



Four Bed Carbon Dioxide Scrubber Engineering Development Unit Cabin Air Inlet Testing

52nd International Conference on Environmental Systems
July 16-20, 2023

Authors:

J. Knox[†], G. Cmarik, A. Waddle



ICES-2023-119

[†] - Corresponding author, presenter



FBCO₂ Scrubber 2022-2023 Outline



- Introduction
- Operation of the FBCO₂ scrubber
- FBCO₂ Scrubber Engineering Development Unit
- Cabin Air Inlet Test Conditions and Configuration
- Impacts of Increased Temperature and Humidity
- Overall Results Summary
- Transient data for 2.0 torr inlet ppCO₂
- Transient data for 2.5 torr inlet ppCO₂
- Baseline and cabin air percent holdup and breakthrough losses
- Impacts of de-integration from the CCAA on removal rate
- Conclusions and Recommendations

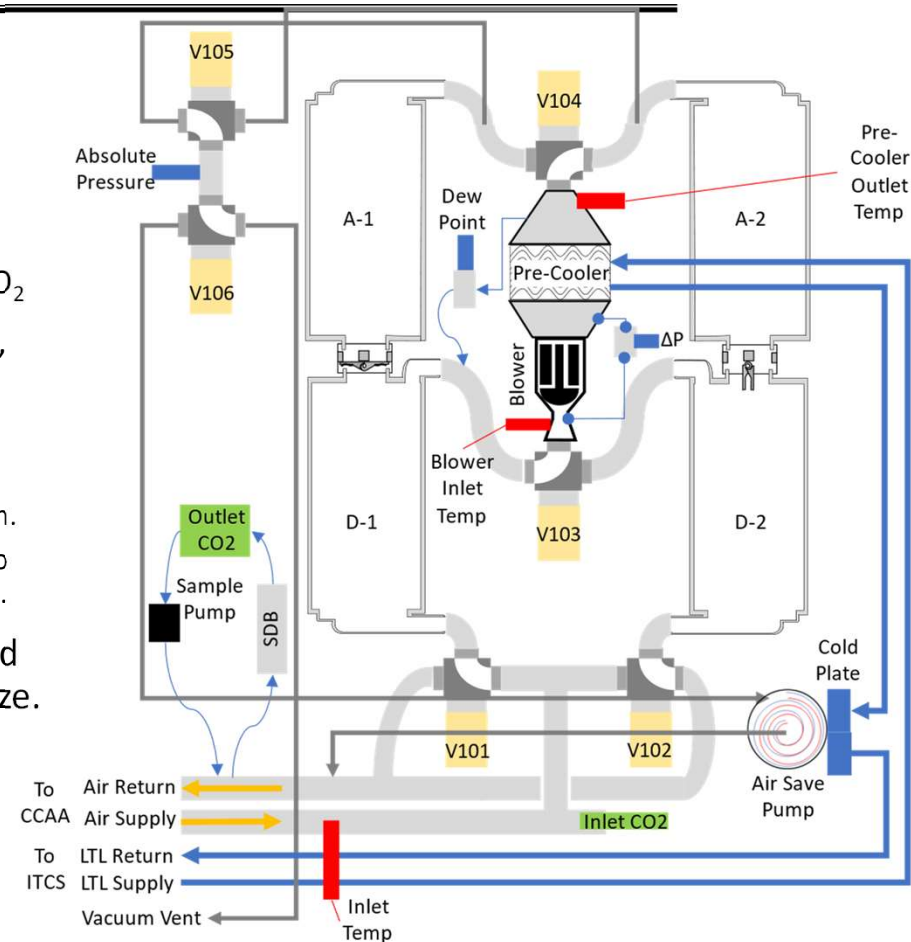


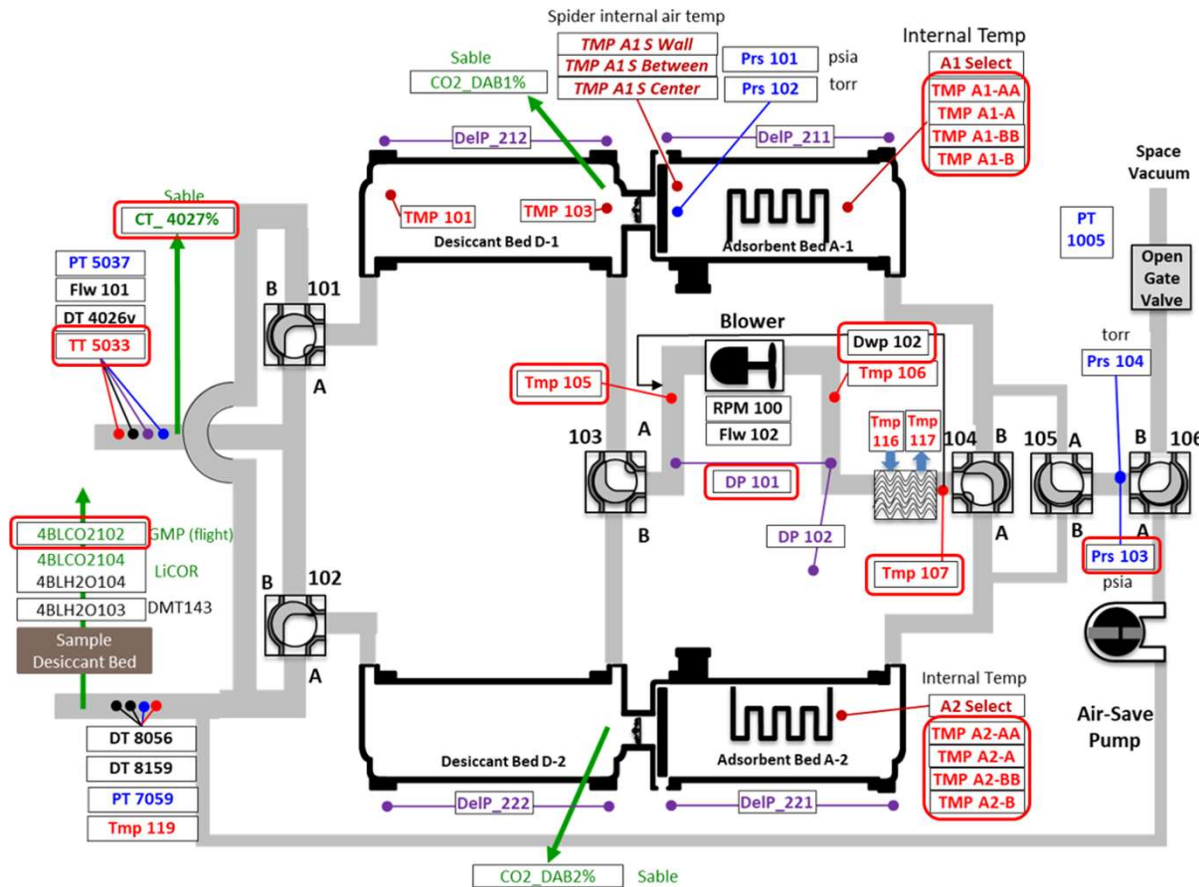
- Four Bed Carbon Dioxide Scrubber
 - ISS CO₂ Removal Technology Demonstration
 - Launched August 10, 2021
 - Activated onboard ISS September 2021
 - Total run time of 1.5 years on ~ June 4, 2023



Operation of the FBCO₂ scrubber

- Operations are split into half-cycles (HC) A and B
 - These are mirrors of each other. Schematic shows HC A
- Tracing the flow path through system:
 1. Air is drawn from cabin air system (CCAA). Air contains O₂/N₂, H₂O, and CO₂
 2. Air flow path is supply duct, V101, bed D-1, V103, blower, pre-cooler, V104, bed A-2, bed D-2, V102, return duct
 1. In this path, D-1 is scrubbing H₂O, but CO₂ and O₂/N₂ pass.
 2. Then, A-2 is scrubbing CO₂, but O₂/N₂ pass.
 3. Finally, the air passing through bed D-2 picks up H₂O and returns it to the cabin.
 4. While this is happening, A-1 is heated and connected to vacuum to vent CO₂ to space through V105 and V106. This heat will be used to desorb D-1 next cycle.
 3. Half-cycle time is part of design process and can be adjusted based on volume of air flow, humidity at supply, heating rate, and bed size.
 4. At end of HC A transitioning to HC B, all 6 valves rotate.
 1. V106 links the Air Save Pump to the now-desorbing bed A-2 to recover O₂/N₂ trapped in voids of ducts and bed.
 2. Once air save is complete, A-2 is linked to space vacuum to vent CO₂

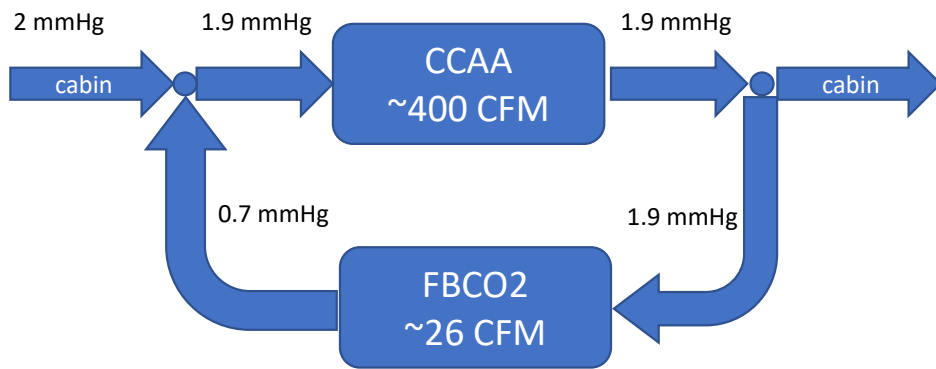




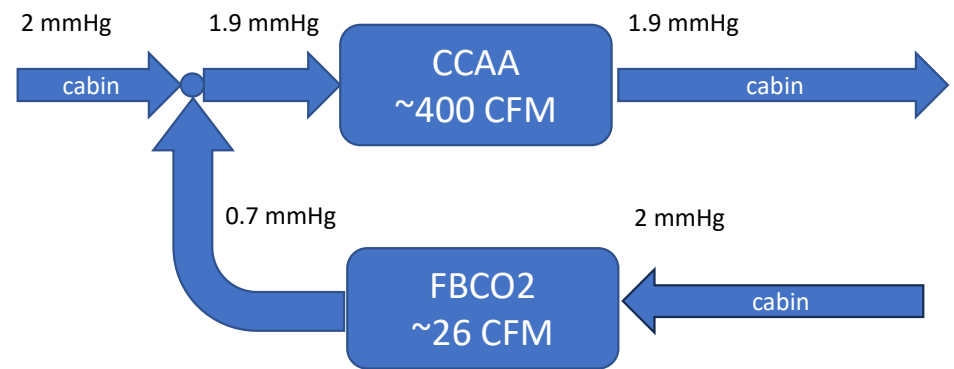
- Red boxes indicate system sensors retained on the flight system
- Abundance of sensors allows for greater visibility into the physics of the adsorption process
- Sampling CO2 sorbent bed effluent provides CO2 sorbent bed breakthrough
- Flight system measures only system CO2 effluent after the desiccant bed has significantly altered the breakthrough curve

Cabin Air Inlet Test Conditions and Configuration

	Air Flow Rate, SCFM	Total Cycle Time, Min	Inlet Temp., degF	Inlet Dewpoint, degF	P/C In H2O Temp., degF	P/C In H2O flow, GPM	Heater Setpoint, degF
Cabin Air Inlet Test	24.4	160	75	54	49	0.4	408
Baseline Conditions	24.4	160	56	50	49	0.4	408

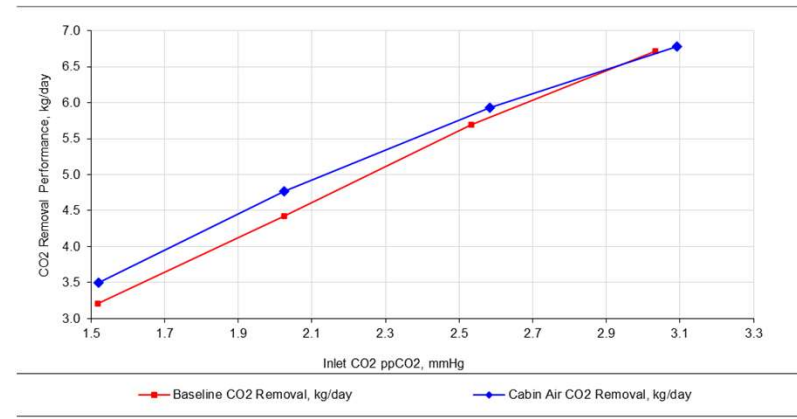
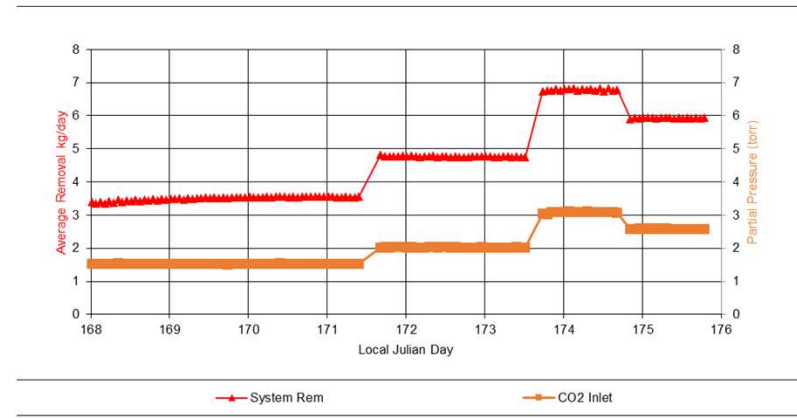


Baseline Configuration

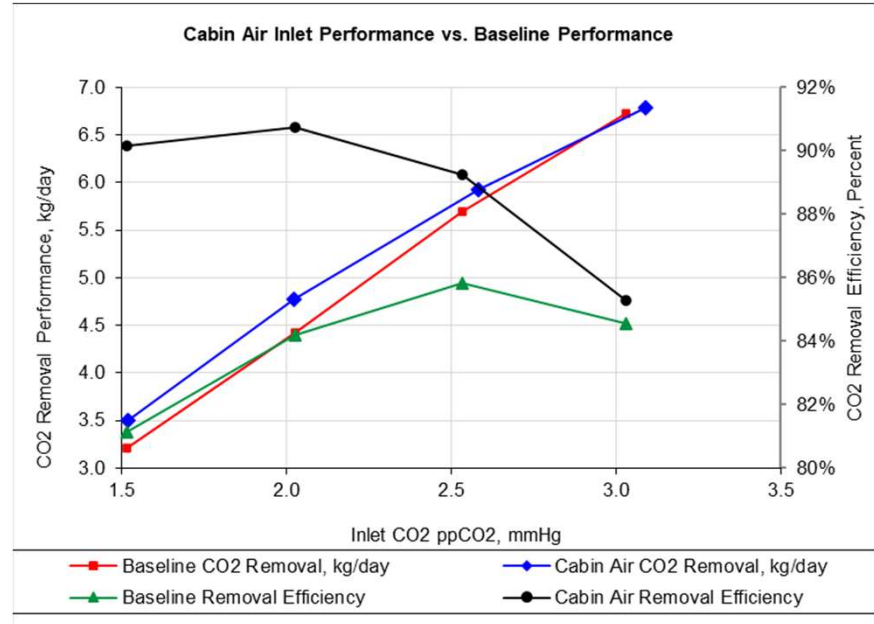
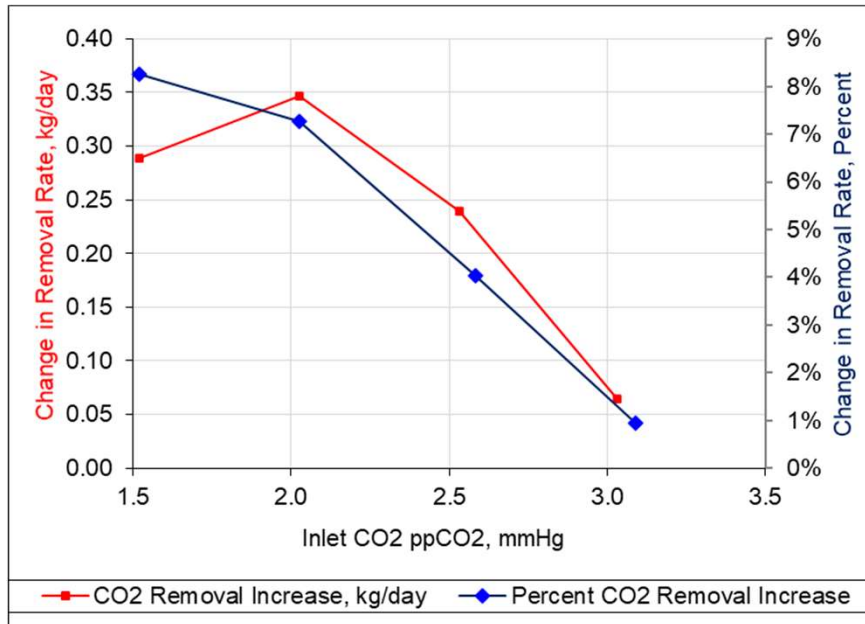


Cabin Air Inlet Configuration

- Top plot shows timeline of CO₂ inlet partial pressure and CO₂ removal rates over the test series
- Bottom plot shows change in CO₂ removal rate and efficiency for various inlet CO₂ partial pressures
- Increased CO₂ removal rate due to reduction in desiccant bed CO₂ holdup via:
 1. Increased inlet temperature (immediate impact)
 2. Increased humidity (gradual impact)



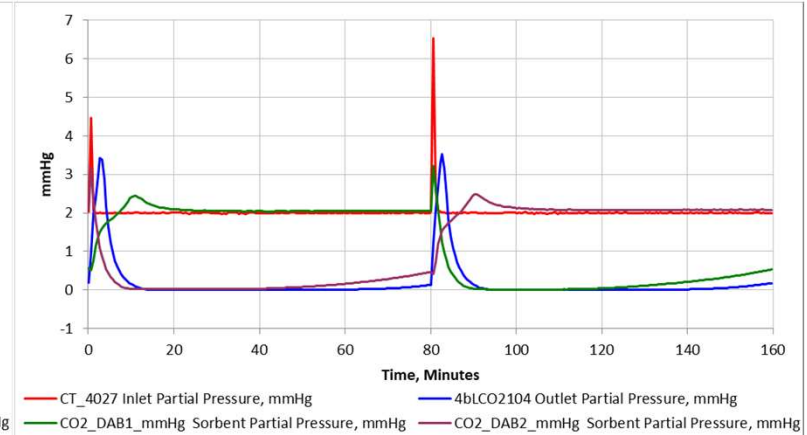
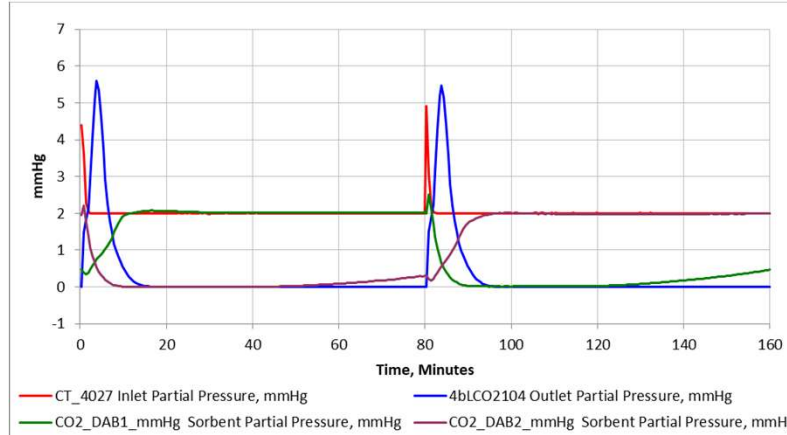
Overall Results Summary



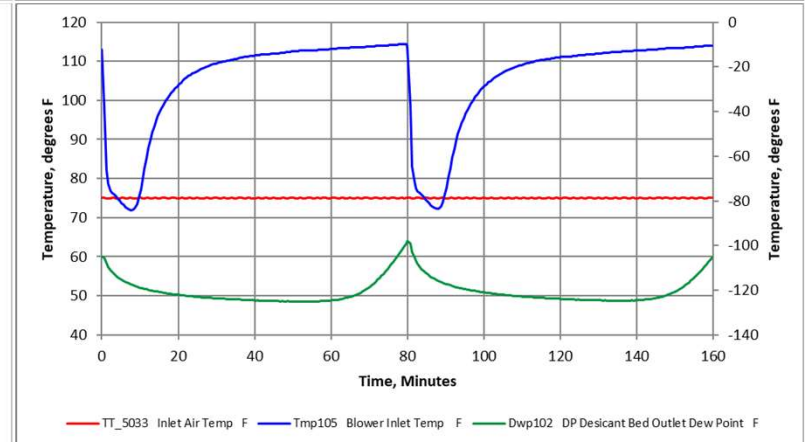
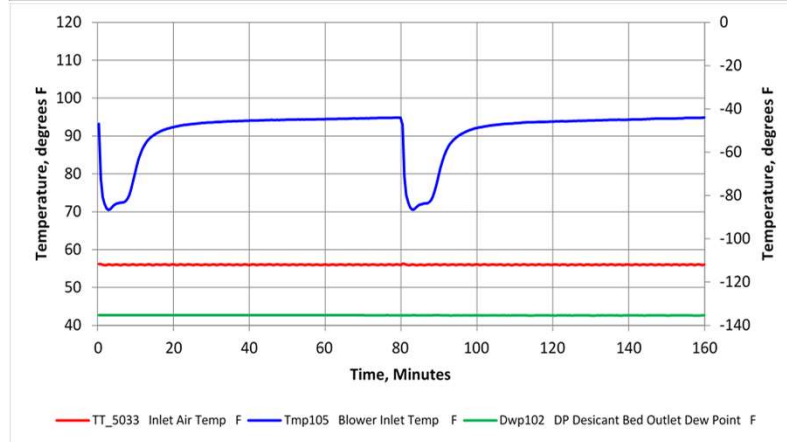
Graphical performance results from baseline and cabin air inlet test points

Transient data for 2 torr inlet ppCO₂

Inlet (red), system outlet (blue), and sorbent outlet CO₂ partial pressures (green and brown) at 2 torr inlet



Desiccant bed inlet (red) and outlet temperatures (blue) and outlet dewpoint (green) at 2 torr inlet

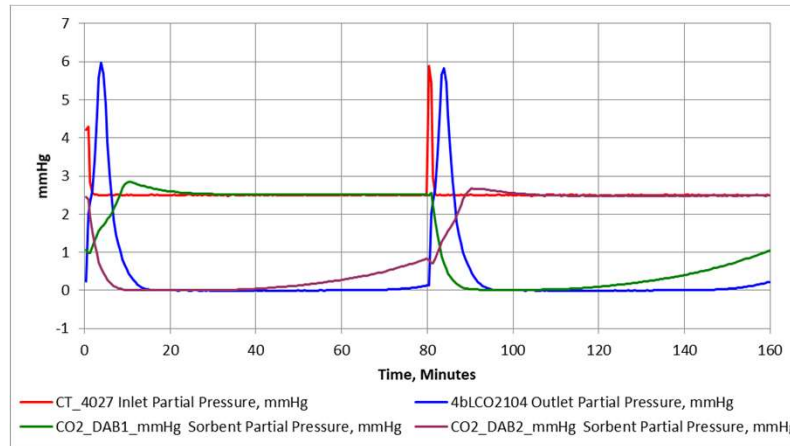


Baseline air inlet

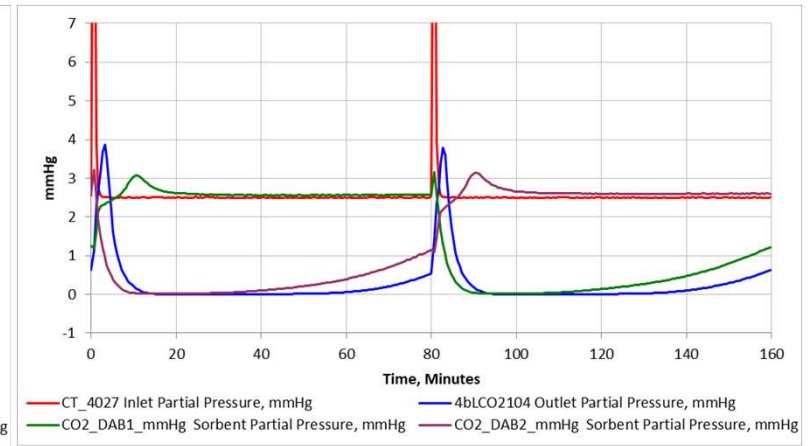
Cabin air inlet

Transient data for 2.5 torr inlet ppCO₂

Inlet (red), system outlet (blue), and sorbent outlet CO₂ partial pressures (green and brown) at 2 torr inlet

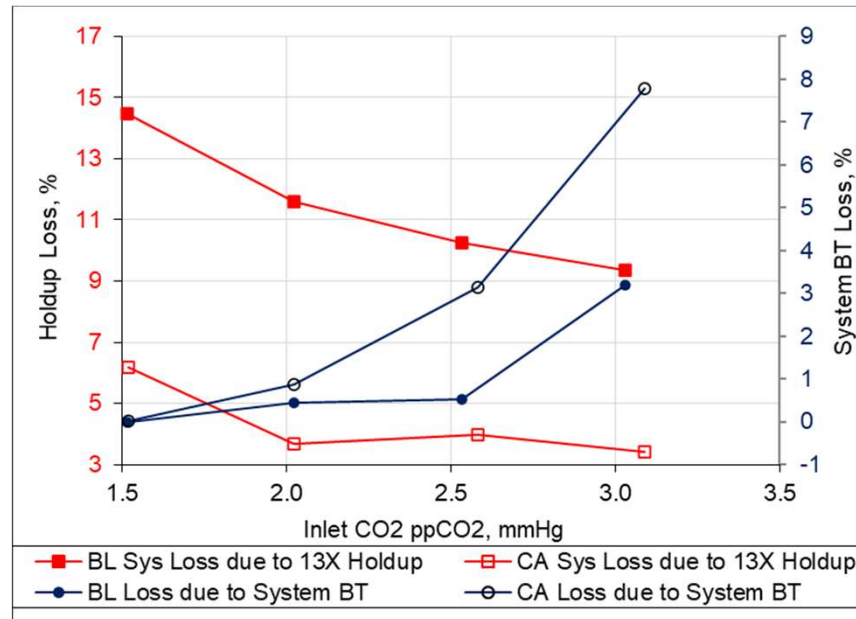


Baseline air inlet



Cabin air inlet

Baseline and cabin air percent holdup and breakthrough losses



Baseline (BL) and cabin air (CA) percent holdup and system breakthrough losses as a function of inlet pp CO₂



Impacts of de-integration from the CCAA on removal rate



Baseline Inlet ppCO ₂ , mmHg	Baseline CO ₂ Removal, kg/day	Baseline Removal Efficiency	Cabin Air Inlet ppCO ₂ , mmHg	Cabin Air CO ₂ Removal, kg/day	Cabin Air Removal Efficiency	CO ₂ Removal Increase, kg/day	Percent CO ₂ Removal Increase
1.52	3.21	81%	1.52	3.50	90%	0.29	8.3%
2.03	4.42	84%	2.02	4.77	91%	0.35	7.3%
2.53	5.69	86%	2.58	5.93	89%	0.24	4.0%
3.03	6.72	85%	3.09	6.78	85%	0.06	0.9%

Baseline Inlet ppCO ₂ , mmHg	Baseline CO ₂ Removal, kg/day	Cabin Air Inlet ppCO ₂ , mmHg	Predicted Cabin Air CO ₂ Removal, kg/day	Percent CO ₂ Removal Increase
1.52	3.21	1.58	3.65	13.7%
2.03	4.42	2.12	4.97	12.5%
2.53	5.69	2.64	6.18	8.6%
3.03	6.72	3.16	7.08	5.4%

De-integration of the FBCO₂ Scrubber inlet air with the CCAA would also eliminate flow rate limitations due to:

- pressure drop associated with the ducting from the CCAA to the FBCO₂ inlet
- competition of the Carbon Dioxide Removal Assembly (CDRA) for the same CCAA air supply





Conclusions and Recommendations



- Further investigation of using cabin air as the inlet to the FBCO₂ Scrubber is warranted based on the results shown
- The current test series should be repeated with Cabin Air inlet ppCO₂ values based on dilution calculations
- The test duration should be extended to determine if increased desiccant bed water vapor breakthrough will occur under these inlet conditions
- If the extended test series proves successful, this operational configuration should be considered as part of the ISS FBCO₂ Scrubber Technology demonstration

