



Computational Analysis on the Effects of High-Lift Propellers and Wingtip Cruise Propellers on X-57

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Outline

- Introduction
- Computational Tools
- Results
- Conclusion



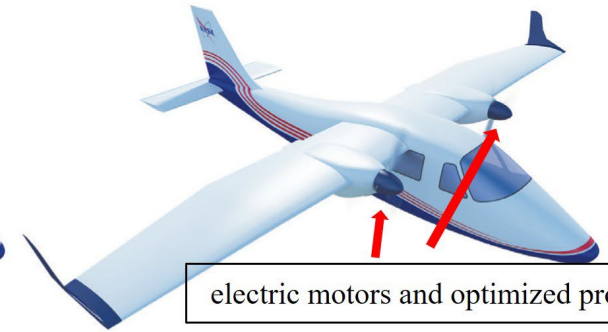


Introduction – X-57

- Demonstrate technologies intended to improve aerodynamic efficiency and reduce carbon footprint
- Separated into multiple phases or modifications, denoted as “Mod”
 - Electrical motors for propulsion
 - Optimized high aspect ratio wing and high lift nacelle
 - Wingtip mounted cruise propellers for reducing induced drag
 - High-lift system to augment flow to generate more lift

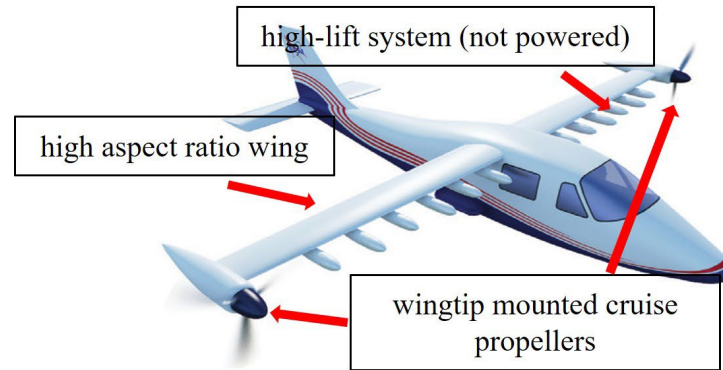


Mod-I: original Tecnam P2006T



electric motors and optimized propellers

Mod-II: electric motors and optimized propellers

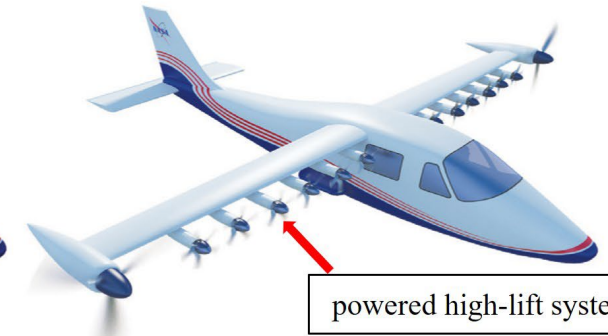


high-lift system (not powered)

high aspect ratio wing

wingtip mounted cruise propellers

Mod-III: high aspect ratio wing, high-lift system (not powered), wingtip mounted cruise propellers



powered high-lift system

Mod-IV: high aspect ratio wing, powered high-lift system, wingtip mounted cruise propellers





Introduction – Mod-III

- High-aspect ratio wing
 - $C_{mac} = 2.13$ ft (48.4% of original wing)
 - $AR = 15$ (170.4% of original wing)
 - Wing area = 66.7 ft² (58% of original wing)
- Wingtip mounted cruise propellers
 - Powered by electric motor
 - 3 blades per propellers
 - 5 ft radius
 - Rotate outboard direction



<https://www.nasa.gov/specials/X57/modification.html#3>





Introduction – Mod-IV

- High-aspect ratio wing
 - $C_{mac} = 2.13$ ft (48.4% of original wing)
 - $AR = 15$ (170.4% of original wing)
 - Wing area = 66.7 ft² (58% of original wing)
- Wingtip mounted cruise propellers
 - Powered by electric motor
 - 3 blades per propellers
 - 5 ft radius
 - Rotate outboard direction
- High-Lift System
 - 12 propellers (6 each side)
 - 5 blades per propeller
 - 1.89 ft radius
 - Rotate outboard direction
 - Powered on during terminal phase of flight



<https://www.nasa.gov/specials/X57/modification.html#4>

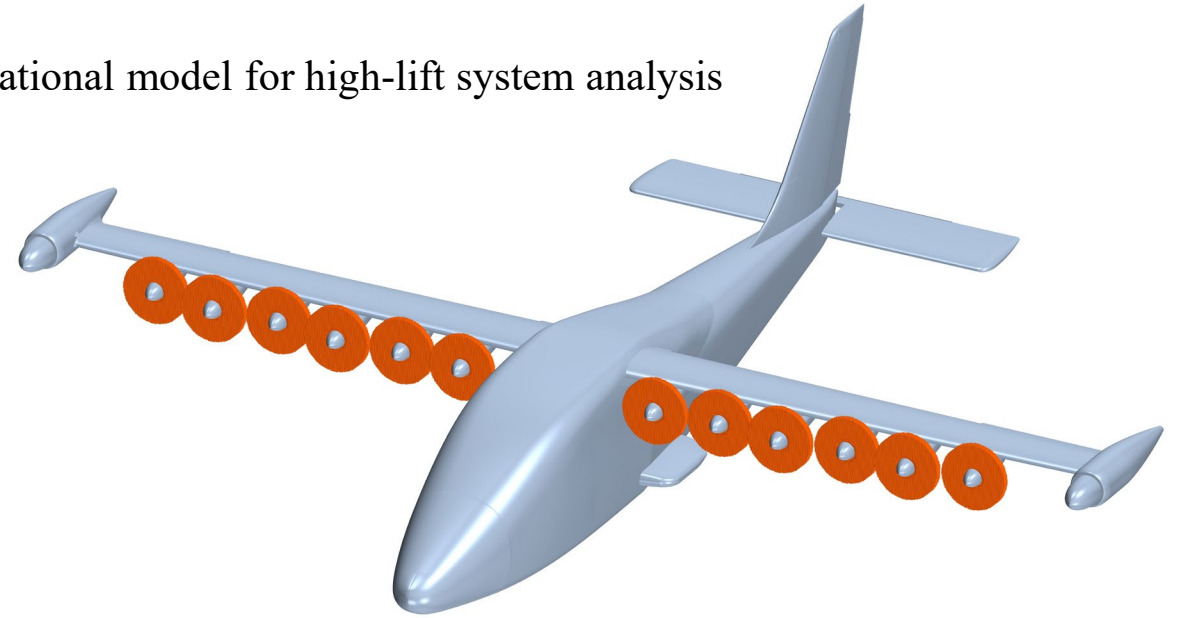




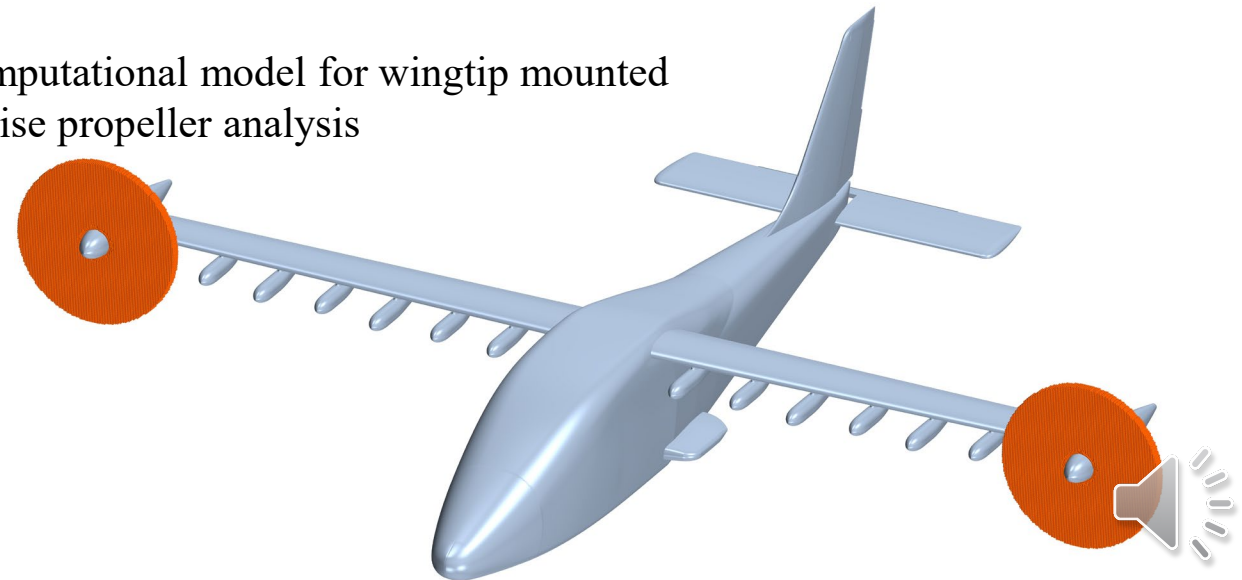
Introduction

- Study focused on effects of high-lift propellers and wingtip mounted cruise propellers
- High-lift propellers and wingtip mounted cruise propellers modeled separately
- Understanding of the aerodynamics of the vehicle
- Performance benefit

computational model for high-lift system analysis



computational model for wingtip mounted cruise propeller analysis





Computational Tools

<p>STAR-CCM+ (v13.04.10)</p> <ul style="list-style-type: none">• Grid<ul style="list-style-type: none">– Unstructured polyhedral mesh with prism layer• Solver<ul style="list-style-type: none">– Steady state RANS– 2nd order Roe flux-differencing spatial scheme with implicit Gauss-Siedel relaxation scheme– SA-RC-QCR• Propeller modeling<ul style="list-style-type: none">– Actuator disk with X-57 specific performance curve based on blade-element-momentum-theory for high-lift propellers and Goldstein distribution for cruise propellers	<p>Launch Ascent Vehicle Analysis Framework (LAVA)</p> <ul style="list-style-type: none">• Grid<ul style="list-style-type: none">– Structured, curvilinear, overset grids• Solver<ul style="list-style-type: none">– Steady state RANS structured curvilinear solver– 2nd order Roe flux discretization with Koren limiter and Alternating Line-Jacobi method– SA-RC-QCR• Propeller modeling<ul style="list-style-type: none">– Actuator disk with X-57 specific performance curve based on blade-element-momentum-theory for high-lift propellers and Goldstein distribution for cruise propellers
<p>USM3D</p> <ul style="list-style-type: none">• Grid<ul style="list-style-type: none">– Unstructured tetrahedral mesh• Solver<ul style="list-style-type: none">– Time-accurate RANS solver with global time-marching scheme– 2nd order Roe flux-differencing spatial scheme with implicit Gauss-Seidel scheme– SA-QCR• Propeller modeling<ul style="list-style-type: none">– Actuator disk with triangular distribution for high-lift propellers and cruise propellers	<p>Kestrel</p> <ul style="list-style-type: none">• Grid<ul style="list-style-type: none">– Mixed element, unstructured tetrahedral core mesh with prism layer• Solver<ul style="list-style-type: none">– Time-accurate RANS solver with global time-marching scheme– HLLE++ with implicit Gauss-Seidel method– SA-RC• Propeller modeling<ul style="list-style-type: none">– Actuator disk with triangular distribution for high-lift propellers and cruise propellers





Results

- High-Lift Propellers
- Wingtip Mounted Cruise Propeller





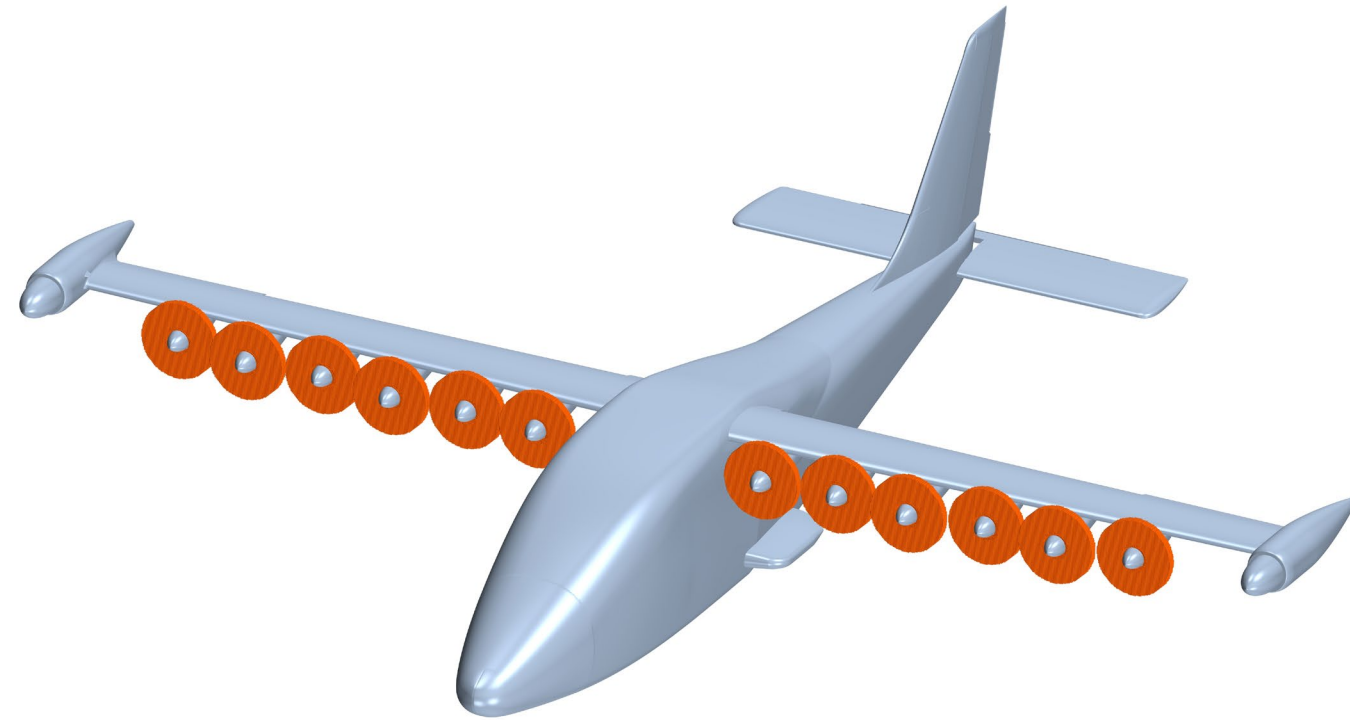
High-Lift Propeller Results





Results – High-Lift Propellers

- Atmospheric Condition
 - Altitude 2500 ft, Mach 0.092, 58 KCAS
 - Density 2.2078E-3 kg/m³
 - Static pressure 92499.6 Pa
 - Static temperature 283.2K
 - Reynolds number 6.1E5
- Aircraft configuration
 - All control surfaces at 0° deflection
 - Flap 30° deflection
 - High-lift system powered on
 - 49.1 lbf thrust (maximum thrust)
 - Propellers rotate outboard direction
 - Cruise propellers not modeled

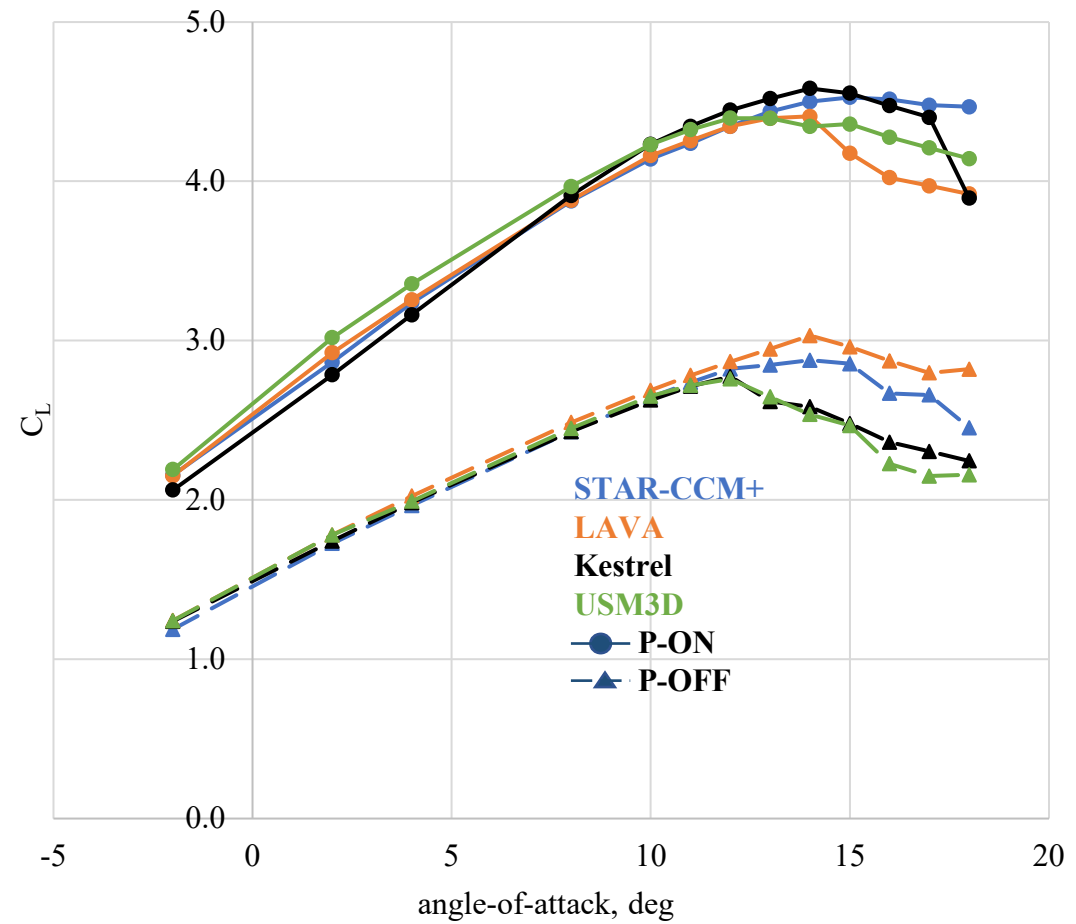




Results – High-Lift Propellers

Lift Coefficient

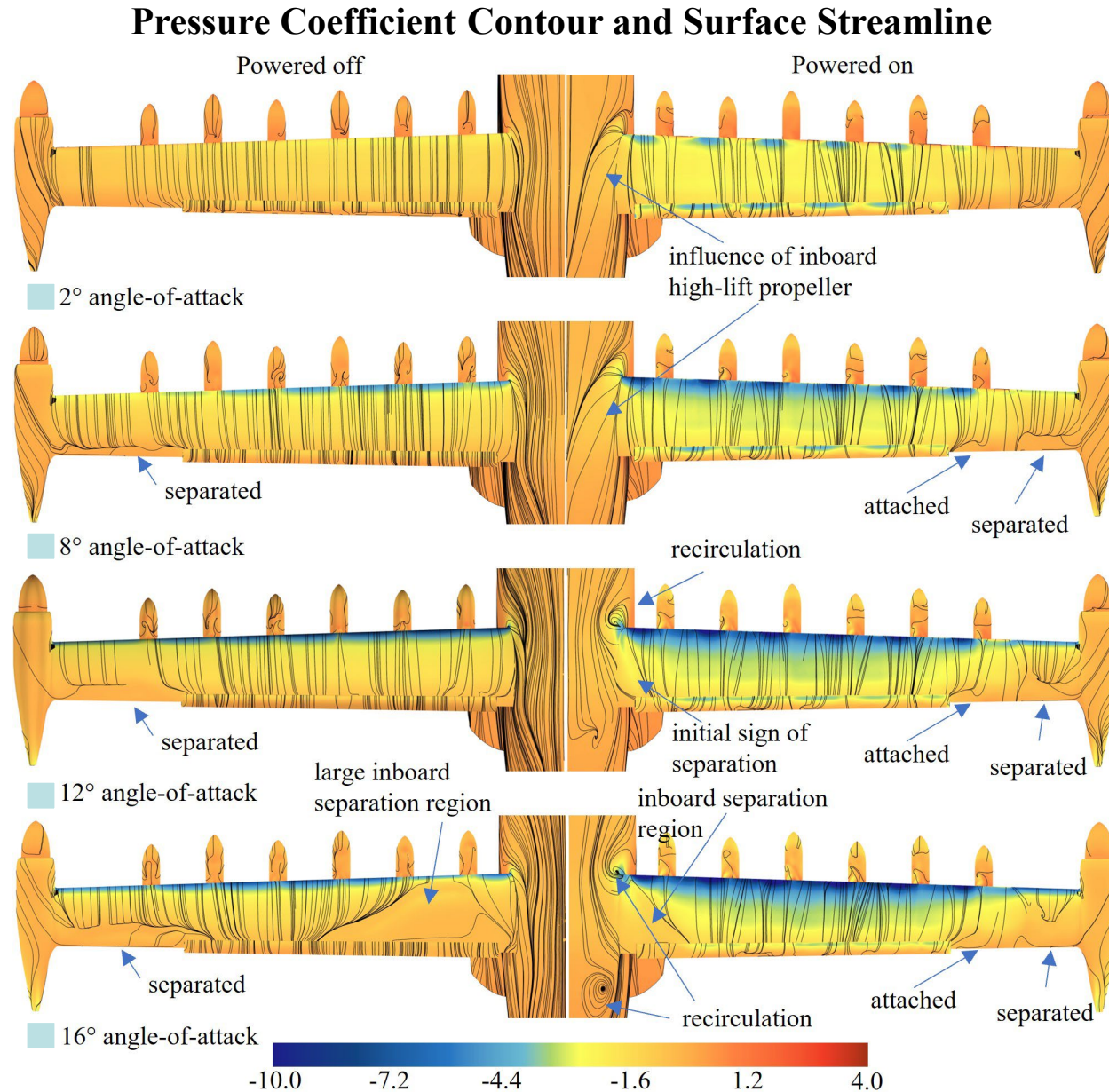
- Power-off results
 - Shows good comparison in the linear region
 - Difference in $C_{L,max}$ and angle-of-attack for it
 - Sharper drop in C_L for Kestrel and USM3D compared to STAR-CCM+ and LAVA
- Power-on results
 - Increased lift and lift-curve-slope per angle-of-attack
 - As much as 65.4% increase $C_{L,max}$
 - Reduced loss of lift post $C_{L,max}$
 - Variation in C_L in linear region due to difference in performance curve in actuator disk





Results – High-Lift Propellers

Comparison Between Powered On and Powered Off Configuration

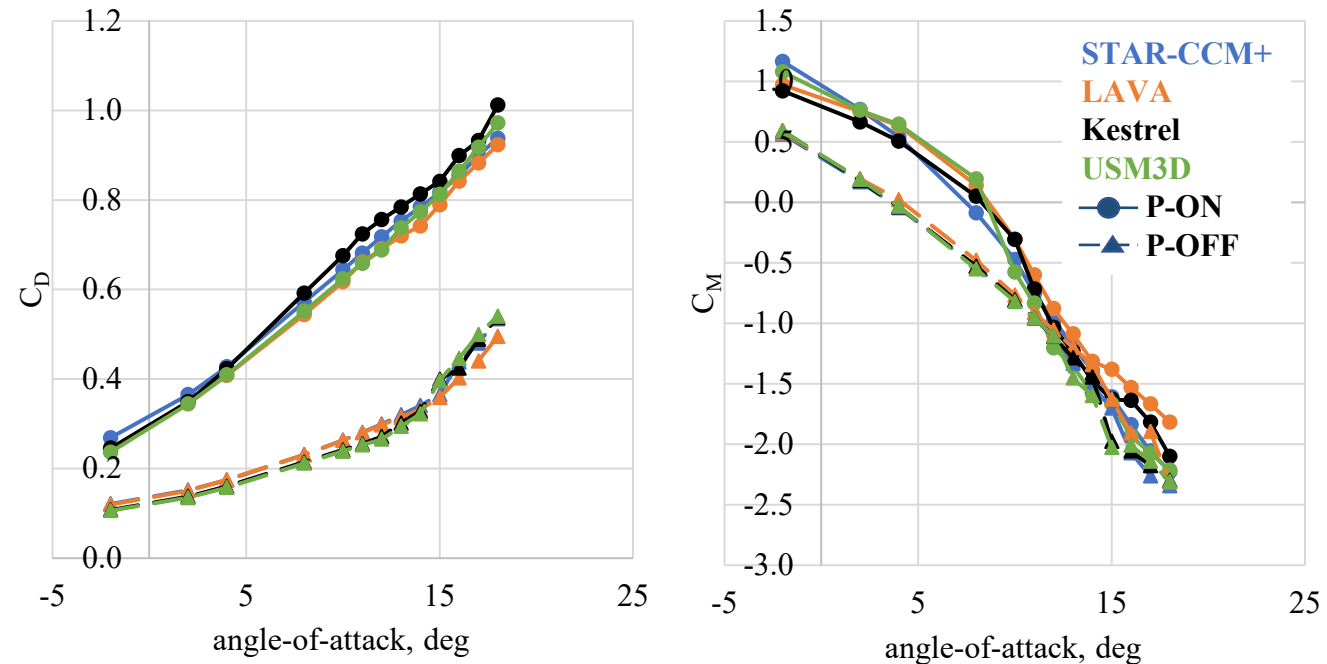




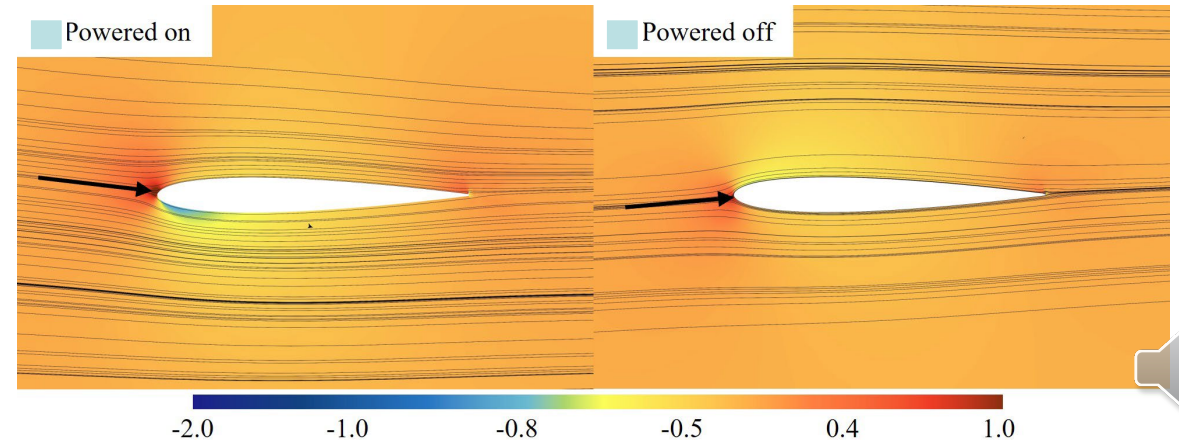
Results – High-Lift Propellers

Drag and Pitching Moment Coefficients

- Powered on configuration has more nose-up pitching moment
 - Less lift generated by stabilator
 - Higher drag on wing, since it sits higher than the MRC, will create nose-up pitching moment
- Effect of high-lift propellers diminishes with increase in angle-of-attack
 - Less influence on stabilator



Stabilator Section: Pressure Coefficient Contour and Streamline
8° angle-of-attack





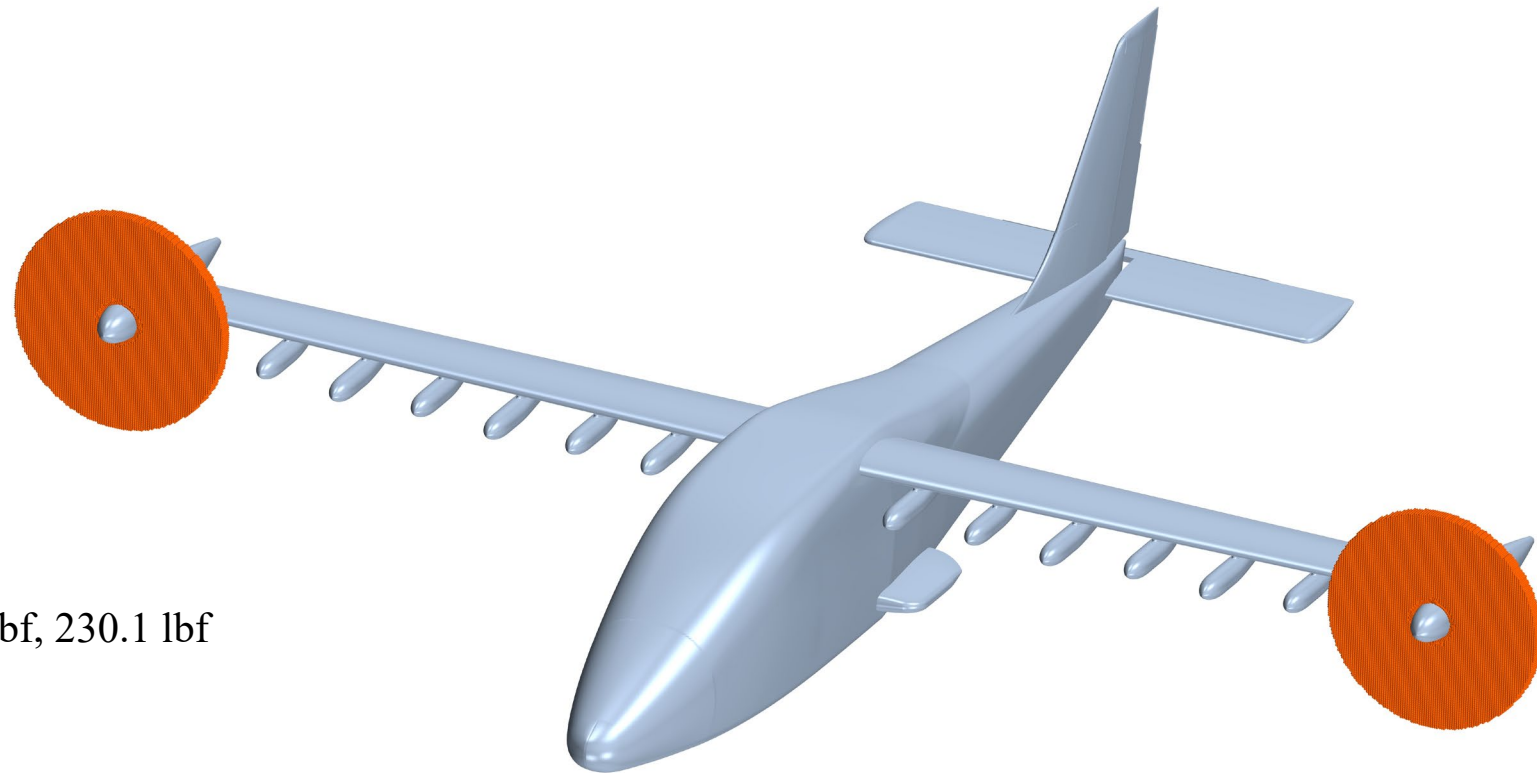
Wingtip Mounted Cruise Propeller Results





Results – Cruise Propellers

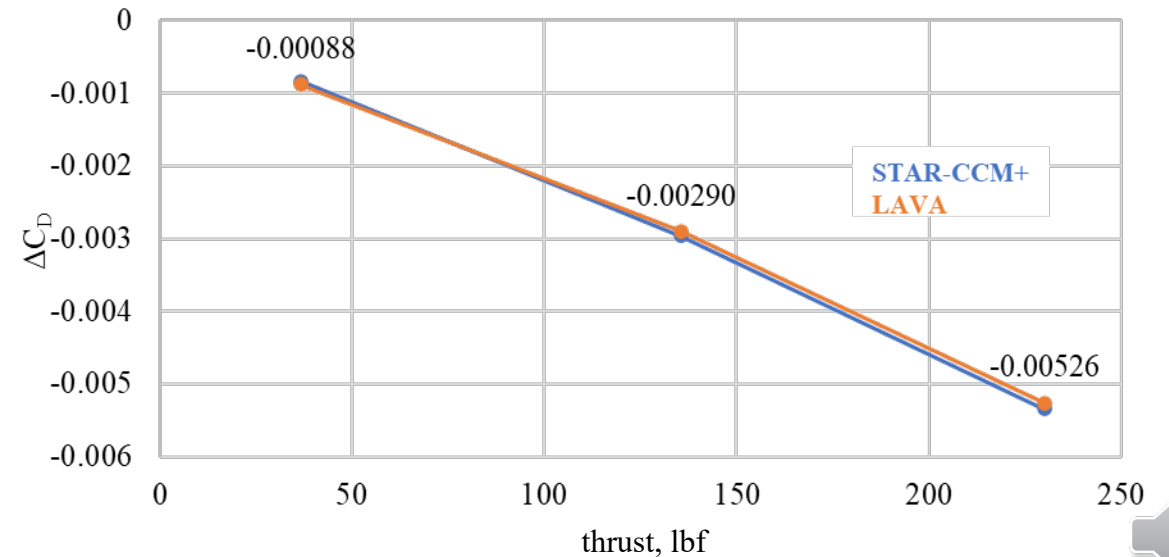
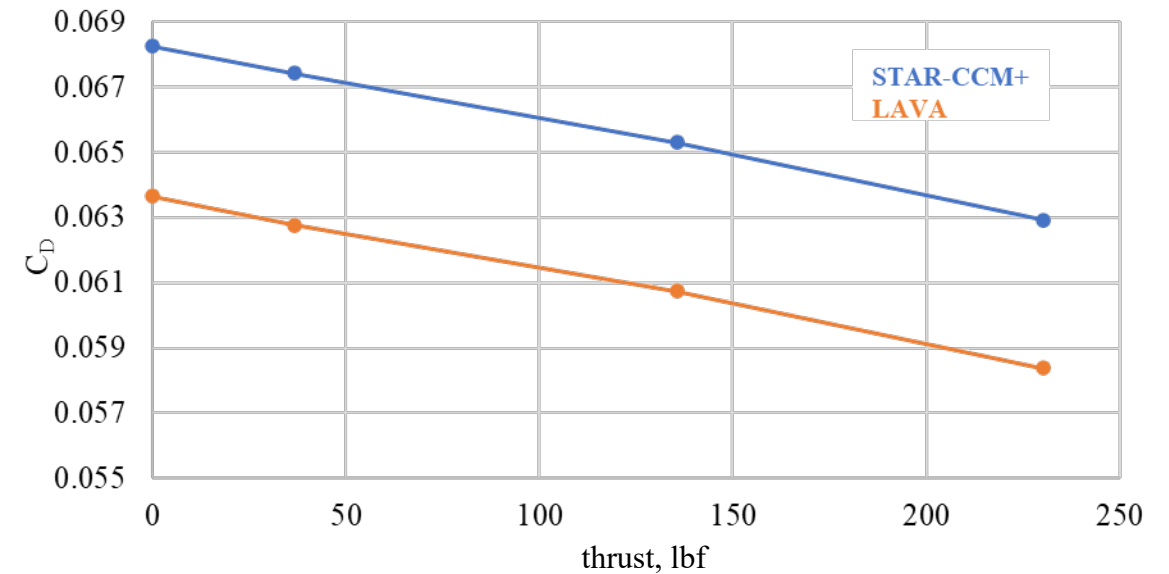
- Atmospheric Condition
 - Altitude 8000 ft, Mach 0.233, 133 KCAS
 - Density 1.8628E-3 kg/m³
 - Static pressure 75262.3 Pa
 - Static temperature 272.3K
 - Reynolds number 1.32E6
 - 2° angle-of-attack
- Aircraft configuration
 - All control surfaces at 0° deflection
 - Flap 0° deflection
 - Cruise propellers Thrust: 36.6 lbf, 135.6 lbf, 230.1 lbf
 - High-lift propellers not modeled
- Results focused on drag





Results – Cruise Propellers Aircraft Drag Coefficient

- STAR-CCM+ results show higher C_D compared to LAVA, but 2 solvers compare ΔC_D very well
 - ΔC_D relative error between STAR-CCM+ and LAVA within 1.5%
- Decreasing drag with increase in cruise propeller thrust
 - At cruise power of 230.1 lbf of thrust, 52.6 drag count reduction

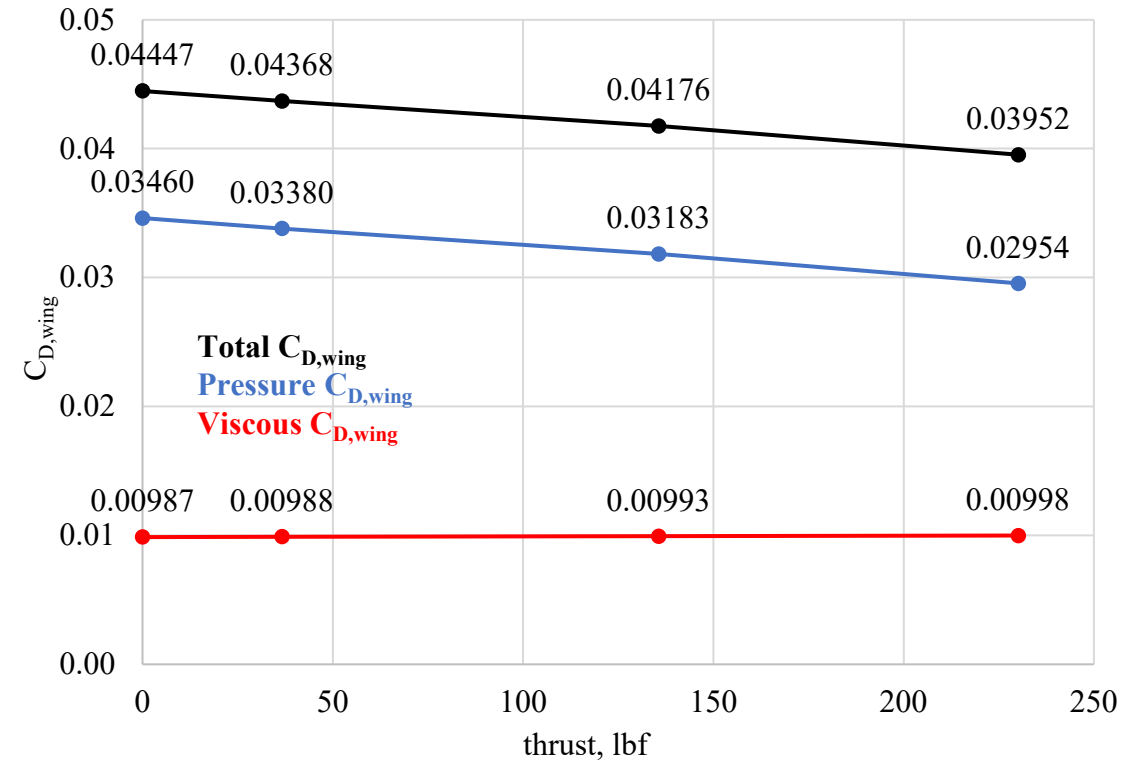




Results – Cruise Propellers

Wing Drag Coefficient

- Decreasing wing drag with increase in cruise propeller thrust
 - At cruise thrust of 230.1 lbf, 49.5 drag count reduction
- Much of drag reduction is due to decrease in pressure drag
 - 50.6 drag count decrease
- Viscous drag remains almost constant with increase in wingtip propeller thrust
 - 1.1 drag count increase





Conclusion

- Cruise propellers and high-lift system modeled and analyzed individually
 - Powered on results compared with powered off results
- High-lift Propellers
 - Increases lift and lift-curve-slope for power on configuration compared to power off
 - Increases $C_{L,max}$ as much as 65.4%
 - Gentler flow separation after $C_{L,max}$
- Cruise Propellers
 - Decreases drag with increase in thrust
 - Decrease in wing drag is due to reduction in pressure drag
 - At cruise thrust of 230.1 lbf, CFD predicts 52.6 drag count reduction with cruise propellers powered on

