS provided sufficient robustness without any upwinding
 - Both Cartesian, BCC and FCC meshes produced correct turbulent energy cascade
- 30P30N:
 - Excellent agreement with experiments when using the hexagonal prism Voronoi mesh
 - Cartesian mesh of same spacing was still mesh sensitive, displaying correct trend with refinement
 - Hexagonal mesh has higher effective resolution, although with higher computational cost

Acknowledgements



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- We would like to thank the members of the LAVA Voronoi development team for their invaluable efforts in building the meshing tool that enabled this work. Apart from the co-authors, members of the Voronoi team include:
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 - Abram Rodgers
 - Keshav Sriram
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