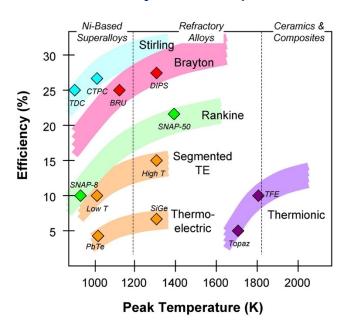
Small Closed Brayton Cycle Engines for Space Applications

MIT Gas Turbine Workshop

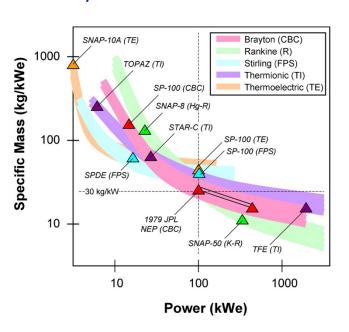
Lee Mason 2 May 2023

System Trends & Discriminators

Efficiency vs Temperature

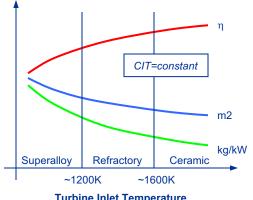


Specific Mass vs Power



Power Technology Options for Nuclear Electric Propulsion, <u>IECEC 2002</u>

Brayton Systems Analysis Trends



Turbine Inlet Temperature



Increasing TIT:

- · Larger temp ratio
- · Greater efficiency
- · Less Qin, smaller heat source
- · Less Qrej, smaller radiator But.
- TRL of advanced materials
- Greater thermal stress
- · Possible life issues

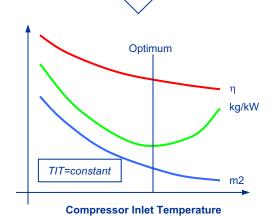
Increasing CIT:

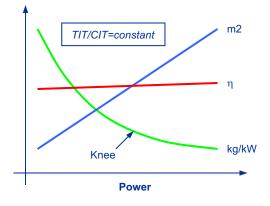
- · Higher heat reject temp
- Smaller radiator (∞T⁴)

But,

- · Smaller temp ratio
- Lower efficiency
- · More Qin, larger heat source

Results in optimum mass







Increasing Power:

- Slight efficiency increase
- · Linear area increase
- · Large economy of scale benefits in Brayton

But.

· TRL issues at high power

Mass curve has steep slope at low power & knee

Space Brayton Development History







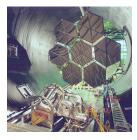




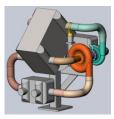












- 10 kW Brayton Rotating Unit (BRU)
- 2 kW Mini-BRU
- 1.3 kW Brayton Isotope Power System (BIPS)
- 100 kW to MW Class Nuclear Concepts

- 25 kW Solar Dynamic (SD)
 Power Module for Space
 Station Freedom
- 20 to 500 kW SP-100 Brayton Designs
- 6 kW Dynamic Isotope Power System (DIPS)

- 0.5 to 2.5 kW DIPS for Science & Exploration
- 2 kW SD Ground Test Demonstration
- 2 kW SD-Mir Flight Experiment
- 2 kW Brayton Testbed

- 200 kW Brayton for Jupiter Icy Moons Orbiter (JIMO)
- 20 kW Dual Capstone Brayton Test Loop
- 12 kW Fission Surface Power (FSP) Brayton

2000

1970

Brayton Rotating Unit

First-ever Closed Brayton Cycle (CBC) power conversion system for space (1968-76)

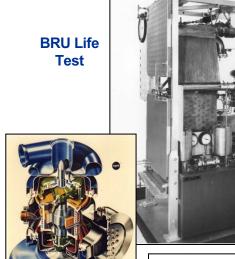
- 4 BRUs Fabricated by AiResearch and Tested at Lewis Research Center
- Included Brayton Heat Exchanger Unit (BHXU) combined Recuperator and Cooler
- 1 Unit (BRU-F) Modified with Foil Bearings

BRU Program Successfully Demonstrated:

- Manufacturing & Assembly
- Jacking Gas Startup
- High Conversion Efficiency (>25%)
- Material Compatibility
- Tilt-Pad Bearings
- Extended Life: 38000 Hrs Operation on One Unit Without Degradation, Approx. 50000 Hrs Total on Four Units

Performance Parameters:

- Alternator Output 2.25 to 15 kWe
- Turbine Inlet Temp 1144 K (1600 F)
- Compressor Inlet Temp 300 K (80 F)
- Compressor Exit Pressure 310 kPa (45 psia)
- 36000 RPM, 1200 Hz, 208 V
- 65 kg BRU, 200 kg BHXU

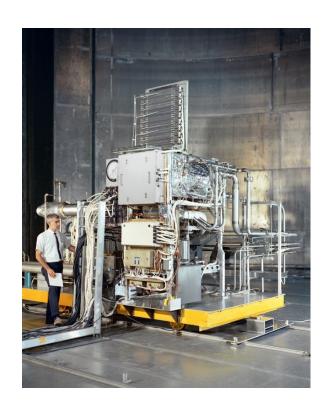


BRAYTON POWER SYSTEM

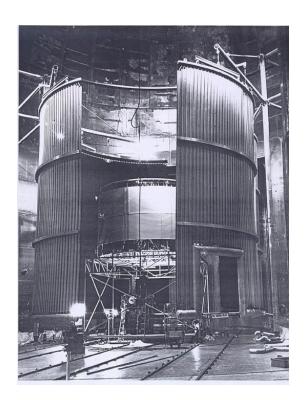




1972 BRU System Test at SPF







Mini-BRU

Mini-BRU and Recuperator developed for use with Modular Isotope Heat Source (1974-78)

- Built by AiResearch, Tested by Lewis
- Major Differences from BRU: Lower Power, Foil Bearings, Internal Stator Cooling
- Interchangeable Superalloy and Refractory Turbine Plenums Fabricated

Led to 1.3 kW Brayton Isotope Power System (BIPS) development (DOE)

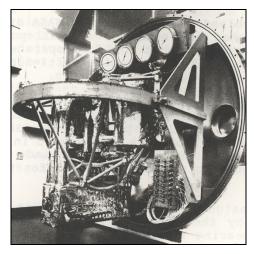
No Flight, but 1000 Hr Workhorse Loop Test

Mini-BRU Successfully Demonstrated:

- High Efficiency (>25%) at Lower Power
- Foil Bearings
- Alternator Motoring Startup
- Leak-Free Recuperator Designs

Performance Parameters:

- Alternator Output 650 to 2100 watts
- Turbine Inlet Temp 1144 K (1600 F)
- Compressor Inlet Temp 300 K (80 F)
- Compressor Exit Pressure 730 kPa (106 psia)
- 52000 RPM, 1733 Hz, 67 V
- 17 kg mini-BRU, 59 kg Recuperator



BIPS Workhorse Loop

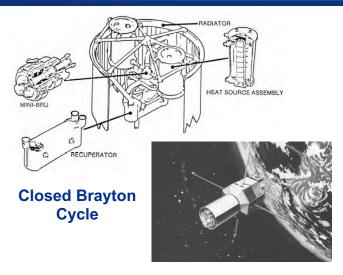


Turboalternator-Compressor

Mini-BRU Recuperator

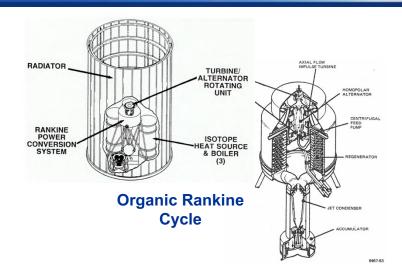


BIPS vs. KIPS (1978)





- AirResearch/Garrett Corp.
- 2 MHW Heat Sources (4.8 kWt input)
- 1144K Turbine Inlet, 263K Comp. Inlet (HeXe working fluid)
- 1.3 kWe net power (27% eff.)
- 210 kg, 12.4 m2 radiator



Kilowatt Isotope Power System

- Sundstrand Energy Systems
- 3 MHW Heat Sources (7.2 kWt input)
- 620K Turbine Inlet, 349K Cond. Inlet, (Dowtherm A working fluid)
- 1.3 kWe net power (18% eff.)
- 215 kg, 10.1 m2 radiator

A Brief History of Rankine

Years	Project	Power	Working Fluid	Status
1960s	ORC	6 kWe	645K Dowtherm	PCU test (3,000 hr)
1960s	K-Rankine	500 kWe	1400 K Potassium	Concept
1960s	SNAP-2	5 kWe	895 K Mercury	PCU test (30,000 hr)
1960s	SNAP-8	35 kWe	950 K Mercury	PCU test (10,000 hr)
1960s	SNAP-50	300 kWe	1365 K Potassium	Concept
1960s	MPRE	140 or 300 kWe	1100 K or 1365K Potassium	Material & loop tests
1970s	KIPS	1.3 kWe	620 K Dowtherm	PCU test (11,000 hr)
1980s	SSF SD	25 kWe	675 K Toluene	Design
1980s	AF DIPS	6 kWe	675 K Toluene	Concept

Solar Dynamic Brayton - Space Station Freedom

25 kW Solar Dynamic Power Module for Space Station Freedom (1986-91)

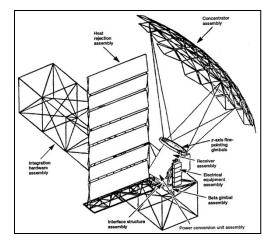
- Part of Hybrid PV/SD Power System
- Reduced Life Cycle Costs Compared to PV/Battery System
- 15 year On-Orbit Life
- Human-Rated System

Phase C/D Design Completed

- Higher Risk Components Built & Tested (e.g., Concentrator, Heat Receiver)
- Power Conversion Unit Considered Low Risk due to BRU Heritage

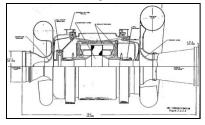
Performance Parameters:

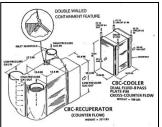
- Alternator Output 36 kWe
- Cycle Efficiency 27%
- Turbine Inlet Temp 1034 K (1400 F)
- Compressor Inlet Temp 338 K (148 F)
- Compressor Exit Pressure 560 kPa (81 psia)
- 32000 RPM, 120V
- 104 kg Turboalternator-Compressor, 162 kg Recuperator, 85 kg Gas Cooler



SD Flight Configuration

Turboalternator-Compressor





Recuperator/ Cooler

Solar Dynamic Ground Test Demonstration

2 kW Solar Dynamic Ground Test Demonstration (1994-98)

- Congressional Ear-Mark Following Cancellation of SD Option for SSF
- Full End-to-End System Test in Solar-Thermal-Vacuum (TRL6)
- Government/Industry Team: NASA Lewis, Allied Signal, Harris, Loral-Vought, Rocketdyne

Extensive Test Program:

- 33 Separate Tests, 372 LEO Orbit Cycles
- 800 Hours of Operational Experience
- No Performance Degradation

Led to US/Russian 2 kW Mir SD Flight Demo (1996-98)

- Shuttle Delivery Mission Redirected for Logistics Resupply
- Multiple Brayton Unit Configurations
 - Mini-BRU with 120V Rice Alternator
 - SD Mir Development Unit with 28V Permanent Magnet (PM) Alternator
 - SD Mir Unit with Rewound 120V PM Alternator

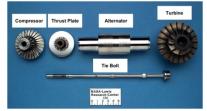


View from Solar Sim. Window Port

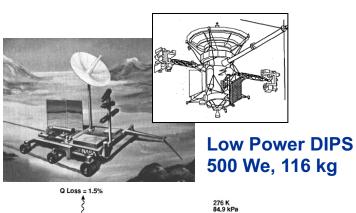


Heat Receiver & Power Conversion Unit

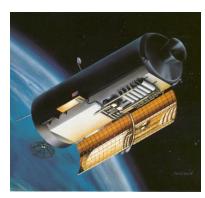
Rotor Components

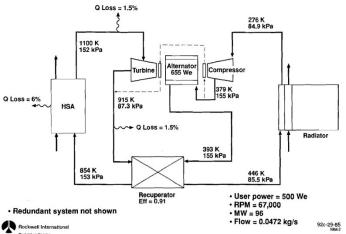


Brayton DIPS (early 1990s)



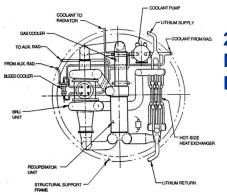
Air Force BSTS DIPS 6 kWe, 675 kg







1990s Brayton Concepts & Studies

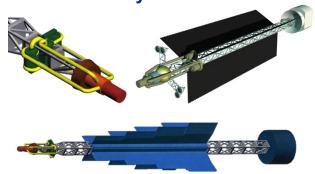


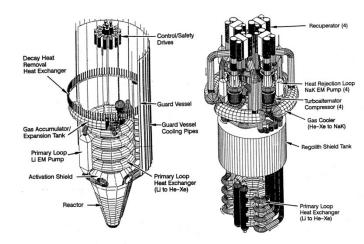
20 kW Brayton for Near-Term SP-100 Flight Demo









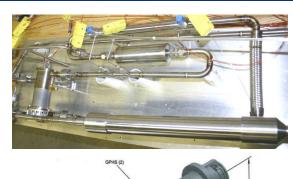


550 kW SP-100 Brayton for Lunar Surface

Creare Turbo-Brayton for RPS (2001)

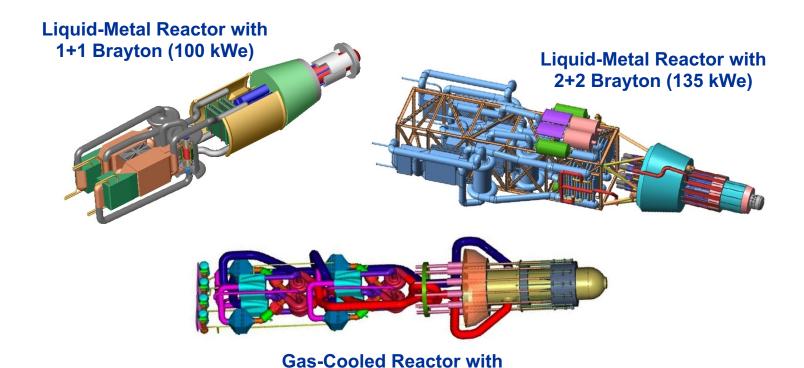
Started as SBIR in 2001

- Phase I preliminary design and rotor testing to 3500 rev/s
- Phase II breadboard converter test unit with commercial recuperator (not successful – thrust bearing issues)
- Transitioned to NASA Radioisotope Power Conversion Technology NRA Contract in 2004 (Goal ~ TRL5)
 - Partners included Boeing/Rocketdyne, Ball Aerospace, Jackson & Tull
 - Year 1 converter design and thermo-mechanical analysis
 - Year 2 component fabrication and test
 - Year 3 system integration and thermal-vac test
 - Contract cancelled after first year due to NRA budget constraints
- 100 W Flight System with redundant Brayton units (2 GPHS) 26 kg
 - 200 W Flight System (4 GPHS) 33 kg





Jupiter Icy Moons Orbiter Concepts (2002-2005)

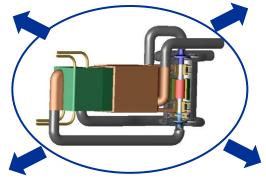


2+2 Brayton (200 kWe)

JIMO-era Brayton Technology Advancements



- 2 kW Brayton-Ion Demo NASA/TM-2004-212960
- 2 kW Mechanical-**Dynamic Vibration Test** NASA/TM-2005-213880





- Superalloy Material Creep Testing NASA/TM-2006-214110
- Dissimilar Metallic Joining STAIF 2007
- HeXe/Superalloy Compatibility <u>IECEC 2004</u>



- 50 kW Alternator Test Unit
- Alternator-Thruster **Integration Lab**
- NASA/TM-2005-213895



- High Temperature Journal **Bearing Tests**
- High Pressure Gas Foil **Bearing Tests**
- NASA/TM-2007-214470

Fission Surface Power Studies (2006)

Liquid Metal Reactor & PbTe/TAGS Thermoelectrics

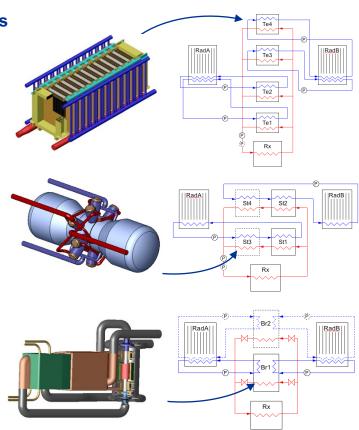
- NaK primary, 900K exit, 100K ∆T, 15% ALIP
- 850K hot-shoe, 500K cold-shoe
- Conductively-coupled TE modules in compact HXs
- 4 converters, 4 required for full power
- NaK secondary, 100K ΔT, 20% ALIP
- 200 Vdc PMAD interface

Liquid Metal Reactor & Free-Piston Stirling

- NaK primary, 900K exit, 50K ∆T, 15% ALIP
- 850K heater head, 450K cooler
- Dual-opposed piston converters in serial pairs
- 4 converters, 2 required for full power
- H2O secondary, 25K ΔT, 20% mech. pump
- 300 Vac, 1Ø, 100 Hz PMAD interface

Gas Cooled Reactor & Direct Brayton

- HeXe primary, 900K exit, ~200K ΔT
- 900K turbine inlet, 370K compressor inlet
- Recuperated-turboalternator with gas cooler
- 2 converters, 1 required for full power
- H2O secondary, ~100K ΔT, 20% mech. pump
- 440 Vac, 3Ø, 2000 Hz PMAD interface

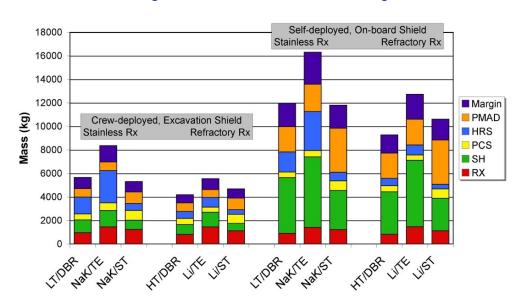


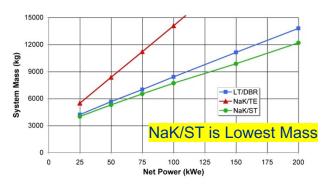
Fission Surface Power Studies (2006)

50 kWe Lunar Surface Reactor Power Systems

- 900K Direct HeXe Brayton
- 900K NaK Thermoelectric
- 900K NaK Stirling

- 1150K Direct HeXe Brayton
- 1300K Li Thermoelectric
- 1100K Li Stirling





Low Temp Reactors with Excavation Shielding



High Temp Reactors with Excavation Shielding

A Comparison of Fission Power System Options for Lunar and Mars Surface Applications NASA/TM-2006-214120

Dual Capstone Brayton Test Loop (2008)

Designed and Built by Barber Nichols

- Uses two commercial Capstone micro-turbine generators modified for closed-loop operation
- Common nitrogen gas loop; no isolation valves
- Shared (180 kW) electrical resistance heater; water cooling

First-of-a-Kind Test System

- Based on Naval Reactor JIMO concept with direct-gas reactor and redundant Brayton power conversion units
- Permits evaluation of operational interactions and transients

GRC Testing Completed May 2008

- Operated up to 22 kW total output power, 950K turbine inlet, 90000 rpm
- Equal & unequal shaft speeds
- Single and dual unit operation
- Staggered & simultaneous startup
- Analytical model validation





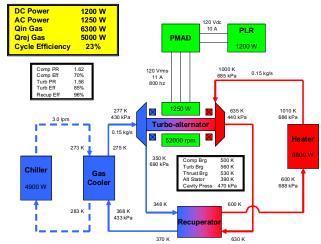
Experimental and Analytical Performance of a Dual Brayton Power Conversion System NASA/TM-2009-215511

Direct Drive Gas – Brayton Test (2009)

- Glenn supplied 2 kW Brayton Power Conversion Unit
- Marshall supplied Direct Drive Gas (DDG) Reactor Simulator
- Testing at GRC Vacuum Facility #6
- Collaboration with Texas A&M and DOE/INL to validate reactor transient analytical models
 - Heater output power control tests
 - Heater exit temperature control tests
 - Simulated reactivity control tests

Test Results From a Direct Drive Gas Reactor Simulator Coupled to a Brayton Power Conversion Unit NASA/TM-2010-215843





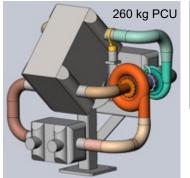
12 kWe Brayton Power Conversion Unit (2010)

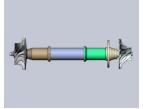
Barber Nichols - Closed Brayton Cycle Power Conversion Unit for Fission Surface Power (NASA Contract NNC08CA64C)

- 12 kWe generator output at 400 Vac
- NaK heating at 850 K +/-25 K
- H2O cooling at 375 K +/-25 K
- Parasitic load control with regulated 120 Vdc power bus
- Thermal-vac test environment of 10-6 torr and 200 K

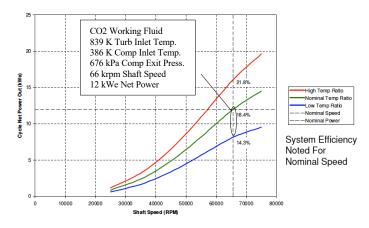
Prioritized Development Goals:

- Close relevance to future flight designs, including the potential for 8 yr service life
- Credible development path and maturation approach to achieve TRL6 in less than 3 yrs
- Low development cost and risk
- Extensible to Mars (materials and design strategies)
- High thermal-to-electric efficiency
- Minimum complexity
- Low mass and volume





30 kg Rotating Unit 30 kg NaK Plate-Fin HX 110 kg CO2 Recuperator 35 kg H2O Gas Cooler



Closed Brayton Cycle Power Conversion Unit for Fission Surface Power Phase I Final Report NASA/CR-2010-215673

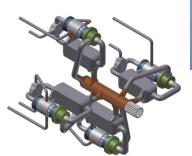
Creare Turbo-Brayton for Fission (2011-13)

2011 SBIR

- 1 kWe Brayton Design for Small Fission Systems (Kilopower)
- Compressor (Ti6Al4V) & Turbine (Rene 41) fabrication trials
- 1050 K Turbine Inlet with Mar-M247
- Phase II not selected

2013 SBIR

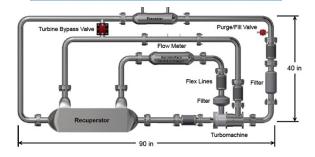
- 12 kWe Brayton Design for Fission Surface Power (TDU)
- Scale-up from 1 kWe
- 875 K Turbine Inlet, 375 K Compressor Inlet
- Phase II selected to build 1 kWe breadboard test system
- Design and component fabrication completed; testing to begin soon
- Oct 2016 Phase II contract conclusion with possible Phase IIE



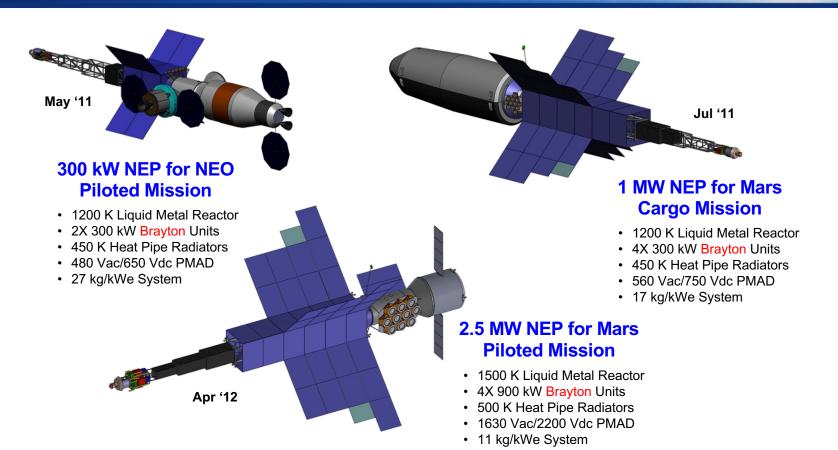








High-Power NEP Vehicle Studies (2011-12)



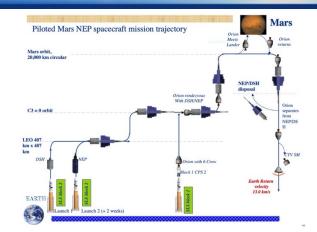
Mars Design Reference Architecture 5.0 (2014)

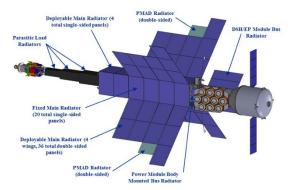
Piloted NEP Propulsion Option

- 2.5 MW reactor power system with Brayton conversion
- Large deployable radiator with stowed package sized for SLS fairing
- Ten 280 kW Xenon gridded annular ion thrusters
- 1630 Vac to 2200 Vdc Direct Drive (5000s Isp)

Conjunction-class Mission

- Two SLS launches (2037)
- Un-crewed spiral from 407 km LEO
- Rendezvous with 6-person Deep Space Hab and Orion at earth escape
- Mars capture at 20,000 km circular
- 980-day total mission
- 400-day Mars surface stay





NASA/SP-2009-566-ADD2 (Addendum #2, March 2014) https://www.nasa.gov/sites/default/files/files/NASA-SP-2009-566-ADD2.pdf

Mars Transportation Assessment Study (2020-21)

Nuclear Power Subsystem

- Reference 1.9 MWe, 25t (13 kg/kWe) NEP power system includes:
 - 1200 K Lithium-cooled HA-LEU TRISO reactor with YH moderator
 - Four 500 kWe Supercritical gas Brayton converters
 - One 2500 m² deployable radiator module designed to fit within SLS launch fairing
 - 960 Vac, 2.5 kHz PMAD architecture delivers 650 Vdc to Hall thrusters and 120 Vdc to spacecraft

Reactor

Alternative fast-spectrum HEU reactor based on SP-100 technology increases TRL and reduces system mass to 21.5t (11 kg/kWe)

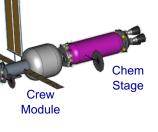
EP Subsystem

- High-power Hall Thrusters
 - Twenty 100 kW thrusters (18+2 config), 600 V/167A operating point, 2.5 kg/kW sp mass
 - 2600 seconds lsp, ~60% string efficiency
 - Advanced magnetic shielding supports 13t Xe throughput and 22,000 hr thruster lifetime
- High-efficiency Direct Drive Units (DDUs)
 - Primary plasma discharge direct drive from Brayton units
 - Auxiliary supplies for magnets, cathode heater, keeper, filtering and communications

Commercial-derived Xenon Flow Controller

With supercritical Xe storage in COPV tanks

100 kW
Effect Tr





Nuclear Power Concepts and Development Strategies for High-Power Electric Propulsion Missions to Mars, NASA/TM-20210016968

Li-cooled Reactor & Bravton Assembly

Space Brayton Technology Challenges

Biggest challenge is to finally get a Brayton converter into space!

Other key challenges include:

- Limited supplier base for niche design requirements
- Life and reliability demonstration (with modern test unit)
- Thermal interfaces at the heat source and heat sink
- Ground test complications due to thermal requirements
- Transient, off-nominal operations
- Achieving competitive mass (with Stirling) at low power level
- Space-rated electronics to process the electric power

Summary

- Long history for Brayton space power systems with significant hardware development and testing
 - Glory days were 1960s and 1970s
 - Technologies are well-suited for power levels from kilowatts to Multi-megawatts
- Brayton technology experienced revivals for Space Station Freedom (late 1980s) and Prometheus (early 2000s)
 - 25 kW SD system pursued, and 2 kW ground test demo completed
 - 200 kW NEP system pursued, and variety of ground demos from 2 to 50 kW completed
- Current NASA interests in Brayton are focused on low-power RPS (<1 kW), mid-power FSP (40 kW), and high-power NEP (>1 MW)
 - RPS Program built and tested a 300 W Brayton prototype with Creare
 - Two contractor teams are pursuing Brayton options for FSP
 - Brayton is the preferred technology for large-scale NEP systems
- Continued NASA investments in turbine-based energy conversion technologies provides increased flexibility for future space systems

References

Prometheus Bibliography

- 1. Power Technologies for Nuclear Electric Propulsion <u>IECEC 2002</u>
- Status of Brayton Cycle Power Conversion Development at NASA GRC NASA/TM-2002-211304
- A Power Conversion Concept for the Jupiter Icy Moons Orbiter <u>NASA/TM-2003-212596</u>
- Experimental Results From a 2kW Brayton Power Conversion Unit <u>NASA/TM-2003-211999</u>
- Performance Expectations of Closed-Brayton-Cycle Heat Exchangers in 100-kWe Nuclear Space Power Systems NASA/TM-2003-212597
- System Mass Variation and Entropy Generation in 100–kWe Closed-Brayton-Cycle Space Power Systems NASA/TM-2004-212741
- Experimental Investigations From the Operation of a 2 kW Brayton Power Conversion Unit and a Xenon Ion Thruster NASA/TM-2004-212960
- Design and Off-Design Performance of 100 kWe-Class Brayton Power Conversion Systems NASA/TM-2005-213626
- Verification of a 2 kWe Closed-Brayton-Cycle Power Conversion System Mechanical Dynamics Model NASA/TM-2005-213880
- Performance and Mass Modeling Subtleties in Closed-Brayton-Cycle Space Power Systems NASA/TM-2005-213985
- Performance and Operational Characteristics for a Dual Brayton Space Power System With Common Gas Inventory <u>NASA/TM-2006-214393</u>
- Carbon-Carbon Recuperators in Closed-Brayton-Cycle Space Power Systems NASA/TM-2006-213302
- The 2kW Mini-BRU Electrical Controls Concept and Transient Performance NASA/TM-2006-214043
- Initial Test Results of a Dual Closed-Brayton-Cycle Power Conversion System NASA/TM-2007-214981
- Two-Dimensional Viscoelastic Stress Analysis of a Prototypical JIMO Turbine Wheel NASA/TM-2005-213650
- Tensile and Creep Property Characterization of Potential Brayton Cycle Impeller and Duct Materials NASA/TM-2006-214110
- Compatibility of Niobium Alloys and Superalloys in a Flowing He-Xe Power Conversion System IECEC 2004
- Evaluation of Silicon Nitride for Brayton Turbine Wheel Application <u>NASA/TM-2008-214803</u>

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